

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52824300 Date 4/20/11 Initials CW Region (A B C D)
Site 06423500 Location 2.2 NE Waste on Old Waste Road
Q100 = 43800 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 43800 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 1000 ft. Flow angle at bridge = 20 degrees Abut. Skew = 0 degrees Effective Skew = 20 degrees
Width (W2) iteration = 1000 959
Avg. flow depth at bridge, y2 iteration = 8.1 8.3
Corrected channel width at bridge Section = W2 times cos of flow angle = 901.17 ft* q2 = Q2/W2 = 48.6 ft^2/s
Bridge Vel, V2 = 5.9 ft/s Final y2 = q2/V2 = 8.3 ft Delta h = 0.7 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 9.0 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = ft
n (Channel) =
n (LOB) =
n (ROB) =
Pier Width = 4.5 4.5 ft
Pier Length = 23.5 4.5 ft
Piers for 100 yr =

Level 1.5 not well suited to this site. Analysis not completed. Bridge too long.

CONTRACTION SCOUR

Width of main channel at approach section W1 = ft
Width of left overbank flow at approach, Wlob = ft Average left overbank flow depth, ylob = ft
Width of right overbank flow at approach, Wrob = ft Average right overbank flow depth, yrob = ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [(q2/(D50^(1/3) y1^(7/6)))^(6/7) - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = Using pier width a on Figure 11, xi = Pier scour yps = ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = ft right abutment, yaRT = ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = and psiRT =
Left abutment scour, yas = psiLT (K1/0.55) = ft Right abutment scour yas = psiRT (K1/0.55) = ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52824300 Date 4/20/11 Initials CW Region (A B C D) C
 Site _____ Location 2.2 NE Waste on Old Waste Road
 $Q_{500} = 53400$ by: drainage area ratio _____ flood freq. anal. regional regression eq. _____
 Bridge discharge (Q_2) = 53400 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 1000 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °
 Width (W_2) iteration = 1000 978
 Avg. flow depth at bridge, y_2 iteration = 9.0 9.1
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 919.02 ft* $q_2 = Q_2/W_2 = 56.1$ ft²/s
 Bridge Vel, $V_2 = 6.4$ ft/s Final $y_2 = q_2/V_2 = 7.1$ ft $\Delta h = 0.8$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 9.9$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = _____ ft
 n (Channel) = _____
 n (LOB) = _____
 n (ROB) = _____
 Pier Width = 4.5 ft
 Pier Length = 4.5 ft
 # Piers for 500 yr = _____ ft

*Level. 1.5 not well suited to this site
 - Bridge too long.
 Analysis not completed*

CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ _____ ft
 Width of left overbank flow at approach, $W_{lob} =$ _____ ft Average left overbank flow depth, $y_{lob} =$ _____ ft
 Width of right overbank flow at approach, $W_{rob} =$ _____ ft Average right overbank flow depth, $y_{rob} =$ _____ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ _____ From Figure 9 W_2 (effective) = _____ ft $y_{cs} =$ _____ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 = 1.0$
 Froude # at bridge = _____ Using pier width a on Figure 11, $\xi =$ _____ Pier scour $y_{ps} =$ _____ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ _____ ft right abutment, $y_{aRT} =$ 0.55 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ _____ and $\psi_{RT} =$ _____
 Left abutment scour, $y_{as} = \psi_{LT} (K_1 / 0.55) =$ _____ ft Right abutment scour $y_{as} = \psi_{RT} (K_1 / 0.55) =$ _____ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route Old Wasta Road Stream Cheyenne River MRM _____ Date 4/20/11 Initials CW
 Bridge Structure No. 52824300 Location 2.2 NE Waste on Old Wasta Road
 GPS coordinates: N 44° 04' 51.1" taken from: USL abutment X centerline of \uparrow MRM end _____
W 102° 24' 07.8" Datum of coordinates: WGS84 X NAD27 _____
 Drainage area = 12720.18 sq. mi. 23.9
 The average bottom of the main channel was 24.0 ft below top of guardrail at a point 459 ft from left abutment.
 Method used to determine flood flows: Freq. Anal. _____ drainage area ratio _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>43800</u>			Q ₅₀₀ = <u>53400</u>		
Estimated flow passing through bridge						
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping						
Chance of Pressure flow						
Armored appearance to channel						
Lateral instability of channel						

Riprap at abutments? _____ Yes _____ No _____ Marginal
 Evidence of past Scour? _____ Yes _____ No _____ Don't know
 Debris Potential? _____ High _____ Med _____ Low

Does scour countermeasure(s) appear to have been designed?

Riprap _____ Yes _____ No _____ Don't know _____ NA
 Spur Dike _____ Yes _____ No _____ Don't know _____ NA
 Other _____ Yes _____ No _____ Don't know _____ NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay _____ Sand _____ Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Summary of Results

	Q100	Q500
Bridge flow evaluated		
Flow depth at left abutment (yaLT), in feet		
Flow depth at right abutment (yaRT), in feet		
Contraction scour depth (y _{cs}), in feet		
Pier scour depth (y _{ps}), in feet		
Left abutment scour depth (y _{as}), in feet		
Right abutment scour depth (y _{as}), in feet		
Flow angle of attack		

See Comments/Diagram for justification where required