

OK TRJ

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 63039010 Date 10-11-10 Initials RRL Region (A B C D) C

Site \_\_\_\_\_ Location 2.9 E Dalton

$Q_{100} =$ 9720 $$ by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 9720 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 150 ft. Flow angle at bridge = 15° Abut. Skew = 20° Effective Skew = 5°

Width ( $W_2$ ) iteration = 150 144 145

Avg. flow depth at bridge,  $y_2$  iteration = 11.4 11.6

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 144.45 ft\*  $q_2 = Q_2/W_2 =$ 67.3 ft<sup>2</sup>/s


Bridge Vel,  $V_2 =$ 5.8 ft/s Final  $y_2 = q_2/V_2 =$ 11.6 ft  $\Delta h =$ 0.7 ft

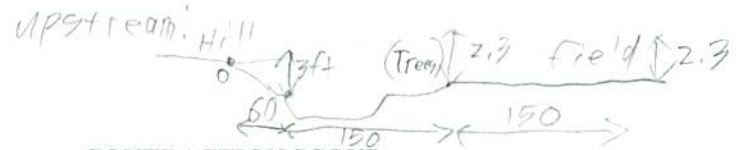
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$ 12.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.5 ft  
Low Steel Elev. = 19.7 ft  
 $n$  (Channel) = 0.028  
 $n$  (LOB) = 0.04  
 $n$  (ROB) = 0.037  
Pier Width = 2 ft  
Pier Length = 2 ft  
# Piers for 100 yr = 4 ft

\* overbank has been removed under bridge  
Bride view:  Dug out. i.e. Deposition may occur



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$ 150 ft

Width of left overbank flow at approach,  $W_{lob} =$ 60 ft Average left overbank flow depth,  $y_{lob} =$ 1.5 ft

Width of right overbank flow at approach,  $W_{rob} =$ 150 ft Average right overbank flow depth,  $y_{rob} =$ 2.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 1.96 From Figure 9  $W_2$  (effective) = 136.5 ft  $y_{cs} =$ 2.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$ \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$ \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ \_\_\_\_\_ From Figure 10,  $y_{cs} =$ \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$ 1

Froude # at bridge = 0.3 Using pier width  $a$  on Figure 11,  $\xi =$ 8 Pier scour  $y_{ps} =$ 6.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$ 1.5 ft right abutment,  $y_{aRT} =$ 2.3 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$ 6.3 and  $\psi_{RT} =$ 9.4

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$ 6.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$ 9.4 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

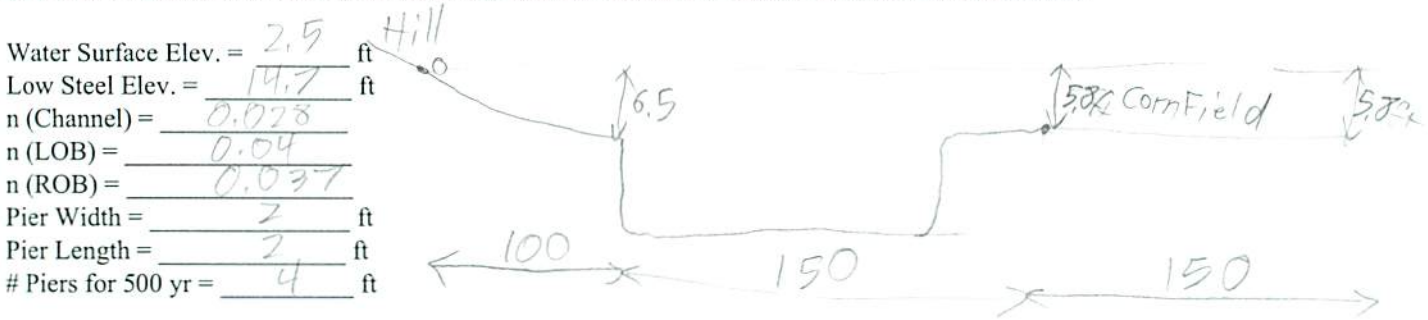
**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 63039010 Date 10-11-16 Initials RRL Region (A B C D) C  
 Site \_\_\_\_\_ Location 2.9 E Dalton  
 $Q_{500} =$  17100 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 16297 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 150 ft. Flow angle at bridge = 15 ° Abut. Skew = 20 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 150  
 Avg. flow depth at bridge,  $y_2$  iteration = 14.7  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 149.43 ft\*  $q_2 = Q_2/W_2 =$  108.7 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.4 ft/s Final  $y_2 = q_2/V_2 =$  14.7 ft  $\Delta h =$  1.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  15.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  150 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  100 ft Average left overbank flow depth,  $y_{lob} =$  3.25 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  150 ft Average right overbank flow depth,  $y_{rob} =$  5.8 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.9 From Figure 9  $W_2$  (effective) = 141.4 ft  $y_{cs} =$  4.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.34 Using pier width a on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  6.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.25 ft right abutment,  $y_{aRT} =$  5.8 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12 and  $\psi_{RT} =$  16.5  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  12 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  16.5 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



Route 269 St Stream W Fork Vermillion Riv MRM \_\_\_\_\_ Date 10-11-10 Initials RRL

Bridge Structure No. 63039010 Location 2.9 E Dolton

GPS coordinates: N 43° 29' 268" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 47° 19' 760" Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 309.24 sq. mi.

The average bottom of the main channel was 18.5 ft below top of guardrail at a point 30 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>9720</u>			Q <sub>500</sub> = <u>17100</u>		
Estimated flow passing through bridge	<u>9720</u>			<u>16237</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>863</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1 - Bridge Deck  
 2 - Upstream  
 3 - Downstream  
 4 - Left Overbank  
 5 - Right Overbank  
 6 - Left Abutment  
 7 - Right Abutment  
 8 - Pier 9  
 Note: channel has been dug out under bridge on right side.

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>9720</u>	<u>16237</u>
Flow depth at left abutment (yaLT), in feet	<u>1.5</u>	<u>3.25</u>
Flow depth at right abutment (yaRT), in feet	<u>2.3</u>	<u>5.8</u>
Contraction scour depth (yca), in feet	<u>2.5</u>	<u>4.5</u>
Pier scour depth (ypp), in feet	<u>6.7</u>	<u>6.8</u>
Left abutment scour depth (yab), in feet	<u>6.3</u>	<u>12</u>
Right abutment scour depth (yab), in feet	<u>9.4</u>	<u>16.5</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required