

OK RTT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 68134120 Date 5/29/12 Initials rat Region (A B C D)

Site Location 1.5 E of HWY 81 on 303 St

Q100 = 50 65100 by: drainage area ratio flood freq. anal. regional regression eq. X

Bridge discharge (Q2) = 65900 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 456 ft. Flow angle at bridge = 5 degrees Abut. Skew = 0 degrees Effective Skew = 5 degrees

Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =

Corrected channel width at bridge Section = W2 times cos of flow angle = 454.26 ft\* q2 = Q2/W2 = 143.3 ft^2/s

Bridge Vel, V2 = 8.5 ft/s Final y2 = q2/V2 = 16.9 ft Delta h = 1.5 ft

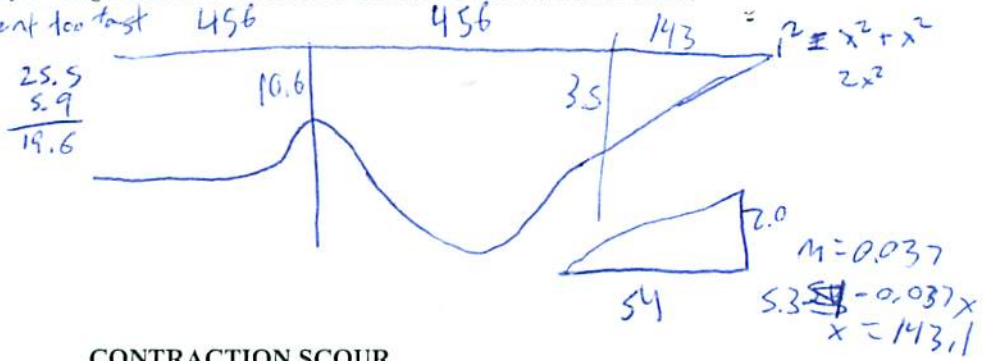
Average main channel depth at approach section, y1 = Delta h + y2 = 18.4 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(a) + a cos(a)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = UNK - current too fast 456 ft
Low Steel Elev. = 19.2 ft
n (Channel) = 0.045
n (LOB) = 0.050
n (ROB) = 0.040
Pier Width = 2.4 ft
Pier Length = 2.4 ft
# Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section W1 = 456 ft

Width of left overbank flow at approach, Wlob = 456 ft Average left overbank flow depth, ylob = 10.6 ft

Width of right overbank flow at approach, Wrob = 143 ft Average right overbank flow depth, yrob = 3.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 7.66 From Figure 9 W2 (effective) = 444.7 ft ycs = 8.5 ft

5.3 - 2/3 = 10.6/3

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PGRM: Contract

PGRM: CWCSNEW

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1

Froude # at bridge = 0.36 Using pier width a on Figure 11, xi = 9.2 Pier scour yps = 7.9 ft

PGRM: Pier

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 10.6 ft right abutment, yarT = 3.5 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, psiLT = 21.8 and psiRT = 12.4

Left abutment scour, yas = psiLT(K1/0.55) = 21.8 ft Right abutment scour yas = psiRT(K1/0.55) = 12.4 ft

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

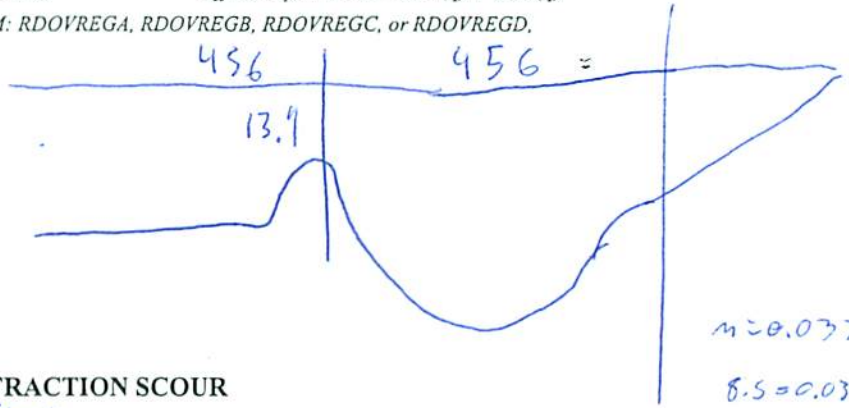
Bridge Structure No. 6813420 Date 5/29/12 Initials RAL Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.5 E of Hwy 81 on 303 St  
 $Q_{500} = 104000$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 87823 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 456 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 454.26 ft\*  $q_2 = Q_2/W_2 = 193.3$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 9.9$  ft/s Final  $y_2 = q_2/V_2 = 19.6$  ft  $\Delta h = 2$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 21.6$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = UNK ft  
 Low Steel Elev. = 19.6 ft  
 n (Channel) = 0.015  
 n (LOB) = 0.050  
 n (ROB) = 0.040  
 Pier Width = 2.4 ft  
 Pier Length = 2.4 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 456$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 456$  ft Average left overbank flow depth,  $y_{lob} = 13.8$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 230$  ft Average right overbank flow depth,  $y_{rob} = 5.7$  ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x = 11.36$  From Figure 9  $W_2$  (effective) = 444.7 ft  $y_{cs} = 12.4$  ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.39 Using pier width a on Figure 11,  $\xi = 9.2$  Pier scour  $y_{ps} = 8$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 13.8$  ft right abutment,  $y_{aRT} = 5.7$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 24.5$  and  $\psi_{RT} = 16.3$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 24.5$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 16.3$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 303 St Stream James River MRM Date 5/29/12 Initials RAT  
 Bridge Structure No. 68134120 Location 1.5 E of Hwy 81 on 303 St  
 GPS coordinates: N 42° 59' 45.6" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 28' 9.4" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 16904.67 sq. mi.  
 The average bottom of the main channel was 25.5 ft below top of guardrail at a point 202 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>50</sub> <sup>50</sup> = <u>65100</u>			Q <sub>500</sub> <sup>100</sup> = <u>104000</u>		
Estimated flow passing through bridge	<u>65100</u>			<u>87823</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>16177</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

5/23  
 2 | 973  
 5 | 6210  
 10 | 15300  
 25 | 37800  
 50 | 65100  
 100 | 104000  
 500 | 255000

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal *- eroded*  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *piec, contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA *at one time*  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) main channel (100) right abut  
 2) left abut 8-9) right abut  
 3) left abut 10-11) left ab  
 4) piers 12-13) right ab  
 5) pier scour 14) main channel  
 6-7) scour

Summary of Results

	Q <sub>100</sub> <sup>50</sup>	Q <sub>500</sub> <sup>100</sup>
Bridge flow evaluated	<u>65100</u>	<u>87823</u>
Flow depth at left abutment (yaLT), in feet	<u>10.6</u>	<u>13.9</u>
Flow depth at right abutment (yaRT), in feet	<u>3.5</u>	<u>5.7</u>
Contraction scour depth (yca), in feet	<u>4.5</u>	<u>12.4</u>
Pier scour depth (yca), in feet	<u>2.9</u>	<u>8</u>
Left abutment scour depth (yca), in feet	<u>21.8</u>	<u>29.5</u>
Right abutment scour depth (yca), in feet	<u>12.4</u>	<u>16.3</u>
Flow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required