	Bridge Structure No. 58064260 Date 10-5-12 Initials RFT Region (ABCD)
	Site Location 2.7 W from S. edge Redfield on 1745+
	Q <sub>100</sub> = 16800 by: drainage area ratio flood freq. anal. regional regression eq.
	Bridge discharge $(Q_2) = 14.800$ (should be $Q_{100}$ unless there is a relief bridge, road overflow, or bridge overtopping)
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method
	Delta 1914 101 0 Delta 19 Delt
ionB	Width $(W_2)$ iteration = $158$ $157$
"Reg	Avg. flow depth at bridge, y <sub>2</sub> iteration = 14.9 15
A". ≷egid	Corrected channel width at bridge Section = $W_2$ times cos of flow angle = $\frac{1/49.3  \text{L}}{1000  \text{M}}$ ft <sup>2</sup> /s
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Bridge Vel, $V_2 = 7.5$ ft/s Final $y_2 = q_2/V_2 = 15.0$ ft $\Delta h = 1.2$ ft
	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 16$ , ft
:RM: cgiol	* NOTE: repeat above calculations until $y_2$ changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
	If y <sub>2</sub> is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,
	Water Surface Elev. = 4, / ft
	Low Steel Floy = 21./. A
	n  (Channel) = 0.030 $n  (LOB) = 0.035$ $n  (ROB) = 0.035$
	$n \text{ (LOB)} = \frac{35}{5.9}$
	Pier Width = $\frac{2.75}{1.75}$ ft Pier Length = $\frac{2.75}{1.75}$ ft
	Pier Length = $\frac{2.75}{100}$ ft ft $\frac{3^{31}}{100}$
	CONTRACTION SCOUR This site is somewhat impainded
_	Width of main channel at approach section $W_1 = 228$ ft from dam new Red field
ıtrac	Width of left overbank flow at approach, $W_{lob} = 18$ ft Average left overbank flow depth, $y_{lob} = 2.95$ ft
<u>.</u>	Width of right overbank flow at approach, $W_{rob} = 99$ ft Average right overbank flow depth, $y_{rob} = 4.28$ ft
'GRM: Contract	
	Live Bed Contraction Scour (use if bed material is small cobbles or finer)
	$x = 10.57$ From Figure 9 $W_2$ (effective) = 143.8 ft $y_{cs} = 11.6$ ft
}	Clear Water Contraction Scour (use if bed material is larger than small cobbles)
GKM: CWCSNE	Estimated bed material $D_{50} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$
× >	Estimated bed material $D_{50} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$ Critical approach velocity, $V_2 = \frac{11.17y_1^{1/6}D_{50}^{1/3}}{11.17y_1^{1/6}D_{50}^{1/3}} = \frac{ft/s}{11.17y_1^{1/6}D_{50}^{1/3}}$
Ξ	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
ž	
	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = \underline{\qquad \qquad \text{ft}}$ $Otherwise, \ \chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = \underline{\qquad \qquad }$ $\text{ft}$ $From \ \text{Figure 10, } y_{cs} = \underline{\qquad \qquad }$
7 25	PIER SCOUR CALCULATIONS
GRM: Pier	L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 = /
3	Froude # at bridge = $0.3  \text{H}$ Using pier width a on Figure 11, $\xi = 10.1$ Pier scour $y_{ps} = 8.6$ ft
_	ABUTMENT SCOUR CALCULATIONS
E E	Average flow depth blocked by: left abutment, $y_{al.T} = \frac{2.9.5}{1}$ right abutment, $y_{aRT} = \frac{4.28}{1}$
ğ	Shape coefficient $K_1$ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, (0.55 for spill-through
.: <u>\</u>	Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = 11.4$ and $\psi_{RT} = 13.7$
<b>5</b>	Left abutment scour, $v_{re} = w_{re} + (K_1/0.55) = 1/LU$ ft Right abutment scour $v_{re} = w_{re} + (K_1/0.55) = 13.7$ ft

Route 174 St Stream Intle	Creek	MRM	Dat	te	Ini	tials	_	
Bridge Structure No. 5806 4260	Location 2	7m: 11/f	Com S.	edos	Roda	idd on	1745	
GPS coordinates: <u>N 44° 51.906'</u> W 98° 34.676'	taken fron	n: USL abutmer	11 /	centerline o	fî MRM	end		
W 98° 34.676'	Datum of	coordinates: W	GS84	NAD27_				
Drainage area = $1403.48$ sq.	mi.							
The average bottom of the main channel was	28, 4 ft bel	ow top of guard	rail at a poin	ι 4 /	ft from le	ft abutment.		
Method used to determine flood flows:F								
	_				•			
Flows		IEOUS CONSI	DEKATIO		3 30	<u>~ `</u>	1	
Estimated flow passing through bridge	<u> </u>	$Q_{100} = 16800$			$Q_{500} = 33900$			
Estimated road overflow & overtopping		0			33906			
Consideration	Yes	No	Possibly	Yes	No	Possibly	i	
Chance of overtopping		V	1 000.00			1 000.0.,	ĺ	
Chance of Pressure flow		V			V		i	
Armored appearance to channel					V		ĺ	
Lateral instability of channel								
Debris Potential?High  Does scour countermeasure(s) appear to have to Riprap  Spur Dike  Other  Bed Mate	Med been designed?YesYesYes erial Classificat	No Do No Do No Do ion Based on M	n't know n't know n't know edian Particl	NA NA		bud nis	Lib Lal	
Material Silt/Clay Sand	d	Gravel		Cobbles		Boulders		
Size range, in mm <0.062 0.06	2-2.00	2.00-64		64-250		>250		
Comments, Diagrams & orientation of digital p	photos							
str, no.	viah	tabut.						
bridge from approach								
FOB from BOB	appr	approach from bridge						
	• •							
ROB								
left abut.								
Summary of Results								

	Q100	Q500
Bridge flow evaluated	16800	3 3900
Flow depth at left abutment (yaLT), in feet	2,95	5, 8
Flow depth at right abutment (yaRT), in feet	4.28	7.76
Contraction scour depth (ycs), in feet	11,6	12.4
Pier scour depth (yps), in feet	8.6	8.8
Left abutment scour depth (yas), in feet	11.4	16.5
Right abutment scour depth (yas), in feet	13.7	19.6
1Flow angle of attack	180	180

See Comments/Diagram for justification where required

