

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 68121204 Date 5/29/12 Initials fat Region (A B C D) C
Site Cedar St + Marne ck in Yankton
Q100 = 2570 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 2570 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 105 ft. Flow angle at bridge = 60 degrees Abut. Skew = 45 degrees Effective Skew = 15 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 101.42 ft\* q2 = Q2/W2 = 253 ft^2/s

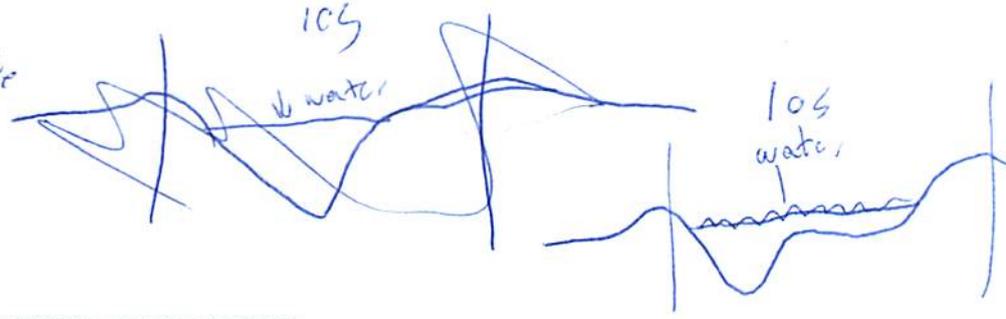
Bridge Vel, V2 = 3.6 ft/s Final y2 = q2/V2 = 7.1 ft Delta h = 0.3 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 7.4 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0.05 ft
Low Steel Elev. = 7.9 ft
n (Channel) = 0.020 - concrete
n (LOB) = 0.030
n (ROB) = 0.045
Pier Width = 0.8 ft
Pier Length = 79 ft
# Piers for 100 yr = 1



CONTRACTION SCOUR

Width of main channel at approach section W1 = 105 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 0.32 From Figure 9 W2 (effective) = 100.6 ft ycs = 0.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 11.17 y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PRGM: Contract

PRGM: CWCNEW

PIER SCOUR CALCULATIONS

L/a ratio = 98.75 Correction factor for flow angle of attack (from Table 1), K2 = 2.5
Froude # at bridge = 0.24 Using pier width a on Figure 11, xi = 3.9 Pier scour yps = 7.8 ft

PRGM: Pier

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 0 ft right abutment, yaRT = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 0 and psiRT = 0
Left abutment scour, yas = psiLT (K1/0.55) = 0 ft Right abutment scour yas = psiRT (K1/0.55) = 0 ft

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

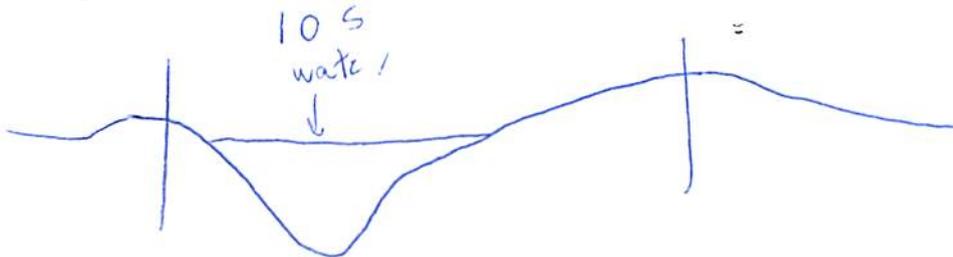
Bridge Structure No. 6812204 Date 5/29/12 Initials RAT Region (A B C D) C  
 Site \_\_\_\_\_ Location Cedar St & Marne Ck in Yankton  
 $Q_{500} =$  5130 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 3177 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 105 ft. Flow angle at bridge = 60° Abut. Skew = 45° Effective Skew = 15°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 101.42 ft\*  $q_2 = Q_2/W_2 =$  31.3 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4 ft/s Final  $y_2 = q_2/V_2 =$  7.9 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-0.5 ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = 0.020  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.045  
 Pier Width = 0.8 ft  
 Pier Length = 79 ft  
 # Piers for 500 yr = 1 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  105 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.35 From Figure 9  $W_2$  (effective) = 100.6 ft  $y_{cs} =$  0.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 V_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 98.75 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  2.5  
 Froude # at bridge = 0.25 Using pier width  $a$  on Figure 11,  $\xi =$  3.9 Pier scour  $y_{ps} =$  7.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

Route Cedar Ck Stream Marne Ck MRM \_\_\_\_\_ Date 5/29/12 Initials RAT  
 Bridge Structure No. 68121204 Location Cedar St + Marne Ck in Yankton  
 GPS coordinates: N 42° 52' 30.2" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 23' 13.3" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 30.65 sq. mi.  
 The average bottom of the main channel was 14.9 ft below top of guardrail at a point 32 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>2570</u>			Q <sub>500</sub> = <u>5130</u>		
Estimated flow passing through bridge	<del>2570</del> <u>2570</u>			<u>3177</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>1953</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/26  
 2 | 91.8  
 5 | 327  
 10 | 620  
 25 | 1200  
 50 | 1800  
 100 | 2570  
 500 | 5110

Riprap at abutments? \_\_\_ Yes  No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *ab. pier, contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

5/22  
 2 | 92  
 5 | 328  
 10 | 622  
 25 | 1200  
 50 | 1800  
 100 | 2570  
 500 | 5130

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other Concrete walkway  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1-4) main channel
- 5) left abutment
- 6) right abutment
- 7-9) left abutment damage
- 10) pier scour
- 11) right CB
- 12) left CB

note: dike has been constructed along right abutment at road level and left overbank is along the road.

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>2570</u>	<u>5130</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>0.5</u>	<u>0.6</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>2.8</u>	<u>2.9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>0</u>	<u>0</u>
Flow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required