

ok RT

### SCOUR ANALYSIS AND REPORTING FORM

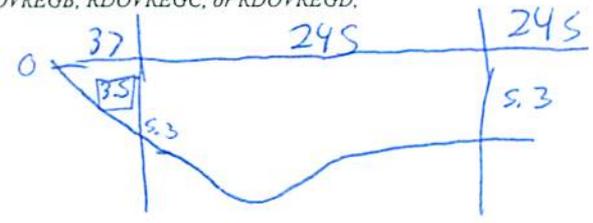
Bridge Structure No. 63210185 Date 5/23/12 Initials RAT Region (A B C D) C  
 Site \_\_\_\_\_ Location 1.4 mi S of Davis on 961 Ave  
 $Q_{100} = Q_{50}$  17900 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 17900 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 245 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 241.28 ft\*  $q_2 = Q_2/W_2 =$  73.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.1 ft/s Final  $y_2 = q_2/V_2 =$  12.1 ft  $\Delta h =$  0.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  12.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-3.0 ft  
 Low Steel Elev. = 13.3 ft  
 $n$  (Channel) = 0.050  
 $n$  (LOB) = 0.060  
 $n$  (ROB) = 0.080  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  245 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  37 ft Average left overbank flow depth,  $y_{lob} =$  3.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  245 ft Average right overbank flow depth,  $y_{rob} =$  5.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.76 From Figure 9  $W_2$  (effective) = 233.3 ft  $y_{cs} =$  3.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.31 Using pier width  $a$  on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  6.7 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.5 ft right abutment,  $y_{aRT} =$  5.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.4 and  $\psi_{RT} =$  15.6  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  12.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  15.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

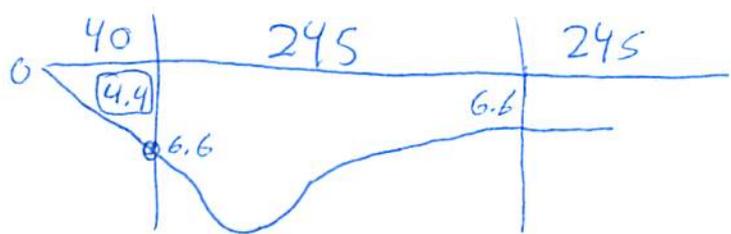
**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 63210/85 Date 5/23/12 Initials Rat Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.4 mi S of Davis Cr 461 Ave  
 $Q_{500} = Q_{oe}$  25000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 21456 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 245 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 241.25 ft\*  $q_2 = Q_2/W_2 =$  88.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.7 ft/s Final  $y_2 = q_2/V_2 =$  13.3 ft  $\Delta h =$  0.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  14.2 ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-3.0 ft  
 Low Steel Elev. = 13.3 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.060  
 n (ROB) = 0.050  
 Pier Width = 2.0 ft  
 Pier Length = 2.0 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  245 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  40 ft Average left overbank flow depth,  $y_{lob} =$  4.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  245 ft Average right overbank flow depth,  $y_{rob} =$  6.6 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x =$  3.07 From Figure 9  $W_2$  (effective) = 240.5 ft  $y_{cs} =$  3.7 ft  
3.6 233.3 4.2

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1)^{7/6}$  = \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.32 Using pier width a on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  6.3 ft  
6.7

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.4 ft right abutment,  $y_{aRT} =$  6.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  14 and  $\psi_{RT} =$  17.9  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  14 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  17.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCNEW  
 PGRM: Pie  
 PGRM: Abutment

Route 461 Ave Stream Vermillion River MRM Date 5/23/12 Initials Rat  
 Bridge Structure No. 63210185 Location 1.4 mi S of Davis on 461 Ave  
 GPS coordinates: N 93° 43' 14" 13.7" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 59' 1.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 1027.97 sq. mi.  
 The average bottom of the main channel was 17.8 ft below top of guardrail at a point 107.127 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_{50} = 17800$			$Q_{500} = Q_{100} = 25000$		
Estimated flow passing through bridge	17800			21456		
Estimated road overflow & overtopping	0			3544		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

522  
 2 | 1400  
 5 | 3960  
 10 | 6820  
 25 | 12200  
 50 | 17800  
 100 | 25000  
 500 | 49100

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) Right abutment
- 2-3) left abutment
- 4) main channel
- 5) left CB
- 6) main channel
- 7) right CB

Summary of Results

	$Q_{100} = Q_{50}$	$Q_{500} = Q_{100}$
Bridge flow evaluated	17800	21456
Flow depth at left abutment (yaLT), in feet	3.5	4.4
Flow depth at right abutment (yaRT), in feet	5.3	6.6
Contraction scour depth (y <sub>cs</sub> ), in feet	2.3	<del>3.7</del> 4.2
Pier scour depth (y <sub>ps</sub> ), in feet	6.7	6.7
Left abutment scour depth (y <sub>as</sub> ), in feet	12.4	14
Right abutment scour depth (y <sub>rs</sub> ), in feet	15.6	17.9
Flow angle of attack	10	10

See Comments/Diagram for justification where required