

OK - Rat

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 56094010 Date 9-28-12 Initials RFT Region (A B C D)
Site Location 40345 221 St, James River
Q100 = 26400 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 26400 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

246/272

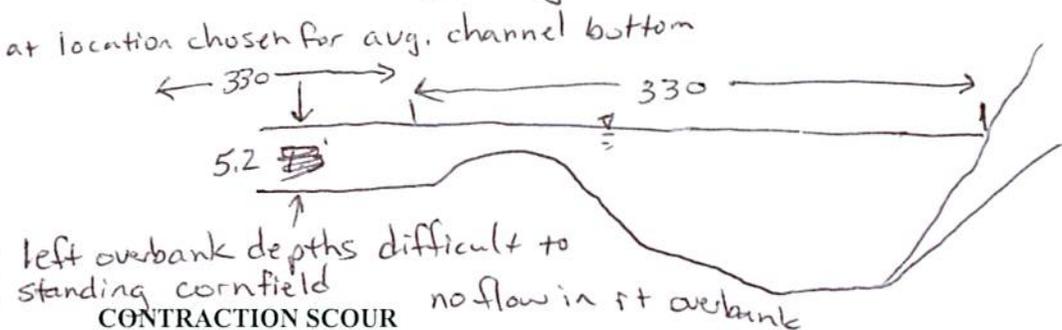
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 330 ft. Flow angle at bridge = 0 degrees Abut. Skew = 0 degrees Effective Skew = 0 degrees
Width (W2) iteration = 330 272 291 278 280
Avg. flow depth at bridge, y2 iteration = 12.6 13.9 13.4 13.7 13.7
Corrected channel width at bridge Section = W2 times cos of flow angle = 280 ft* q2 = Q2/W2 = 94.3 ft^2/s
Bridge Vel, V2 = 6.9 ft/s Final y2 = q2/V2 = 13.7 ft Delta h = 1.0 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 14.7 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,
road overflow will begin at y2 ~ 18.3 ft

Water Surface Elev. = 20.0 ft
Low Steel Elev. = 19 ft
n (Channel) = .03
n (LOB) = .04
n (ROB) = .029
Pier Width = 2.25 ft
Pier Length = 3.75 ft
Piers for 100 yr = 3



Width of main channel at approach section W1 = 330 ft
Width of left overbank flow at approach, Wlob = 330 ft Average left overbank flow depth, ylob = 5.2 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

PRGM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 5.41 From Figure 9 W2 (effective) = 273.3 ft ycs = 6.1 ft

PRGM: CWCNEW

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(1/6))^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PRGM: Pier

PIER SCOUR CALCULATIONS

L/a ratio = 1.667 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.33 Using pier width a on Figure 11, xi = 8.8 Pier scour yps = 7.4 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 5.2 ft right abutment, yart = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yart on figure 12, psiLT = 15.4 and psiRT = 0
Left abutment scour, yas = psiLT (K1/0.55) = 15.4 ft Right abutment scour yas = psiRT (K1/0.55) = 0 ft

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 56094010 Date _____ Initials _____ Region (A B C D) _____

Site _____ Location 40345 221 St

$Q_{500} =$ 45200 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____

Bridge discharge (Q_2) = 45200 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 330 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°

Width (W_2) iteration = 305 301

Avg. flow depth at bridge, y_2 iteration = 17.2 17.3

Corrected channel width at bridge Section = W_2 times cos of flow angle = 301 ft* $q_2 = Q_2/W_2 =$ 150.2 ft²/s

Bridge Vel, $V_2 =$ 8.7 ft/s Final $y_2 = q_2/V_2 =$ 17.3 ft $\Delta h =$ 1.5 ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 18.8 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2

Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

road overflow will occur at $y_2 \approx 18.3$, which is ~~below~~ has

Water Surface Elev. = 20.0 ft top width of water at bridge of $W_2 \approx 305$

Low Steel Elev. = 19 at avg bottom

n (Channel) = .030 mostly smooth, but some rocks

n (LOB) = .040 cornfield

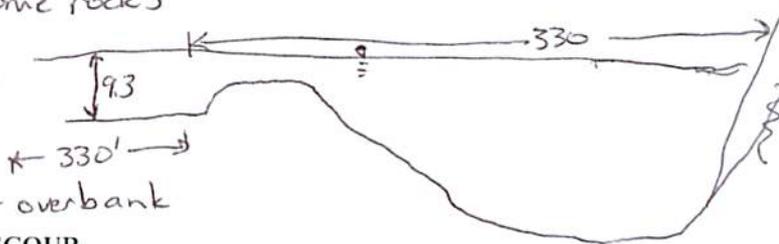
n (ROB) = .029 ungrazed pasture

Pier Width = 2.25 ft

Pier Length = 3.75 ft

Piers for 500 yr = 3 ft

no flow in right overbank



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 330 ft

Width of left overbank flow at approach, $W_{lob} =$ 330 ft Average left overbank flow depth, $y_{lob} =$ 9.3 ft

Width of right overbank flow at approach, $W_{rob} =$ 0 ft Average right overbank flow depth, $y_{rob} =$ 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 6.98 From Figure 9 W_2 (effective) = 296.5 ft $y_{cs} =$ 7.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.667 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1

Froude # at bridge = 0.37 Using pier width a on Figure 11, $\xi =$ 8.8 Pier scour $y_{ps} =$ 7.5 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 9.3 ft right abutment, $y_{aRT} =$ 0 ft

Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 20.8 and $\psi_{RT} =$ 0

Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 20.8 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 221 St Stream James River MRM _____ Date _____ Initials _____

Bridge Structure No. 56094010 Location 40345 221 St

GPS coordinates: N 44° 11.065' taken from: USL abutment centerline of \uparrow MRM end _____
W 98° 8.524' Datum of coordinates: WGS84 NAD27 _____

Drainage area = 14872.99 sq. mi. 14022.36

The average bottom of the main channel was 24.5 ft below top of guardrail at a point 56 ft from left abutment.

Method used to determine flood flows: _____ Freq. Anal. drainage area ratio _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

| | | | | | | |
|---------------------------------------|---------------------------------|-------------------------------------|----------|---------------------------------|-------------------------------------|-------------------------------------|
| Flows | Q ₁₀₀ = <u>26400</u> | | | Q ₅₀₀ = <u>45200</u> | | |
| Estimated flow passing through bridge | <u>26400</u> | | | <u>45200</u> | | |
| Estimated road overflow & overtopping | <u>0</u> | | | <u>0</u> | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly |
| Chance of overtopping | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Chance of Pressure flow | | <input checked="" type="checkbox"/> | | | | <input checked="" type="checkbox"/> |
| Armored appearance to channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Lateral instability of channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |

719
 2 | 1160
 5 | 6520
 10 | 15400
 25 | 37100
 50 | 63200
 100 | 100000
 500 | 240000

Riprap at abutments? _____ Yes No _____ Marginal _____ Evidence of past Scour? Yes _____ No _____ Don't know _____ Debris Potential? _____ High _____ Med 1 Low _____

Some field stone present, but it may be native material, not placed.

Does scour countermeasure(s) appear to have been designed?

Riprap _____ Yes No _____ Don't know _____ NA
 Spur Dike _____ Yes _____ No _____ Don't know NA
 Other _____ Yes _____ No _____ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay Sand _____ Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

structure no.
 approach from bridge
 LOB from bridge
 ROB from LOB approach
 bridge from approach

left abut.
 right abut.
 local erosion on left abut.

Summary of Results

| | | |
|--|--------------|--------------|
| | Q100 | Q500 |
| Bridge flow evaluated | <u>26400</u> | <u>45200</u> |
| Flow depth at left abutment (yaLT), in feet | <u>5.2</u> | <u>9.3</u> |
| Flow depth at right abutment (yaRT), in feet | <u>0</u> | <u>0</u> |
| Contraction scour depth (yca), in feet | <u>6.1</u> | <u>7.8</u> |
| Pier scour depth (ypp), in feet | <u>7.4</u> | <u>7.5</u> |
| Left abutment scour depth (yab), in feet | <u>15.4</u> | <u>20.8</u> |
| Right abutment scour depth (yab), in feet | <u>0</u> | <u>0</u> |
| If flow angle of attack | <u>0°</u> | <u>0°</u> |

See Comments/Diagram for justification where required