

OK JCT

SCOUR ANALYSIS AND REPORTING FORM

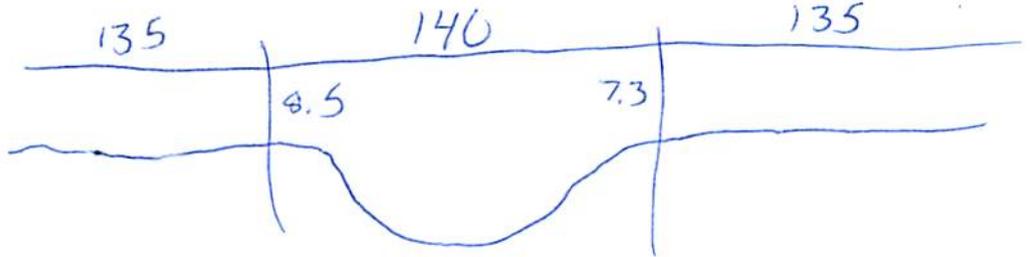
Bridge Structure No. 53281151 Date 8/9/11 Initials CW Region (A B C D) Site Location 17.2 mi NE of Bison on White Butte Rd 143 Ave Q100 = 4410 by: drainage area ratio flood freq. anal. regional regression eq. Bridge discharge (Q2) = 4410 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 135 ft. Flow angle at bridge = 10 degrees Abut. Skew = 0 degrees Effective Skew = 10 degrees Width (W2) iteration = 135 73 74 76 Avg. flow depth at bridge, y2 iteration = 6.8 9.3 9.0 9.1 Corrected channel width at bridge Section = W2 times cos of flow angle = 74.85 ft\* q2 = Q2/W2 = 58.9 ft^2/s Bridge Vel, V2 = 6.4 ft/s Final y2 = q2/V2 = 9.1 ft Delta h = 0.8 ft Average main channel depth at approach section, y1 = Delta h + y2 = 10.0 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q) If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft Low Steel Elev. = 13.9 ft n (Channel) = 0.045 n (LOB) = 0.055 n (ROB) = 0.055 Pier Width = 2.75 ft Pier Length = 2.75 ft # Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 140 ft Width of left overbank flow at approach, Wlob = 135 ft Average left overbank flow depth, ylob = 8.5 ft Width of right overbank flow at approach, Wrob = 135 ft Average right overbank flow depth, yrob = 7.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 31.76 From Figure 9 W2 (effective) = 69.4 ft ycs = 24.0 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s

Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [(q2/(D50^(1/3) y1^(7/6)))^(6/7) - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0 Froude # at bridge = 0.37 Using pier width a on Figure 11, xi = 10.1 Pier scour yps = 8.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 8.5 ft right abutment, yarT = 7.3 ft Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through Using values for yalT and yarT on figure 12, psiLT = 20.2 and psiRT = 19.1 Left abutment scour, yas = psiLT (K1/0.55) = 20.2 ft Right abutment scour yas = psiRT (K1/0.55) = 19.1 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

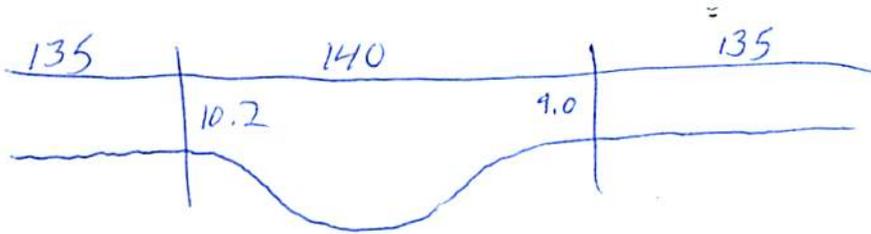
Bridge Structure No. 53281151 Date 8/9/11 Initials Cur Region (A B C D) D  
 Site \_\_\_\_\_ Location 17.2 mile NE of Bison on White Butte Rd  
 $Q_{500} =$  7390 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 7390 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 135 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 135 77 100 97  
 Avg. flow depth at bridge,  $y_2$  iteration = 4.9 11.9 10.4 10.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 95.53 ft\*  $q_2 = Q_2/W_2 =$  77.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.3 ft/s Final  $y_2 = q_2/V_2 =$  10.6 ft  $\Delta h =$  1.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 13.9 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.055  
 $n$  (ROB) = 0.055  
 Pier Width = 2.75 ft  
 Pier Length = 2.75 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  140 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  135 ft Average left overbank flow depth,  $y_{lob} =$  10.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  135 ft Average right overbank flow depth,  $y_{rob} =$  9.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  27.18 From Figure 9  $W_2$  (effective) = 90 ft  $y_{cs} =$  21.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.4 Using pier width  $a$  on Figure 11,  $\xi =$  10.1 Pier scour  $y_{ps} =$  8.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  10.2 ft right abutment,  $y_{aRT} =$  9.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  21.5 and  $\psi_{RT} =$  20.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  21.5 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  20.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route White Butte Rd Stream Lodgepole CK MRM Date 3/9/11 Initials CJ  
 Bridge Structure No. 53281151 Location 17.2 mi NE of Bison on White Butte Rd  
 GPS coordinates: N 45° 43' 55.3" taken from: USL abutment  centerline of  MRM end   
W 102° 22' 24.2" Datum of coordinates: WGS84  NAD27

Drainage area = 76.33 sq. mi.  
 The average bottom of the main channel was 19.5 ft below top of guardrail at a point 35 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal.  drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4410</u>			Q <sub>500</sub> = <u>7390</u>		
Estimated flow passing through bridge	<u>4410</u>			<u>7390</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Peak Flows calc'd on 8/8

PK 2	295
5	488
10	1540
25	2480
50	3380
100	4410
500	7390

Riprap at abutments?  Yes  No  Marginal  
 Evidence of past Scour?  Yes  No  Don't know  
 Debris Potential?  High  Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other  Yes  No  Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand  Gravel  Cobbles  Boulders   
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Mature corn in flood plains → poor visibility → lots of estimating

Photos  
 1839 - ID  
 40 - US  
 41 - US RB  
 42 - US LB  
 43 - Scour/Erosion @ L. Abut.  
 44 - R. Abut  
 45 - L. Abut  
 46 - US Face of bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>4410</u>	<u>7390</u>
Flow depth at left abutment (yaLT), in feet	<u>8.5</u>	<u>10.2</u>
Flow depth at right abutment (yaRT), in feet	<u>7.3</u>	<u>9.0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>24.0</u>	<u>21.6</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>8.7</u>	<u>8.8</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>20.2</u>	<u>21.5</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>19.1</u>	<u>20.6</u>
Flow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required