

SCOUR ANALYSIS AND REPORTING FORM

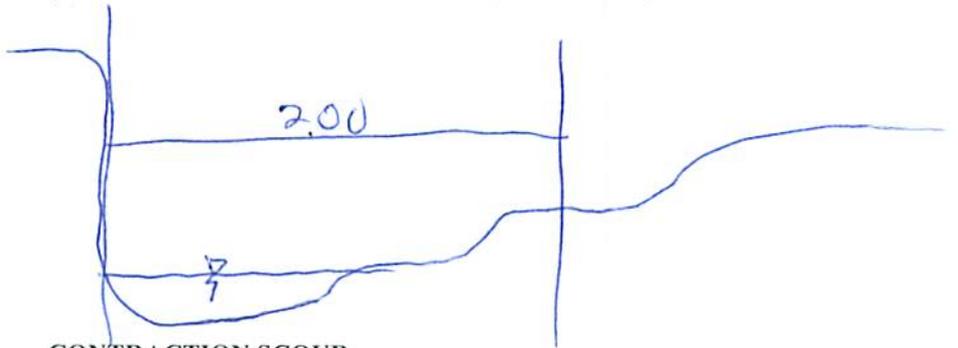
Bridge Structure No. 53290102 Date 7/13/11 Initials CW Region (A B C D) A  
 Site 06355500 Location approx. 9.5 mi S White Butte on 183<sup>rd</sup> Ave  
 $Q_{100} =$  8730 by: drainage area      flood frequency anal.  regional regression eq.       
 Bridge discharge ( $Q_2$ ) = 8730 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 154 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 154 ~~85~~ ~~83~~ ~~86~~  
 Avg. flow depth at bridge,  $y_2$  iteration = 9.0 ~~16.3~~ 12.5 12.3  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 89.69 ft\*  $q_2 = Q_2/W_2 =$  103.1 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  8.4 ft/s Final  $y_2 = q_2/V_2 =$  12.3 ft  $\Delta h =$  1.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. =      ft  
 Low Steel Elev. =      ft  
 n (Channel) = 0.040  
 n (LOB) = 0.045  
 n (ROB) = 0.045  
 Pier Width = 2.0 ft  
 Pier Length = 30 ft  
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  200 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  25 ft Average right overbank flow depth,  $y_{rob} =$  1.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  20.20 From Figure 9  $W_2$  (effective) = 80.7 ft  $y_{cs} =$  17.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$       ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$       ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$       ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$       ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$       From Figure 10,  $y_{cs} =$       ft

PIER SCOUR CALCULATIONS

L/a ratio = 15 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  2.0  
 Froude # at bridge = 0.42 Using pier width a on Figure 11,  $\xi =$  8.0 Pier scour  $y_{ps} =$  14.0 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0 ft

~~0.78~~<sup>2</sup>

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

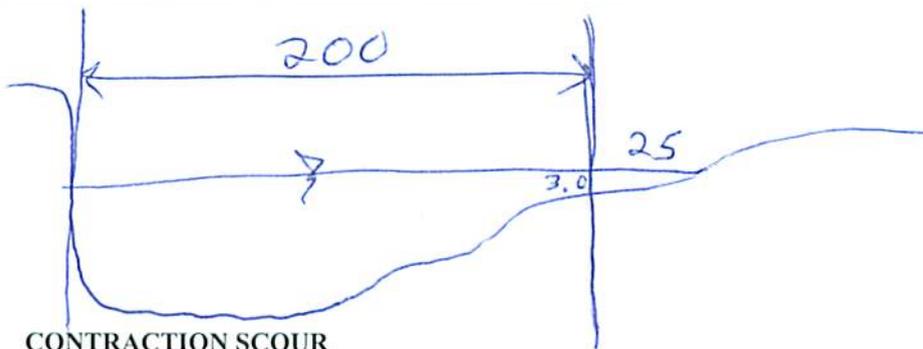
Bridge Structure No. 53290102 Date 7/13/11 Initials Ch Region (A B C D) A  
 Site 06355500 Location approx 9.5 mi S White Butte on 183<sup>rd</sup> Ave  
 $Q_{500} =$  14700 by: drainage area      flood frequency anal.  regional regression eq.       
 Bridge discharge ( $Q_2$ ) = 14700 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 154 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 154 65 95 93  
 Avg. flow depth at bridge,  $y_2$  iteration = 11.9 16.3 15.3 15.5  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 91.59 ft\*  $q_2 = Q_2/W_2 =$  160.5 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  10.4 ft/s Final  $y_2 = q_2/V_2 =$  15.5 ft  $\Delta h =$  2.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  17.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. =      ft  
 Low Steel Elev. =      ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.045  
 $n$  (ROB) = 0.045  
 Pier Width = 2.0 ft  
 Pier Length = 30 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  200 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  25 ft Average right overbank flow depth,  $y_{rob} =$  1.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  22.79 From Figure 9  $W_2$  (effective) = 87.6 ft  $y_{cs} =$  19.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$       ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$       ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$       ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$       ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$       From Figure 10,  $y_{cs} =$       ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 15 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  2.0  
 Froude # at bridge = 22.79 Using pier width  $a$  on Figure 11,  $\xi =$  8.0 Pier scour  $y_{ps} =$  19.2 ft  
0.47 14.2

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  1.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.53 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  6.3  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  8.9 ft  
6.3

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

~~0.78~~

Route 183 Ave Stream N. Fork Grand Riv MRM Date 7/13/11 Initials Ch  
 Bridge Structure No. 53290102 Location Approx 9.5 mi S White Butte on 183rd Ave  
 GPS coordinates: N 45° 45' 08.5" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 102° 21' 44.2" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 1201.76 sq. mi. 29.8  
 The average bottom of the main channel was 30.3 ft below top of guardrail at a point 58 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal. \_\_\_\_\_ drainage area adjustment \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>8730</u>			Q <sub>500</sub> = <u>14700</u>		
Estimated flow passing through bridge	<u>8730</u>			<u>14700</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

Riprap at abutments?  Yes  No  Marginal  
 Evidence of past Scour?  Yes  No  Don't know  
 Debris Potential?  High  Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other \_\_\_\_\_  Yes  No  Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

\* Used constricted section - not full width - Old bridge abut on LB constricts flow to L. pier → L pier to R. Abut used for width

1622-45  
 23-45 Old Bridge Abut on L. B  
 24-45 RB  
 25-45 LB  
 26-R. Abut  
 27-L. Abut  
 28-45 Face  
 29-ID

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>8730</u>	<u>14700</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.6</u>	<u>1.5</u>
Contraction scour depth (yca), in feet	<u>17.9</u>	<u>19.2</u>
Pier scour depth (yps), in feet	<u>14.0</u>	<u>14.2</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>6.3</u>
Flow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required