

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 55240041 Date 8/2/12 Initials Rat Region (A B C D)
Site Location 0.3 mi N of Rosholt on 473 Ave
Q100 = Q25 1320 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 1320 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

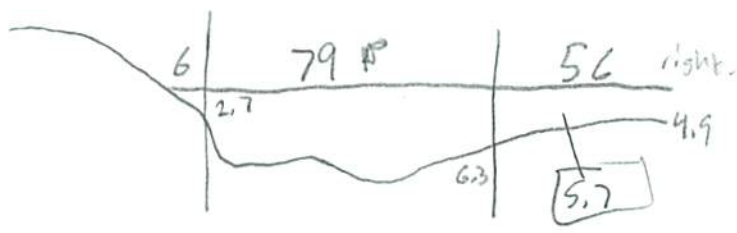
Bridge Width = 56 ft. Flow angle at bridge = 45 degrees Abut. Skew = 0 degrees Effective Skew = 45 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 39.6 ft\* q2 = Q2/W2 = 33.3 ft^2/s

Bridge Vel, V2 = 4.1 ft/s Final y2 = q2/V2 = 8.1 ft Delta h = 0.3 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 8.5 ft

\*NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0-0.5 ft
Low Steel Elev. = 9.4 ft
n (Channel) = 0.045
n (LOB) = 0.030
n (ROB) = 0.030
Pier Width = 1.55 ft
Pier Length = 1.55 ft
# Piers for 100 yr = 2



= left 6.3 = 4.9 sc

CONTRACTION SCOUR

Width of main channel at approach section W1 = 79 ft
Width of left overbank flow at approach, Wlob = 56 ft Average left overbank flow depth, ylob = 5.7 ft
Width of right overbank flow at approach, Wrob = 6 ft Average right overbank flow depth, yrob = 1.4 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 20.05 From Figure 9 W2 (effective) = 36.5 ft ycs = 17.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1 W1) =
Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) =
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [(q2/(D50^(1/3) y1^(7/6)))^(6/7) - y1 = From Figure 10, ycs =

PIER SCOUR CALCULATIONS

L/a ratio =
Froude # at bridge = 0.25
Correction factor for flow angle of attack (from Table 1), K2 = 1
Using pier width a on Figure 11, xi = 6.6 Pier scour yps = 5.4 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 5.7 ft right abutment, yaRT = 1.4 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 16.3 and psiRT = 5.9
Left abutment scour, yas = psiLT (K1/0.55) = 16.3 ft Right abutment scour yas = psiRT (K1/0.55) = 5.9 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 55240041 Date 8/3/12 Initials Lat Region (A B C D) D  
 Site \_\_\_\_\_ Location 0.3 mi. N of Rasholt on 473 Ave  
 $Q_{500} =$  Q<sub>500</sub> 1800 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1757 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 56 ft. Flow angle at bridge = 45 ° Abut. Skew = 0 ° Effective Skew = 45 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 39.6 ft\*  $q_2 = Q_2/W_2 =$  44.4 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.7 ft/s Final  $y_2 = q_2/V_2 =$  9.4 ft  $\Delta h =$  0.4 ft

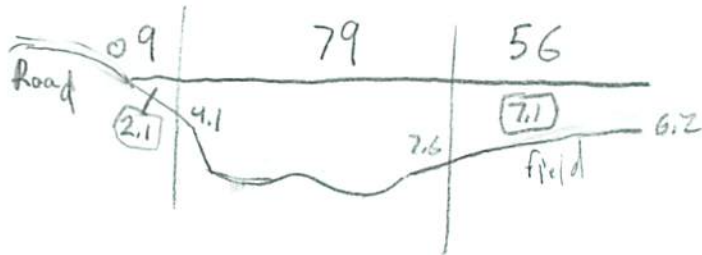
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0-0.5 ft  
 Low Steel Elev. = 9.4 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 1.55 ft  
 Pier Length = 1.55 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  79 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  56 ft Average left overbank flow depth,  $y_{lob} =$  7.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  9 ft Average right overbank flow depth,  $y_{rob} =$  2.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  24.87 From Figure 9  $W_2$  (effective) = 36.5 ft  $y_{cs} =$  20.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PGRM: Contract

PGRM: CWCNEW

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi =$  6.6 Pier scour  $y_{ps} =$  5.4 ft

PGRM: Pie

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  7.1 ft right abutment,  $y_{aRT} =$  2.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  18.8 and  $\psi_{RT} =$  8.6  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  18.8 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  8.6 ft

PGRM: Abutment



Route 473 Ave Stream Big Slough Ck MRM \_\_\_\_\_ Date 8/3/12 Initials RA  
 Bridge Structure No. 55240041 Location 0.3 mi N of Rosholt on 473 Ave  
 GPS coordinates: N 450 52' 35.2" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 960 43' 46.2" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 89.28 sq. mi.  
 The average bottom of the main channel was 13.2 ft below top of guardrail at a point 29 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>Q<sub>75</sub> 1320</u>			Q <sub>500</sub> = <u>Q<sub>50</sub> 1900</u>		
Estimated flow passing through bridge				1757		
Estimated road overflow & overtopping	0			43		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>				
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/2  
 25 | 162  
 5 | 474  
 10 | 789  
 25 | 1320  
 50 | 1900  
 100 | 2350  
 500 | 3850

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *heavy abutment, significant contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low *see pictures*

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left abutment  
 2) main channel  
 3) right abutment  
 4-6) right abutment  
 7-8) pier  
 9-11) left abutment  
 Note: noticeable flow west-east which contradicts map. Local resident confirmed flow moves west to east.

Summary of Results

	Q <sub>100</sub> <u>Q<sub>75</sub></u>	Q <sub>500</sub> <u>Q<sub>50</sub></u>
Bridge flow evaluated	1320	1757
Flow depth at left abutment (yaLT), in feet	5.7	7.1
Flow depth at right abutment (yaRT), in feet	4.4	2.1
Contraction scour depth (yca), in feet	17.7	20.3
Pier scour depth (ypp), in feet	5.4	5.4
Left abutment scour depth (yas), in feet	16.3	18.8
Right abutment scour depth (yas), in feet	5.9	6.6
Flow angle of attack	45	45

See Comments/Diagram for justification where required