| | SCOUR ANALYSIS AND REPORTING FORM |
|---|--|
| | Bridge Structure No. 55151250 Date 10-11-11 Initials ZT Region (A BCD) |
| | Site Location From Peever, 1E, 2N, 1.1 F |
| | Q ₁₀₀ = 3160 by: drainage area ratio flood freq. anal. regional regression eq. |
| | Bridge discharge $(Q_2) = 2590$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping) |
| "RegionA", "RegionB", C", or "RegionD" | Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = 39 ft. Flow angle at bridge = 0 o Abut. Skew = 0 o Effective Skew = 0 o Width (W ₂) iteration = 39 Avg. flow depth at bridge, y ₂ iteration = 11.5 |
| nA", Regi | Corrected channel width at bridge Section = W_2 times cos of flow angle = 39 ft* $q_2 = Q_2/W_2 = 66.4$ ft ² /s |
| egion | Bridge Vel, $V_2 = 5.8$ ft/s Final $y_2 = q_2/V_2 = 11.5$ ft $\Delta h = 0.7$ ft |
| 1: "R onc" | Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 12.2$ ft |
| GRN Regid | *NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q) If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, |
| <u> </u> | low point east of road is just below bridge deck (109') |
| | Water Surface Elev. = 0.7 ft Bridge will not pass est. Q100. Assume Qmax scour (Channel) = .028 OCCUPS at 11.5, or Q \sim 2590 |
| | $n(LOB) = \underbrace{078}_{+53} + \underbrace{53}_{-54}$ |
| | $ \frac{n (ROB) = 0.028}{Pier Width = 1.0} \text{ ft} 3.6 5.1 7.7 $ |
| | |
| | # Piers for $100 \text{ yr} = \frac{\text{O}}{\text{ft}}$ and $31.6 = 5$ |
| | CONTRACTION SCOUR |
| | Width of main channel at approach section $W_1 = 66$ ft |
| ract | Width of left overbank flow at approach, $W_{lob} = 78$ ft Average left overbank flow depth, $y_{lob} = 50$ ft |
| PGRM: Contract | Width of right overbank flow at approach, $W_{rob} = \frac{78}{78}$ ft Average right overbank flow depth, $y_{rob} = \frac{4-2}{2}$ ft $\frac{2}{5}$ bridge widths |
| PG | Live Bed Contraction Scour (use if bed material is small cobbles or finer) |
| | $x = 18.09$ From Figure 9 W_2 (effective) = 39 ft $y_{cs} = 16.7$ ft |
| PGRM: CWCSNEW | Clear Water Contraction Scour (use if bed material is larger than small cobbles) Estimated bed material $D_{50} = ft$ Critical approach velocity, $V_c = 11.17y_1^{1/6}D_{50}^{1/3} = ft/s$ |
| Æ: C | If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. |
| GR | $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =ft 	 If D_{50} >= D_{c50}, \chi = 0.0$ |
| | Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =ft$ |
| | |
| PGRM: Pier | PIER SCOUR CALCULATIONS |
| GRM | L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 = ft Froude # at bridge = Using pier width a on Figure 11, ξ = ft |
| Ā | Froude # at bridge = Osnig pust within a on Figure 11, ζ = |
| PGRM: Abutment | APUTMENT SCOUR CALCULATIONS Average flow depth blocked by: left abutment, $y_{aLT} = 5.0$ ft right abutment, $y_{aRT} = 4.2$ ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 1.5$ and $\psi_{RT} = 1.00$ |
| PG | Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 22.4$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 20.3$ ft |

| Route 125th St Stream Jorgenson 1 | Ziver | MRM | Dat | te | Init | ials | | | |
|--|------------------|--|----------|--|-------------|---|----------|--|--|
| Bridge Structure No. 55/5/1250 Loc | ation from | Peever. | 15 | 2 N. 1 | .15 | | | | |
| Bridge Structure No. 55151250 Location From Peever, 1E, 2N, 1.15 GPS coordinates: N 45° 34.342′ taken from: USL abutment centerline of \(\hat{1}\) MRM end \[\sqrt{96° 54.902′}\) Datum of coordinates: WGS84 \(\sqrt{NAD27}\) | | | | | | | | | |
| Drainage area = 131.21 (cont.) sq. mi. | | | | | | | | | |
| The state of the s | | | | | | | | | |
| The average bottom of the main channel was | | | | | | | | | |
| Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations. | | | | | | | | | |
| MISCELLANEOUS CONSIDERATIONS | | | | | | | | | |
| | | | | | 5180 | | 1 | | |
| Flows | $Q_{100} = 3160$ | | | $Q_{500} =$ | 2180 | | ł | | |
| Estimated flow passing through bridge | 2590 | | | | | | ł | | |
| Estimated road overflow & overtopping | Yes | 570 No | Possibly | Yes | No | Possibly | ł | | |
| Character of everter in a | 1 63 | NU | POSSIDIY | 1 68 | NO | 1 Ossibly | 1 | | |
| Chance of overtopping Chance of Pressure flow | 1/ | | 1 | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | | <u> </u> | 1 | | |
| | | | - | | | | | | |
| Armored appearance to channel | | | | | | + | ł | | |
| Lateral instability of channel | | <u> </u> | <u> </u> | L | <u> </u> | <u> </u> | i | | |
| Riprap at abutments? Yes | No. | / Marginal | | | | | | | |
| Riprap at abutments? Yes | | Niaigiliai | 1.00 | م مردا ب | · | | doc l | | |
| Evidence of past Scour? Yes No Don't know Contraction Scour pool waer | | | | | | | | | |
| Evidence of past Scour? Yes No Don't know contraction Scour pool under le Debris Potential? High Med X Low no piers National Pool under le Med X Low no piers | | | | | | | | | |
| | | | | | | | | | |
| Does scour countermeasure(s) appear to have been designed? | | | | | | | | | |
| Riprap Yes No Don't know NA | | | | | | | | | |
| Spur Dike Ye | esN | NoDor | i't know | NA_ | | | | | |
| Other YesNo Don't knowNA | | | | | | | | | |
| | | | | | | | | | |
| Bed Material Classification Based on Median Particle Size (D ₅₀) | | | | | | | | | |
| | ✓_ Gravel | | | Cobbles Boulders | | | | | |
| · | | | | | | | ******** | | |
| Size range, in mm <0.062 0.062-2. | 00 | 2.00-04 | | 7hoto5 | | ~230 | | | |
| C | | · | | | • | | | | |
| Comments, Diagrams & orientation of digital phot | | Struct | ure nu | mber | | | | | |
| Based on trash line on right | SC | Bridges | | | pproac | h | | | |
| over bank, whis social o | ۴ | 1221 000 | orlana l | , | • | | | | |
| to low steel this sp. J | | 1014 00 | a walaa. | .\. | | | | | |
| Based on trash line on right overbank, water level was close to low steel this spring or summer. Bridge section from approach icft overbank right overbank approach from bridge | | | | | | | | | |
| approach from bridge | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| Summary of Results | | | | | | | | | |
| | | Q100 | | | Q500 | |] | | |
| Bridge flow evaluated | | 2590 | | | | ····· | 1 | | |
| Flow depth at left abutment (yaLT), in feet | r | 5 | | | | | 1 | | |
| Flow depth at right abutment (yaRT), in feet | | 4.2 | | | | | 1 | | |
| Contraction scour depth (ycs), in feet | 16.7 | | | | | | 1 | | |
| Pier scour depth (yps), in feet | | NA | | | | *************************************** | 1 | | |
| Left abutment scour depth (yas), in feet | 22.4 | | | | | | 1 | | |
| Right abutment scour depth (yas), in feet | | zo.3 | , | | | |] | | |
| 1Flow angle of attack | | 0" | | | | |] | | |

Basin Characteristics from Provisional Stream Stats 10-7-11 Cont. D.A. = 131.21 PII = 0.92 100% Subregion A

Manually Calculated Peaks

 $Q_{100} = 3160 \text{ efs}$ $Q_{500} = 5180 \text{ efs}$