

OK RT

SCOUR ANALYSIS AND REPORTING FORM

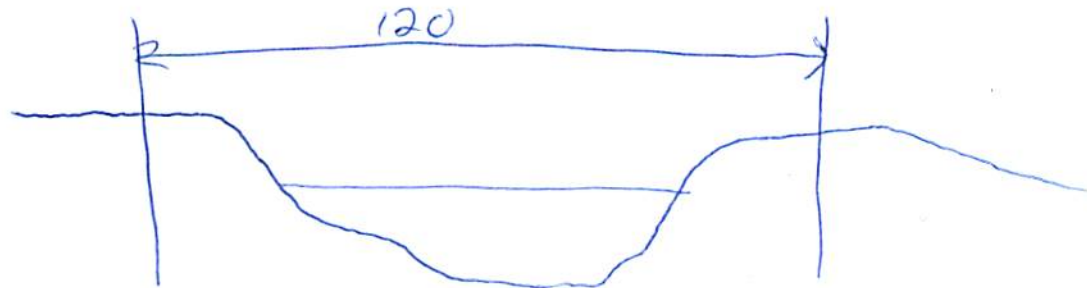
Bridge Structure No. 62229220 Date 8/16/11 Initials CAJ Region (A B C D)
Site Location 5.4 mi N + 2.9 mi E of Winner on 272 St
Q100 = 4610 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 4610 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 116 ft. Flow angle at bridge = 0 degrees Abut. Skew = 0 degrees Effective Skew = 0 degrees
Width (W2) iteration = 116 88 90
Avg. flow depth at bridge, y2 iteration = 7.4 8.6 8.5
Corrected channel width at bridge Section = W2 times cos of flow angle = 90 ft\* q2 = Q2/W2 = 51.2 ft^2/s
Bridge Vel, V2 = 6.0 ft/s Final y2 = q2/V2 = 8.5 ft Delta h = 0.7 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 9.2 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = ft
Low Steel Elev. = ft
n (Channel) = 0.040
n (LOB) = 0.035
n (ROB) = 0.045
Pier Width = 2.0 ft
Pier Length = 2.0 ft
# Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 120 ft
Width of left overbank flow at approach, Wlob = 0.0 ft Average left overbank flow depth, ylob = 0.0 ft
Width of right overbank flow at approach, Wrob = 116 ft 0.0 Average right overbank flow depth, yrob = 1.4 ft 0.0

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 3.64 From Figure 9 W2 (effective) = 86 ft ycs = 4.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = ft From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.36 Using pier width a on Figure 11, xi = 8.0 Pier scour yps = 6.9 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 0.0 ft right abutment, yaRT = 0.0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 0.0 and psiRT = 0.0
Left abutment scour, yas = psiLT (K1/0.55) = 0.0 ft Right abutment scour yas = psiRT (K1/0.55) = 0.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

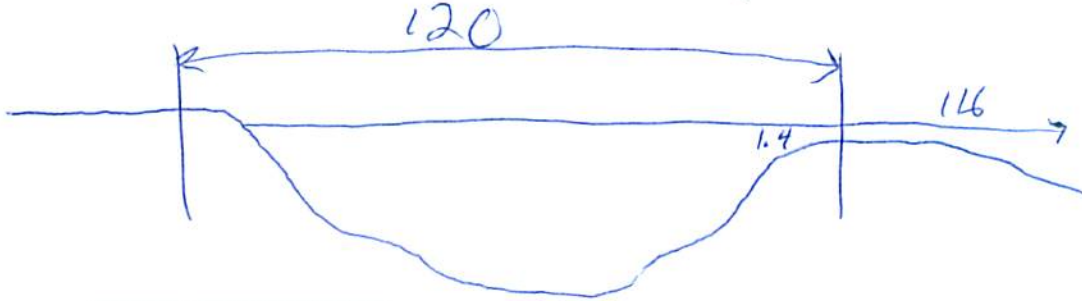
Bridge Structure No. 62229220 Date 8/16/11 Initials Ch Region (A B C D) B  
 Site \_\_\_\_\_ Location 5.4 N + 2.9 E of Winner on 272 St  
 $Q_{500} = 7730$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 7730 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 116 ft. 116 Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 9.8 116  
 Avg. flow depth at bridge,  $y_2$  iteration = 9.8 vert wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 116 ft\*  $q_2 = Q_2/W_2 = 66.6$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 6.4$  ft/s Final  $y_2 = q_2/V_2 = 9.8$  ft  $\Delta h = 1.0$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 10.7$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.045  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 120$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 0$  ft Average left overbank flow depth,  $y_{lob} = 0.0$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 116$  ft Average right overbank flow depth,  $y_{rob} = 1.4$  ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x = 1.1$  From Figure 9  $W_2$  (effective) = 112 ft  $y_{cs} = 1.6$  ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 = 6.0$   
 Froude # at bridge = 0.38 Using pier width a on Figure 11,  $\xi = 8.0$  Pier scour  $y_{ps} = 6.9$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 0.0$  ft right abutment,  $y_{aRT} = 1.4$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0.0$  and  $\psi_{RT} = 5.9$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 0.0$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 5.9$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

Route 272 St Stream Thunder Ck MRM \_\_\_\_\_ Date 8/16/11 Initials Car  
 Bridge Structure No. 62229220 Location 5.4 mi N + 2.9 mi E of Wimmer on 272 St  
 GPS coordinates: N 43° 27' 31.2" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 99° 47' 37.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 82.7 sq. mi.  
 The average bottom of the main channel was 16.4 ft below top of guardrail at a point 63 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

PK calc'd 8/8  
 2 308  
 5 936  
 10 1610  
 25 2600  
 50 3540  
 100 4610  
 500 7730

Flows	Q <sub>100</sub> = <u>4610</u>			Q <sub>500</sub> = <u>7730</u>		
Estimated flow passing through bridge	<u>4610</u>			<u>7730</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *At approach XS + in ditch*  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low *Log Jam*

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1941 - ID  
 42 - US  
 43 - US RB  
 44 - US LB  
 45 - L. Abut  
 46 - R. Abut  
 47 - US Face

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>4610</u>	<u>7730</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>1.4</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>4.3</u>	<u>1.6</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.7</u>	<u>6.9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>5.9</u>
Flow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required