

Dup  
OK-RAT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 55060438 Date 10-10-12 Initials RFT Region (A B C D)   
 Site  Location 1.8 mi S Hwy 12 on 455 Ave  
 $Q_{100} =$  1000 by: drainage area ratio  flood freq. anal.  regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1000 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 37 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 37  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.4

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 36.86 ft\*  $q_2 = Q_2/W_2 =$  27.1 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3.7 ft/s Final  $y_2 = q_2/V_2 =$  7.4 ft  $\Delta h =$  0.3 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

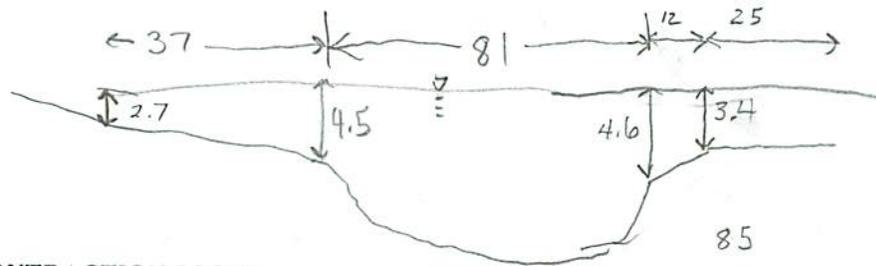
Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = dry ft  
 Low Steel Elev. = 9.0 ft  
 $n$  (Channel) = .033  
 $n$  (LOB) = .030  
 $n$  (ROB) = .030  
 Pier Width = 1.33 ft  
 Pier Length = 1.33 ft  
 # Piers for 100 yr = 1 ft

moved approach upstream to get out of ditch



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  81 ft

Width of left overbank flow at approach,  $W_{lob} =$  37 ft

Average left overbank flow depth,  $y_{lob} =$  3.6 ft

Width of right overbank flow at approach,  $W_{rob} =$  37 ft

Average right overbank flow depth,  $y_{rob} =$  3.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$   From Figure 9  $W_2$  (effective) =  ft  $y_{cs} =$   ft

riprap lines channel through bridge. Assume CWCS

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.6 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  0.85 ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  13.21 ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  0.01 ft

If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$

From Figure 10,  $y_{cs} =$  0 ft

PGRM: Contract

PGRM: CWCSNEW

PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.24

Using pier width  $a$  on Figure 11,  $\xi =$  5.9 Pier scour  $y_{ps} =$  4.8 ft

PGRM: Pier

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.6 ft right abutment,  $y_{aRT} =$  3.6 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, (0.82) for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.6 and  $\psi_{RT} =$  12.6

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  18.7 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  18.7 ft

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 55060438 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) (D)  
 Site \_\_\_\_\_ Location 1.8 mi S Hwy 12 on 455 Ave  
 $Q_{500} =$  1600 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1600 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 37 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 37

Avg. flow depth at bridge,  $y_2$  iteration = 9.3

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 36.86 ft\*  $q_2 = Q_2/W_2 =$  43.4 ft<sup>2</sup>/s

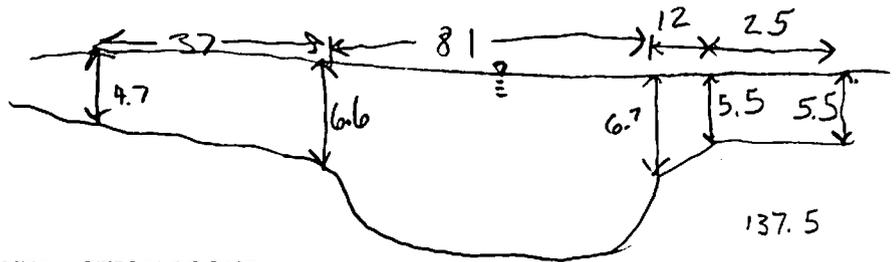
Bridge Vel,  $V_2 =$  4.7 ft/s Final  $y_2 = q_2/V_2 =$  9.3 ft  $\Delta h =$  0.4 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = diy ft  
 Low Steel Elev. = 9.0 ft  
 $n$  (Channel) = .033  
 $n$  (LOB) = .030  
 $n$  (ROB) = .030  
 Pier Width = 1.33 ft  
 Pier Length = 1.33 ft  
 # Piers for 500 yr = 1 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  81 ft

Width of left overbank flow at approach,  $W_{lob} =$  37 ft

Average left overbank flow depth,  $y_{lob} =$  5.65 ft

Width of right overbank flow at approach,  $W_{rob} =$  37 ft

Average right overbank flow depth,  $y_{rob} =$  5.69 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

riprap lines channel through bridge Assume CWC S

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.6 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  1.06 ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  13.76 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  0.017 ft

If  $D_{50} \geq D_{c50}$   $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  0 ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.27

Using pier width  $a$  on Figure 11,  $\xi =$  5.9 Pier scour  $y_{ps} =$  4.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.65 ft right abutment,  $y_{aRT} =$  5.69 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, (0.82) for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  16.2 and  $\psi_{RT} =$  16.3

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  24.1 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  24.2 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWC S NEW

PRGM: Pic

PRGM: Abutment

Route 455 Ave Stream Big Sioux River MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 55060438 Location 1.8 mi S. Hwy 12 on 455 ave  
 GPS coordinates: N 45° 18.014' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 06.171' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 13.14 sq. mi.

The average bottom of the main channel was 13.5 ft below top of guardrail at a point 8.0 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1000</u>			Q <sub>500</sub> = <u>1600</u>		
Estimated flow passing through bridge	<u>1000</u>			<u>1600</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal Riprap has been placed all throughout bridge  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know past contraction, abutment and pier scour  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles  see photos Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

\* riprap will likely mitigate some of the estimated abutment scour

str. no.  
 approach from bridge  
 ROB from bridge  
 LOB from ditch

bridge from ditch  
 left abut.  
 rt. abut.  
 riprap lining bridge

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>1000</u>	<u>1600</u>
Flow depth at left abutment (yaLT), in feet	<u>3.6</u>	<u>5.65</u>
Flow depth at right abutment (yaRT), in feet	<u>3.6</u>	<u>5.69</u>
Contraction scour depth (y <sub>c</sub> ), in feet	<u>0</u>	<u>0</u>
Pier scour depth (y <sub>p</sub> ), in feet	<u>4.8</u>	<u>4.8</u>
Left abutment scour depth (y <sub>a</sub> ), in feet	<u>* 18.7</u>	<u>* 24.1</u>
Right abutment scour depth (y <sub>a</sub> ), in feet	<u>* 18.7</u>	<u>* 24.2</u>
Flow angle of attack	<u>5°</u>	<u>5°</u>

See Comments/Diagram for justification where required