

OK RT

SCOUR ANALYSIS AND REPORTING FORM

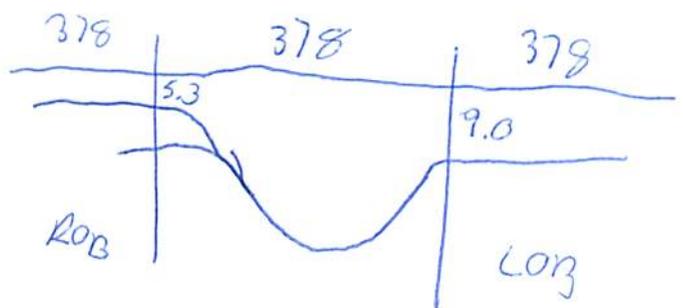
Bridge Structure No. 680 30018 Date 6/9/12 Initials Lat Region (A B C D)
Site Location 6.1 S of Menno on 431 Ave
Q100 = Q25 49000 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 49000 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 378 ft. Flow angle at bridge = 80.25 Abut. Skew = 0 Effective Skew = 25
Width (W2) iteration =
Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 312.58 ft\* q2 = Q2/W2 = 143 ft^2/s
Bridge Vel, V2 = 8.5 ft/s Final y2 = q2/V2 = 16.9 ft Delta h = 1.5 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 18.3 ft
\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(a) + a cos(a)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0-6 ft 21 22.13
Low Steel Elev. = 16.9 ft 5.4
n (Channel) = 0.035 0.040 16.9
n (LOB) = 0.030
n (ROB) = 0.035
Pier Width = 7.2 ft
Pier Length = 2.5 ft
# Piers for 100 yr = 4 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 378 ft
Width of left overbank flow at approach, Wlob = 378 ft Average left overbank flow depth, ylob = 9.0 ft
Width of right overbank flow at approach, Wrob = 378 ft Average right overbank flow depth, yrob = 5.3 ft

PRGM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 13.89 From Figure 9 W2 (effective) = 333.9 ft ycs = 14.4 ft

PRGM: CWCNEW

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.17 y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PRGM: Pier

PIER SCOUR CALCULATIONS

L/a ratio = 1.14 Correction factor for flow angle of attack (from Table 1), K2 = 1.03
Froude # at bridge = 0.36 Using pier width a on Figure 11, xi = 8.6 Pier scour yps = 7.6 ft

PRGM: Abutment

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 9.0 ft right abutment, yarT = 5.3 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 20.6 and psiRT = 15.6
Left abutment scour, yas = psiLT (K1/0.55) = 20.6 ft Right abutment scour yas = psiRT (K1/0.55) = 15.6 ft

**SCOUR ANALYSIS AND REPORTING FORM**

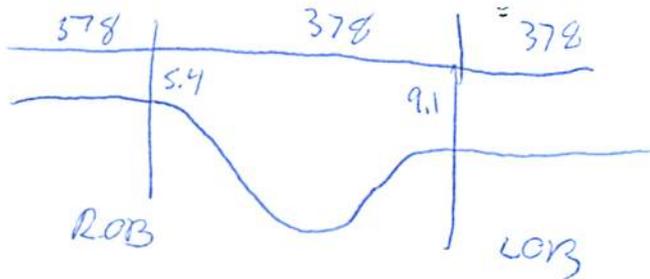
Bridge Structure No. 68030018 Date 6/9/12 Initials RAT Region (A B C D) C  
 Site 6.1 S of Menno on 431st Ave  
 $Q_{500} = Q_{50} = \underline{83500}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 47234 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)  
49221

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 378 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 312.58 ft\*  $q_2 = Q_2/W_2 = \underline{143.7}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{6.5}$  ft/s Final  $y_2 = q_2/V_2 = \underline{16.9}$  ft  $\Delta h = \underline{1.5}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{18.4}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-60 ft  
 Low Steel Elev. = 16.9 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.030  
 n (ROB) = 0.035  
 Pier Width = 2.2 ft  
 Pier Length = 2.5 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{378}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{578}$  ft Average left overbank flow depth,  $y_{lob} = \underline{9.1}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{378}$  ft Average right overbank flow depth,  $y_{rob} = \underline{5.4}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{14.12}$  From Figure 9  $W_2$  (effective) = 333.8 ft  $y_{cs} = \underline{14.5}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.14 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1.03}$   
 Froude # at bridge = 0.36 Using pier width a on Figure 11,  $\xi = \underline{8.6}$  Pier scour  $y_{ps} = \underline{7.6}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{9.1}$  ft right abutment,  $y_{aRT} = \underline{5.4}$  ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{20.6}$  and  $\psi_{RT} = \underline{15.7}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{20.6}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{15.7}$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

Route 431 Ave Stream Jenny River MRM \_\_\_\_\_ Date 6/9/12 Initials RAT  
 Bridge Structure No. 68030018 Location 6.1 S of Menno on 431 Ave  
 GPS coordinates: N 430 81 428.11 taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 970 39 36.41 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 16756.41 sq. mi.  
 The average bottom of the main channel was 223 ft below top of guardrail at a point 313 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_{25} \quad 49000$			$Q_{50} = Q_{25} \quad 83500$		
Estimated flow passing through bridge	<u>49000</u>			<u>49221</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>34279</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

5/22  
 2 | 1730  
 S | 8860  
 10 | 20900  
 25 | 49000  
 50 | 83500  
 100 | 133000  
 500 | 329000

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *contraction pier*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) main channel
- 2) right ab
- 3) left ab is more
- 4) piers
- 5) right abutment
- 6) left abutment
- 8) pier scour
- 9) right abutment
- 10) main channel
- 11) left ab
- 12) left ab

Summary of Results

	$Q_{100} \quad Q_{25}$	$Q_{500} \quad Q_{50}$
Bridge flow evaluated	<u>49000</u>	<u>49221</u>
Flow depth at left abutment (yaLT), in feet	<u>9.0</u>	<u>9.1</u>
Flow depth at right abutment (yaRT), in feet	<u>5.3</u>	<u>5.4</u>
Contraction scour depth (yca), in feet	<u>14.4</u>	<u>14.5</u>
Pier scour depth (yca), in feet	<u>7.6</u>	<u>7.6</u>
Left abutment scour depth (yca), in feet	<u>20.6</u>	<u>20.6</u>
Right abutment scour depth (yca), in feet	<u>15.4</u>	<u>15.7</u>
Flow angle of attack	<u>25</u>	<u>25</u>

See Comments/Diagram for justification where required