

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 65170185 Date 10-28 Initials RT Region (A B C D) (C)

Site _____ Location Swan creek 0.5 S Alaska

$Q_{100} =$ 9970 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.

Bridge discharge (Q_2) = 9970 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 104 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width (W_2) iteration = 104

Avg. flow depth at bridge, y_2 iteration = 13.8

Corrected channel width at bridge Section = W_2 times cos of flow angle = 104 ft* $q_2 = Q_2/W_2 =$ 95.9 ft²/s

Bridge Vel, $V_2 =$ 6.9 ft/s Final $y_2 = q_2/V_2 =$ 13.8 ft $\Delta h =$ 1 ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 14.8 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2

Effective pier width = $L \sin(\alpha) + a \cos(\alpha)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

bridge flows abutment to abutment at Q_{100}

Water Surface Elev. \approx -3.1 ft

Low Steel Elev. = 16.5 ft

n (Channel) = .032

n (LOB) = .027

n (ROB) = .029

Pier Width = 2.25 ft

Pier Length = 2.25 ft

Piers for 100 yr = 2 ft

*some trees/brush and dead timber in high flow channel
grazed pasture
pasture with trees, not grazed
the bridge may be the low point in the roadway. possibly lower point over road in Alaska*

CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 104 ft

Width of left overbank flow at approach, $W_{lob} =$ 208 ft - *2x bridge opening* Average left overbank flow depth, $y_{lob} =$ 1.8 ft

Width of right overbank flow at approach, $W_{rob} =$ 94 ft (to trees) Average right overbank flow depth, $y_{rob} =$ 2.8 ft

right overbank is higher, trees will minimize right overbank flow

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 2.73 From Figure 9 W_2 (effective) = 99.5 ft $y_{cs} =$ 3.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1

Froude # at bridge = 0.33 Using pier width a on Figure 11, $\xi =$ 8.8 Pier scour $y_{ps} =$ 7.4 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 1.8 ft right abutment, $y_{aRT} =$ 2.8 ft

Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 7.4 and $\psi_{RT} =$ 11.2

Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 7.4 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 11.2 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. _____ Date _____ Initials _____ Region (A B C D) _____

Site _____ Location _____

$Q_{500} = 21,200$ by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.

Bridge discharge (Q_2) = 16,200 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 104 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width (W_2) iteration = 104

Avg. flow depth at bridge, y_2 iteration = 17.6

Corrected channel width at bridge Section = W_2 times cos of flow angle = 104 ft* $q_2 = Q_2/W_2 = 155.8$ ft²/s

Bridge Vel, $V_2 = 8.9$ ft/s Final $y_2 = q_2/V_2 = 17.6$ ft $\Delta h = 1.6$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 19.2$ ft

*NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(\theta) + a \cos(\theta)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = -3.1 ft

Low Steel Elev. = 16.5 ft

n (Channel) = .032

n (LOB) = .027

n (ROB) = .029

Pier Width = 2.25 ft

Pier Length = 2.25 ft

Piers for 500 yr = 2 ft

$Q_{max\ scour} < Q_{500}$

$Q_{max\ scour} \approx 16,200\ cfs \approx 17.6'$

CONTRACTION SCOUR

Width of main channel at approach section $W_1 = 104$ ft

Width of left overbank flow at approach, $W_{lob} = 208$ ft

Average left overbank flow depth, $y_{lob} = 5.0$ ft

Width of right overbank flow at approach, $W_{rob} = 94$ ft

Average right overbank flow depth, $y_{rob} = 5.9$ ft

↑ to trees

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 8.72$ From Figure 9

W_2 (effective) = 99.5 ft

$y_{cs} = 9.6$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ _____ ft

If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____

From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1), $K_2 = 1$

Froude # at bridge = 0.37

Using pier width a on Figure 11, $\xi = 8.8$

Pier scour $y_{ps} = 7.6$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = 5.0$ ft right abutment, $y_{aRT} = 7.6$ ft

Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 15$ and $\psi_{RT} = 16.6$

Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 15$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 16.6$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

20.8
13.2
17.6

Route 303 Ave Stream Swan Creek MRM _____ Date _____ Initials _____

Bridge Structure No. 65170185 Location 0.5 mi S. Akaska

GPS coordinates: 45° 19.614' taken from: USL abutment centerline of ↑ MRM end _____
100° 7.233' Datum of coordinates: WGS84 NAD27 _____

Drainage area = ~~521.32~~ 521.32 sq. mi.

The average bottom of the main channel was 20.8 ft below top of guardrail at a point 39 ft from left abutment.

Method used to determine flood flows: _____ Freq. Anal. _____ drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>9970</u>			Q ₅₀₀ = <u>21,200</u>		
Estimated flow passing through bridge	<u>9970</u>			<u>16,200</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>5000</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

Riprap at abutments? _____ Yes No _____ Marginal
 Evidence of past Scour? Yes _____ No _____ Don't know
 Debris Potential? _____ High Med _____ Low

there appears to be a contraction scour pool below bridge. Possibly some minor pier scour.

Does scour countermeasure(s) appear to have been designed?

Riprap _____ Yes _____ No _____ Don't know NA
 Spur Dike _____ Yes _____ No _____ Don't know NA
 Other _____ Yes _____ No _____ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand _____	Gravel _____	Cobbles _____	Boulders _____
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos
right abutment scour will probably be less than estimate because trees will slow overbank flow and create an ineffective flow area

photos
 structure number
 approach from bridge center
 left overbank from bridge
 right overbank from bridge
 bridge opening from left approach
 scour pool underneath bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>9970</u>	<u>16,200</u>
Flow depth at left abutment (yaLT), in feet	<u>1.8</u>	<u>5.0</u>
Flow depth at right abutment (yaRT), in feet	<u>2.8</u>	<u>5.9</u>
Contraction scour depth (yca), in feet	<u>3.3</u>	<u>9.6</u>
Pier scour depth (yca), in feet	<u>7.4</u>	<u>7.6</u>
Left abutment scour depth (yca), in feet	<u>7.4</u>	<u>1.5</u>
Right abutment scour depth (yca), in feet	<u>11.2</u>	<u>16.6</u>
IFlow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required

Basin characteristics from
Provisional Stream Stats 10-17-11

$$\text{Cont. D.A.} = \frac{521.32}{\cancel{32.37}} \text{ mi}^2 \quad (544-22.68)$$

$$\text{PII} = 0.65$$

100% Subregion B

Manually calculated peaks

$$Q_{100} = \cancel{1760 \text{ cfs}} \quad 9970 \text{ cfs}$$

$$Q_{500} = \cancel{3370 \text{ cfs}} \quad 21,200 \text{ cfs}$$