

OK-121

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 63139120 Date 10-16-12 Initials RFT Region (A B C D)

Site Location 2.1 mi W Hwy 19 on 280 St

Q100 = 1040 by: drainage area ratio flood freq. anal. regional regression eq. ✓

Bridge discharge (Q2) = 1040 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 33 ft \*Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°

Width (W2) iteration = 33

Avg. flow depth at bridge, y2 iteration = 7.9

Corrected channel width at bridge Section = W2 times cos of flow angle = 33 ft\* q2 = Q2/W2 = 31.5 ft²/s

Bridge Vel, V2 = 4.0 ft/s Final y2 = q2/V2 = 7.9 ft Δh = 0.3 ft

Average main channel depth at approach section, y1 = Δh + y2 = 8.2 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

low flow channel angles west, but this happens more than 1 bridge width upstream

Water Surface Elev. = dry ft road overflow begins when y2 ≈ 7.9 ft

Low Steel Elev. = 5.2 ft

n (Channel) = .030 smooth, tall veg.

n (LOB) = .035 } cornfields

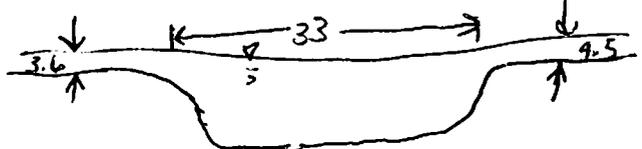
n (ROB) = .035 }

Pier Width = 1.35 ft

Pier Length = 1.35 ft

# Piers for 100 yr = 2

Q100 ≈ Qmax scour approach section is fence line



CONTRACTION SCOUR

Width of main channel at approach section W1 = 33 ft

Width of left overbank flow at approach, Wlob = 33 ft\* Average left overbank flow depth, ylob = 3.6 ft

Width of right overbank flow at approach, Wrob = 33 ft Average right overbank flow depth, yrob = 4.5 ft

a field approach on left side helps guide flow to bridge and reduces overbank depth

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 5.49 From Figure 9 W2 (effective) = 30.3 ft ycs = 6.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(W1) = ft/s

Critical approach velocity, Vc = 11.17y1^(1/6)D50^(1/3) = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^(7/6))^3 = ft If D50 >= Dc50, χ = 0.0

Otherwise, χ = 0.122y1[q2/(D50^(1/3)y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1

Froude # at bridge = 0.25 Using pier width a on Figure 11, ξ = 6 Pier scour yps = 4.8 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 3.6 ft right abutment, yart = 4.5 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yart on figure 12, ψLT = 12.6 and ψRT = 14.1

Left abutment scour, yas = ψLT(K1/0.55) = 18.7 ft Right abutment scour yas = ψRT(K1/0.55) = 21.1 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

00

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 63139120 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region ( A B C D )

Site \_\_\_\_\_ Location \_\_\_\_\_

Q<sub>500</sub> = \_\_\_\_\_ by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge (Q<sub>2</sub>) = \_\_\_\_\_ (should be Q<sub>500</sub> unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 33 ft. Flow angle at bridge = \_\_\_\_\_ ° Abut. Skew = \_\_\_\_\_ ° Effective Skew = \_\_\_\_\_ °

Width (W<sub>2</sub>) iteration = \_\_\_\_\_

Avg. flow depth at bridge, y<sub>2</sub> iteration = \_\_\_\_\_

Corrected channel width at bridge Section = W<sub>2</sub> times cos of flow angle = \_\_\_\_\_ ft\* q<sub>2</sub> = Q<sub>2</sub>/W<sub>2</sub> = \_\_\_\_\_ ft<sup>2</sup>/s

Bridge Vel, V<sub>2</sub> = \_\_\_\_\_ ft/s Final y<sub>2</sub> = q<sub>2</sub>/V<sub>2</sub> = \_\_\_\_\_ ft Δh = \_\_\_\_\_ ft

Average main channel depth at approach section, y<sub>1</sub> = Δh + y<sub>2</sub> = \_\_\_\_\_ ft

\* NOTE: repeat above calculations until y<sub>2</sub> changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y<sub>2</sub> is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft

Low Steel Elev. = 5.2 ft

n (Channel) = \_\_\_\_\_

n (LOB) = \_\_\_\_\_

n (ROB) = \_\_\_\_\_

Pier Width = \_\_\_\_\_ ft

Pier Length = \_\_\_\_\_ ft

# Piers for 500 yr = \_\_\_\_\_ ft

Q<sub>maxscour</sub> ≈ Q<sub>100</sub> see page 1

**CONTRACTION SCOUR**

Width of main channel at approach section W<sub>1</sub> = \_\_\_\_\_ ft

Width of left overbank flow at approach, W<sub>lob</sub> = \_\_\_\_\_ ft Average left overbank flow depth, y<sub>lob</sub> = \_\_\_\_\_ ft

Width of right overbank flow at approach, W<sub>rob</sub> = \_\_\_\_\_ ft Average right overbank flow depth, y<sub>rob</sub> = \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = \_\_\_\_\_ From Figure 9 W<sub>2</sub> (effective) = \_\_\_\_\_ ft y<sub>cs</sub> = \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D<sub>50</sub> = \_\_\_\_\_ ft Average approach velocity, V<sub>1</sub> = Q<sub>500</sub>/(y<sub>1</sub> W<sub>1</sub>) = \_\_\_\_\_ ft/s

Critical approach velocity, V<sub>c</sub> = 11.17y<sub>1</sub><sup>1/6</sup>D<sub>50</sub><sup>1/3</sup> = \_\_\_\_\_ ft/s

If V<sub>1</sub> < V<sub>c</sub> and D<sub>50</sub> >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

D<sub>c50</sub> = 0.0006(q<sub>2</sub>/y<sub>1</sub><sup>7/6</sup>)<sup>3</sup> = \_\_\_\_\_ ft If D<sub>50</sub> >= D<sub>c50</sub>, χ = 0.0

Otherwise, χ = 0.122y<sub>1</sub>[q<sub>2</sub>/(D<sub>50</sub><sup>1/3</sup>y<sub>1</sub><sup>7/6</sup>)]<sup>6/7</sup> - y<sub>1</sub> = \_\_\_\_\_ From Figure 10, y<sub>cs</sub> = \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1), K<sub>2</sub> = \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11, ξ = \_\_\_\_\_ Pier scour y<sub>ps</sub> = \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment, y<sub>aLT</sub> = \_\_\_\_\_ ft right abutment, y<sub>aRT</sub> = \_\_\_\_\_ ft

Shape coefficient K<sub>1</sub> = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y<sub>aLT</sub> and y<sub>aRT</sub> on figure 12, ψ<sub>LT</sub> = \_\_\_\_\_ and ψ<sub>RT</sub> = \_\_\_\_\_

Left abutment scour, y<sub>as</sub> = ψ<sub>LT</sub>(K<sub>1</sub>/0.55) = \_\_\_\_\_ ft Right abutment scour y<sub>as</sub> = ψ<sub>RT</sub>(K<sub>1</sub>/0.55) = \_\_\_\_\_ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 280 St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 63139120 Location 2.1 W Hwy 19 on 280 St  
 GPS coordinates N43° 19.776' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 7.469' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 7.23 sq. mi.

The average bottom of the main channel was 9.3 ft below top of guardrail at a point 14 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	$Q_{100} = 1040 = Q_{max\ scour} \approx Q_{500} =$						2	49.8
Estimated flow passing through bridge	1040 ?						5	157
Estimated road overflow & overtopping	0 ?						10	283
Consideration	Yes	No	Possibly	Yes	No	Possibly	25	517
Chance of overtopping	<input checked="" type="checkbox"/>						50	752
Chance of Pressure flow	<input checked="" type="checkbox"/>						100	1040
Armored appearance to channel		<input checked="" type="checkbox"/>					500	1970
Lateral instability of channel		<input checked="" type="checkbox"/>						

9-26-12  
 PK Q  
 2 49.8  
 5 157  
 10 283  
 25 517  
 50 752  
 100 1040  
 500 1970

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *contraction, abutment, pier*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size ( $D_{50}$ )**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

str. no.  
 approach from bridge left abut.  
 WOB/field approach rt. abut.  
 ROB  
 bridge from approach old pier scour hole

**Summary of Results**

	$Q_{100}$	=	$Q_{max\ scour} \approx Q_{500}$
Bridge flow evaluated	1040		
Flow depth at left abutment ( $y_{aLT}$ ), in feet	3.6		
Flow depth at right abutment ( $y_{aRT}$ ), in feet	4.5		
Contraction scour depth ( $y_{cs}$ ), in feet	6.2		
Pier scour depth ( $y_{ps}$ ), in feet	4.8		
Left abutment scour depth ( $y_{as}$ ), in feet	18.7		
Right abutment scour depth ( $y_{as}$ ), in feet	21.1		
Flow angle of attack	0°		

See Comments/Diagram for justification where required