

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52692290 Date 8/11/11 Initials CW Region (A B C D) C

Site \_\_\_\_\_ Location 2.2 mi E of Exit 84 on HWY 1416

Q<sub>100</sub> = 427 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.

Bridge discharge (Q<sub>2</sub>) = 427 (should be Q<sub>100</sub> unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 33 ft. Flow angle at bridge = 30° Abut. Skew = 0° Effective Skew = 30°

Width (W<sub>2</sub>) iteration = 33

Avg. flow depth at bridge, y<sub>2</sub> iteration = 6.3 vert wall

Corrected channel width at bridge Section = W<sub>2</sub> times cos of flow angle = 28.54 ft\* q<sub>2</sub> = Q<sub>2</sub>/W<sub>2</sub> = 28.9 ft<sup>2</sup>/s

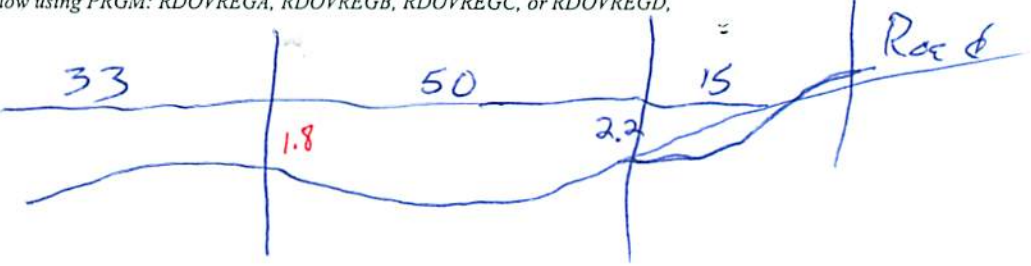
Bridge Vel, V<sub>2</sub> = 4.6 ft/s Final y<sub>2</sub> = q<sub>2</sub>/V<sub>2</sub> = 6.3 ft Δh = 0.4 ft

Average main channel depth at approach section, y<sub>1</sub> = Δh + y<sub>2</sub> = 6.7 ft

\*NOTE: repeat above calculations until y<sub>2</sub> changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y<sub>2</sub> is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = \_\_\_\_\_ ft  
Low Steel Elev. = 7.3 ft  
n (Channel) = 0.045  
n (LOB) = 0.035  
n (ROB) = 0.035  
Pier Width = 2.1 ft  
Pier Length = 2.1 ft  
# Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section W<sub>1</sub> = 50 ft

Width of left overbank flow at approach, W<sub>lob</sub> = 33 ft Average left overbank flow depth, y<sub>lob</sub> = 1.8 ft

Width of right overbank flow at approach, W<sub>rob</sub> = 15 ft Average right overbank flow depth, y<sub>rob</sub> = 1.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = \_\_\_\_\_ From Figure 9 W<sub>2</sub> (effective) = \_\_\_\_\_ ft y<sub>cs</sub> = \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D<sub>50</sub> = 0.5 ft Average approach velocity, V<sub>1</sub> = Q<sub>100</sub>/(y<sub>1</sub>W<sub>1</sub>) = 1.26 ft/s

Critical approach velocity, V<sub>c</sub> = 11.17y<sub>1</sub><sup>1/6</sup>D<sub>50</sub><sup>1/3</sup> = 12.17 ft/s

If V<sub>1</sub> < V<sub>c</sub> and D<sub>50</sub> >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

D<sub>c50</sub> = 0.0006(q<sub>2</sub>/y<sub>1</sub><sup>7/6</sup>)<sup>3</sup> = 0.019 ft If D<sub>50</sub> >= D<sub>c50</sub>, χ = 0.0

Otherwise, χ = 0.122y<sub>1</sub>[q<sub>2</sub>/(D<sub>50</sub><sup>1/3</sup>y<sub>1</sub><sup>7/6</sup>)]<sup>6/7</sup> - y<sub>1</sub> = 0.0 From Figure 10, y<sub>cs</sub> = 0.0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K<sub>2</sub> = 1.0

Froude # at bridge = 0.32 Using pier width a on Figure 11, ξ = 8.3 Pier scour y<sub>ps</sub> = 7.0 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, y<sub>aLT</sub> = 1.4 ft right abutment, y<sub>aRT</sub> = 1.1 ft

Shape coefficient K<sub>1</sub> = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y<sub>aLT</sub> and y<sub>aRT</sub> on figure 12, ψ<sub>LT</sub> = 7.4 and ψ<sub>RT</sub> = 4.7

Left abutment scour, y<sub>as</sub> = ψ<sub>LT</sub>(K<sub>1</sub>/0.55) = 11.1 ft Right abutment scour y<sub>as</sub> = ψ<sub>RT</sub>(K<sub>1</sub>/0.55) = 7.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

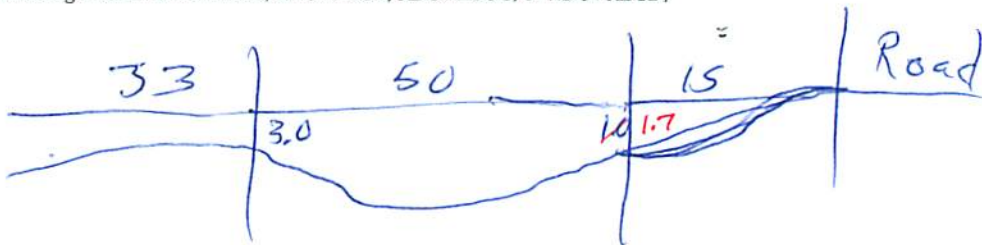
Bridge Structure No. 5.2692290 Date 8/11/11 Initials CW Region (A B C D) B  
 Site \_\_\_\_\_ Location 2.2 mi E of Exit 84 on Hwy 141  
 $Q_{500} =$  1430 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = ~~1430~~ 1097 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 33 ft. Flow angle at bridge = 30° Abut. Skew = 0° Effective Skew = 30°  
 Width ( $W_2$ ) iteration = 33  
 Avg. flow depth at bridge,  $y_2$  iteration = 6.4 > LS  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 28.58 ft\*  $q_2 = Q_2/W_2 =$  38.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.3 ft/s Final  $y_2 = q_2/V_2 =$  7.3 ft  $\Delta h =$  0.6 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 7.3 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 2.1 ft  
 Pier Length = 2.1 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  50 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  33 ft Average left overbank flow depth,  $y_{lob} =$  3.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  15 ft Average right overbank flow depth,  $y_{rob} =$  0.5 ft  
 $1 \div 2 = 0.5$

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.5 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  1.42 ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  12.51 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  0.024 ft <sup>0.021</sup> If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  0.0 From Figure 10,  $y_{cs} =$  0.0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.35 Using pier width  $a$  on Figure 11,  $\xi =$  8.3 Pier scour  $y_{ps} =$  7.1 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.0 ft right abutment,  $y_{aRT} =$  0.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.5 and  $\psi_{RT} =$  2.37  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  17.2 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  3.4 ft <sup>10.5</sup>

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



Route HWY 1416 Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 8/11/11 Initials Ca  
 Bridge Structure No. 52692290 Location 2.2 mi E of Exit 84 on HWY 1416  
 GPS coordinates: N 44° 05' 46.5" W 102° 39' 53.3" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 3.97 sq. mi.  
 The average bottom of the main channel was 11.6 ft below top of guardrail at a point 5 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

PK calcd 8/8  
 RPK2 54.8  
 5 161  
 10 278  
 25 456  
 50 628  
 100 827  
 500 1430

Flows	Q <sub>100</sub> = <u>827</u>			Q <sub>500</sub> = <u>1430</u>		
Estimated flow passing through bridge	<u>827</u>			<u>1097</u>		
Estimated road overflow & overtopping	<u>333</u>					
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
1899 - 1P 04 - L. Abut  
00 - US 06 - US Face  
01 - US RB  
02 - US LB  
03 - R. Abut

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>827</u>	<u>1097</u>
Flow depth at left abutment (yaLT), in feet	<u>1.8</u>	<u>3.0</u>
Flow depth at right abutment (yaRT), in feet	<u>1.1</u>	<u>0.5 1.7</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>0.0</u>	<u>0.0</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>7.0</u>	<u>7.1</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>11.1</u>	<u>17.2</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>7.0</u>	<u>3.4 10.5</u>
Flow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required

1430  
1097  
333