

OK TET

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 62085390 Date 8/17/11 Initials CW Region (A) B (C) D
Site Location 1.5 mi W of HWY 53 on 289 St
Q100 = 838 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 838 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

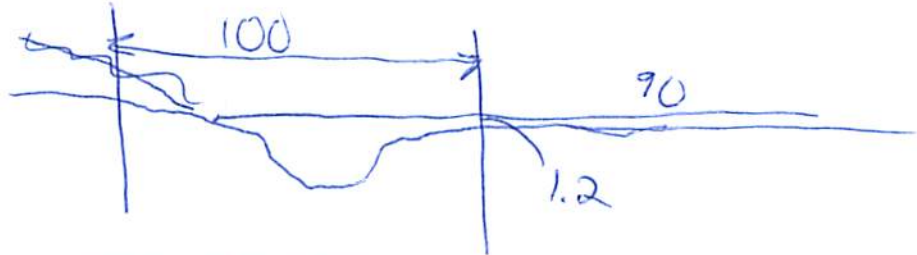
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 90 ft. Flow angle at bridge = 12 degrees Abut. Skew = 0 degrees Effective Skew = 12 degrees
Width (W2) iteration = 90
Avg. flow depth at bridge, y2 iteration = 3.5 Vert Wall
Corrected channel width at bridge Section = W2 times cos of flow angle = 88.03 ft* q2 = Q2/W2 = 9.5 ft^2/s
Bridge Vel, V2 = 2.7 ft/s Final y2 = q2/V2 = 3.5 ft Delta h = 0.1 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 3.6 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = ft
Low Steel Elev. = ft
n (Channel) = 0.035
n (LOB) = 0.035
n (ROB) = 0.035
Pier Width = 1.65 ft
Pier Length = 1.65 ft
Piers for 100 yr = 3



CONTRACTION SCOUR

Width of main channel at approach section W1 = 100 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0.0 ft
Width of right overbank flow at approach, Wrob = 90 ft Average right overbank flow depth, yrob = 1.2 ft

PGRM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 1.36 From Figure 9 W2 (effective) = 83.1 ft ycs = 1.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.17y1^(1/6)D50^(1/3) = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^(1/3)y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PGRM: CWCSNEW

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.25 Using pier width a on Figure 11, xi = 6.9 Pier scour yps = 5.6 ft

PGRM: Pier

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 0.0 ft right abutment, yaRT = 1.2 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 0.0 and psiRT = 5.1
Left abutment scour, yas = psiLT(K1/0.55) = 0.0 ft Right abutment scour yas = psiRT(K1/0.55) = 5.1 ft

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

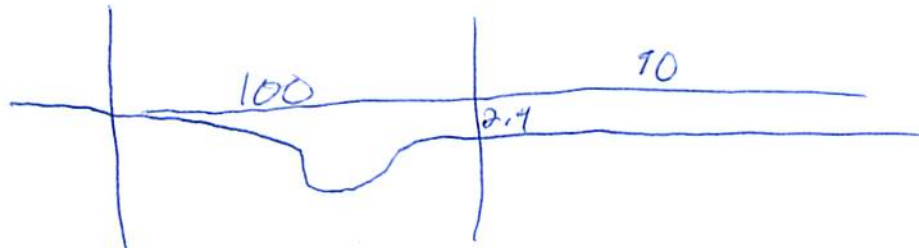
Bridge Structure No. 62085390 Date 8/17/11 Initials Cur Region (A) (B) C D
 Site _____ Location 1.5 mi. W of HWY 53 on 289 St
 $Q_{500} =$ 1370 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = 1370 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 90 ft. Flow angle at bridge = 12 ° Abut. Skew = 0 ° Effective Skew = 12 °
 Width (W_2) iteration = 90
 Avg. flow depth at bridge, y_2 iteration = 4.5 Vert Wall
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 84.03 ft* $q_2 = Q_2/W_2 =$ 15.6 ft²/s
 Bridge Vel, $V_2 =$ 3.4 ft/s Final $y_2 = q_2/V_2 =$ 4.5 ft $\Delta h =$ 0.2 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 4.8 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = _____ ft
 n (Channel) = 0.035
 n (LOB) = 0.035
 n (ROB) = 0.035
 Pier Width = 1.65 ft
 Pier Length = 1.65 ft
 # Piers for 500 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 100 ft
 Width of left overbank flow at approach, $W_{lob} =$ 0 ft Average left overbank flow depth, $y_{lob} =$ 0.0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 90 ft Average right overbank flow depth, $y_{rob} =$ 2.4 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 2.62 From Figure 9 W_2 (effective) = 43.1 ft $y_{cs} =$ 3.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [(q_2/(D_{50}^{1/3} y_1^{7/6}))^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Froude # at bridge = 0.29 Using pier width a on Figure 11, $\xi =$ 6.9 Pier scour $y_{ps} =$ 5.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0.0 ft right abutment, $y_{aRT} =$ 2.4 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0.0 and $\psi_{RT} =$ 9.8
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 0.0 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 9.8 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 289 St Stream Willow CK MRM _____ Date 8/17/11 Initials CH
 Bridge Structure No. 62085370 Location 1.5 mi W of Hwy 53 on 289 St
 GPS coordinates: N 43° 12' 46.1" taken from: USL abutment X centerline of \uparrow MRM end _____
W 100° 04' 33.6" Datum of coordinates: WGS84 X NAD27 _____

Drainage area = 40.41 sq. mi.

The average bottom of the main channel was 11.4 ft below top of guardrail at a point 58 ft from left abutment.

Method used to determine flood flows: ___ Freq. Anal. ___ drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

P/c Calc'd 8/8

Flows	Q ₁₀₀ = <u>838</u>			Q ₅₀₀ = <u>1370</u>			2	106
Estimated flow passing through bridge	<u>838</u>			<u>1370</u>			5	226
Estimated road overflow & overtopping							10	338
Consideration	Yes	No	Possibly	Yes	No	Possibly	25	504
Chance of overtopping		<u>X</u>			<u>X</u>		50	660
Chance of Pressure flow		<u>X</u>			<u>X</u>		106	838
Armored appearance to channel		<u>X</u>			<u>X</u>		500	1370
Lateral instability of channel			<u>X</u>			<u>X</u>		

Riprap at abutments? ___ Yes X No ___ Marginal

Evidence of past Scour? ___ Yes ___ No X Don't know *channel cutting toward R. Abut*

Debris Potential? ___ High X Med ___ Low

Does scour countermeasure(s) appear to have been designed?

Riprap ___ Yes ___ No ___ Don't know X NA

Spur Dike ___ Yes ___ No ___ Don't know X NA

Other ___ Yes ___ No ___ Don't know X NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay X Sand ___ Gravel ___ Cobbles ___ Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1882-1D
 83-LS
 84-USRB
 85-USLB
 86-L. Abut
 87-R. Abut
 88-US Face

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>838</u>	<u>1370</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>1.2</u>	<u>2.4</u>
Contraction scour depth (y _{cs}), in feet	<u>1.8</u>	<u>3.2</u>
Pier scour depth (y _{ps}), in feet	<u>5.6</u>	<u>5.7</u>
Left abutment scour depth (y _{as}), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y _{as}), in feet	<u>5.1</u>	<u>9.8</u>
Flow angle of attack	<u>12°</u>	<u>12°</u>

See Comments/Diagram for justification where required