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SCOUR ANALYSIS AND REPORTING FORM

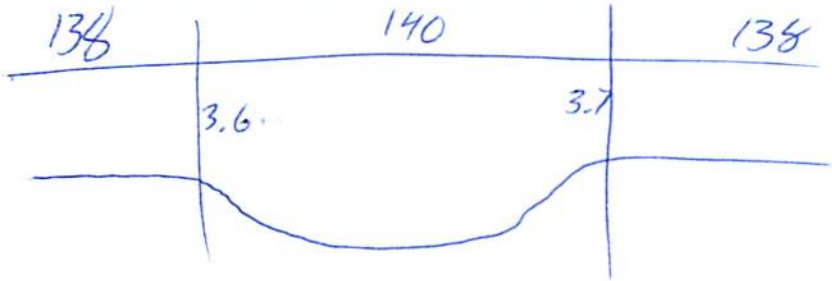
Bridge Structure No. 58205000 Date 6/28/11 Initials CW Region (A B C D)
Site Location from Stratford, SS, 0.5E
Q100 = 3390 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 3390 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 138 ft. Flow angle at bridge = 28 degrees Abut. Skew = 28 degrees Effective Skew = 0 degrees
Width (W2) iteration = 138 134
Avg. flow depth at bridge, y2 iteration = 9.9 9.9
Corrected channel width at bridge Section = W2 times cos of flow angle = 138 ft* q2 = Q2/W2 = 24.6 ft^2/s
Bridge Vel, V2 = 2.5 ft/s Final y2 = q2/V2 = 9.9 ft Delta h = 0.1 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 10 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = 10.3 ft
n (Channel) = 0.040
n (LOB) = 0.037
n (ROB) = 0.037
Pier Width = 1.1 ft
Pier Length = 1.1 ft
Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section W1 = 140 ft
Width of left overbank flow at approach, Wlob = 138 ft Average left overbank flow depth, ylob = 3.6 ft
Width of right overbank flow at approach, Wrob = 138 ft Average right overbank flow depth, yrob = 3.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 4.64 From Figure 9 W2 (effective) = 133.6 ft ycs = 5.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.52y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.14 Using pier width a on Figure 11, xi = 5.2 Pier scour yps = 3.9 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 3.6 ft right abutment, yaRT = 3.7 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 12.6 and psiRT = 12.7
Left abutment scour, yas = psiLT(K1/0.55) = 15.8 ft Right abutment scour yas = psiRT(K1/0.55) = 16.0 ft
12.6 23.2

Handwritten circled number 0.69 with a checkmark and initials CW.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

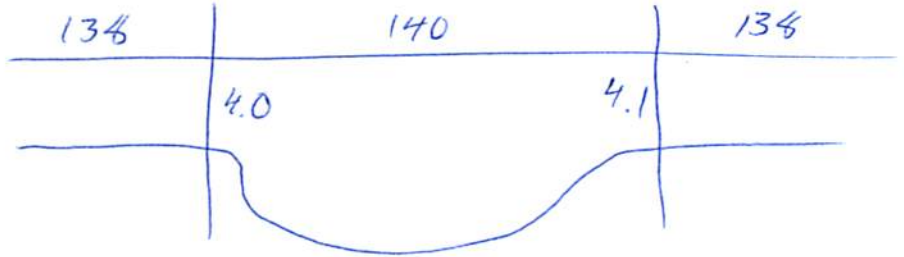
Bridge Structure No. 58205000 Date 6/29/11 Initials CW Region (A B C D) (D)
 Site _____ Location from Stratford, SS, 0.5E
 $Q_{500} =$ 7800 by: drainage area ratio flood freq. anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 3680 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 138 ft. Flow angle at bridge = 28 ° Abut. Skew = 28 ° Effective Skew = 0 °
 Width (W_2) iteration = 138
 Avg. flow depth at bridge, y_2 iteration = 15.3 > 10.3 → RD overflow
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 138 ft* $q_2 = Q_2/W_2 =$ 26.7 ft²/s
 Bridge Vel, $V_2 =$ 2.6 ft/s Final $y_2 = q_2/V_2 =$ 10.3 ft $\Delta h =$ 0.1 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 10.4 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(\alpha) + a \cos(\alpha)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = 10.3 ft
 n (Channel) = 0.040
 n (LOB) = 0.037
 n (ROB) = 0.037
 Pier Width = 1.1 ft
 Pier Length = 1.1 ft
 # Piers for 500 yr = 4 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 140 ft
 Width of left overbank flow at approach, $W_{lob} =$ 138 ft Average left overbank flow depth, $y_{lob} =$ 4.0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 138 ft Average right overbank flow depth, $y_{rob} =$ 4.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x =$ 5.32 From Figure 9 W_2 (effective) = 133.6 ft $y_{cs} =$ 6.0 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Froude # at bridge = 0.14 Using pier width a on Figure 11, $\xi =$ 5.2 Pier scour $y_{ps} =$ ~~2.9~~ ft 3.9

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 4.0 ft right abutment, $y_{aRT} =$ 4.1 ft
 Shape coefficient $K_1 =$ R 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 13.3 and $\psi_{RT} =$ 13.4
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 16.6 ft 13.3 Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 16.8 ft 24.4

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PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 148 St Stream Mud Creek MRM _____ Date 6/28/11 Initials CW
 Bridge Structure No. 58205000 Location from Stratford, 5S, 0.5 E
 GPS coordinates: N 45° 14' 29.3" taken from: USL abutment centerline of ↑ MRM end _____
W 96° 17' 58.3" Datum of coordinates: WGS84 NAD27 _____
 Drainage area = 637.09 sq. mi.
 The average bottom of the main channel was 14.1 ft below top of guardrail at a point 30 ft from left abutment.
 Method used to determine flood flows: ___ Freq. Anal. drainage area ratio ___ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>3390</u>			Q ₅₀₀ = <u>7800</u>		
Estimated flow passing through bridge	<u>3390</u>			<u>3688</u>		
Estimated road overflow & overtopping				<u>4112</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? ___ Yes No ___ Marginal
 Evidence of past Scour? Yes ___ No ___ Don't know
 Debris Potential? ___ High ___ Med Low

Does scour countermeasure(s) appear to have been designed?
 Riprap ___ Yes ___ No ___ Don't know NA
 Spur Dike ___ Yes ___ No ___ Don't know NA
 Other ___ Yes ___ No ___ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)
 Material Silt/Clay Sand ___ Gravel ___ Cobbles ___ Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos
 1670-1D 75- US L. Abut, 80- App XS looking @ L B
 71- US L 76- " 81- App XS looking @ RB
 72- US 77- Piers 82- L embankment
 73- US RB 78- L. Abut 83- R embankment
 74- US LB 79- US face bridge

Summary of Results

	Q ₁₀₀	Q ₅₀₀
Bridge flow evaluated	<u>3390</u>	<u>3688</u>
Flow depth at left abutment (yaLT), in feet	<u>3.6</u>	<u>4.0</u>
Flow depth at right abutment (yaRT), in feet	<u>3.7</u>	<u>4.1</u>
Contraction scour depth (y _{cs}), in feet	<u>5.3</u>	<u>6.0</u>
Pier scour depth (y _{ps}), in feet	<u>3.9</u>	<u>3.9</u>
Left abutment scour depth (y _{as}), in feet	<u>aw 15.4 12.6</u>	<u>aw 16.6 13.3</u>
Right abutment scour depth (y _{as}), in feet	<u>aw 16.0 23.2</u>	<u>aw 16.8 24.4</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required