

DUP ok-RAT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 53240235 Date 9-17-12 Initials RFT Region (A B C D)

Site \_\_\_\_\_ Location 5.5 mi N. Bison on White Butte Rd

Q100 = 116900 by: drainage area ratio [checked] flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge (Q2) = \_\_\_\_\_ (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = \_\_\_\_\_ ft. Flow angle at bridge = \_\_\_\_\_ ° Abut. Skew = \_\_\_\_\_ ° Effective Skew = \_\_\_\_\_ °

Width (W2) iteration = \_\_\_\_\_

Avg. flow depth at bridge, y2 iteration = \_\_\_\_\_

Corrected channel width at bridge Section = W2 times cos of flow angle = \_\_\_\_\_ ft\* q2 = Q2/W2 = \_\_\_\_\_ ft²/s

Bridge Vel, V2 = \_\_\_\_\_ ft/s Final y2 = q2/V2 = \_\_\_\_\_ ft Δh = \_\_\_\_\_ ft

Average main channel depth at approach section, y1 = Δh + y2 = \_\_\_\_\_ ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft

Low Steel Elev. = \_\_\_\_\_ ft

n (Channel) = \_\_\_\_\_

n (LOB) = \_\_\_\_\_

n (ROB) = \_\_\_\_\_

Pier Width = \_\_\_\_\_ ft

Pier Length = \_\_\_\_\_ ft

# Piers for 100 yr = \_\_\_\_\_ ft

New Bridge under construction?! See photo 5: Str. no. Const. site

CONTRACTION SCOUR

Width of main channel at approach section W1 = \_\_\_\_\_ ft

Width of left overbank flow at approach, Wlob = \_\_\_\_\_ ft Average left overbank flow depth, ylob = \_\_\_\_\_ ft

Width of right overbank flow at approach, Wrob = \_\_\_\_\_ ft Average right overbank flow depth, yrob = \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = \_\_\_\_\_ From Figure 9 W2 (effective) = \_\_\_\_\_ ft ycs = \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = \_\_\_\_\_ ft Average approach velocity, V1 = Q100/(y1 W1) = \_\_\_\_\_ ft/s

Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = \_\_\_\_\_ ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = \_\_\_\_\_ ft If D50 >= Dc50, χ = 0.0

Otherwise, χ = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = \_\_\_\_\_ From Figure 10, ycs = \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_

Correction factor for flow angle of attack (from Table 1), K2 = \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11, ξ = \_\_\_\_\_ Pier scour yps = \_\_\_\_\_ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = \_\_\_\_\_ ft right abutment, yarT = \_\_\_\_\_ ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, ψLT = \_\_\_\_\_ and ψRT = \_\_\_\_\_

Left abutment scour, yas = ψLT(K1/0.55) = \_\_\_\_\_ ft Right abutment scour yas = ψRT(K1/0.55) = \_\_\_\_\_ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 53240235 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D)

Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} = 30400$  by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = \_\_\_\_\_ ft. Flow angle at bridge = \_\_\_\_\_ ° Abut. Skew = \_\_\_\_\_ ° Effective Skew = \_\_\_\_\_ °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = \_\_\_\_\_ ft\*  $q_2 = Q_2/W_2 =$  \_\_\_\_\_ ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  \_\_\_\_\_ ft/s Final  $y_2 = q_2/V_2 =$  \_\_\_\_\_ ft  $\Delta h =$  \_\_\_\_\_ ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  \_\_\_\_\_ ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft

Low Steel Elev. = \_\_\_\_\_ ft

n (Channel) = \_\_\_\_\_

n (LOB) = \_\_\_\_\_

n (ROB) = \_\_\_\_\_

Pier Width = \_\_\_\_\_ ft

Pier Length = \_\_\_\_\_ ft

# Piers for 500 yr = \_\_\_\_\_ ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  \_\_\_\_\_ ft

Width of left overbank flow at approach,  $W_{lob} =$  \_\_\_\_\_ ft Average left overbank flow depth,  $y_{lob} =$  \_\_\_\_\_ ft

Width of right overbank flow at approach,  $W_{rob} =$  \_\_\_\_\_ ft Average right overbank flow depth,  $y_{rob} =$  \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  \_\_\_\_\_ ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  \_\_\_\_\_ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route white Butte Rd Stream S. Fork Grand R MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 53240235 Location 5.5 mi N Bison on White Butte Rd  
 GPS coordinates: \_\_\_\_\_ taken from: USL abutment \_\_\_\_\_ centerline of  $\uparrow$  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 1422.5 sq. mi.

The average bottom of the main channel was \_\_\_\_\_ ft below top of guardrail at a point \_\_\_\_\_ ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>16900</u>			Q <sub>500</sub> = <u>30400</u>		
Estimated flow passing through bridge						
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping						
Chance of Pressure flow						
Armored appearance to channel						
Lateral instability of channel						

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

**Summary of Results**

	Q100	Q500
Bridge flow evaluated		
Flow depth at left abutment (yaLT), in feet		
Flow depth at right abutment (yaRT), in feet		
Contraction scour depth (y <sub>cs</sub> ), in feet		
Pier scour depth (y <sub>ps</sub> ), in feet		
Left abutment scour depth (y <sub>as</sub> ), in feet		
Right abutment scour depth (y <sub>as</sub> ), in feet		
Flow angle of attack		

See Comments/Diagram for justification where required