

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 64058050 Date 5/26/12 Initials RAT Region (A B C D) D  
 Site \_\_\_\_\_ Location 5.1 mi E of Ex't 42 on 302 St  
 $Q_{100} =$  3350 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 3350 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 143 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 123.81 ft\*  $q_2 = Q_2/W_2 =$  27.1 ft<sup>2</sup>/s

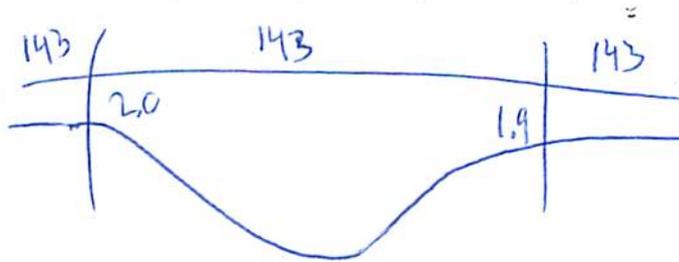
Bridge Vel,  $V_2 =$  3.7 ft/s Final  $y_2 = q_2/V_2 =$  7.3 ft  $\Delta h =$  0.3 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.6 ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_1$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.5 ft 12.8  
 Low Steel Elev. = 9.0 ft 3.8  
 $n$  (Channel) = 0.04 0.035 9.0  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.03  
 Pier Width = 1.85 ft  
 Pier Length = 1.85 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  143 ft

Width of left overbank flow at approach,  $W_{lob} =$  143 ft Average left overbank flow depth,  $y_{lob} =$  2.0 ft

Width of right overbank flow at approach,  $W_{rob} =$  143 ft Average right overbank flow depth,  $y_{rob} =$  1.9 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.82 From Figure 9  $W_2$  (effective) = 116.4 ft  $y_{cs} =$  4.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.24 Using pier width  $a$  on Figure 11,  $\xi =$  7.5 Pier scour  $y_{ps} =$  6.1 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.0 ft right abutment,  $y_{aRT} =$  1.9 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  8.2 and  $\psi_{RT} =$  7.9  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  8.2 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  7.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCSNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

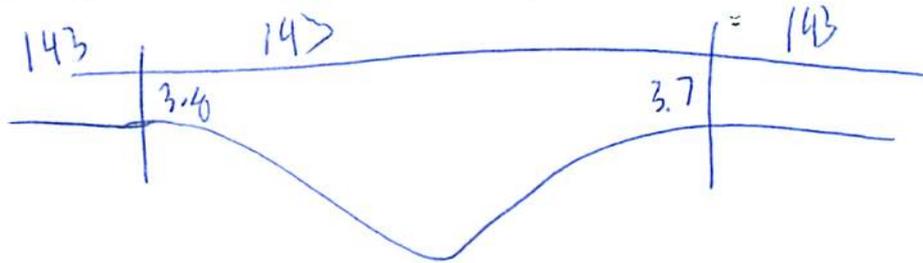
Bridge Structure No. 64058050 Date 5/26/12 Initials Ral Region (A B C D) C  
 Site \_\_\_\_\_ Location 5.1 mi E of Exit 42 on 302 St  
 $Q_{500} =$  5050 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 5037 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 143 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 123.84 ft\*  $q_2 = Q_2/W_2 =$  40.7 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.5 ft/s Final  $y_2 = q_2/V_2 =$  9 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5-1.5 ft  
 Low Steel Elev. = 9.0 ft  
 $n$  (Channel) = 0.1035  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.030  
 Pier Width = 1.85 ft  
 Pier Length = 1.85 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  143 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  143 ft Average left overbank flow depth,  $y_{lob} =$  3.8 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  143 ft Average right overbank flow depth,  $y_{rob} =$  3.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  7.54 From Figure 9  $W_2$  (effective) = 116.4 ft  $y_{cs} =$  8.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.26 Using pier width  $a$  on Figure 11,  $\xi =$  7.5 Pier scour  $y_{ps} =$  6.2 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.8 ft right abutment,  $y_{aRT} =$  3.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.9 and  $\psi_{RT} =$  12.7  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  12.9 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  12.7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 302 St Stream East Brake Ck MRM \_\_\_\_\_ Date 8/26/12 Initials RA  
 Bridge Structure No. 64058050 Location 5.1 mi E of Exit 42 on 302 St  
 GPS coordinates: N 43° 00' 00" W 96° 41' 35.9" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84  NAD27

Drainage area = 65.95 sq. mi.  
 The average bottom of the main channel was 12.8 ft below top of guardrail at a point 67 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

flows	Q <sub>10</sub> <sup>10</sup> = <u>3350</u>	Q <sub>25</sub> <sup>25</sup> = <u>5050</u>				
Estimated flow passing through bridge	<u>0</u>	<u>5037</u>				
Estimated road overflow & overtopping	<u>0</u>	<u>13</u>				
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/26  
 2 945  
 5 2230  
 10 3350  
 25 5050  
 50 6510  
 100 8100  
 500 12300

Vegetation at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know plac. contractor  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

8/26  
 2 945  
 5 2230  
 10 3350  
 25 5050  
 50 6510  
 100 8100  
 500 12300

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material \_\_\_\_\_ Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

- Comments, Diagrams & orientation of digital photos  
 1) main channel 2) right ab.  
 3) pier scour 3) right OB  
 4) left ab 4) main channel  
 5) left ab 5) left OB  
 6) right ab

Summary of Results

	Q <sub>100-10</sub>	Q <sub>500-25</sub>
Bridge flow evaluated	<u>3350</u>	<u>5037</u>
Flow depth at left abutment (yaLT), in feet	<u>2.0</u>	<u>3.8</u>
Flow depth at right abutment (yaRT), in feet	<u>1.9</u>	<u>3.7</u>
Entrapment scour depth (yca), in feet	<u>4.4</u>	<u>8.4</u>
Abutment scour depth (yca), in feet	<u>6.1</u>	<u>6.2</u>
Left abutment scour depth (yas), in feet	<u>8.2</u>	<u>12.9</u>
Right abutment scour depth (yas), in feet	<u>7.8</u>	<u>12.7</u>
Flow angle of attack	<u>30</u>	<u>30</u>

Comments/Diagram for justification where required