

OK RT

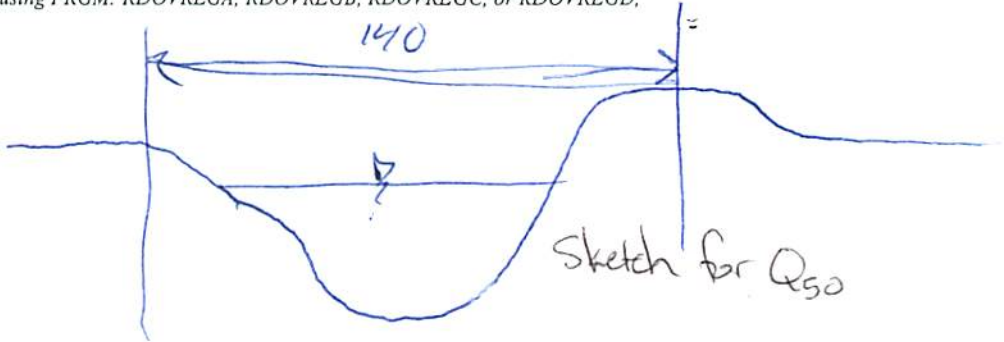
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 52430307 Date 3/11/14 Initials CV Region (A/B/C/D) 0  
 Site \_\_\_\_\_ Location 0.3 mi N of Exit 101 on Jensen Rd  
 $Q_{100} =$  13600 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 12614 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 96  
 Avg. flow depth at bridge,  $y_2$  iteration = 14.5 ~~> LS~~  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 96 ft\*  $q_2 = Q_2/W_2 =$  132.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  9.4 ft/s Final  $y_2 = q_2/V_2 =$  14 ft  $\Delta h =$  1.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  15.4 ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 14.0 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 100 yr = 2



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  140 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0.0 ft 96 Average left overbank flow depth,  $y_{lob} =$  0.0 <sup>1.2</sup> ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0.0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

Q50 Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  8.24 From Figure 9  $W_2$  (effective) = 92 ft  $y_{cs} =$  9.1 <sup>9.4</sup> ft  
8.53

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.44 Using pier width a on Figure 11,  $\xi =$  8.0 Pier scour  $y_{ps} =$  7.1 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.0 <sup>1.2</sup> ft right abutment,  $y_{aRT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.051 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0.0 ft  
5.1

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWC/SNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

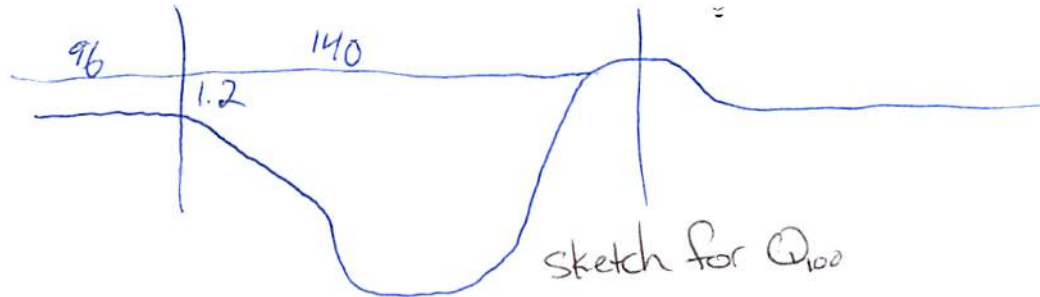
Bridge Structure No. 52830307 Date 8/11/11 Initials lw Region (A/B/C/D) A  
 Site \_\_\_\_\_ Location 0.3 mi. N of Exit 101 on Jensen Rd  
Q50  $Q_{50} = 4860$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 4660 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 96 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 96  
 Avg. flow depth at bridge,  $y_2$  iteration = 11.6 → Vert Wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 96 ft\*  $q_2 = Q_2/W_2 = 92.3$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 4.0$  ft/s Final  $y_2 = q_2/V_2 = 11.6$  ft  $\Delta h = 1.3$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 12.9$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 14.0 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 140$  ft 0.0  
 Width of left overbank flow at approach,  $W_{lob} = 96$  ft Average left overbank flow depth,  $y_{lob} = 1.2$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 0.0$  ft Average right overbank flow depth,  $y_{rob} = 0.0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 7.06$  From Figure 9  $W_2$  (effective) = 92 ft  $y_{cs} = 7.5$   
6.73  $y_{cs} = 7.9$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.0$   
 Froude # at bridge = 0.41 Using pier width a on Figure 11,  $\xi = 4.0$  Pier scour  $y_{ps} = 7.0$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 1.20$  ft right abutment,  $y_{aRT} = 0.0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 5.10$  and  $\psi_{RT} = 0.0$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 5.10$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 0.0$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route Jensen Rd Stream Bull Ck MRM \_\_\_\_\_ Date 8/11/11 Initials CW  
 Bridge Structure No. 52930307 Location 0.3 mi N of Exit 10 on Jensen Rd  
 GPS coordinates: N 44° 04' 20.3" taken from: USL abutment X centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 102° 23' 13.2" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_  
 Drainage area = 51.48 sq. mi.  
 The average bottom of the main channel was 15.0 ft below top of guardrail at a point 29 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio ✓ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Peak Calc'd @  
 PK2 | 297  
 5 | 1200  
 10 | 2520  
 25 | 5470  
 50 | 8860  
 100 | 13600  
 500 | 31500

Flows	Q <sub>100</sub> = <u>13600</u>			<del>Q<sub>500</sub></del> = <u>Q<sub>50</sub> = 8860</u>		
Estimated flow passing through bridge	<u>12694</u>			<u>8860</u>		
Estimated road overflow & overtopping	<u>906</u>					
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping	<u>X</u>				<u>X</u>	
Chance of Pressure flow	<u>X</u>				<u>X</u>	
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? X Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes X No \_\_\_ Don't know  
 Debris Potential? X High \_\_\_ Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No X Don't know \_\_\_ NA  
 Spur Dike X Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know X NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay X Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1907 - IP  
 06 - US ~~RTB~~  
 09 - US RTB/spur dike  
 10 - US LB  
 11 - R. Abut  
 12 - L. Abut  
 13 - US Face  
 14 - Spur dike

Summary of Results

	Q100	<del>Q500</del> Q50
Bridge flow evaluated	<u>12694</u>	<u>8860</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0 1.2</u>	<u>1.2 0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>0.0</u>
Contraction scour depth (yca), in feet	<del>9.1</del> <u>9.4</u>	<u>7.5 7.9</u>
Pier scour depth (yps), in feet	<u>7.1</u>	<u>7.0</u>
Left abutment scour depth (yas), in feet	<u>0.0 5.1</u>	<u>5.1 0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required

13600  
 51.48  
 2694  
 906