

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 62234220 Date 8/16/11 Initials CW Region (A) B (C) D

Site Location 5.4 mi N + 3.3 mi E of Winner on 272 St

Q100 = 1450 by: drainage area ratio flood freq. anal. regional regression eq. [check]

Bridge discharge (Q2) = 1450 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 70 ft. Flow angle at bridge = 30 degrees Abut. Skew = 0 degrees Effective Skew = 30 degrees

Width (W2) iteration = 70

Avg. flow depth at bridge, y2 iteration = 5.7 Vert Wall

Corrected channel width at bridge Section = W2 times cos of flow angle = 60.62 ft q2 = Q2/W2 = 23.9 ft^2/s

Bridge Vel, V2 = 4.2 ft/s Final y2 = q2/V2 = 5.7 ft Delta h = 0.4 ft

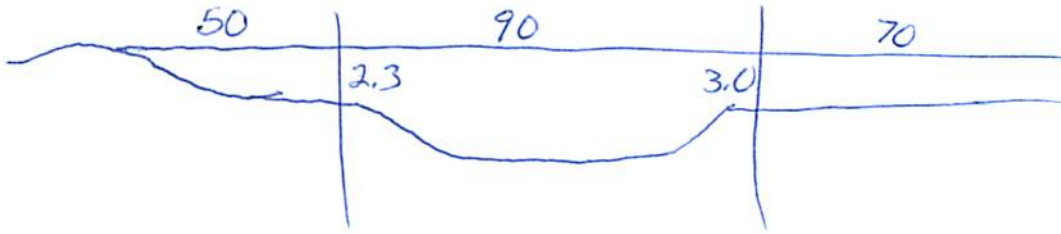
Average main channel depth at approach section, y1 = Delta h + y2 = 6.0 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

- Water Surface Elev. = ft
Low Steel Elev. = 4.3 ft
n (Channel) = 0.060
n (LOB) = 0.030
n (ROB) = 0.030
Pier Width = 2.0 ft
Pier Length = 2.0 ft
# Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 90 ft

Width of left overbank flow at approach, Wlob = 50 ft Average left overbank flow depth, ylob = 2.3 ft

Width of right overbank flow at approach, Wrob = 70 ft Average right overbank flow depth, yrob = 3.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 10.35 From Figure 9 W2 (effective) = 56.6 ft ycs = 11.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PGRM: Contract

PGRM: CWC/SNEW

PGRM: Pier

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0

Froude # at bridge = 0.31 Using pier width a on Figure 11, xi = 8.0 Pier scour yps = 6.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yALT = 2.3 ft right abutment, yART = 3.0 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yALT and yART on figure 12, psiLT = 9.4 and psiRT = 11.5

Left abutment scour, yas = psiLT(K1/0.55) = 9.4 ft Right abutment scour yas = psiRT(K1/0.55) = 11.5 ft

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

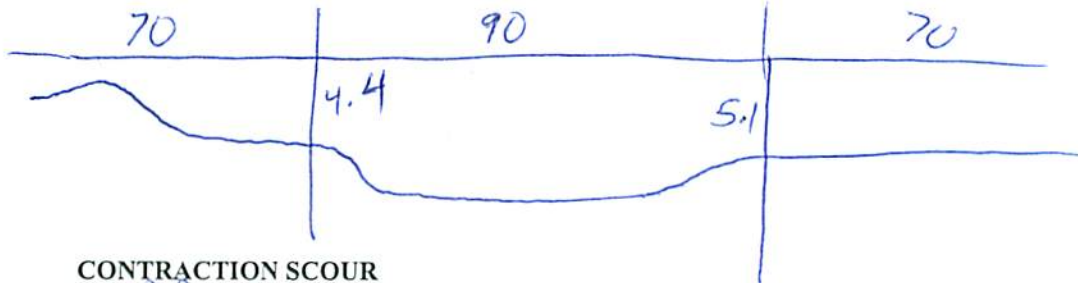
Bridge Structure No. 62234220 Date 8/16/11 Initials CW Region (A)(B)(C)(D) B  
 Site \_\_\_\_\_ Location 5.4 mi N + 3.3 mi E of Winner on 272 St  
 $Q_{500} = \underline{2480}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 2480 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 70 ft. Flow angle at bridge = 30° Abut. Skew = 0° Effective Skew = 30°  
 Width ( $W_2$ ) iteration = 70  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.5 Vert wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 60.62 ft\*  $q_2 = Q_2/W_2 = \underline{40.9}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{5.4}$  ft/s Final  $y_2 = q_2/V_2 = \underline{7.5}$  ft  $\Delta h = \underline{0.6}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{8.1}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 4.3 ft  
 n (Channel) = 0.060  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{90}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{70}$  ft Average left overbank flow depth,  $y_{lob} = \underline{4.4}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{70}$  ft Average right overbank flow depth,  $y_{rob} = \underline{5.1}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = \underline{21.28}$  From Figure 9  $W_2$  (effective) = 56.6 ft  $y_{cs} = \underline{18.4}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1.0}$   
 Froude # at bridge = 0.35 Using pier width a on Figure 11,  $\xi = \underline{8.0}$  Pier scour  $y_{ps} = \underline{6.8}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{4.4}$  ft right abutment,  $y_{aRT} = \underline{5.1}$  ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{14.0}$  and  $\psi_{RT} = \underline{15.2}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{14.0}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{15.2}$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 272 St Stream Dog Ear Crk MRM Date 5/16/11 Initials Lu  
 Bridge Structure No. 62234220 Location 5.4 mi N + 3.3 mi E of Winner on 272 St  
 GPS coordinates: N 43° 27' 36.3" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 99° 47' 03.5" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 10.74 sq. mi.

The average bottom of the main channel was 12.0 ft below top of guardrail at a point 53 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1450</u>			Q <sub>500</sub> = <u>2480</u>		
Estimated flow passing through bridge	<u>1450</u>			<u>2480</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

pk calcd 8/8  
 2 | 46.3  
 5 | 285  
 10 | 493  
 25 | 805  
 50 | 1100  
 100 | 1450  
 500 | 2480

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Photos  
 1949 - ~~IP~~ IP  
 50 - US  
 51 - US RB  
 52 - US LB  
 53 - R. Abut  
 54 - US Face  
 55 - US Face  
 56 - ~~US RB~~  
 L. Abut

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>1450</u>	<u>2480</u>
Flow depth at left abutment (yaLT), in feet	<u>2.3</u>	<u>4.4</u>
Flow depth at right abutment (yaRT), in feet	<u>3.0</u>	<u>5.1</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>11.3</u>	<u>18.4</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.7</u>	<u>6.8</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>9.4</u>	<u>14.0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>11.5</u>	<u>15.2</u>
Flow angle of attack	<u>30°</u>	<u>30°</u>

See Comments/Diagram for justification where required