

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 58190023 Date 7/18/12 Initials [signature] Region (A B C D)
Site 5030 Location from Brentford, 3.8 N, Mud Creek
Q100 = 11110700 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 76800 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 223 ft. Flow angle at bridge = 5 degrees Abut. Skew = 6 degrees Effective Skew = 5 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 222.15 ft* q2 = Q2/W2 = 322.6/223 = 1.45 ft/s

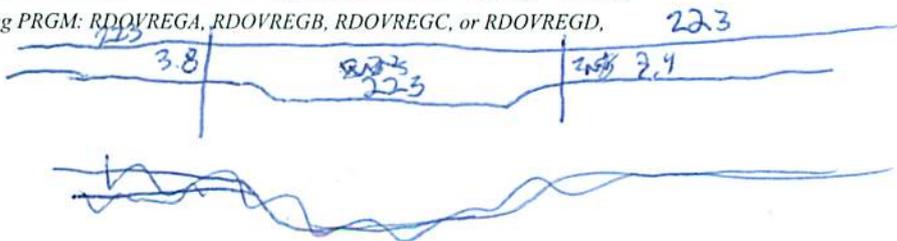
Bridge Vel, V2 = 2.4 ft/s Final y2 = q2/V2 = 1.45/2.4 = 0.6 ft Delta h = 0.2 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 0.8 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, 223

Water Surface Elev. = 0 ft
Low Steel Elev. = 11.1 ft
n (Channel) = 0.033
n (LOB) = 0.035
n (ROB) = 0.035
Pier Width = 2 ft
Pier Length = 2 ft
Piers for 100 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 223 ft
Width of left overbank flow at approach, Wlob = 223 ft Average left overbank flow depth, ylob = 3.8 ft
Width of right overbank flow at approach, Wrob = 223 ft Average right overbank flow depth, yrob = 3.4 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 3.97 From Figure 9 W2 (effective) = 216.2 ft ycs = 4.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s
Critical approach velocity, Vc = 11.52y1^1/6 D50^1/7 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.14 Using pier width a on Figure 11, xi = 8 Pier scour yps = 5.9 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 3.8 ft right abutment, yaRT = 3.4 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 12.9 and psiRT = 12.2
Left abutment scour, yas = psiLT(K1/0.55) = 12.9 ft Right abutment scour yas = psiRT(K1/0.55) = 12.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

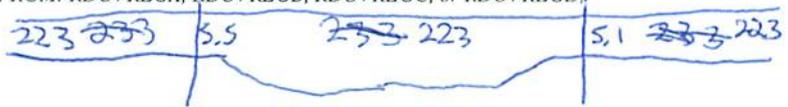
SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 58190023 Date 7/18/12 Initials RAJ Region (A B C D) (D)
 Site 220' Location from Brentford, 3.8 N
 $Q_{500} = \frac{Q_{100} \cdot 79000}{149000}$ by: drainage area ratio ✓ flood freq. anal. _____ regional regression eq. ✓
 Bridge discharge (Q_2) = 10165 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)
6835

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 223 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °
 Width (W_2) iteration = _____
 Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 222.15 ft* $q_2 = Q_2/W_2 = \frac{30.8}{4.26}$ ft²/s
 Bridge Vel, $V_2 = \frac{223}{2.8}$ ft/s Final $y_2 = q_2/V_2 = \frac{13.0}{11.1}$ ft $\Delta h = \frac{0.7}{11.2}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \frac{13.7}{11.2}$ ft

*NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(\alpha) + a \cos(\alpha)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.



Water Surface Elev. = 0 ft
 Low Steel Elev. = 2.0 ft
 n (Channel) = 0.033
 n (LOB) = 0.035
 n (ROB) = 0.035
 Pier Width = 2.0 ft
 Pier Length = 2.0 ft
 # Piers for 500 yr = 3 ft

CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \frac{223}{223}$ ft 223
 Width of left overbank flow at approach, $W_{lob} = \frac{223}{223}$ ft 223 Average left overbank flow depth, $y_{lob} = \frac{5.5}{5.5}$ ft
 Width of right overbank flow at approach, $W_{rob} = \frac{223}{223}$ ft 223 Average right overbank flow depth, $y_{rob} = \frac{5.1}{5.1}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = \frac{6.62}{6.62}$ From Figure 9 W_2 (effective) = 216.2 ft $y_{cs} = \frac{7.4}{7.4}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} = \frac{1}{1}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \frac{1}{1}$ ft/s
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \frac{1}{1}$ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} = \frac{1}{1}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \frac{1}{1}$ From Figure 10, $y_{cs} = \frac{1}{1}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = \frac{1}{1}$
 Froude # at bridge = 0.15 Using pier width a on Figure 11, $\xi = \frac{8}{8}$ Pier scour $y_{ps} = \frac{6}{6}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \frac{5.5}{5.5}$ ft right abutment, $y_{aRT} = \frac{5.1}{5.1}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \frac{15.9}{15.9}$ and $\psi_{RT} = \frac{15.2}{15.2}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \frac{15.9}{15.9}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \frac{15.2}{15.2}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

Route 395 Ave Stream Mud Creek MRM Date 7/18/12 Initials Lat

Bridge Structure No. 58190023 Location from Brentford, 3.8 N

GPS coordinates: N 45° 12' 40.9" taken from: USL abutment centerline of \uparrow MRM end
W 98° 19' 45.9" Datum of coordinates: WGS84 NAD27

Drainage area = 652.73 sq. mi. 563.27

The average bottom of the main channel was 16.6 ft below top of guardrail at a point 53 ft from left abutment.

Method used to determine flood flows: Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS Q₁₀₀ 7200

| Flows | Q ₅₀ 5030 | | | Q ₁₀₀ 7200 | | | Q ₅₀₀ 14300 | | |
|---------------------------------------|----------------------|-------------------------------------|----------|-------------------------------------|-------------------------------------|-------------------------------------|------------------------|-------------------------------------|-------------------------------------|
| Estimated flow passing through bridge | 5030 | | | 7200 | | | 6835 | | |
| Estimated road overflow & overtopping | 0 | | | 0 | | | 3634 | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly | Yes | No | Possibly |
| Chance of overtopping | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> |
| Chance of Pressure flow | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | | | | |
| Armored appearance to channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Lateral instability of channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |

7/12

| | |
|-----|-------|
| 2 | 243 |
| 5 | 893 |
| 10 | 1710 |
| 25 | 3330 |
| 50 | 5030 |
| 100 | 7200 |
| 500 | 14300 |

Riprap at abutments? Yes No Marginal
 Evidence of past Scour? Yes No Don't know *minor pier/contractor*
 Debris Potential? High Med Low

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes No Don't know NA
 Spur Dike Yes No Don't know NA
 Other Yes No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

| Material | Silt/Clay <input checked="" type="checkbox"/> | Sand <input type="checkbox"/> | Gravel <input type="checkbox"/> | Cobbles <input type="checkbox"/> | Boulders <input type="checkbox"/> |
|-------------------|---|-------------------------------|---------------------------------|----------------------------------|-----------------------------------|
| Size range, in mm | <0.062 | 0.062-2.00 | 2.00-64 | 64-250 | >250 |

Comments, Diagrams & orientation of digital photos
 1). left abutment
 2). main channel
 3). right abutment
 4-4). pier
 5-6). right abutment
 7-8). left abutment
 9). pier scour
 10). main channel

Summary of Results

| | Q ₁₀₀ Q ₅₀ | Q ₅₀₀ Q ₁₀₀ |
|--|----------------------------------|-----------------------------------|
| Bridge flow evaluated | 5030 | 6835 |
| Flow depth at left abutment (yaLT), in feet | 3.8 | 5.5 |
| Flow depth at right abutment (yaRT), in feet | 3.9 | 5.1 |
| Contraction scour depth (yca), in feet | 4.6 | 7.4 |
| Pier scour depth (yps), in feet | 5.9 | 6 |
| Left abutment scour depth (yas), in feet | 12.9 | 15.9 |
| Right abutment scour depth (yas), in feet | 12.2 | 15.2 |
| Flow angle of attack | 5 | 5 |

See Comments/Diagram for justification where required