

## Appendix 7. Example Application

The general procedure for estimating the magnitude of a flood discharge at a selected recurrence interval by using the methods described in the report is illustrated in the following example. A random location on Wells River, Vermont, was selected for this example. The drainage area, the areal percentage of wetlands in the basin, and the basin-wide mean of the average annual precipitation were determined to be 71.6 square miles (mi<sup>2</sup>), 3.87 percent, and 44.05 inches, respectively.

An estimate of the 1-percent annual exceedance probability peak discharge ( $Q_1$ ) is needed for this rural, ungaged stream in Vermont. To determine the magnitude of the peak discharge having a 1-percent annual exceedance probability in cubic feet per second, equation 8 would be solved as

$$\begin{aligned} Q_1 &= 0.251A^{0.854}W^{0.297}P^{1.809} \\ Q_1 &= 0.251(71.6)^{0.854}(3.87+1)^{-0.297}(44.05)^{1.809} \\ Q_1 &= 5,670 \text{ ft}^3/\text{s} . \end{aligned} \quad (8)$$

The variance of prediction for this estimate would be computed by using equation 11. The row vector,  $x_i$ , in equation 11 is based on the basin characteristics and is as follows:

$$\begin{aligned} x_i &= [1 \log_{10}(71.6) \log_{10}(3.87+1) \log_{10}(44.05)] \text{ or} \\ x_i &= [1 \ 1.855 \ 0.688 \ 1.644] . \end{aligned}$$

From table 5, the model error variance,  $\gamma^2$ , is 0.0352, and the  $(X^T A^{-1} X)^{-1}$  matrix is

$$(X^T A^{-1} X)^{-1} =$$

$$\begin{bmatrix} 4.80981\text{e} - 01 & 3.00081\text{e} - 03 & -1.39098\text{e} - 02 & -2.84463\text{e} - 01 \\ 3.00081\text{e} - 03 & 8.08573\text{e} - 04 & -6.16775\text{e} - 04 & -2.43038\text{e} - 03 \\ -1.39098\text{e} - 02 & -6.16775\text{e} - 04 & 3.98077\text{e} - 03 & 7.43891\text{e} - 03 \\ -2.84463\text{e} - 01 & -2.43038\text{e} - 03 & 7.43891\text{e} - 03 & 1.69693\text{e} - 01 \end{bmatrix} .$$

After inserting  $x_i$ ,  $\gamma^2$ , and  $(X^T A^{-1} X)^{-1}$  into equation 11, the variance of prediction is

$$\begin{aligned} V_{pred} &= \mathbf{g}^2 + x_i (X^T A^{-1} X)^{-1} x_i^T \\ V_{pred} &= 0.0352 + 0.00139 \text{ or} \\ V_{pred} &= 0.0366 . \end{aligned} \quad (11)$$

The standard error of prediction is

$$\begin{aligned} SE_{pred} &= V_{pred}^{1/2} \\ SE_{pred} &= 0.0366^{1/2} \text{ or} \\ SE_{pred} &= 0.191 . \end{aligned} \quad (12)$$

The standard error of prediction for the estimate in percent is then computed by using equations 13 and 14:

$$S_{pos} = 100(10^{SE_{pred}} - 1) \text{ and} \quad (13)$$

$$S_{neg} = 100(10^{-SE_{pred}} - 1) \quad (14)$$

or

$$S_{pos} = 100(10^{0.191} - 1) \text{ and}$$

$$S_{neg} = 100(10^{-0.191} - 1) .$$

Thus,  $S_{pos} = 55.2$  percent, and  $S_{neg} = -35.6$  percent.

The confidence intervals for this estimate can be computed by using equations 15 and 16. For example, if the 90-percent confidence interval were required, the critical value from a Student's t-distribution for the appropriate confidence interval would be found by using any standard statistics textbook. The value for  $t_{0.05,141}$  is 1.66, and the standard error of prediction was found earlier to be 0.191. Equations 15 and 16 are solved as follows:

$$CI_{upper} = Q_{pred} 10^{(t_{\alpha/2, n-p} SE_{pred})} \quad (15)$$

$$CI_{upper} = 5,670 * 10^{(1.66 * 0.191)}$$

$$CI_{upper} = 11,800 \text{ cubic feet per second (ft}^3 / \text{s)}$$

$$CI_{lower} = \frac{Q_{pred}}{10^{(t_{\alpha/2, n-p} SE_{pred})}} \quad (16)$$

$$CI_{lower} = \frac{5,670}{10^{(1.66 * 0.191)}}$$

$$CI_{lower} = 2,730 \text{ ft}^3 / \text{s}$$

Because the site is relatively close to a streamgage, Wells River at Wells River, Vt., the regression equation result of the 100-year discharge shown can be improved by weighting the result with the 1-percent annual exceedance probability flood discharge determined from the frequency analysis of the streamgage data. To weight the result at the ungaged location, a weighted result at the gaged location is first determined. A weighted average ( $Q_w$ ) of the regression estimate ( $Q_{r(g)}$ ) and the flood discharge estimate from a frequency analysis of the streamgage record ( $Q_s$ ) can be computed by using equation 17.

$$\log_{10} Q_w = \frac{\log_{10} Q_s (V_{pred}) + \log_{10} Q_{r(g)} (V_s)}{V_{pred} + V_s} \quad (17)$$

## Estimation of Flood Discharges at Selected Annual Exceedance Probabilities for Unregulated, Rural Streams in Vermont

From the results of frequency analysis of the streamgage data shown in appendix 3, the 1-percent annual exceedance probability discharge ( $Q_s$ ) is 5,570 ft<sup>3</sup>/s. The variance of estimate,  $V_s$ , for this streamgage at the 1-percent annual exceedance probability is 0.0040 and can be found in appendix 8. At the streamgage location, the drainage area is 98.9 mi<sup>2</sup>, the percentage of the basin covered by wetlands is 3.31 percent, and the basin-wide mean of the average annual precipitation is 43.3 inches. When these values are put into equation 8, the regression equation estimate of the 1-percent annual exceedance probability discharge at the gaged location ( $Q_{r(g)}$ ) is 7,510 ft<sup>3</sup>/s. The variance of prediction ( $V_{pred}$ ) is then computed by using equation 11 with the basin characteristics at the gaged location and the appropriate model error variance,  $g^2$ , and  $(X'AX)^{-1}$  matrix from table 5. These values are put into equation 17 as follows:

$$\log_{10} Q_w = \frac{\log_{10} 5,570(0.0368) + \log_{10} 7,520(0.0040)}{0.0368 + 0.0040}$$

$$Q_w = 5,740 \text{ ft}^3 / \text{s}.$$

The weighted flood discharge,  $Q_w$ , is for the gaged location. Because a weighted estimate is desired at an ungaged site near a streamgage, the weighted estimate,  $Q_u$ , can be determined by using equations 19 and 20.

$$c = \frac{\log_{10} \left( \frac{Q_{r(u)}}{Q_{r(g)}} \right)}{\log_{10} \left( \frac{A_u}{A_g} \right)} + \frac{\log_{10} \left( \frac{Q_{r(g)}}{Q_w} \right)}{\log_{10} (a)} \quad (19)$$

$$c = \frac{\log_{10} \left( \frac{5,670}{7,520} \right)}{\log_{10} \left( \frac{71.6}{98.9} \right)} + \frac{\log_{10} \left( \frac{7,520}{5,740} \right)}{\log_{10} (0.5)}$$

$$c = 0.485$$

$$Q_u = Q_w \left( \frac{A_u}{A_g} \right)^c \quad (20)$$

$$Q_u = 5,740 \left( \frac{71.6}{98.9} \right)^{0.485}$$

$$Q_u = 4,910 \text{ ft}^3 / \text{s}$$