

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 64010119 Date 5/27/12 Initials rat Region (A B C D) C  
 Site \_\_\_\_\_ Location 30890 471 Ave, Brule Creek 308-309 st  
 $Q_{100} = \underline{7830}$   $12500$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 12500 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 124 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 124

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 122.12 ft\*  $q_2 = Q_2/W_2 = \frac{102.4}{104}$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = \underline{7.2}$  ft/s Final  $y_2 = q_2/V_2 = \underline{14.3}$  ft  $\Delta h = \underline{1.1}$  ft

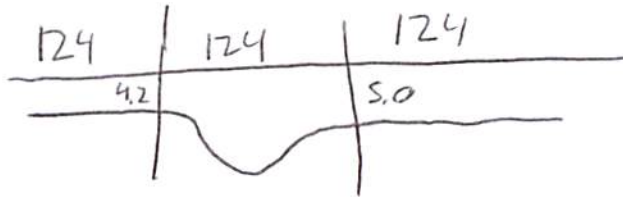
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{15.3}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0-1.3 ft 20.9  
 Low Steel Elev. = 15.2 ft 15.2  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.03  
 Pier Width = 2.35 ft  
 Pier Length = 2.35 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{124}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{124}$  ft Average left overbank flow depth,  $y_{lob} = \underline{5.0}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{124}$  ft Average right overbank flow depth,  $y_{rob} = \underline{4.2}$  ft

PRGM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{2.43}$  From Figure 9  $W_2$  (effective) = 117.4 ft  $y_{cs} = \underline{9.2}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = \underline{\hspace{2cm}}$  ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) = \underline{\hspace{2cm}}$  ft/s

Critical approach velocity,  $V_c = 1.52 y_1^{1/6} D_{50}^{1/3} = \underline{\hspace{2cm}}$  ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 = \underline{\hspace{2cm}}$  ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\hspace{2cm}}$  From Figure 10,  $y_{cs} = \underline{\hspace{2cm}}$  ft

PRGM: CWCNEW

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.34 Using pier width  $a$  on Figure 11,  $\xi = \underline{9.1}$  Pier scour  $y_{ps} = \underline{7.7}$  ft

PRGM: Pier

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{5.0}$  ft right abutment,  $y_{aRT} = \underline{4.2}$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{15}$  and  $\psi_{RT} = \underline{13.6}$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = \underline{15}$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = \underline{13.6}$  ft

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

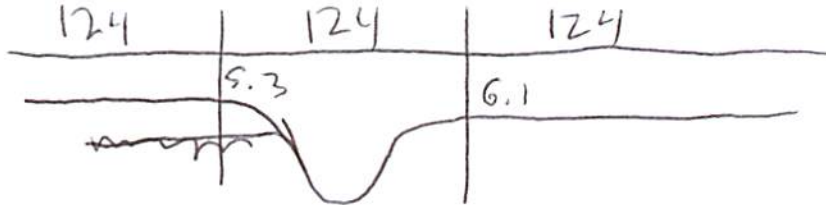
Bridge Structure No. 64010119 Date 5/27/12 Initials Rai Region ( A B C D ) C  
 Site \_\_\_\_\_ Location 30890 471 8 Ave  
 $Q_{500} = \frac{12300 \cdot 1910^0}{1}$  by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 14189 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 124 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 122.12 ft\*  $q_2 = Q_2/W_2 = \frac{14189}{124} = 116.2$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \frac{14189}{124 \cdot 10} = 7.6$  ft/s Final  $y_2 = q_2/V_2 = \frac{116.2}{7.6} = 15.2$  ft  $\Delta h = 1.2$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 16.4$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.5 ft  
 Low Steel Elev. = 15.2 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2.35 ft  
 Pier Length = 2.35 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 124$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 124$  ft Average left overbank flow depth,  $y_{lob} = 6.1$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 124$  ft Average right overbank flow depth,  $y_{rob} = 5.3$  ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x = 9.87$  From Figure 9  $W_2$  (effective) = 117.4 ft  $y_{cs} = 10.8$  ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.34 Using pier width  $a$  on Figure 11,  $\xi = 9.1$  Pier scour  $y_{ps} = 7.7$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 6.1$  ft right abutment,  $y_{aRT} = 5.3$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 17$  and  $\psi_{RT} = 15.6$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 17$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 15.6$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

Route 471 Ave Stream Brule Creek MRM \_\_\_\_\_ Date Apr 5/27/12 Initials Lat

Bridge Structure No. 64010119 Location 30890 471 Ave

GPS coordinates: N 42° 54' 44.11" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 47' 8.611" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 154.42 ~~134.37~~ sq. mi.

The average bottom of the main channel was 20.9 ft below top of guardrail at a point 46 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. WATER drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

|                                       |  |                                     |                                     |  |                                     |          |
|---------------------------------------|--|-------------------------------------|-------------------------------------|--|-------------------------------------|----------|
| Flows                                 | Q <sub>100</sub> = <del>12500</del> <u>12500</u> |                                     |                                     | Q <sub>500</sub> = <del>14189</del> <u>14189</u> |                                     |          |
| Estimated flow passing through bridge |  |                                     |                                     |  |                                     |          |
| Estimated road overflow & overtopping | <u>0</u>   |                                     |                                     | <u>4911</u>                                      |                                     |          |
| Consideration                         | Yes  | No                                  | Possibly                            | Yes  | No                                  | Possibly |
| Chance of overtopping                 |  | <input checked="" type="checkbox"/> |                                     | <input checked="" type="checkbox"/>              |                                     |          |
| Chance of Pressure flow               |  |                                     | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/>              |                                     |          |
| Armored appearance to channel         |  | <input checked="" type="checkbox"/> |                                     |  | <input checked="" type="checkbox"/> |          |
| Lateral instability of channel        |  | <input checked="" type="checkbox"/> |                                     |  | <input checked="" type="checkbox"/> |          |

5/24  
 2 | 102  
 5 | 324  
 10 | 561  
 25 | 973  
 50 | 1360  
 100 | 1810  
 500 | 3080

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know pier contraction  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

5/24  
 2 | 1420  
 5 | 3350  
 10 | 5060  
 25 | 7670  
 50 | 9950  
 100 | 12500  
 500 | 19100

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA rose quartz  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

- Comments, Diagrams & orientation of digital photos
- 1) main channel
  - 2) right OB
  - 3) right ab.
  - 4) piers
  - 5) pier scours
  - 6) left OB
  - 7) left ab
  - 8) main channel
  - 9) main channel

Summary of Results

|  |              |              |
|--|--------------|--------------|
|  | Q100         | Q500         |
| Bridge flow evaluated                        | <u>12500</u> | <u>14189</u> |
| Flow depth at left abutment (yaLT), in feet  | <u>5.0</u>   | <u>6.1</u>   |
| Flow depth at right abutment (yaRT), in feet | <u>4.2</u>   | <u>5.3</u>   |
| Contraction scour depth (yca), in feet       | <u>8.2</u>   | <u>10.8</u>  |
| Pier scour depth (yps), in feet              | <u>7.7</u>   | <u>7.7</u>   |
| Left abutment scour depth (yas), in feet     | <u>15</u>    | <u>17</u>    |
| Right abutment scour depth (yas), in feet    | <u>13.6</u>  | <u>15.6</u>  |
| Flow angle of attack                         | <u>10</u>    | <u>10</u>    |

See Comments/Diagram for justification where required