

OK 121

SCOUR ANALYSIS AND REPORTING FORM

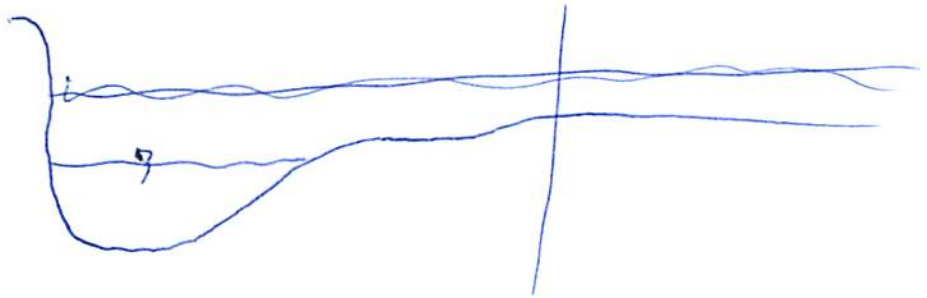
Bridge Structure No. 69158176 Date 8/10/11 Initials CU Region (A B C D) B
 Site _____ Location 4.25 mi NW of int of 224 Ave + 157 St
 $Q_{100} = \underline{36300}$ by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = 36300 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 332 ft. Flow angle at bridge = 19° Abut. Skew = 10° Effective Skew = 5°
 Width (W_2) iteration = 332 195 204 200
 Avg. flow depth at bridge, y_2 iteration = 12.7 16.8 16.4 16.6
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 199.24 ft* $q_2 = Q_2/W_2 = \underline{182.2}$ ft²/s
 Bridge Vel, $V_2 = \underline{11}$ ft/s Final $y_2 = q_2/V_2 = \underline{16.6}$ ft $\Delta h = \underline{2.5}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{19.1}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = _____ ft
 n (Channel) = 0.033
 n (LOB) = 0.035
 n (ROB) = 0.030
 Pier Width = 2.55 ft
 Pier Length = 30 ft
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{332}$ ft 332
 Width of left overbank flow at approach, $W_{lob} = \underline{0}$ ft Average left overbank flow depth, $y_{lob} = \underline{0}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{0}$ ft Average right overbank flow depth, $y_{rob} = \underline{0}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = \underline{13.96}$ From Figure 9 W_2 (effective) = 194.1 ft $y_{cs} = \underline{14.2}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} = \underline{\hspace{2cm}}$ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) = \underline{\hspace{2cm}}$ ft/s
 Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\hspace{2cm}}$ ft/s
 If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{\hspace{2cm}}$ ft If $D_{50} >= D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\hspace{2cm}}$ From Figure 10, $y_{cs} = \underline{\hspace{2cm}}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 11.4 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1.5}$
 Froude # at bridge = 0.44 Using pier width a on Figure 11, $\xi = \underline{9.7}$ Pier scour $y_{ps} = \underline{13.0}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{0}$ ft right abutment, $y_{aRT} = \underline{0}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{0}$ and $\psi_{RT} = \underline{0}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{0.0}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{0.0}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

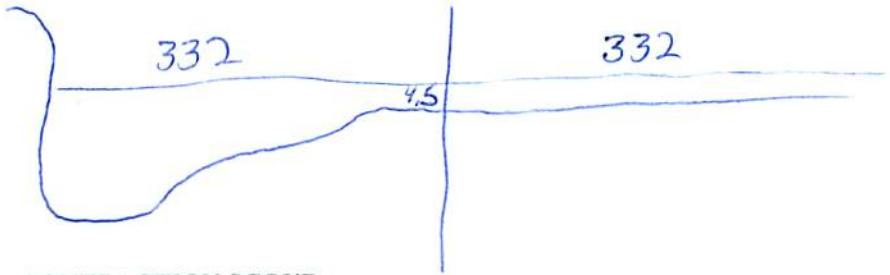
Bridge Structure No. 69154178 Date 8/10/14 Initials CG Region (A B C D) B
 Site _____ Location 0.25 mi NW of int of 224 Ave & 157 St
 $Q_{500} =$ 61100 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = 61100 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 332 ft. Flow angle at bridge = 15 ° Abut. Skew = 10 ° Effective Skew = 5 °
 Width (W_2) iteration = 332 203 228 218 221
 Avg. flow depth at bridge, y_2 iteration = 16.7 21.6 20.3 20.8 20.7
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 220.16 ft* $q_2 = Q_2/W_2 =$ 277.5 ft²/s
 Bridge Vel, $V_2 =$ 13.4 ft/s Final $y_2 = q_2/V_2 =$ 20.7 ft $\Delta h =$ 3.7 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 24.4 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = _____ ft
 n (Channel) = 0.033
 n (LOB) = 0.035
 n (ROB) = 0.030
 Pier Width = 2.55 ft
 Pier Length = 30 ft
 # Piers for 500 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ ~~332~~ 332 ft
 Width of left overbank flow at approach, $W_{lob} =$ 0 ft Average left overbank flow depth, $y_{lob} =$ 0 ft
 Width of right overbank flow at approach, $W_{rob} =$ 332 ft Average right overbank flow depth, $y_{rob} =$ 4.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x =$ 15.74 From Figure 9 W_2 (effective) = 215.1 ft $y_{cs} =$ 15.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s
 Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 11.8 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.5
 Froude # at bridge = 0.52 Using pier width a on Figure 11, $\xi =$ 9.7 Pier scour $y_{ps} =$ 13.1 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0.0 ft right abutment, $y_{aRT} =$ 4.5 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0.0 and $\psi_{RT} =$ 14.1
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 0.0 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 14.1 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route Thunder Bolt Rd Stream Morcan River MRM _____ Date 8/10/11 Initials CS
 Bridge Structure No. 69158178 Location 8.25 mi NW of int of 224 Ave & 157 st
 GPS coordinates: N 45° 12' 53.8" taken from: USL abutment centerline of ↑ MRM end _____
W 101° 41' 43.4" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 2955 sq. mi.
 The average bottom of the main channel was 41.6 ft below top of guardrail at a point 77 ft from left abutment.
 Method used to determine flood flows: ___ Freq. Anal. ___ drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

PK calc'd on 8/8

Flows	Q ₁₀₀ = <u>36300</u>			Q ₅₀₀ = <u>61100</u>		
Estimated flow passing through bridge	<u>36300</u>			<u>61100</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

PK 2	2350
5	7350
10	12800
25	20500
50	27900
100	36300
500	61100

Riprap at abutments? ___ Yes No ___ Marginal
 Evidence of past Scour? Yes ___ No ___ Don't know
 Debris Potential? High Med ___ Low

Does scour countermeasure(s) appear to have been designed?
 Riprap ___ Yes ___ No ___ Don't know NA
 Spur Dike Yes ___ No ___ Don't know ___ NA
 Other _____ ___ Yes ___ No ___ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay Sand ___ Gravel ___ Cobbles ___ Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Large log jam on pier

- 1477 - ID
- 78 - spur dike
- 79 - US Face
- 80 - US Face
- 81 - R. Abut

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>36300</u>	<u>61100</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>4.5</u>
Contraction scour depth (yca), in feet	<u>14.2</u>	<u>15.4</u>
Pier scour depth (yps), in feet	<u>13.0</u>	<u>13.1</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>14.1</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required