

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 68119196 Date 5/28/12 Initials Rat Region (A B C D)
Site Location Manne Ck + Locust St in Yankton
Q100 = Q50 1490 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 1490 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 52 ft. Flow angle at bridge = 0 degrees Abut. Skew = 0 degrees Effective Skew = 0 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 52 ft\* q2 = Q2/W2 = 28.7 ft^2/s

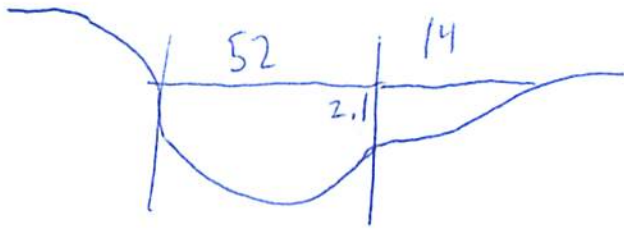
Bridge Vel, V2 = 3.9 ft/s Final y2 = q2/V2 = 7.6 ft Delta h = 0.3 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 7.9 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0 ft
Low Steel Elev. = 7.9 ft
n (Channel) = 0.050
n (LOB) = 0.013
n (ROB) = 0.025
Pier Width = 0 ft
Pier Length = 0 ft
# Piers for 100 yr = 0 ft

16.3



CONTRACTION SCOUR

Width of main channel at approach section W1 = 52 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 14 ft Average right overbank flow depth, yrob = 2.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 0.97 From Figure 9 W2 (effective) = 52 ft ycs = 0.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.17 y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 =
Froude # at bridge = Using pier width a on Figure 11, xi = Pier scour yps = ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yALT = 0 ft right abutment, yART = 2.1 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yALT and yART on figure 12, psiLT = 0 and psiRT = 8.6
Left abutment scour, yas = psiLT (K1/0.55) = 0 ft Right abutment scour yas = psiRT (K1/0.55) = 12.9 ft

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

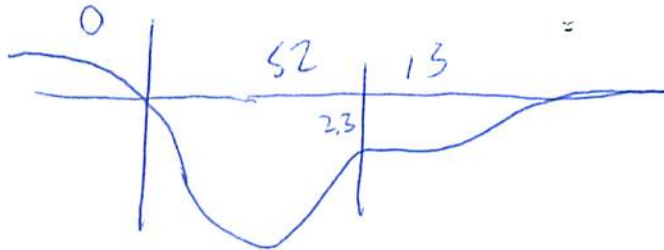
Bridge Structure No. 68119196 Date 5/25/12 Initials Rat Region (A B C D) D  
 Site \_\_\_\_\_ Location Marne Ck + Locust St in Yankton  
 $Q_{500} = Q_{100} \cdot 2.120$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1500 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 52 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 52 ft\*  $q_2 = Q_2/W_2 = 30.5$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 3.9$  ft/s Final  $y_2 = q_2/V_2 = 7.8$  ft  $\Delta h = 0.3$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 8.1$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 7.8 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.013  
 n (ROB) = 0.025  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 52$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 0$  ft Average left overbank flow depth,  $y_{lob} = 0$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 15$  ft Average right overbank flow depth,  $y_{rob} = 2.3$  ft

$3.4 \cdot \frac{2}{3} = \frac{6.8}{3} = 2.3$

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 0.57$  From Figure 9  $W_2$  (effective) = 52 ft  $y_{cs} = 1$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 1.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [(q_2 / (D_{50}^{1/3} y_1^{7/6}))^{0.7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 0$  ft right abutment,  $y_{aRT} = 2.3$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0$  and  $\psi_{RT} = 0.4$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 0$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 14$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



Route Locust St Stream Marne Ck MRM \_\_\_\_\_ Date 8/26/12 Initials Rat  
 Bridge Structure No. 69119116 Location Marne Ck + Locust St in Yankton  
 GPS coordinates: N 42° 54' 10.1" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 77° 23' 56.6" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 22.4 sq. mi.  
 The average bottom of the main channel was 16.3 ft below top of guardrail at a point 21 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>50</sub> <sup>50</sup> = <u>1490</u>			Q <sub>500</sub> <sup>100</sup> = <u>2120</u>		
Estimated flow passing through bridge	<u>1490</u>			<u>1585</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>5.30</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/26  
 2 | 80.5  
 5 | 279  
 10 | 524  
 25 | 1000  
 50 | 1490  
 100 | 2120  
 500 | 4170

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes  No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

*malmost dry abutment + contraction scour*

5/22

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other concrete walkway  Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

2 | 80.5  
 5 | 279  
 10 | 524  
 25 | 1000  
 50 | 1490  
 100 | 2120  
 500 | 4170

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand  Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) main channel
- 2) abutment scour (left)
- 3) left abut
- 4) left abut
- 5) right abut
- 6) right abut
- 7) pier scour
- 8) right over-bank
- 9) left OB
- 10) left OB
- 11) right OB

Summary of Results

	Q <sub>100</sub> <sup>50</sup>	Q <sub>500</sub> <sup>100</sup>
Bridge flow evaluated	<u>1490</u>	<u>1585</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>2.1</u>	<u>2.3</u>
Contraction scour depth (yca), in feet	<u>0.5</u>	<u>1</u>
Pier scour depth (yps), in feet	<u>NA</u>	<u>NA</u>
Left abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (yas), in feet	<u>12.9</u>	<u>14</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required