

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 63165070 Date 5/23/12 Initials RAT Region (A B C D) C  
 Site \_\_\_\_\_ Location 2.5 mi E of Parker on 275 St  
 $Q_{100} = Q_{gr} = 11300$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 11300 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 157 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 147.52 ft\*  $q_2 = Q_2/W_2 = 76.6$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 6.2$  ft/s Final  $y_2 = q_2/V_2 = 12.3$  ft  $\Delta h = 0.8$  ft

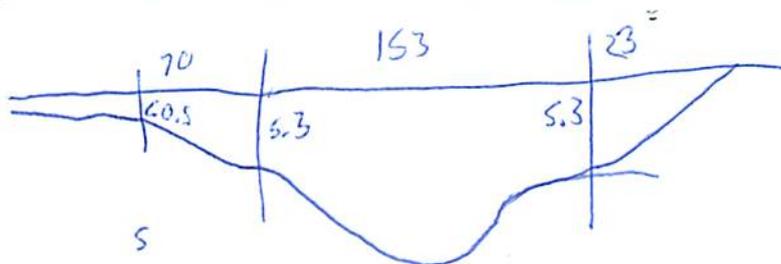
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 13.1$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 17.40 ft  
 Low Steel Elev. = 13.1 ft 16.5  
 $n$  (Channel) = 0.030 -5.4  
 $n$  (LOB) = 0.035 13.1  
 $n$  (ROB) = 0.035  
 Pier Width = 2.1 ft  
 Pier Length = 2.1 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 157$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 70$  ft Average left overbank flow depth,  $y_{lob} = 3.6$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 23$  ft Average right overbank flow depth,  $y_{rob} = 2.7$  ft

~~Live Bed Contraction Scour~~ (use if bed material is small cobbles or finer)

~~$x = 2.02$  From Figure 9  $W_2$  (effective) = 143.3 ft  $y_{cs} = 2.5$  ft~~

~~Clear Water Contraction Scour~~ (use if bed material is larger than small cobbles)

~~Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s~~

~~Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s~~

~~If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.~~

~~$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$~~

~~Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft~~

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.31 Using pier width  $a$  on Figure 11,  $\xi = 8.3$  Pier scour  $y_{ps} = 7$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.6$  ft right abutment,  $y_{aRT} = 2.7$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 12.6$  and  $\psi_{RT} = 11$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 12.6$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 11$  ft

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 63165070 Date 5/23/12 Initials Rat Region (A B C D) C  
 Site J Location 2.5 mi E of Parker on 275 St  
 $Q_{500} = Q_{500}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 12726 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 157 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 147.52 ft\*  $q_2 = Q_2/W_2 = 86.3$  ft<sup>2</sup>/s

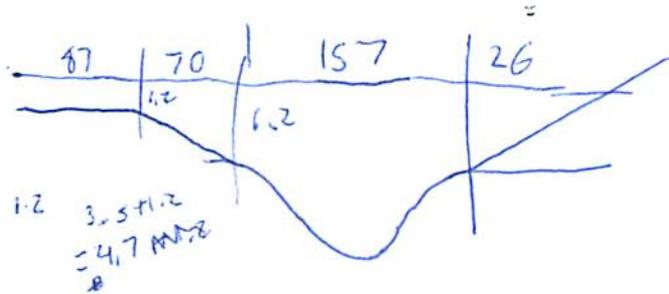
Bridge Vel,  $V_2 = 6.6$  ft/s Final  $y_2 = q_2/V_2 = 13.1$  ft  $\Delta h = 0.9$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 14$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-2.0 ft  
 Low Steel Elev. = 13.1 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 2.1 ft  
 Pier Length = 2.1 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 157$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 25$  ft Average left overbank flow depth,  $y_{lob} = 1.8$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 26$  ft Average right overbank flow depth,  $y_{rob} = 3.1$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 1.94$  From Figure 9  $W_2$  (effective) = 143.3 ft  $y_{cs} = 2.5$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.32 Using pier width  $a$  on Figure 11,  $\xi = 8.3$  Pier scour  $y_{ps} = 7$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 1.8$  ft right abutment,  $y_{aRT} = 3.1$  ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 7.4$  and  $\psi_{RT} = 11.7$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 7.4$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 11.7$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 275 St Stream E. Fork Vermillion R. MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 63165070 Location 2.5 mi E of Parker on 275 St  
 GPS coordinates: N 43° 24' 2.5" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 4' 19.5" Datum of coordinates: WGS84  NAD27

Drainage area = 483 sq. mi.  
 The average bottom of the main channel was 16.5 ft below top of guardrail at a point 33 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS  $Q_{200} =$

Flows	$Q_{100} = Q_{50} = 11300$			$Q_{500} = Q_{100} = 15200$		
Estimated flow passing through bridge	11300			12726		
Estimated road overflow & overtopping	0			2477		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		X				X
Chance of Pressure flow			X	X		
Armored appearance to channel		X			X	
Lateral instability of channel		X			X	

S/22  
 2 | 1110  
 5 | 2950  
 10 | 4840  
 25 | 8140  
 50 | 11300  
 100 | 15200  
 500 | 27300

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal *pie, contraction*  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material Silt/Clay  Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1. main channel L.R. OB
- 2. Piers 2. Main channel
- 3. P. Ab 5. LOB
- 4. L. Ab
- 5. Scour

Summary of Results

	$Q_{100} = Q_{50}$	$Q_{500} = Q_{100}$
Bridge flow evaluated	11300	12726
Flow depth at left abutment (yaLT), in feet	3.6	1.8
Flow depth at right abutment (yaRT), in feet	2.7	3.1
Contraction scour depth (yca), in feet	2.5 2.5	2.5
Pier scour depth (yps), in feet	7	7
Left abutment scour depth (yas), in feet	12.6 12.6	24
Right abutment scour depth (yas), in feet	11	11.7
Flow angle of attack	20	20

See Comments/Diagram for justification where required