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SCOUR ANALYSIS AND REPORTING FORM

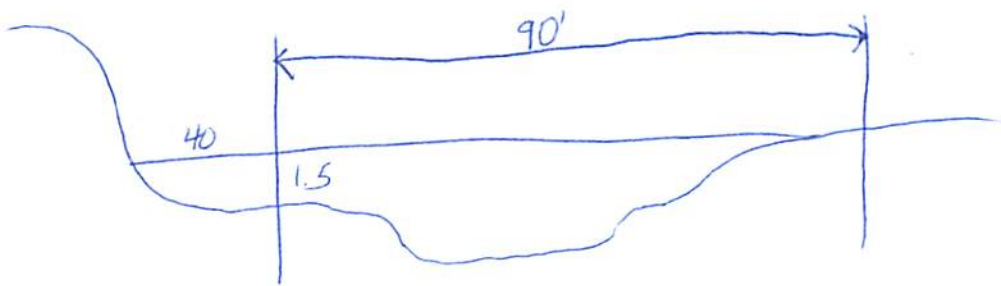
Bridge Structure No. 52450399 Date 11/5/10 Initials CV Region (A)BCD
 Site 06408500 Location Spring Creek on 145th Avenue
 $Q_{100} = \underline{1670}$ by: drainage area ratio flood freq. anal. regional regression eq.
 Bridge discharge (Q_2) = 1670 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 47 ft. Flow angle at bridge = 15 ° Abut. Skew = 15 ° Effective Skew = 0 °
 Width (W_2) iteration = 47 66 75 69
 Avg. flow depth at bridge, y_2 iteration = 3.6 4.2 3.9 4.1
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 69 ft* $q_2 = Q_2/W_2 = \underline{242}$ ft²/s
 Bridge Vel, $V_2 = \underline{5.1}$ ft/s Final $y_2 = q_2/V_2 = \underline{4.1}$ ft $\Delta h = \underline{0.7}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{4.9}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
 Low Steel Elev. = 4.2 ft
 n (Channel) = 0.040
 n (LOB) = 0.035
 n (ROB) = 0.037 0.045
 Pier Width = 0.9 ft
 Pier Length = 32 ft
 # Piers for 100 yr = 1 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{90}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{40}$ ft Average left overbank flow depth, $y_{lob} = \underline{1.5}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{0}$ ft Average right overbank flow depth, $y_{rob} = \underline{0.0}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = \underline{ }$ From Figure 9 W_2 (effective) = ft $y_{cs} = \underline{ }$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) ~~$z = 2.267$~~ ~~$z = 0.763$~~ $z = 0$
 Estimated bed material $D_{50} = \underline{0.2}$ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) = \underline{3.87}$ ft/s 2.68
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{8.48}$ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{0.035}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{X} \underline{0}$ From Figure 10, $y_{cs} = \underline{0.0}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 35.6 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1.0}$
 Froude # at bridge = 0.59 Using pier width a on Figure 11, $\xi = \underline{4.4}$ Pier scour $y_{ps} = \underline{4.0}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{1.5}$ ft right abutment, $y_{aRT} = \underline{0.0}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{6.3}$ and $\psi_{RT} = \underline{0.0}$
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) = \underline{6.3}$ ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) = \underline{0.0}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

Handwritten calculations:
 $1670 / 47 = 35.3$
 $1670 / 69 = 24.2$
 $1670 / 75 = 22.3$
 $1670 / 66 = 25.3$
 $1670 / 47 = 35.3$
 $1670 / 47 = 35.3$

SCOUR ANALYSIS AND REPORTING FORM

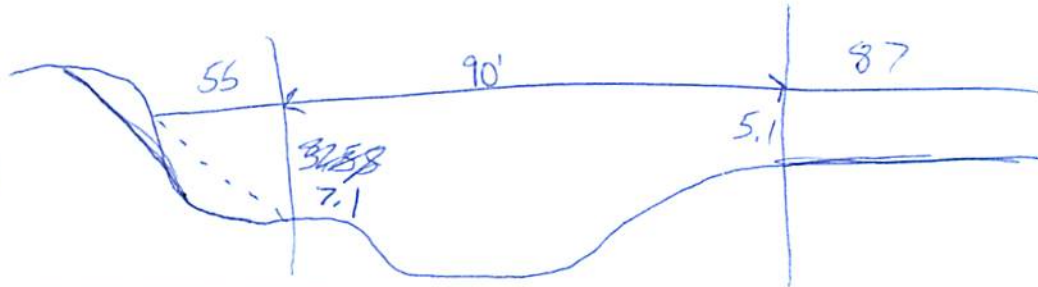
Bridge Structure No. 52450399 Date 11/5/10 Initials AW Region (A) B (C) D
 Site 06408500 Location Spring Creek on 145th Avenue
 $Q_{500} =$ 27000 by: drainage area ratio _____ flood freq. anal. regional regression eq. _____
 Bridge discharge (Q_2) = 7344 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 87 ft. Flow angle at bridge = 15 ° Abut. Skew = 15 ° Effective Skew = 0 °
 Width (W_2) iteration = 87
 Avg. flow depth at bridge, y_2 iteration = 16.7 > 9.2 RD Overflow
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 87 ft* $q_2 = Q_2/W_2 =$ 84.9 ft²/s
 Bridge Vel, $V_2 =$ 10.4 ft/s Final $y_2 = q_2/V_2 =$ 8.2 ft $\Delta h =$ 2.2 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 10.4 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = — ft
 Low Steel Elev. = 6.2 ft
 n (Channel) = 0.040
 n (LOB) = ~~0.040~~ 0.035
 n (ROB) = ~~0.035~~ 0.045
 Pier Width = ~~0.637~~ 0.645 ft 0.9
 Pier Length = 32 ft
 # Piers for 500 yr = 1 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 90 ft
 Width of left overbank flow at approach, $W_{lob} =$ 55 ft Average left overbank flow depth, $y_{lob} =$ 3.55 ft
 Width of right overbank flow at approach, $W_{rob} =$ 87 ft Average right overbank flow depth, $y_{rob} =$ 5.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles) ~~2=2.269~~ 2=0

Estimated bed material $D_{50} =$ 0.2 ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ 7.89 ft/s 3.06

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ 9.65 ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$ 0.101 ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 35.6 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Froude # at bridge = 0.64 Using pier width a on Figure 11, $\xi =$ 4.4 Pier scour $y_{ps} =$ 4.1 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 3.55 ft right abutment, $y_{aRT} =$ 5.1 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 12.5 and $\psi_{RT} =$ 15.2
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) =$ 12.5 ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) =$ 15.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 145th Ave Stream Spring Creek MRM _____ Date 11/5/10 Initials Ch
 Bridge Structure No. 52450399 Location Spring Creek on 145th Avenue
 GPS coordinates: N 43° 56' 30.1" taken from: USL abutment centerline of \hat{M} MRM end _____
W 103° 09' 32.7" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 205.60 sq. mi.
 The average bottom of the main channel was 12.7 ft below top of guardrail at a point 25 ft from left abutment.
 Method used to determine flood flows: Freq. Anal. _____ drainage area ratio _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>1670</u>			Q ₅₀₀ = <u>27000</u>		
Estimated flow passing through bridge	<u>1670</u>			<u>7388</u>		
Estimated road overflow & overtopping	<u>19612</u>					
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? Yes No Marginal
 Evidence of past Scour? Yes No Don't know *scour out sed ~~to~~ left of R. abut*
 Debris Potential? High Med Low *See Photo*

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes No Don't know NA
 Spur Dike Yes No Don't know NA
 Other _____ Yes No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay _____ Sand _____ Gravel Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

app. XSE @ Staff gage

Photos -

*1445-ID
46- US
47- US RB*

*44- US LB
49- L. Abut
50- R. Abut*

*51- Pier config
52- Scour
53- US Face Bridge*

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>1670</u>	<u>7388</u>
Flow depth at left abutment (yaLT), in feet	<u>1.5</u>	<u>3.55</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>5.1</u>
Contraction scour depth (yca), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (ypr), in feet	<u>4.0</u>	<u>4.1</u>
Left abutment scour depth (yas), in feet	<u>6.3</u>	<u>12.5</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>15.2</u>
Flow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required

$0.2 \text{ ft} \left(\frac{12 \text{ in}}{1 \text{ ft}} \right) = 2.4 \text{ in} = 6.096 \text{ cm}$
 60 in