

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 60190165 Date 7/10/12 Initials RAJ Region (A B C D)

Site Location East of Okobajo on 291 Ave

Q100 = Q25 3750 by: drainage area ratio flood freq. anal. regional regression eq. X

Bridge discharge (Q2) = 3750 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 94 ft. Flow angle at bridge = 10 degrees Abut. Skew = 0 degrees Effective Skew = 10 degrees

Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =

Corrected channel width at bridge Section = W2 times cos of flow angle = 92.57 ft\* q2 = Q2/W2 = 40.5 ft^2/s

Bridge Vel, V2 = 4.5 ft/s Final y2 = q2/V2 = 9 ft Delta h = 0.4 ft

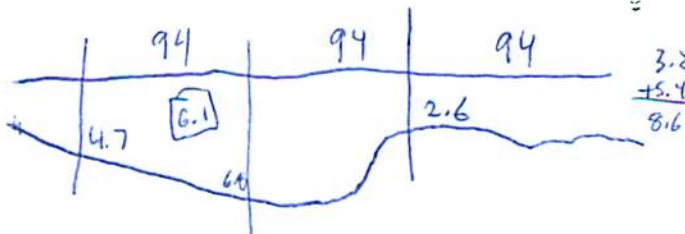
Average main channel depth at approach section, y1 = Delta h + y2 = 9.4 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(a) + a cos(a)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Handwritten calculations: 9.5 + 1.7 = 11.2, 2.16 - 1.9 = 0.26

Water Surface Elev. = 11.1 ft
Low Steel Elev. = 9.5 ft
n (Channel) = 0.035
n (LOB) = 0.030
n (ROB) = 0.030
Pier Width = 2.3 ft
Pier Length = 2.15 ft
# Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 94 ft

Width of left overbank flow at approach, Wlob = 94 ft

Average left overbank flow depth, ylob = 6.1 ft

Width of right overbank flow at approach, Wrob = 94 ft

Average right overbank flow depth, yrob = 2.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 7.72 From Figure 9 W2 (effective) = 88 ft ycs = 8.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

Note: large amount of cobbles under bridge; consider clear water contraction

PIER SCOUR CALCULATIONS

L/a ratio = 0.935

Correction factor for flow angle of attack (from Table 1), K2 = 1

Froude # at bridge = 0.26

Using pier width a on Figure 11, xi = 8.9 Pier scour yps = 2.3 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 6.1 ft right abutment, yarT = 2.6 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, psiLT = 17 and psiRT = 10.6

Left abutment scour, yas = psiLT(K1/0.55) = 30.9 ft Right abutment scour yas = psiRT(K1/0.55) = 19.3 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

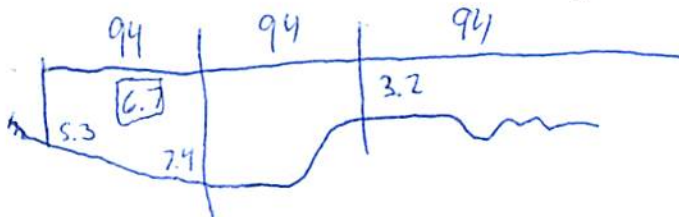
Bridge Structure No. 60190165 Date 7/10/12 Initials RAT Region (A B C D) (D)  
 Site \_\_\_\_\_ Location E of Okobajo on 291 Ave  
 $Q_{500} = Q_{500} 5960 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 4196 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)$

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 94 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 92.57 ft\*  $q_2 = Q_2/W_2 =$  453 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.8 ft/s Final  $y_2 = q_2/V_2 =$  9.5 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 9.5 ft  
 n (Channel) = 0.035  
 n (LOB) = 0.030  
 n (ROB) = ~~0.035~~ 0.03  
 Pier Width = 2.3 ft  
 Pier Length = 2.15 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  94 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  94 ft Average left overbank flow depth,  $y_{lob} =$  6.7 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  91 ft Average right overbank flow depth,  $y_{rob} =$  3.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  ~~8.65~~ 8.95 From Figure 9  $W_2$  (effective) = ~~82~~ 82 ft  $y_{cs} =$  ~~9.6~~ 9.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 0.935 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi =$  8.9 Pier scour  $y_{ps} =$  7.3 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.7 ft right abutment,  $y_{aRT} =$  3.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  18.1 and  $\psi_{RT} =$  11.9  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  32.8 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  21.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

Route 291 Ave Stream Okobajo Ck MRM \_\_\_\_\_ Date 7/10/12 Initials L.T.  
 Bridge Structure No. 60190165 Location East of Okobajo on 291 Ave  
 GPS coordinates: N 44° 39' 24.8" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 100° 19' 28.2" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 39.6 sq. mi.  
 The average bottom of the main channel was 15.3 ft below top of guardrail at a point 15.368 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>25</sub> <u>3750</u>			Q <sub>500</sub> = Q <sub>50</sub> <u>5960</u>		
Estimated flow passing through bridge	<u>3750</u>			<u>4196</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>1764</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/2  
 2 | 160  
 5 | 800  
 10 | 1730  
 25 | 3750  
 50 | 5960  
 100 | 8870  
 500 | 15700

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal - moderate amount of cobblestones at abutment/spilling into main channel  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know - minor pier contraction  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) left ab
- 2) main channel
- 3) right ab
- 4-5) left abutment
- 6) pier
- 7-8) right abutment
- 9) channel bed
- 10) main channel

Summary of Results

	Q <sub>100</sub> Q <sub>25</sub>	Q <sub>500</sub> Q <sub>50</sub>
Bridge flow evaluated	<u>3750</u>	<u>4196</u>
Flow depth at left abutment (yaLT), in feet	<u>6.1</u>	<u>6.7</u>
Flow depth at right abutment (yaRT), in feet	<u>2.6</u>	<u>3.2</u>
Contraction scour depth (y <sub>c</sub> ), in feet	<u>8.6</u>	<u>9.6</u> <u>9.8</u>
Pier scour depth (y <sub>p</sub> ), in feet	<u>7.3</u>	<u>7.3</u>
Left abutment scour depth (y <sub>a</sub> ), in feet	<u>30.4</u>	<u>32.8</u>
Right abutment scour depth (y <sub>a</sub> ), in feet	<u>14.3</u>	<u>21.6</u>
Flow angle of attack	<u>10</u>	<u>10</u>

- Note: bed channel is about 50% cobble/50% silt, coarse, clear water, contraction scour, pier 9.

See Comments/Diagram for justification where required