

OK-RAT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 56110046 Date 9-27-12 Initials RFT Region (A B C D)
Site Location 22455 405th Ave, James River
Q100 = 26400 by: drainage area ratio [checked] flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 26400 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

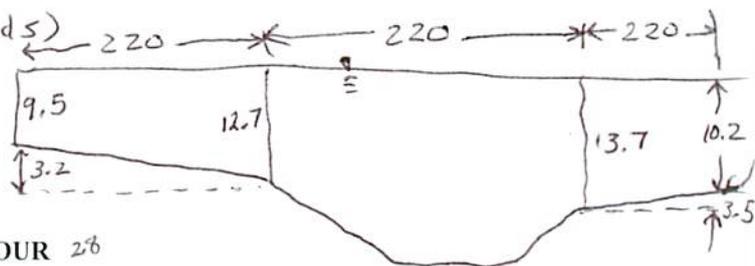
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 220 ft. Flow angle at bridge = 30 degrees Abut. Skew = 30 degrees Effective Skew = 0 degrees
Width (W2) iteration = 186 212 220
Avg. flow depth at bridge, y2 iteration = 18 16.9 16.6
Corrected channel width at bridge Section = W2 times cos of flow angle = 190.53 ft* q2 = Q2/W2 = 138.6 ft^2/s
Bridge Vel, V2 = 8.3 ft/s Final y2 = q2/V2 = 16.6 ft Delta h = 1.4 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 18.0 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

water will reach low steel at Q100

Water Surface Elev. = 20.0 ft
Low Steel Elev. = 15.3 ft (at location of avg. channel bottom)
n (Channel) = .023 mostly smooth + straight
n (LOB) = .025 (bare field w/ few weeds)
n (ROB) = .030 taller weeds
Pier Width = 3 ft
Pier Length = 3 ft
Piers for 100 yr = 2



CONTRACTION SCOUR 26

Width of main channel at approach section W1 = 220 ft
Width of left overbank flow at approach, Wlob = 220 ft Average left overbank flow depth, ylob = 11.1 ft
Width of right overbank flow at approach, Wrob = 220 ft Average right overbank flow depth, yrob = 11.95 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 20.59 From Figure 9 W2 (effective) = 184.5 ft ycs = 18.0 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6)) = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.36 Using pier width a on Figure 11, xi = 10.7 Pier scour yps = 9.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 11.1 ft right abutment, yarT = 11.95 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 22.2 and psiRT = 23.0
Left abutment scour, yas = psiLT (K1/0.55) = 22.2 ft Right abutment scour yas = psiRT (K1/0.55) = 23.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 56110046 Date _____ Initials _____ Region (A B C D) C

Site _____ Location 22455 405th Ave

$Q_{500} =$ 45300 by: drainage area ratio _____ flood freq. anal. regional regression eq. _____

Bridge discharge (Q_2) = 34248 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 220 ft. Flow angle at bridge = 30 ° Abut. Skew = 30 ° Effective Skew = 0 °

Width (W_2) iteration = 220

Avg. flow depth at bridge, y_2 iteration = 18.9

Corrected channel width at bridge Section = W_2 times cos of flow angle = 190.53 ft* $q_2 = Q_2/W_2 =$ 179.8 ft²/s

Bridge Vel, $V_2 =$ 9.5 ft/s Final $y_2 = q_2/V_2 =$ 18.9 ft $\Delta h =$ 1.9 ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 20.8 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

road overflow will occur at $y_2 \approx 18.9$ Assume this coincides with $Q_{max\ scour} \approx 34248$ cfs

Water Surface Elev. = 20.0 ft

Low Steel Elev. = 15.3 ft

n (Channel) = .023

n (LOB) = .025

n (ROB) = .030

Pier Width = 3 ft

Pier Length = 3 ft

Piers for 500 yr = 2 ft

CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 220 ft

Width of left overbank flow at approach, $W_{lob} =$ 220 ft Average left overbank flow depth, $y_{lob} =$ 13.9 ft

Width of right overbank flow at approach, $W_{rob} =$ 220 ft Average right overbank flow depth, $y_{rob} =$ 14.75 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 26.37 From Figure 9 W_2 (effective) = 184.5 ft $y_{cs} =$ 21.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1

Froude # at bridge = 0.39

Using pier width a on Figure 11, $\xi =$ 10.7 Pier scour $y_{ps} =$ 9.3 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 13.9 ft right abutment, $y_{aRT} =$ 14.75 ft

Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 24.6 and $\psi_{RT} =$ 25.3

Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) =$ 24.6 ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) =$ 25.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 405 Ave Stream James River MRM _____ Date _____ Initials _____

Bridge Structure No. 56110046 Location 22455 405th Ave

GPS coordinates: N 44° 7.993' taken from: USL abutment centerline of MRM end _____
W 98° 6.646' Datum of coordinates: WGS84 NAD27 _____

Drainage area = 14882.87 sq. mi. 14622.39

The average bottom of the main channel was 22.9 ft below top of guardrail at a point 37 ft from left abutment.
 Method used to determine flood flows: _____ Freq. Anal. drainage area ratio _____ regional regression equations.

stream stats
 ↓
7/3
 2 | 1160
 5 | 6580
 10 | 18100
 25 | 37100
 50 | 63200
 100 | 100000
 500 | 294000

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>26400</u>			Q ₅₀₀ = <u>45300</u>		
Estimated flow passing through bridge	<u>26400</u>			<u>34248</u>		
Estimated road overflow & overtopping				<u>11052</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? Yes No Marginal field stone + boulders
 Evidence of past Scour? Yes No Don't know
 Debris Potential? High Med Low

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes No Don't know NA possibly
 Spur Dike Yes No Don't know NA
 Other _____ Yes No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay X Sand _____ Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

str. no.
 approach from bridge
 LOB from bridge
 ROB from bridge
 Bridge from ROB
 left abut.
 rt. abut.
 concrete poured on rt abut
 flood debris on pier caps

Summary of Results

	Q100	Q500 max Scour
Bridge flow evaluated	<u>26400</u>	<u>34248</u>
Flow depth at left abutment (yaLT), in feet	<u>11.1</u>	<u>13.9</u>
Flow depth at right abutment (yaRT), in feet	<u>11.95</u>	<u>14.75</u>
Contraction scour depth (yca), in feet	<u>18.0</u>	<u>21.1</u>
Pier scour depth (yps), in feet	<u>9.2</u>	<u>9.3</u>
Left abutment scour depth (yas), in feet	<u>22.2</u>	<u>24.6</u>
Right abutment scour depth (yas), in feet	<u>23.0</u>	<u>25.3</u>
Flow angle of attack	<u>30° (0° eff)</u>	<u>30° (0° eff)</u>

See Comments/Diagram for justification where required