

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 65170165 Date 7/12/17 Initials Rat Region (A B C D) C
Site Location 1.4 mi N of Akaska on 303 Arc
Q100 = 2230 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 2230 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 104 ft. Flow angle at bridge = 15 degrees Abut. Skew = 0 degrees Effective Skew = 15 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 100.46 ft\* q2 = Q2/W2 = 22.2 ft^2/s

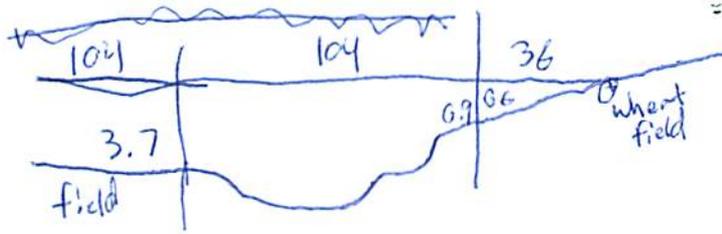
Bridge Vel, V2 = 3.3 ft/s Final y2 = q2/V2 = 6.7 ft Delta h = 0.7 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 6.9 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = dry ft
Low Steel Elev. = 11.4 ft
n (Channel) = 0.040
n (LOB) = 0.030
n (ROB) = 0.035
Pier Width = 1.7 ft
Pier Length = 1.7 ft
# Piers for 100 yr = 4



0.9 - 0.025x = 0
x =

CONTRACTION SCOUR

Width of main channel at approach section W1 = 104 ft
Width of left overbank flow at approach, Wlob = 36 ft Average left overbank flow depth, ylob = 0.6 ft
Width of right overbank flow at approach, Wrob = 104 ft Average right overbank flow depth, yrob = 3.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 3.92 From Figure 9 W2 (effective) = 93.7 ft ycs = 4.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PGRM: Contract

PGRM: CWCNSNEW

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.22 Using pier width a on Figure 11, xi = Pier scour yps = 5.6 ft

PGRM: Pier

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 0.6 ft right abutment, yarT = 3.7 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 2.7 and psiRT = 12.7
Left abutment scour, yas = psiLT (K1/0.55) = 2.7 ft Right abutment scour yas = psiRT (K1/0.55) = 12.7 ft

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 65170165 Date 7/12/12 Initials Rat Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.4 mi N of Akaska on 363 Ave  
 $Q_{500} =$  4340 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = ~~4340~~ 4340 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

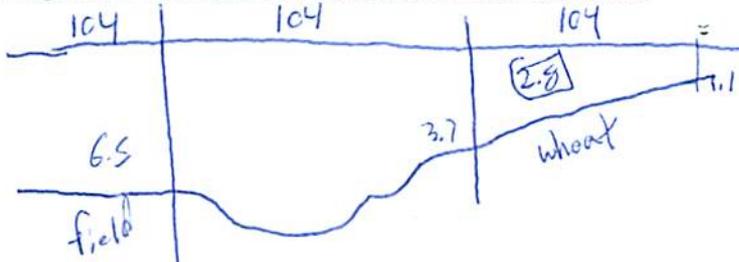
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 104 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 100.46 ft\*  $q_2 = Q_2/W_2 =$  43.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.7 ft/s Final  $y_2 = q_2/V_2 =$  9.3 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft  
 Low Steel Elev. = 11.4 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030 0.035  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  104 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  104 ft Average left overbank flow depth,  $y_{lob} =$  2.8 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  104 ft Average right overbank flow depth,  $y_{rob} =$  6.5 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x =$  ~~10.25~~ 9.2 From Figure 9  $W_2$  (effective) = 93.7 ft  $y_{cs} =$  ~~11.2~~ 10.1 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^{3/2} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.8 ft right abutment,  $y_{aRT} =$  6.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.2 and  $\psi_{RT} =$  17.7  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  11.2 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  17.7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 303 Ave Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 7/12/12 Initials RAT  
 Bridge Structure No. 65170165 Location 1.4 mi N of Akaska on 303 Ave  
 GPS coordinates: N 45° 21' 18.5" W 100° 7' 14.0" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 47.5 sq. mi.  
 The average bottom of the main channel was 15.1 ft below top of guardrail at a point 67 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>2230</u>			Q <sub>500</sub> = <u>4340</u>		
Estimated flow passing through bridge	<u>2230</u>			<u>4340</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/2  
8/26  
2 59.7  
5 256  
10 514  
25 1030  
50 1560  
100 2230  
500 4340

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *some pt of contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_\_\_ \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4-5). right abutment
- 6). pier
- 7-8). left abutment
- 9). main channel

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>2230</u>	<u>4340</u>
Flow depth at left abutment (yaLT), in feet	<u>0.6</u>	<u>2.9</u>
Flow depth at right abutment (yaRT), in feet	<u>3.7</u>	<u>6.5</u>
Contraction scour depth (yca), in feet	<u>4.6</u>	<u>11.2</u> <u>10.1</u>
Pier scour depth (yca), in feet	<u>5.6</u>	<u>5.9</u>
Left abutment scour depth (yca), in feet	<u>2.7</u>	<u>11.2</u>
Right abutment scour depth (yca), in feet	<u>12.7</u>	<u>17.7</u>
Flow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required