

Dup. OK-RAT

**SCOUR ANALYSIS AND REPORTING FORM**

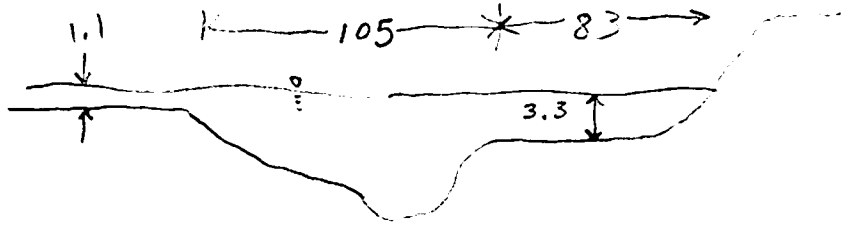
Bridge Structure No. 61390096 Date 10-12-12 Initials RFT Region (A B C D) B  
 Site \_\_\_\_\_ Location 2.5W + 1.4N of Hidden Timber on 150 Oil St or Hidden Timber Rd  
 $Q_{100} =$  1920 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.  Timber Rd  
 Bridge discharge ( $Q_2$ ) = 1920 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 93 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 93  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.3  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 93 ft\*  $q_2 = Q_2/W_2 =$  20.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.9 ft/s Final  $y_2 = q_2/V_2 =$  5.3 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = .035  
 $n$  (LOB) = .035  
 $n$  (ROB) = .035  
 Pier Width = 1.67 ft  
 Pier Length = 1.67 ft  
 # Piers for 100 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  105 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  93 ft Average left overbank flow depth,  $y_{lob} =$  1.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  83 ft Average right overbank flow depth,  $y_{rob} =$  3.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.49 From Figure 9  $W_2$  (effective) = 89.7 ft  $y_{cs} =$  4.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.3 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.1 ft right abutment,  $y_{aRT} =$  3.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  4.7 and  $\psi_{RT} =$  12  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  4.7 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  12 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 61390096 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A(B)C D)

Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} =$  3370 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.

Bridge discharge ( $Q_2$ ) = 3370 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 93 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width ( $W_2$ ) iteration = 93

Avg. flow depth at bridge,  $y_2$  iteration = 7.1

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 93 ft\*  $q_2 = Q_2/W_2 =$  36.2 ft<sup>2</sup>/s

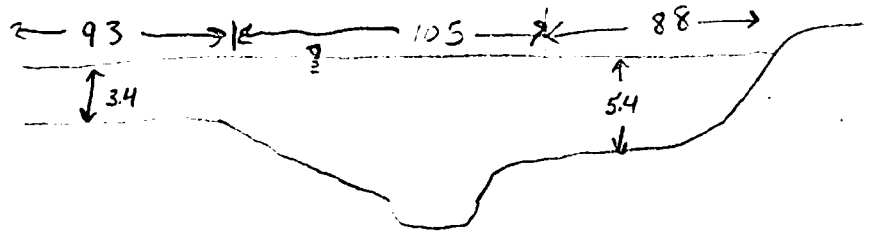
Bridge Vel,  $V_2 =$  5.1 ft/s Final  $y_2 = q_2/V_2 =$  7.1 ft  $\Delta h =$  0.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = .035  
 $n$  (LOB) = .035  
 $n$  (ROB) = .035  
 Pier Width = 1.67 ft  
 Pier Length = 1.67 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  105 ft

Width of left overbank flow at approach,  $W_{lob} =$  93 ft

Average left overbank flow depth,  $y_{lob} =$  3.4 ft

Width of right overbank flow at approach,  $W_{rob} =$  88 ft

Average right overbank flow depth,  $y_{rob} =$  5.4 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  7.58 From Figure 9  $W_2$  (effective) = 87.7 ft  $y_{cs} =$  2.4 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6.7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.34

Using pier width a on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.4 ft right abutment,  $y_{aRT} =$  5.4 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.2 and  $\psi_{RT} =$  15.7

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  12.2 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  15.7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Hidden

Route Timber Rd Stream Antelope Creek MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
Bridge Structure No. 61390096 Location 2.5 W + 1.4 N of Hidden Timber on 150 Q1 St  
GPS coordinates: N 43° 15.119' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 100° 28.294' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 167 sq. mi.

The average bottom of the main channel was 12 ft below top of guardrail at a point 45 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1920</u>			Q <sub>500</sub> = <u>3370</u>		
Estimated flow passing through bridge	<u>1920</u>			<u>3370</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know left abut. + pier  
Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand <sup>fine</sup> X Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Str. no. right abut. pier scour remnant  
bridge from approach left abut  
LOB approach from  
ROB bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>1920</u>	<u>3370</u>
Flow depth at left abutment (yaLT), in feet	<u>1.1</u>	<u>3.4</u>
Flow depth at right abutment (yaRT), in feet	<u>3.3</u>	<u>5.4</u>
Contraction scour depth (yca), in feet	<u>4.1</u>	<u>2.4</u>
Pier scour depth (yps), in feet	<u>5.8</u>	<u>5.9</u>
Left abutment scour depth (yas), in feet	<u>4.7</u>	<u>12.2</u>
Right abutment scour depth (yas), in feet	<u>12.0</u>	<u>15.7</u>
Flow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required