

Prepared in cooperation with the Trinity River Restoration Project

Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011



Scientific Investigations Report 2015–5046

Cover: Photo mosaic showing 2011 peak flow release from Lewiston Dam and concurrent gravel augmentation at Lewiston gaging station (1.5 floodplain kilometers downstream from Lewiston Dam). Sawmill rehabilitation site and juvenile coho, 4 floodplain kilometers downstream from Lewiston Dam. Photo credit: Trinity River Restoration Program on-line photo archives.

Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

By Jennifer A. Curtis, Scott A. Wright, J. Toby Minear, and Lorraine E. Flint

Prepared in cooperation with the Trinity River Restoration Program

Scientific Investigations Report 2015–5046

U.S. Department of the Interior
U.S. Geological Survey

U.S. Department of the Interior
SALLY JEWELL, Secretary

U.S. Geological Survey
Suzette M. Kimball, Acting Director

U.S. Geological Survey, Reston, Virginia: 2015

For more information on the USGS—the Federal source for science about the Earth, its natural and living resources, natural hazards, and the environment—visit <http://www.usgs.gov> or call 1–888–ASK–USGS.

For an overview of USGS information products, including maps, imagery, and publications, visit <http://www.usgs.gov/pubprod/>.

Any use of trade, firm, or product names is for descriptive purposes only and does not imply endorsement by the U.S. Government.

Although this information product, for the most part, is in the public domain, it also may contain copyrighted materials as noted in the text. Permission to reproduce copyrighted items must be secured from the copyright owner.

Suggested citation:

Curtis, J.A., Wright, S.A., Minear, J.T., and Flint, L.E., 2015, Assessing geomorphic change along the Trinity River downstream from Lewiston Dam, California, 1980–2011: U.S. Geological Survey Scientific Investigations Report 2015–5046, 69 p., plus appendix, <http://dx.doi.org/10.3133/sir20155046>.

ISSN 2328-0328 (online)

Contents

Abstract.....	1
Introduction.....	1
Purpose and Scope	3
Study Area.....	3
In-Stream Effects of the Trinity River Diversion.....	4
Methods.....	8
Estimating Geomorphic Change	9
Interpretation of Geomorphic Mapping	12
Uncertainty and Error Analysis	12
Assessing Natural and Managed Drivers of Geomorphic Change	15
Streamflow and Sediment Supply.....	15
Sediment Management and Mechanical Channel Rehabilitation.....	17
Results	17
Spatial and Temporal Analysis of Geomorphic Change	17
Natural and Managed Drivers of Geomorphic Change.....	23
Streamflow and Sediment Supply.....	31
Sediment Management and Mechanical Channel Rehabilitation.....	37
Summary of Bar and Bank Processes	40
Discussion.....	44
Channel Change Potential.....	44
Trajectories of Geomorphic Response and Primary Controls	46
Geomorphology and Habitat Linkages	47
Conclusions.....	52
References Cited.....	53
Appendix A.....	57

Figures

1. Map showing study area, Trinity River, California.....	2
2. Map showing Trinity River restoration reach, in California, from Lewiston Dam downstream to the North Fork Trinity confluence and 13 geomorphic reaches, within 3 river-channel segments, used as the spatial framework for interpretation of mapping results	5
3. Graph showing elevation profile of the Trinity River restoration reach, California, estimated from 10-meter-resolution digital elevation data.....	6
4. Raster hydrograph showing mean daily flows measured 1.5 kilometers downstream from Lewiston Dam along the Trinity River, California.....	7
5. Photo showing example of the topographic relations among depositional and constructed features for the Trinity River downstream from Lewiston Dam, California	11
6. Graphs showing areal extent of riparian and channel features along the Trinity River downstream from Lewiston Dam, California, <i>A</i> , in 1980, and change in active-channel area for five periods from 1980 to 2011: <i>B</i> , 1980 to 1997; <i>C</i> , 1997 to 2001; <i>D</i> , 2001 to 2006; <i>E</i> , 2006 to 2009; and <i>F</i> , 2009 to 2011	18
7. Bar graphs showing areal extent of lower elevation riparian features along the Trinity River downstream from Lewiston Dam, California, in <i>A</i> , 1980; <i>B</i> , 1997; <i>C</i> , 2001; <i>D</i> , 2006; <i>E</i> , 2009; and <i>F</i> , 2011	19
8. Bar graphs showing areal extent of channel-complexity features within the active channel along the Trinity River downstream from Lewiston Dam, California, in <i>A</i> , 1980; <i>B</i> , 1997; <i>C</i> , 2001; <i>D</i> , 2006; <i>E</i> , 2009; and <i>F</i> , 2011.....	20
9. Graphs showing area of uplands along the Trinity River downstream from Lewiston Dam, California, and change in upland area from 1980 to 2011: <i>A</i> , cumulative area by reach; <i>B</i> , cumulative change in area per year by reach; <i>C</i> , area by study reach and segments over time.....	21
10. Graphs showing area of riparian features along the Trinity River downstream from Lewiston Dam, California, and change in riparian area from 1980 to 2011: <i>A</i> , cumulative area by study reach; <i>B</i> , cumulative change in area per year by study reach; <i>C</i> , area by study reach and segments over time.....	22
11. Graphs showing area of the pre-dam floodplain along the Trinity River downstream from Lewiston Dam, California, and change in pre-dam floodplain area from 1980 to 2011: <i>A</i> , cumulative area by study reach; <i>B</i> , cumulative change in area per year by study reach; <i>C</i> , area by study reach and river segments over time.....	24
12. Graphs showing area of post-dam benches along the Trinity River downstream from Lewiston Dam, California, and change in post-dam bench area from 1980 to 2011: <i>A</i> , cumulative area by study reach; <i>B</i> , cumulative change in area per year by study reach; <i>C</i> , area by study reach and river segments over time.....	25
13. Graphs showing area of constructed floodplains along the Trinity River downstream from Lewiston Dam, California, and change in constructed floodplain area from 1980 to 2011: <i>A</i> , cumulative area by study reach; <i>B</i> , cumulative change in area per year by study reach; <i>C</i> , area by study reach and river segments over time	26
14. Graphs showing area of stable bars along the Trinity River downstream from Lewiston Dam, California, and change in stable bar area from 1980 to 2011: <i>A</i> , cumulative area by study reach; <i>B</i> , cumulative change in area per year by study reach; <i>C</i> , area by study reach and river segments over time	27

Figures—Continued

15. Graphs showing area of the active channel along the Trinity River downstream from Lewiston Dam, California, and change in active channel area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time28
16. Graphs showing area of active bars along the Trinity River downstream from Lewiston Dam, California, and change in active bar area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time29
17. Graphs showing area of secondary water features along the Trinity River downstream from Lewiston Dam, California, and change in secondary water feature area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.....30
18. Graphs showing temporal changes in the active-channel from 1980 to 2011 for the Trinity River downstream from Lewiston Dam, California: *A*, baseflow shoreline length; *B*, active-channel width31
19. Graphs showing streamflow measured at the Lewiston gage on the Trinity River, California, 1.5 km downstream from Lewiston Dam, from 1980 to 2011: *A*, mean daily and annual peak flows; *B*, annual average flows. ROD, Record of Decision32
20. Boxplots showing mean daily flows from 1980 to 2011, grouped by month with minimum in-stream flow, for the Lewiston gage on the Trinity River, California: *A*, pre-ROD (Record of Decision) period; *B*, post-ROD period34
21. Graph showing contributing drainage area for 13 geomorphic reaches, delineated by vertical lines and described in table 2, along the Trinity River downstream from Lewiston Dam, California.....35
22. Graph showing the mean annual flow measured at five mainstem gages on the Trinity River, California, downstream of Lewiston Dam, California, from 1996 to 2011....35
23. Graphs showing mean daily flows measured at five mainstem gaging stations on the Trinity River, California, downstream from Lewiston Dam, from 1980 to 2011, and annual time series for four wettest years during the study period: *A*, 1997; *B*, 1998; *C*, 2006; *D*, 201136
24. Diagram showing summary of relevant management actions from 1976 to 2011 along the Trinity River downstream from Lewiston Dam, California37
25. Bar graph showing annual and cumulative volumes of sediment extraction and augmentation for Trinity River downstream from Lewiston Dam, California, from 1980 to 201138
26. Summary of constructed riparian and channel features along the Trinity River downstream from Lewiston Dam, California, in 1980, 1997, 2001, 2006, 2009, and 201139
27. Graphs showing changes in active-channel area due to bank erosion and accretion along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 201141
28. Graphs showing changes in active-bar area due to bar scour and accretion along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 201142
29. Graphs showing changes in bar vegetation along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 2011 ...43

Figures—Continued

30.	Graphs showing cumulative downstream change in the areal extent of exposed active bars and of the active channel along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 2011 ...	45
31.	Geomorphic feature maps for the Sven Olbertson Rehabilitation Site on the Trinity River, California, 1.0 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.....	48
32.	Geomorphic feature maps near Junction City on the Trinity River, California, 50.1 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.....	49
33.	Geomorphic feature maps for Conner Creek Rehabilitation Site on the Trinity River, California, 53.8 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.....	50
34.	Geomorphic feature maps at Lime Point on the Trinity River, California, 58.1 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.....	51

Tables

1.	Recommended flow releases to the Trinity River, California, from Lewiston Dam and associated management objectives.....	8
2.	Mapping protocol structure and geomorphic feature descriptions	10
3A.	Geomorphic reach descriptions and restoration history for study segments along the Trinity River, California, downstream from Lewiston Dam: upper river segment.....	13
3B.	Geomorphic reach descriptions and restoration history for study segments along the Trinity River, California, downstream from Lewiston Dam: central river segment....	14
3C.	Geomorphic reach descriptions and restoration history for study segments along the Trinity River, California, downstream from Lewiston Dam: lower river segment.....	14
4.	Uncertainty analysis for six geomorphic maps of the Trinity River, California, downstream from Lewiston Dam.	15
5.	Summary of stream discharge data for the Trinity River, California, downstream from Lewiston Dam.	16
6.	Summary of bar and bank changes during five study periods for the Trinity River, California, downstream from Lewiston Dam.....	40

Conversion Factors

[Inch/pound to International System of Units]

Multiply	By	To obtain
Volume		
acre-foot (acre-ft)	1,233	cubic meter (m ³)
Flow rate		
cubic foot per second (ft ³ /s)	0.02832	cubic meter per second (m ³ /s)

[International System of Units to Inch/pound]

Multiply	By	To obtain
Length		
millimeter (mm)	0.03937	inch (in.)
meter (m)	3.281	foot (ft)
kilometer (km)	0.6214	mile (mi)
Area		
square meter (m ²)	10.76	square foot (ft ²)
square kilometer (km ²)	0.3861	square mile (mi ²)
Volume		
cubic meter (m ³)	264.2	gallon (gal)
Flow rate		
cubic meter per year (m ³ /yr)	0.000811	acre-foot per year (acre-ft/yr)
meter per year (m/yr)	3.281	foot per year (ft/yr)

Datums

Vertical coordinate information is referenced to the North American Vertical Datum of 1988 (NAVD 88).

Horizontal coordinate information is referenced to the North American Datum of 1983 (NAD 83).

Elevation, as used in this report, refers to distance above the vertical datum.

Abbreviations and Acronyms

DTM	digital terrain model
EIS	Environmental Impact Statement
FPkm	floodplain kilometer
GIS	geographic information system
HVT	Hoopa Valley Tribe
RMSE	root mean square error
ROD	Record of Decision
TAF	thousand acre-feet
TRA	Trinity Restoration Associates, Inc.
TRD	Trinity River Division of the Central Valley Project
TRFE	Trinity River Flow Evaluation
TRRP	Trinity River Restoration Program
USFWS	U.S. Fish and Wildlife Service

Acknowledgements

This study benefited from discussions with Bureau of Reclamation staff including Andreas Krause, Dave Gaeuman, and Eric Peterson and members of the Trinity River Restoration Program Physical Workgroup who provided helpful guidance and review.

Rose Wallick (U.S. Geological Survey, Portland, Oregon) and MacKenzie Keith (U.S. Geological Survey, Portland, Oregon) were instrumental in the development and analysis of the mapping geodatabase.

Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

By Jennifer A. Curtis, Scott A. Wright, J. Toby Minear, and Lorraine E. Flint

Abstract

The Trinity River Restoration Program, one of the nation's largest adaptively managed river restoration programs, requires periodic assessment to determine the effectiveness of management actions in restoring channel dynamics and habitat features. This study documents riparian and channel changes along an intensively managed 65-kilometer reach of the Trinity River in California, downstream from Lewiston Dam. The two primary periods of interest, from 1980 to 2001 and from 2001 to 2011, are separated by a shift in restoration activities mandated by the U.S. Department of the Interior December 2000 Record of Decision. The post-2001 restoration strategy increased managed-flow releases, gravel augmentation, watershed restoration, and mechanical channel rehabilitation.

We assessed the nature and extent of geomorphic change and a series of ecological performance measures (channel complexity, shoreline length, and channel–floodplain connectivity) by using a series of maps digitized from available rectified orthophotography acquired during low-flow conditions in 1980, 1997, 2001, 2006, 2009, and 2011. Lateral changes in riparian and channel features were used to quantify alluvial processes, and a review of existing streamflow, sediment, and restoration records was used to assess causal mechanisms. During the study period, natural bank erosion and mechanical rehabilitation of channel margins converted riparian features to channel features and expanded the active-channel area. The primary period of bank erosion and expansion of the active channel was from 1980 to 1997. Subsequent bar accretion from 1997 to 2001, followed by slightly greater bar scour from 2001 to 2006, took place primarily in the central and lower reaches of the study area, downstream of Indian Creek. In comparison, post-2006 bank and bar changes were spatially limited to reaches that had sufficient local transport capacity or sediment supply supported by gravel augmentation, mechanical channel rehabilitation, and tributary contributions.

The highest rates of change in the areal extents of channel and riparian features were observed during the pre-2001 period, which was longer and relatively wetter than the post-2001 period. A series of tributary floods in 1997, 1998, and 2006 increased channel complexity and floodplain

connectivity. During the post-2006 period, managed-flow releases, in the absence of tributary flooding, combined with gravel augmentation and mechanical restoration, caused localized increases in sediment supply and transport capacity that led to smaller, but measurable, increases in channel complexity and floodplain connectivity in the upper river near Lewiston Dam. Extensive pre-2001 channel widening and the muted geomorphic response of channel rehabilitation sites to post-2001 managed flows highlight the need for continued monitoring and assessment of the magnitude, duration, and timing of prescriptive flows and associated geomorphic responses.

Introduction

In 1958, a plan was developed to increase water supplies and generate power for California's Central Valley Project, in part, by transferring water from the Trinity River (fig. 1) to the Sacramento River. The Trinity River Division (TRD) included construction of two main-stem dams. The reservoir behind Trinity Dam began filling in 1960, and Lewiston Dam was completed in 1963. Following closure of the Trinity Dam, annual water diversions commenced, and up to 75 to 90 percent of the upper Trinity River's annual streamflow, measured as inflow to Trinity Lake, was transferred to the upper Sacramento River (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999).

The combination of dam construction, flow diversion, and land-use practices (dredge mining and upland logging) caused channel aggradation, riparian encroachment, and simplification of channel morphology with concurrent reductions in channel complexity and channel–floodplain connectivity downstream from Lewiston Dam (Trinity River Taskforce, 1970). Recognition that riparian and channel changes coincided with declines in salmon and steelhead populations led to an Environmental Impact Statement (EIS; U.S. Fish and Wildlife Service, 1980). The EIS determined the fisheries decline was primarily caused by streambed sedimentation, insufficient streamflow, and inadequate regulation of fish harvests. On the basis of these findings, channel bank rehabilitation and flow increases were recommended to restore salmon and steelhead populations (U.S. Fish and Wildlife Service, 1980).

2 Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

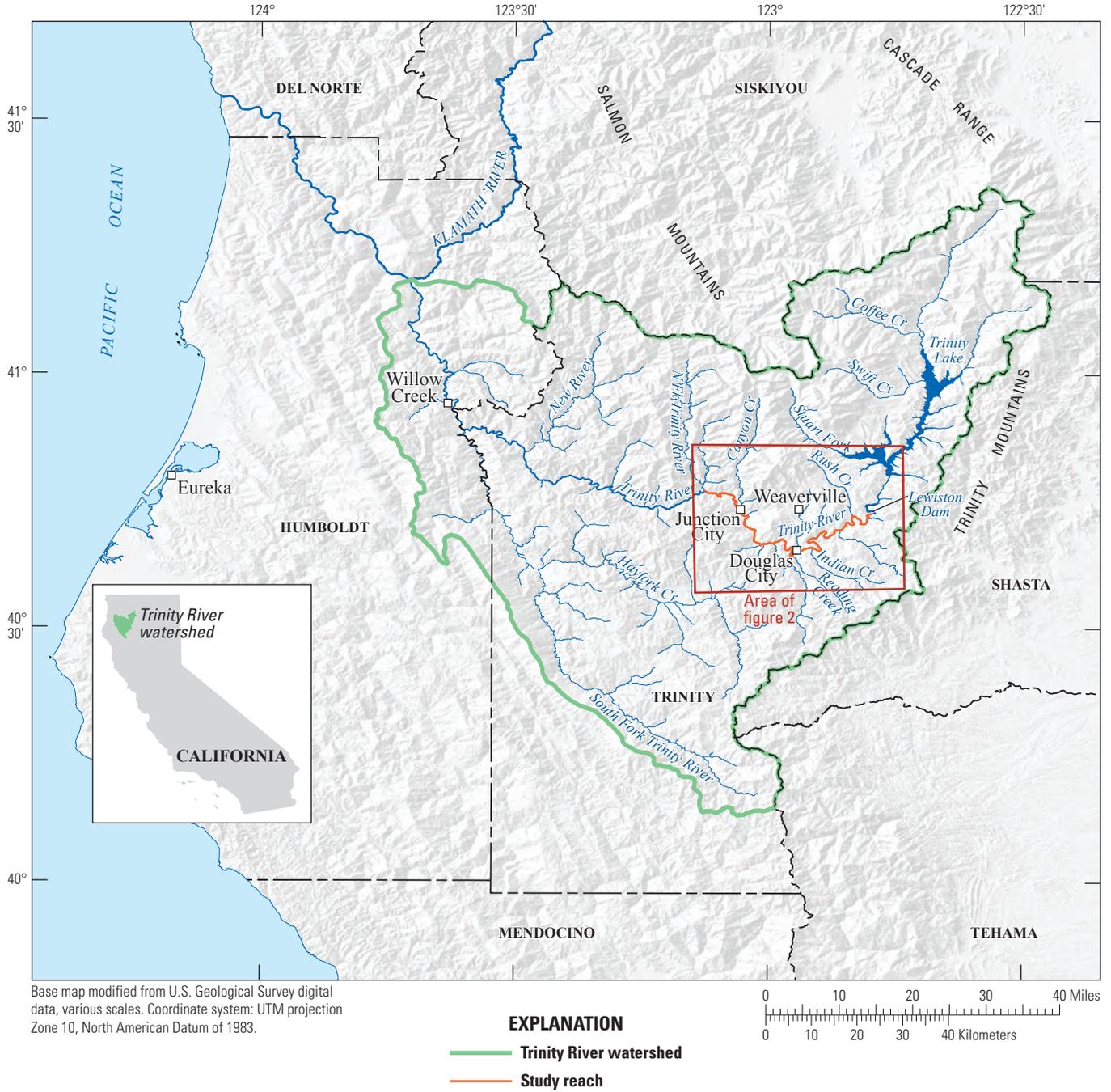


Figure 1. Study area, Trinity River, California.

Although baseflow increases began in 1981, salmon and steelhead populations continued to decline, which led to additional environmental and experimental flow studies summarized in the Trinity River Flow Evaluation (TRFE; U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999). The TRFE presented recommendations that were formally adopted in December 2000 by the U.S. Department of the Interior Record of Decision (ROD; U.S. Department of the Interior, 2000). The ROD explicitly required a restoration strategy that included managed-flow releases, gravel augmentation, mechanical channel rehabilitation, and watershed restoration. The Trinity River Restoration Program (TRRP), a multi-agency partnership, was tasked with overseeing implementation of mandated restoration and adaptive management. The TRRP's mission is to promote geomorphic processes responsible for creating and maintaining habitat sufficient to restore the salmonid fishery to pre-dam levels. Restoration of a dynamic alluvial channel, exhibiting all the characteristics of the pre-dam river, but at a smaller scale, is a primary goal.

Purpose and Scope

The purpose of this report is to provide results from a geomorphic assessment of the 65-kilometer (km) restoration reach along the mainstem Trinity River, downstream from Lewiston Dam, completed by the USGS in cooperation with the TRRP. The study period began in 1980, prior to implementation of baseflow increases in 1981, and covered approximately two decades (1980 to 2001) prior to the ROD and one decade (2001 to 2011) following. The primary study objectives were as follows:

1. To develop a system-wide perspective of geomorphic features.
2. To determine the evolution of geomorphic features and the trajectories of geomorphic change.
3. To quantify ecologically significant measures of geomorphic change relevant to Trinity River fisheries restoration.
4. To evaluate the cumulative effects of natural and managed drivers of change.

We used six available rectified orthophotographs, acquired during baseflow conditions, to construct a series of retrospective geomorphic feature maps that are published in a companion report and geodatabase (Curtis and Guerrero, 2015; <http://dx.doi.org/10.5066/F7TT4P04>). The orthophotographs bracketed five study periods that included two pre-ROD periods (May 1980 to October 1997 and October 1997 to November 2001) and three post-ROD periods (November 2001 to July 2006, July 2006 to April 2009, and April 2009 to August 2011). Using the six geomorphic feature maps, we quantified spatial and temporal changes in riparian

and channel features and assessed a series of ecological performance measures (channel complexity, shoreline length, and channel–floodplain connectivity) identified as primary metrics for understanding linkages between ecosystem benefits and restoration actions (Trinity River Restoration Program and ESSA Technologies Ltd., 2009).

During each of the five study periods, there were concurrent and sequential alterations in flow, sediment supply, and channel morphology. We interpreted cumulative change during each of the five periods in the context of controlling factors related to natural channel processes, flow and sediment management, and mechanical alterations of channel morphology. Results from this study are intended to help inform the design and implementation of future channel rehabilitation projects (Hoopa Valley Tribe and others, 2011a) and adaptive management of the TRRP restoration reach.

Study Area

The Trinity River traverses a region in the Central Klamath Mountain geologic province (Irwin, 1972, 1981) underlain by geologic terranes accreted to western North America during the late Mesozoic Era and early Tertiary Period (Ingersoll and Schweickert, 1986). A progression of eastward dipping thrust faults (Irwin, 1994) juxtaposes younger, Jurassic mixed-volcanic and sedimentary rocks against older, Devonian sedimentary rocks. During and subsequent to accretion, these geologic units were metamorphosed and intruded by igneous plutons, dikes, and sills. The Weaverville Formation, a Cenozoic gold-bearing fluvial deposit, was deposited on older stratigraphy (Diller, 1902) in the study area.

Anomalously high topography and surface exposure of Devonian rocks in the Klamath province indicate a period of geologically recent tectonic uplift. Inferred rapid uplift could be related to plate convergence at the nearby Cascadia subduction zone and Mendocino Triple Junction (Anderson, 2008). Inferred uplift rates also provide a tectonic mechanism for river incision and development of bedrock channels draining the central Klamath Mountains.

The Trinity River flows 270 km westward from its headwaters to its confluence with the Klamath River (fig. 1). The Trinity is the Klamath River's largest tributary and has a total drainage area of 7,670 square kilometers (km²). Approximately one quarter of the Trinity River watershed (1,850 km²) is upstream from Lewiston Dam. The watershed is predominately mountainous and forested. Elevations range from 90 to 2,700 meters (m) above sea level, and the highest elevations were glaciated during the Pleistocene. The channel network is primarily bedrock with intermittent alluvial reaches. Downstream of Lewiston Dam, the river flows southwest through a series of antecedent meanders superimposed across northwest-trending terranes. Near Douglas City, the river turns and flows northwest through a structurally controlled landscape.

The climate in this region is Mediterranean, with hot, dry summers and cool, wet winters. Beginning in November, storm systems from the Pacific Ocean bring winter precipitation. Approximately 80 percent of the annual precipitation falls between November and March. The U.S. Forest Service has operated a weather station in Weaverville since 1905 (Weaverville RS, WVR, <http://www.cdec.water.ca.gov>). The Weaverville station is at an elevation of 625 m, where average annual precipitation is 935 millimeters (mm), and average annual snowfall is 570 mm. The maximum monthly precipitation, 530 mm, fell in December 2005, and the maximum 24-hour precipitation, 140 mm, fell on January 4, 1982. Elevations between 1,220 and 1,820 m are susceptible to rain-on-snow events (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999), which can produce large tributary floods.

The TRRP restoration reach extends from Lewiston Dam downstream to the confluence with the North Fork Trinity River (fig. 2). This 65-km river segment along the mainstem Trinity River was identified as the most severely affected by flow regulation and diversion and was recommended for restoration by the initial flow evaluation (U.S. Fish and Wildlife Service, 1994). The study reach is a partially confined gravel-bed river that has a nearly constant slope of 0.002 meters per meter (fig. 3). The nearly constant slope indicates that bedrock functions as a primary control of channel slope. This assertion is further supported by intermittent bedrock exposures in the active channel throughout the study reach. The channel pattern is primarily single-thread, and the dominant channel type is pool-riffle with intermittent plane-bed and canyon reaches (Montgomery and Buffington, 1998).

From the early 1860s to the early 1900s, large-scale hydraulic mining of the gold-bearing Weaverville Formation and, to a lesser extent, logging increased sediment supplies to the study reach. Deposition of large-diameter mining sediment aggraded the channel and valley bottom by several feet (Trinity River Taskforce, 1970; Krause and others, 2010). Beginning in the late 1800s and continuing until 1960, dredge mining of the mainstem channel overturned more than 70 percent of the floodplain area (Stearns, 1969), depositing large piles of coarse tailings (gravel, cobble, and boulder) up to 12 m high that confine the modern river in some locations (Krause, 2012b). Many of these tailings piles were reworked by the 1955 and 1964 floods (Ritter, 1968), producing an extensive set of historic terraces and inset floodplains. Redistribution of stored mining sediment and tributary confluence aggradation during the 1964 flood led to the first mechanical restoration effort in 1965 that involved confluence channelization. Notably, smaller scale hydraulic mining continued in the study reach until 1970.

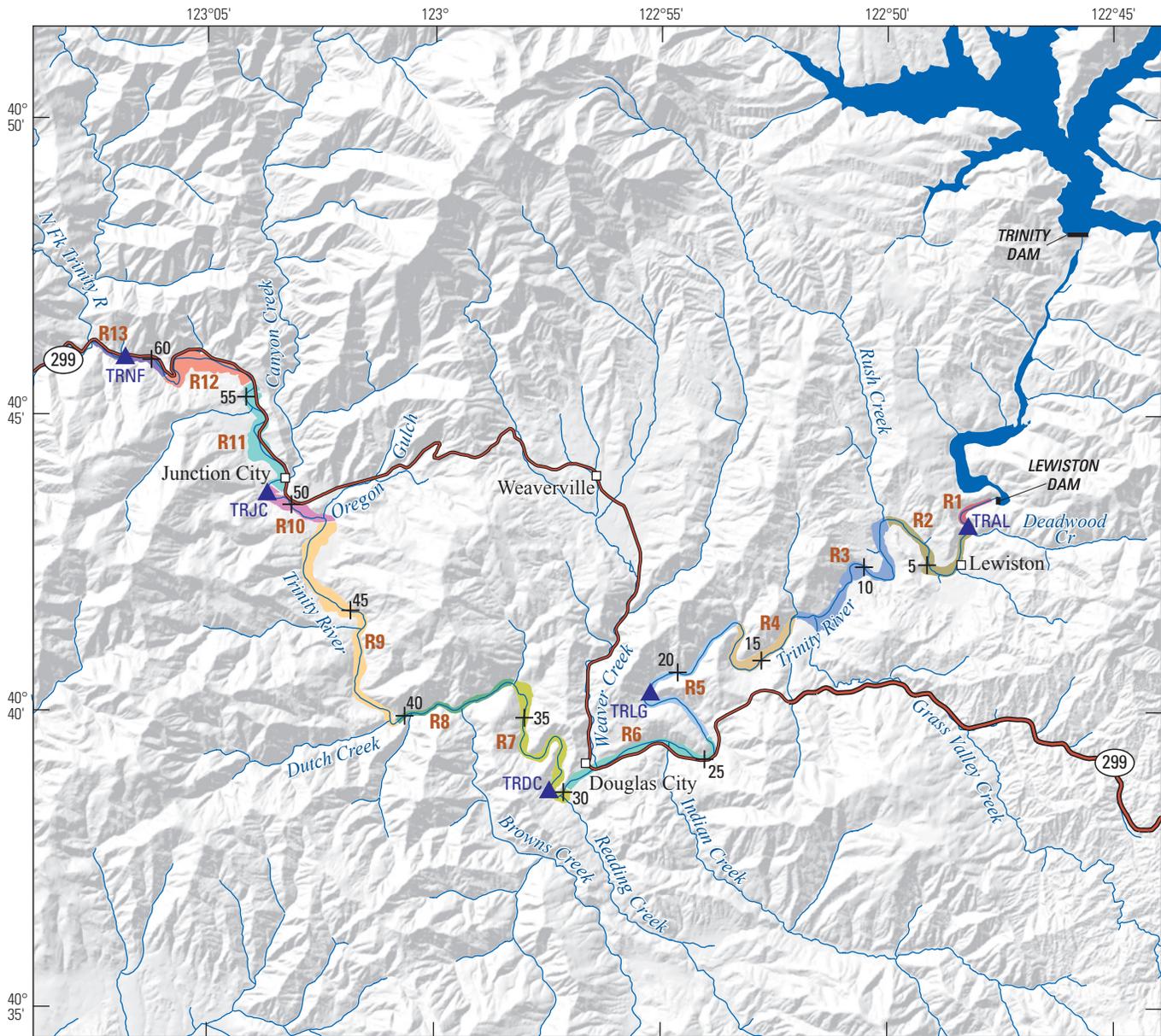
In-Stream Effects of the Trinity River Diversion

In-stream effects related to Trinity River flow diversions are documented explicitly in the TRFE (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999) and numerous project reports. In this report, we review the evolution of flow and sediment management strategies to support a thorough understanding of the study reach history. Note that we use English units, cubic feet per second (ft³/s) and thousand acre-feet (TAF), to characterize flow data because they are commonly used by the Trinity River management community.

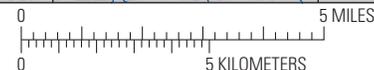
The influence of flow regulation and diversion on streamflow variability is readily apparent in mean daily flows recorded at the Lewiston gaging station (fig. 4; Trinity River at Lewiston, USGS station identification number 11525500), 1.5 km downstream from Lewiston Dam (fig. 2). The pre-dam flow regime included summer base flows, winter-storm peaks, and spring-snowmelt peaks, which created variable seasonal flow conditions. Post-dam flow variability decreased and flow releases from 1964 to 1973 were pursuant to the 1955 Congressional Act, which authorized construction and operation of the TRD by the Bureau of Reclamation. The TRD maintained daily flows between 150 and 250 ft³/s at the Lewiston gage, and the annual flow-release volume was set at 120.5 TAF, with periodic, larger safety-of-dam releases.

Post-dam salmonid habitat deterioration and population declines (Trinity River Taskforce, 1970) prompted a request in 1980 by the California Department of Fish and Game to increase the annual flow release from Lewiston Dam to the Trinity River to 315 TAF. Subsequent investigations of the relation between in-stream flows and salmonid habitat by the U.S. Fish and Wildlife Service (USFWS) were incorporated into an EIS (U.S. Fish and Wildlife Service, 1980), which concluded that insufficient streamflow was the most critical limiting factor for restoring salmonid populations. The EIS explicitly recommended channel rehabilitation by mechanical restoration and increases in minimum annual flow volumes to 140 TAF in critically dry water years, 220 TAF in dry water years, and 340 TAF in normal or wet water years.

In 1981, a Department of the Interior Secretarial Decision was issued that mandated baseflow increases and completion of a flow evaluation study to evaluate the potential effects of implementing prescriptive in-stream flows to mimic variable climatic conditions and provide suitable flows to restore dynamic fluvial processes, maintain channel complexity, and support all stages of the salmonid life cycle. Drier climatic conditions prevailed from 1986 to 1990, which delayed flow increases. In the early 1990s, a series of 3,000 to 6,000 ft³/s experimental flows were released, and in-stream effects were monitored as part of an environmental assessment (EA).



Base map modified from U.S. Geological Survey digital data, various scales. Coordinate system: UTM projection Zone 10, North American Datum of 1983.



EXPLANATION

R1 Study reaches		
Upper river	Central river	Lower river
 R1 - Lewiston	 R6 - Vitzhum Gulch	 R9 - Dutch Creek
 R2 - Sawmill	 R7 - Reading Creek	 R10 - Oregon Gulch
 R3 - Rush Creek	 R8 - Dutton Creek	 R11 - Canyon Creek
 R4 - Stott		 R12 - Lime Point
 R5 - Poker Bar Canyon		 R13 - Pear Tree

U. S. Geological Survey streamgaging station—See table 5 for station names

+ 5 Floodplain kilometer—distance downstream from Lewiston Dam

Figure 2. Trinity River restoration reach, in California, from Lewiston Dam downstream to the North Fork Trinity confluence and 13 geomorphic reaches, within 3 river-channel segments, used as the spatial framework for interpretation of mapping results.

6 Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

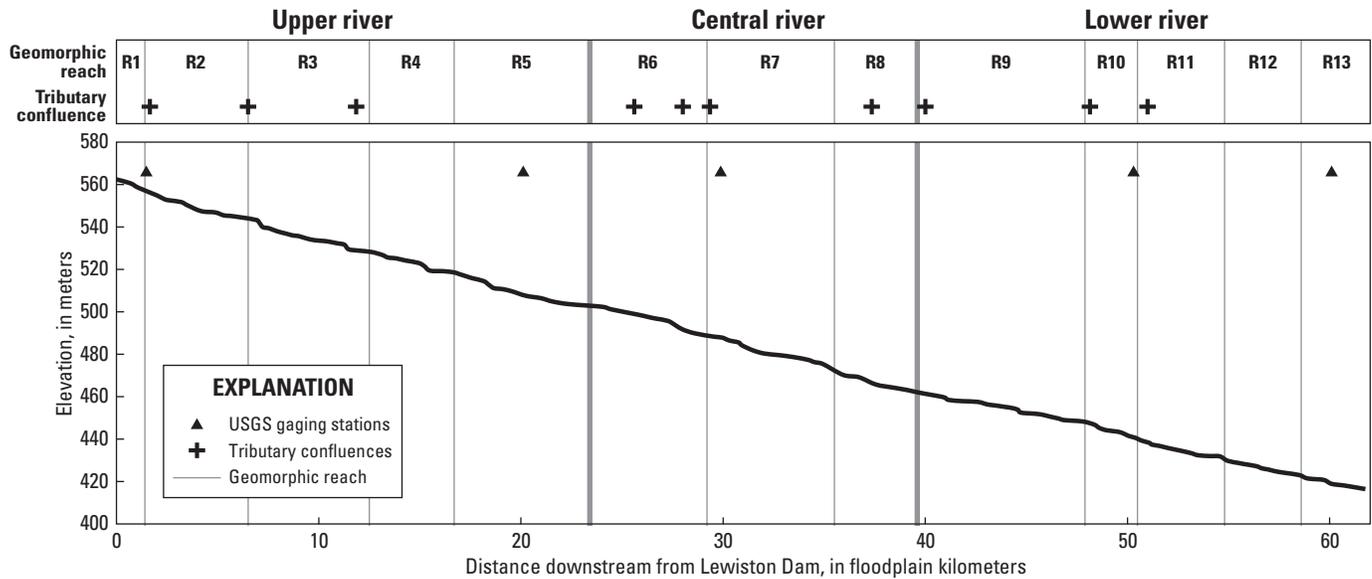


Figure 3. Elevation profile of the Trinity River restoration reach, California, estimated from 10-meter-resolution digital elevation data. See [table 3](#) for description of the 13 geomorphic reaches.

The TRFE was completed in 1999, and flow recommendations were formally adopted in the ROD (U.S. Department of the Interior, 2000), but litigation delayed full implementation of the ROD flows until December 2005. Post-ROD flow management included large increases in annual flow volumes compared to those initially recommended in the 1980 EIS. In critically dry water years, the EIS recommendation of 140 TAF was more than doubled to 369 TAF. The EIS recommendation of 340 TAF was increased to 647 TAF during normal years and to 701 TAF during wet years ([table 1](#)).

An important change in post-ROD flow management was the implementation of an annual spring-flow release with specific geomorphic objectives ([table 1](#)). The annual peak release typically begins in early May and can extend into mid-July depending on the water-year type. Water-year type and the spring-flow release are determined in April of each year on the basis of forecasted annual-flow volumes at the Lewiston stream gage (Krause, 2012a). The peak release can be described as a “benched” hydrograph, with rapid increases in the rising limb, and a gradual decrease in the falling limb that is punctuated by periods of steady flows referred to as “benches” (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999). The “benches” are designed to support bed mobility, scour, and geomorphic objectives listed in [table 1](#).

A post-dam sediment deficit existed downstream of Lewiston Dam (Gaeuman and Krause, 2011). Sediment deficit conditions occur when transport capacity exceeds sediment supply, which often results in scour and evacuation of bed-material to downstream reaches (Schmidt and Wilcock, 2008; Draut and others, 2011). Excess transport capacity immediately downstream from dams, typical for reaches that

lack sufficient sediment supply, can lead to coarsening of the channel bed, decreased bed mobility, and channel incision. Within the study reach, changes in the substrate grain size relative to pre-dam conditions are unknown, but gaging measurements, collected at a cableway 2.5 km downstream from Lewiston Dam, indicated negligible post-dam channel incision (Gaeuman, 2008).

Abundant tributary and in-channel sediment sources exist in downstream study reaches (Graham Matthews and Associates, 2001), where sediment deficit conditions transition to equilibrium or surplus conditions (Gaeuman and Krause, 2011). The transition from deficit to surplus conditions often occurs downstream from the first major tributary confluence (Schmidt and Wilcock, 2008) or in pre-dam aggradation zones, where modern bed and bank processes recruit stored sediment from in-channel or floodplain sources (Draut and others, 2011). Beginning at about 3 km downstream from Lewiston Dam, large amounts of legacy mine tailings are stored along channel margins, but flows in this reach are insufficient to scour and transport this large-diameter material. Prior to construction of sediment-retention ponds in 1986, Grass Valley Creek (11.9 floodplain kilometers, or FPkm) was the first large contributor of sediment downstream from Lewiston Dam (Graham Matthews and Associates, 2001). At the time of writing this report, almost all bed-material sized sediment from Grass Valley Creek is trapped in a series of retention ponds constructed at the confluence in 1986. After 1986, Indian Creek (25.6 FPkm) functioned as the first important contributor of sediment downstream from Lewiston Dam (Graham Matthews and Associates, 2001).

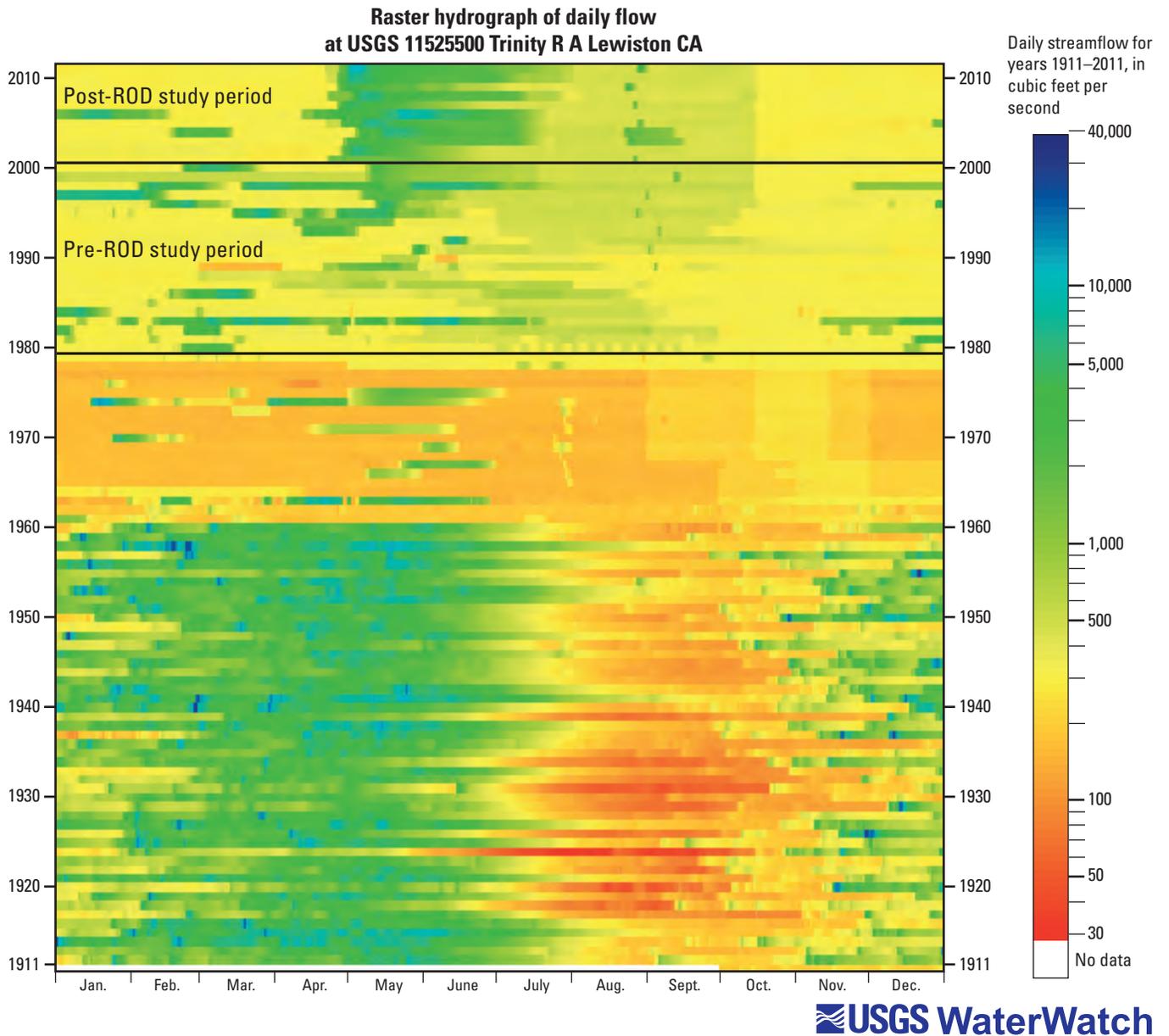


Figure 4. Raster hydrograph (http://waterwatch.usgs.gov/index.php?id=wwchart_rastergraph) showing mean daily flows measured 1.5 kilometers downstream from Lewiston Dam (fig. 2) along the Trinity River, California. Hydrograph shows monthly and annual variability of mean daily flows for 1911 to 2011. Pre- and post-ROD study periods are separated by the U.S. Department of the Interior Record of Decision (U.S. Department of the Interior, 2000). ROD, Record of Decision.

8 Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

Table 1. Recommended flow releases to the Trinity River, California, from Lewiston Dam and associated management objectives.

[See report by Hoopa Valley Tribe and others (2011b) for additional details; acre-ft, acre-foot; D84, particle diameter that represents 84 percent of the grain-size distribution of channel bed sediment; days/yr, days per year; ft³/s, cubic feet per second; ROD, record of decision; yr, year]

Water-year type	Frequency of water-year type during post-ROD period (percent)	Recommended annual flow released to Trinity River (acre-ft)	Recommended peak release at Lewiston (ft ³ /s)	Recommended duration of peak release (days)	Pre-ROD exceedence of recommended peak flow (days/yr)	Post-ROD exceedence of recommended peak flow (days/yr)	Objectives
Critically dry	12	369,000	1,500	36	31	118	Discourage encroachment of riparian vegetation on low bars.
Dry	28	453,000	4,500	5	10	19	Mobilization of gravels in pool tails and mid-channel bars.
Normal	20	647,000	6,000	5	5	8	Channel-bed surface mobilization on bars and riffles. Coarse-sediment transport equal to sediment supply. Tributary confluence maintenance. Channel migration. Managed floodplain inundation and fine-sediment deposition. Scour of 0–1 year old riparian seedlings on lower bar surfaces. Recharge of shallow groundwater table. All effects realized at lower flows.
Wet	28	701,000	8,500	5	0.1	1.7	Scour of bar margins greater than or equal to D84 depth. Coarse sediment movement. Scour of 1–2 year old riparian seedlings and lower bar surfaces. All effects realized at lower flows.
Extremely wet	12	815,000	11,000	5	0	0.5	Scour depth of alternate bars greater than two times D84. Managed floodplain scour. Side-channel maintenance. Scour of 2–3 year old riparian seedlings and lower bar surfaces. All effects realized at lower flows.

Decreases in post-dam flows resulted in aggradation of tributary confluences (Ritter, 1968) and accumulation of undesirable fine bed material primarily downstream of Grass Valley Creek (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999). The TRFE suggested that post-dam decreases in coarse bed material reduced successful salmonid spawning and simplified the structure of available physical habitat (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999). There was concern that the relatively large annual flow releases necessary to mobilize and scour undesirable fine bed material would result in the transport and removal of existing gravel in the reach immediately downstream from Lewiston Dam, which, despite effects related to flow regulation and diversion, continued to function as a primary spawning reach for regional salmonid production (U.S. Fish and Wildlife Service, 1989). To mitigate transport of gravel out of the primary spawning reach, the ROD mandated gravel augmentation in the upper river.

Gravel augmentation in the reach immediately downstream from Lewiston Dam began in 1998 with in-channel placement of coarse-sized bed material. Note that the TRRP defines coarse bed material as all particles greater than 8mm in diameter (Gaeuman and Krause, 2011). Recently, Gaeuman (2008) determined an optimal particle-size distribution (9.5 to 125 mm) and annual quantity (5,400 cubic meters, or m³) for long-term maintenance of coarse bed material in the upper river.

Methods

The objectives of this study were to develop a system-wide perspective of geomorphic features and to assess cumulative geomorphic change and controlling factors during five periods spanning 1980 to 2011. We characterized the spatial distribution of geomorphic features along the study

reach by using a series of retrospective geomorphic maps and completed geospatial analysis to assess cumulative change during each period. Geomorphic changes were interpreted in the context of controlling factors related to natural processes, flow and sediment management, and mechanical restoration.

Estimating Geomorphic Change

Geomorphic maps published in a companion report and geodatabase (Curtis and Guerrero, 2015; <http://dx.doi.org/10.5066/F7TT4P04>) were used to classify upland, riparian, and channel features. The map dates bracket relevant geomorphic events and include three dates that span the pre-ROD period (May 16, 1980; October 20, 1997; November 7, 2001) and three dates that span the post-ROD period (July 25, 2006; April 16, 2009; August 16, 2011). The orthophotographs used as base maps were acquired during baseflow conditions, about 300 ft³/s, when channel features were well exposed.

A map boundary was defined on the basis of the area inundated by a 500-year recurrence interval flood. This boundary, constructed by a one-dimensional flow model (California Department of Water Resources, 2007), roughly defined the valley bottom. The boundary was extended by 30 m to include all features of interest. Geomorphic features larger than 30 m² within the map boundary were digitized at a scale of 1:1,000. Mapping was limited to exposed features because subaqueous features, although evident in some years, could not be consistently digitized.

The hierarchy of the mapping protocol included upland, riparian, and channel features similar to recent studies on the Colorado River and its main tributary, the Green River (Schmidt and others, 1999; Grams and Schmidt, 2002). The protocol was designed to assess spatial and temporal changes in geomorphic features and ecologically important measures of geomorphic change relevant to restoration of Trinity River fisheries. Previous studies determined that the linkage between habitat and channel geomorphology was represented best by channel complexity, channel–floodplain connectivity, and shoreline length, which represent fundamental variables governing the quality and quantity of available salmonid habitat (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999; Trinity River Restoration Program and ESSA Technologies Ltd., 2009). The mapping protocol, geomorphic feature definition, and the ArcGIS (v. 10.0) geodatabase structure are explained in [table 2](#).

Geomorphic features were delineated by orthophoto interpretation, and specific observational criteria are described in [table 2](#). The mapping was further constrained by a contour map derived from a 2009 digital terrain model (DTM, Woolpert, 2010) and a series of water-surface extents constructed by a one-dimensional flow model. The mapping was field checked in the summer of 2012. Observational criteria used to classify geomorphic features included the age, density, and type of vegetation; spatial transitions

among vegetation types; evidence of scour or deposition; and presence of stagnant or flowing water. Although features were primarily delineated on the basis of these criteria, the 2009 contour map helped delineate relatively static features, and modeled water surfaces were used to assess riparian inundation extents and to interpret channel–floodplain connectivity. Water-surface extents were constructed on the basis of flow releases from Lewiston Dam, which ranged from 2,000 to 11,000 ft³/s with tributary flows incorporated downstream. Lower elevation channel features were topographically inset relative to riparian and upland features. This nested topographic relation is illustrated in [figure 5](#). Generally, higher elevation features are older and inundated less frequently by larger flows.

The boundary between the upland and riparian environments is delineated by the pre-dam floodplain, which is a relict depositional landform that is partially inundated at 6,000 ft³/s and fully inundated at about 11,000 ft³/s. Under the regulated-flow regime in use at the time of writing, the upland environment is inundated only during extreme flows that have large tributary contributions.

Three floodplain types were defined: a relatively continuous, higher elevation pre-dam floodplain; a series of intermittent constructed floodplains; and lower elevation topographic benches created by the post-ROD flow regime. Isolated constructed floodplains were created by mechanical rehabilitation (vegetation removal, re-contouring, and surface lowering) as part of the USFWS bank-rehabilitation program in the early 1990s and by the TRRP after 2005. The larger scale TRRP projects included constructed floodplains designed to be inundated by the post-ROD mean annual peak-flow release (about 6,000 ft³/s). The lowest elevation riparian features are post-dam topographic benches composed of coalesced bars. The post-dam benches are composed of previously active bars that were stabilized by 1975 as a result of declines in transport capacity due to flow regulation and concurrent vegetation encroachment. By 1980, these stable bars had coalesced into relatively continuous low-elevation floodplain features. Under the flow regime in use at the time of writing, these benches are inundated by flows ranging between about 2,000 and 4,500 ft³/s. Portions of these features are elevated as a result of vegetation encroachment, which facilitated sediment deposition and development of riparian berms. The extent and frequency of inundation is influenced by the presence of these berms, which act as natural levees.

The active-channel environment ([table 2](#)) includes the baseflow-wetted channel and morphologically active-channel margins characterized by bedload transport. Similar to previous studies (Grant and Swanson, 1995; Church, 2002; Zilliani and Surian, 2012), we delineated a dynamic active-channel boundary that included wetted-channel features and unvegetated or sparsely vegetated bars. The mapping protocol accommodated the transitional boundary between the channel and riparian environments that expands and contracts through time.

10 Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

Table 2. Mapping protocol structure and geomorphic feature descriptions.

[See companion report by Curtis and Guerrero (2015) for additional details. **Abbreviations:** FPkm, floodplain kilometer; ft³/s, cubic foot per second; km, kilometer; km², square kilometer; m, meters; ROD, record of decision; TRRP, Trinity River Restoration Program; USFWS, U.S. Fish and Wildlife Service; %, percent]

Geomorphic setting	Feature description
Terrestrial environment	
Uplands	Uplands include areas underlain by soil, colluvium, alluvium, bedrock, or legacy mine tailings. Unless altered by mechanical restoration, the areal extent of upland features typically persists throughout the historic imagery.
Riparian environment	
Islands	Alluvial features bounded on all sides by water and distinguished from medial bars by denser mature vegetation, greater areal extents, and higher elevations. Although islands existed prior to 1980, most were created by side-channel construction.
Floodplains	Floodplain features typically exhibit a vegetation gradient with the highest density of vegetation along the active-channel margin; density decreases with increasing distance from the channel margin.
Pre-dam floodplain	This broad, relict depositional feature was created and inundated annually by the unregulated pre-dam flow regime, but is inundated periodically under the post-dam flow regime by flows between about 6,000 and 11,000 ft ³ /s.
Constructed floodplains	Discontinuous restoration features created by mechanical vegetation removal, re-contouring, and surface lowering as part of the USFWS bank-rehabilitation program in the early 1990s and since 2005 as part of the TRRP bank-rehabilitation program.
Post-dam topographic bench	Depositional features composed of coalesced bars stabilized prior to 1975 because of declines in scouring flows and the associated encroachment of vegetation. Portions of these features are elevated because of vegetation-facilitated sediment deposition and development of a riparian berm along the channel margin.
Riparian wetlands	These disconnected aquatic features are outside the modern active-channel boundary. Only areas containing water in the base imagery were mapped, even when it was apparent that additional areas would be inundated seasonally.
Other	Unique constructed features, such as borrow pits and gravel-recruitment piles.
Active-channel environment	
Baseflow wetted channel	The primary channel delivers the majority of flow and, where the channel splits, it is identified as the widest channel. Wetted-channel area is delineated by the wetted perimeter, as seen in the base imagery.
Secondary water features	Wetted-channel features that do not deliver the majority of channel flow. Only areas containing water in the base imagery were mapped, even when it was apparent that additional areas were inundated at higher flows.
Alcove	Secondary water feature connected at one end to any wetted channel, including mainstem, tributary, side-channel, or split-flow channel.
Wetland	Secondary water feature completely disconnected from any other wetted-channel feature.
Side-channel	Secondary channels connected to the primary channel at the upstream and downstream ends and distinguished from split-flow channels by conveyance of less than 20% of total summer baseflow and generally less than 10%. The percentage of flow conveyance was estimated from channel widths.
Split-flow channel	Secondary channels created by flow separation that results in a change in the river morphology. Split-flow channels convey between 20 and 50% of baseflow. The percentage of flow conveyance was estimated from channel widths.
Bar	Dynamic features created by bedload transport typically oriented parallel to the primary flow direction. The boundary between bars and adjacent riparian or upland features was delineated by using observational criteria that included morphology, vegetation type and density, and physical evidence of scour or deposition.
Lateral	Depositional channel feature created and maintained by active bedload transport and attached to the channel margin.
Medial	Depositional channel feature created and maintained by active bedload transport and surrounded by water on all sides.

Table 2. Mapping protocol structure and geomorphic feature descriptions.—Continued

[See companion report by Curtis and Guerrero (2015) for additional details. **Abbreviations:** FPkm, floodplain kilometer; ft³/s, cubic foot per second; km, kilometer; km², square kilometer; m, meters; ROD, record of decision; TRRP, Trinity River Restoration Program; USFWS, U.S. Fish and Wildlife Service; %, percent]

Geomorphic setting	Feature description
Active-channel environment—Continued	
Bedrock outcrops	Static, non-alluvial features persistent in most or all years of base imagery. Can be buried by sediment in some years and exposed in others. Bedrock outcrops are typically darker than alluvial features and have a rough tone, jagged boundary, and lineations indicative of bedrock texture.
Other	Unique constructed features, such as hydraulic grade controls, bank stabilization features, and historic bridge pilings.
Additional mapping attributes	
Vegetation density	
Bare to sparse	Vegetation covers less than 10%.
Moderate	Vegetation covers 10 to 40%.
Dense	Vegetation covers greater than 40%.
Restoration features	
Constructed	Features created by in-channel gravel placement or channel and bank rehabilitation.
Bar stability	
Stable	No physical evidence of scour, mobilization, or deposition in the current imagery when compared to the previous imagery. The channel margin can have bare to dense vegetation, but must have a stable areal extent.
Active	Obvious physical evidence of scour, mobilization, or incipient deposition when compared to previous imagery. The baseflow-channel margin and the bar-surface area must be bare to sparsely vegetated in the current imagery.



Figure 5. Example of the topographic relations among depositional and constructed features for the Trinity River downstream from Lewiston Dam, California (photograph by J.A. Curtis). Photo shows left bank downstream of Canyon Creek (51 floodplain kilometers, or FPkm).

Channel features were assigned either to mainstem or tributary environments, and a simple bar classification (medial and lateral) was used (table 2). The presence of flowing or stagnant water delineated the wetted perimeter of baseflow channels and secondary water features (split-flow channels, side channels, alcoves, and aquatic wetlands). For the baseflow channels and secondary water features, only areas containing water were digitized, even when it was apparent that additional areas were inundated at higher flows. Three additional feature attributes were included in the geodatabase: restoration, vegetation density, and bar stability. Constructed features were labeled, which enabled assessment of features created or altered mechanically by in-channel gravel placement, side-channel construction, or bank rehabilitation. Vegetation density was estimated for all bar features, and bar stability was defined by vegetation density estimates, evidence of scour or deposition, and the presence or absence of vegetation along the baseflow-channel margin. Active bars typically have bare-to-sparse vegetation and a dynamic perimeter along the channel margin. In comparison, stable bars can have bare-to-dense vegetation, but more typically are characterized by moderate-to-dense vegetation and generally have a stable areal extent in consecutive orthophotographs.

Interpretation of Geomorphic Mapping

A spatial framework for interpreting results was developed on the basis of longitudinal changes in transport capacity and sediment-supply conditions. The framework was inferred from valley and channel confinement, location of tributary confluences, and the presence of in-channel legacy mine tailings and was used to delineate study reaches. The mainstem was initially divided into upper, central, and lower channel segments and then was subdivided into 13 geomorphic reaches (table 3). Lateral changes in channel and riparian features caused by bar and bank processes were investigated at a 1-km sub-reach scale.

Similar to recent studies by Wallick and others (2010, 2011), floodplain distance, rather than channel distance, was used to reference study-reach locations because distances along this line were static during the study period, whereas channel distances varied with time. Floodplain distance was defined as the distance downstream from Lewiston Dam along a centerline digitized within the pre-dam floodplain boundary. The numbering system begins at Lewiston Dam and ends upstream from the North Fork Trinity River confluence.

Channel lengths were estimated by using channel centerlines, digitized within the baseflow channel boundary for each of the six orthophotographs. Reach-averaged estimates of active-channel widths were calculated by dividing the active-channel area by channel length. The active-channel area included the primary wetted channel; secondary water features; in-channel features, such as bedrock outcrops; and active bars.

Two channel attributes that characterize the quality and quantity of available habitat are channel complexity and shoreline length (Trinity River Restoration Program and ESSA Technologies Ltd., 2009). Channel complexity was estimated by summing the areal extents of active bar and secondary water features. The perimeter of the wetted channel edge, including the primary baseflow channel and all connected secondary water features, was used to estimate the shoreline length.

We created five change maps, which preserved individual map attributes and bracketed the period of interest, by intersecting consecutive maps. Change polygons, which represent the nature and extent of bar and bank processes, were created and summarized for each of the 1-km subreaches by using a series of conditional statements. Bar-accretion polygons were identified by the conversion of a water feature to a bar feature, and bar-scour polygons were identified by the conversion of a bar to water feature. Bank-erosion polygons were identified by the conversion of an upland or riparian feature to a channel feature, and bank-accretion polygons were identified by the conversion of a channel feature to a riparian feature. We also investigated bar-vegetation dynamics by using conditional statements to quantify the area converted from a sparsely vegetated to a densely vegetated bar, indicative of stabilization by vegetation encroachment, and the area converted from a densely vegetated to sparsely vegetated bar, indicative of scour and mobilization.

Uncertainty and Error Analysis

Uncertainty and error result when real world data are transferred to digital formats (Mount and Louis, 2005; Hughes and others, 2006). Errors associated with digitized data include operational errors, discharge differences during photo acquisition, and digitizing errors due to features obscured by vegetation or shadows (table 4). Curtis and Guerrero (2015) determined that operational and variable discharge errors were negligible, and digitizing errors based on the accuracy and precision of the digitizing process were conservatively inferred to be about 10 percent.

In this report, we present an additional error analysis associated with interpreting lateral channel changes. Although the root mean square error (RMSE) is generally regarded as a poor indicator of overall horizontal accuracy (Hughes and others, 2006), it is typically the only metric available to define uncertainty associated with lateral channel changes quantified by using repeat rectified photography (O'Connor and others, 2003; Micheli and others, 2004; Draut and others, 2008; Wallick and others, 2010; Wallick and others, 2011).

The greatest RMSE among the orthophotos was used to determine a threshold polygon area to address the horizontal uncertainty due to poor alignment. Change polygons smaller than the threshold area likely represent rectification errors and were removed from the lateral change analyses. The 1980 imagery had the greatest estimated RMSE (9.8 m; table 4).

Table 3A. Geomorphic reach descriptions and restoration history for study segments along the Trinity River, California, downstream from Lewiston Dam: upper river segment.

[Abbreviations: FPKm, floodplain kilometer; km², square kilometer; m, meters; m/m, meter per meter; ROD, Record of Decision; USGS, U.S. Geological Survey; —, no data]

Study reach	Reach name	Pre-dam annual floodplain width (m)	Floodplain distance (FPkm)	Reach length (FPkm)	Local contributing drainage area (km ²)	Reach slope (m/m)	Geomorphic description	Pre-ROD restoration actions	Post-ROD channel-rehabilitation projects and gravel augmentation
1	Lewiston	103	0–1.4	1.4	1.1	0.004	Channel confined by Lewiston fish-hatchery facility. Contains USGS Lewiston streamgaging station.	Side-channel and riffle construction, coarse-sediment placement.	Sven Olbertson 2008. Hatchery gravel-augmentation site.
2	Sawmill	115	1.4–6.5	5.1	44.0	0.002	Relatively small, local sediment sources include Deadwood Creek and Hoadley Gulch.	Side-channel and riffle construction, pool dredging.	Deadwood, Lewiston Cableway, Hoadley Gulch 2008. Sawmill 2009, Sawmill Point and diversion pool gravel-augmentation sites.
3	Rush Creek	175	6.5–12.5	6.0	171.2	0.002	Local sediment sources include Rush Creek, Grass Valley Creek, and erosion of legacy mine tailings. Contains non-USGS Grass Valley Creek gaging station.	Side-channel and riffle construction, pool dredging, feathered-edge project.	Dark Gulch 2008. Lowden and Trinity House Gulch 2010, Lowden gravel-augmentation site.
4	Stott	111	12.5–16.7	4.2	13.6	0.002	No major local sediment sources.	Riffle construction and pool dredging.	—
5	Poker Bar Canyon	83	16.7–23.4	6.7	13.2	0.002	No major local sediment sources. Confined bedrock canyon. Contains USGS Limekiln Gulch (TRLG) streamgaging station.	Side-channel construction, two feathered edge projects.	—

Table 3B. Geomorphic reach descriptions and restoration history for study segments along the Trinity River, California, downstream from Lewiston Dam: central river segment.

[Abbreviations: FPkm, floodplain kilometer; km², square kilometer; m, meters; m/m, meter per meter; ROD, Record of Decision; USGS, U.S. Geological Survey; —, no data]

Study reach	Reach name	Pre-dam annual floodplain width (m)	Floodplain distance (FPkm)	Reach length (FPkm)	Contributing drainage area (km ²)	Reach slope (m/m)	Geomorphic description	Pre-ROD restoration actions	Post-ROD channel-rehabilitation projects and gravel augmentation
6	Vitzhum	105	23.4–29.2	5.8	225.0	0.002	Local sediment sources include Indian Creek, Weaver Creek, and erosion of legacy mine tailings.	Side-channel construction.	Indian Creek 2007.
7	Reading Creek	97	29.2–35.5	6.3	89.8	0.003	Local sediment sources include Reading Creek. Contains USGS Douglas City streamgaging station.	Feathered-edge project.	Reading Creek 2010.
8	Dutton Creek	65	35.5–39.6	4.1	221.6	0.002	Confined bedrock canyon with relatively small local sediment supply from Brown's Creek.	—	—

Table 3C. Geomorphic reach descriptions and restoration history for study segments along the Trinity River, California, downstream from Lewiston Dam: lower river segment.

[Abbreviations: FPkm, floodplain kilometer; km², square kilometer; m, meters; m/m, meter per meter; ROD, Record of Decision; USGS, U.S. Geological Survey; —, no data]

Study reach	Reach name	Pre-dam annual floodplain width (m)	Floodplain distance (FPkm)	Reach length (FPkm)	Contributing drainage area (km ²)	Reach slope (m/m)	Geomorphic description	Pre-ROD restoration actions	Post-ROD channel-rehabilitation projects and gravel augmentation
9	Dutch Creek	137	39.6–47.9	8.3	67.8	0.002	Local sediment sources include erosion of legacy mine tailings. This reach is fault controlled with the channel turning north to follow the trend of the Siskiyou-North Fork fault system.	Three feathered-edge projects.	—
10	Oregon Gulch	131	47.9–50.5	2.6	31.8	0.002	Local sediment sources include Oregon Gulch and erosion of legacy mine tailings. Notable cutbank erosion is occurring. Contains USGS Junction City streamgaging station.	Side-channel construction.	—
11	Canyon Creek	153	50.5–54.8	4.3	186.0	0.003	Local sediment source at Canyon Creek.	Feathered-edge project.	Hocker Flat 2005.
12	Lime Point	141	54.8–58.6	3.8	9.6	0.002	No major local sediment sources. This reach crosses a regional thrust fault that juxtaposes less resistant Devonian age bedrock and more resistant Jurassic age geologic strata.	Side-channel construction, feathered-edge project.	Canyon Creek Suite (Comer Creek and Valdor Gulch) 2006 and Wheel Gulch 2011.
13	Pear Tree	92	58.6–61.3	2.7	9.9	0.002	No major local sediment sources. Bounded by two regional thrust faults and incised into resistant Jurassic age geologic strata. Contains USGS North Fork Trinity streamgaging station.	—	Canyon Creek Suite (Elkhorn and Pear Tree) 2006.

Table 4. Uncertainty analysis for six geomorphic maps of the Trinity River, California, downstream from Lewiston Dam.

[Note see Curtis and Guerrero (2015) for additional details. **Abbreviations:** ft³/s, cubic feet per second; m, meters; mm/dd/yyyy, month/day/year; RMSE, root mean squared error]

Year	Date (mm/dd/yyyy)	Rectified orthophoto resolution (m)	RMSE ¹ (m)	Stream discharge at Lewiston gage (ft ³ /s)	Difference in water depth ² (m)	Inferred digitizing error ³ (percent)
1980	05/16/1980	0.6	9.8	288.0	0.0	10
1997	10/20/1997	0.2	1.5	285.0	0.0	10
2001	11/07/2001	0.2	1.5	298.0	0.0	10
2006	07/25/2006	0.2	1.5	405.0	0.1	10
2009	04/16/2009	0.2	0.4	291.0	0.0	10
2011	08/16/2011	0.2	0.2	446.0	0.1	10

¹Represents horizontal uncertainty for each ortho-rectified image.

²Error associated with variable discharge during photo acquisition estimated from gaging records.

³Digitizing error based on accuracy and precision of digitizing.

This value was inferred from pixel resolution and national accuracy standards (Curtis and Guerrero, 2015). We checked the alignment between the 1980 and 1997 photography and concluded that 9.8 m represented an overly conservative estimate and determined that 5 m was a more representative estimate of RMSE. By using the less conservative RMSE of 5 m, we estimated a threshold size of 25 m² and rounded this up to 30 m², which also represented the minimum polygon size for features included in the geodatabase. All change polygons smaller than 30 m² were eliminated from the lateral-change analysis.

We did not explicitly quantify uncertainty associated with our geomorphic-change analyses because uncertainty is scale- and location dependent, but here we present some calculations that indicate the error associated with large well-exposed features was about 3 percent compared to about 10 percent for small, obscured features. Curtis and Guerrero (2015) determined digitized-line precision ranged from about 0.85 to 2.0 m. This precision equated to a 7 to 13 percent error, or an average error of plus or minus 10 percent, for a representative 30-m channel width. The mean perimeter of active bars in 2011 was 130 m, and active bars were typically well exposed, so application of the lowest linework precision (plus or minus 0.85 m) was appropriate. For an equi-dimensional feature, with a perimeter of 130 m and area of 1,056 m², the estimated uncertainty was within 3 percent.

Assessing Natural and Managed Drivers of Geomorphic Change

In fluvial systems, geomorphic change is driven by a complex set of interrelated causal mechanisms including numerous climatic, lithologic, topologic, biologic, and anthropogenic factors that often exist concurrently and sequentially, making it difficult to disentangle their relative importance. We specifically investigated the cumulative influence of streamflow, sediment supply, sediment management, and mechanical channel rehabilitation during the five study periods.

Streamflow and Sediment Supply

Flow analysis was limited by a lack of gaging records. We analyzed available records from the five mainstem gaging stations (fig. 2) and focused our analysis on the Lewiston gage, which has the longest period of record that spans the study period (table 5). We inferred ungaged tributary-flows by comparing mainstem-flows at stations upstream and downstream of tributary confluences. Our goal was to characterize the relative differences between mainstem flows during the five study periods. With this in mind, we assessed the magnitude, frequency, timing, and duration of flows and investigated the characteristics of geomorphically important flow events that took place in 1997, 1998, 2006, and 2011.

Previous investigations characterized the study reach as sediment-rich with abundant tributary sediment supplies (Pitlick and Wilcock, 2001). The exception to this generalization was in the upper river immediately downstream from Lewiston Dam, where post-dam sediment-deficit conditions existed (Gaeuman and Krause, 2010). The primary post-dam sediment sources, listed in order of importance, included tributary contributions, localized scour of in-channel sources, and gravel augmentation (Ritter, 1968; Knott, 1974; Trinity River Taskforce, 1979; Trinity Restoration Associates, Inc., 1993; Graham Matthews and Associates, 2001; Pitlick and Wilcock, 2001; Gaeuman and Krause, 2010).

Although there has been extensive monitoring of mainstem sediment transport in the upper river since 2005 (Graham Matthews and Associates, 2012), few measured data were available for the pre-2005 periods. Without direct measurements, sediment supply could only be evaluated indirectly. We assumed there was no supply of bed-material-sized sediment (greater than 0.5 mm) from sources upstream of Lewiston Dam. We then assumed a positive correlation between flow and sediment supply and inferred an increase in sediment supply with increasing mainstem flow.

Table 5. Summary of stream discharge data for the Trinity River, California, downstream from Lewiston Dam.

[Abbreviations: ft³/s, cubic feet per second; FPKm, floodplain kilometer; km², square kilometers; m, meters; NGVD, National Geodetic Vertical Datum; ROD, Record of Decision; USGS, U.S. Geological Survey; WY, water year; —, no data; °, degree; ', minute; ", second]

USGS station identifier	Gage name	Gage name abbreviation	Name used in this report	Location (latitude/longitude)	Drainage area (km ²)	Datum elevation above NGVD 1929 (m)	Available data (WY)	Distance downstream from Lewiston Dam (FPkm)	Mean daily discharge ⁴ (ft ³ /s)	Pre-ROD mean annual peak (ft ³ /s)	Post-ROD mean annual peak (ft ³ /s)
11525500	Trinity River at Lewiston	TRAL	Lewiston	40°43'10" 122°48'09"	1,862	554	1911–2011	1.5	770	3,980	6,550
11525655	Trinity River at Limekiln Gulch	TRLG	Limekiln Gulch	40°40'22" 122°55'10"	2,098	503	1982–1991 2002–2011 ¹	20.4	830	—	7,120
11525854	Trinity River at Douglas City	TRDC	Douglas City	40°38'43" 122°57'24"	2,411	487	1996–2011 ²	29.9	1,230	—	7,570
11526250	Trinity River at Junction City	TRJC	Junction City	40°43'43" 123°03'39"	2,738	440	1996–2011 ³	50.3	1,430	—	9,790
11526400	Trinity River upstream from North Fork near Helena	TRNF	Upstream from North Fork	40°46'00" 123°06'48"	2,945	421	2006–2011	60.1	1,550	—	11,640

¹11525655 missing records WY 1992 to WY2002.

²11525854 operated as non-USGS station WY1997 to WY2002.

³11526250 operated as non-USGS station WY1997 to WY2002, peak data unavailable for WY1997 to 2002.

⁴Mean daily discharge calculated by using the period of record.

Sediment Management and Mechanical Channel Rehabilitation

We compiled, analyzed, and summarized information related to sediment management and mechanical rehabilitation from available reports (Kondolf and Minear, 2004; Gaeuman, 2008; Gaeuman and Krause, 2011; Hoopa Valley Tribe and others, 2011b; Graham Matthews and Associates, 2012; Krause, 2012b) and from communication with TRRP staff. A lack of “as built” surveys, which reflect any changes made during construction, required that we use the original design specifications to identify the location and extent of constructed features. The digitized extent of constructed features do not always represent the actual “as built” extents because geomorphic changes could have occurred between construction and photo acquisition. Although these data required little analysis, they were critical for interpreting management actions that altered river morphology.

Results

Our results focus on spatial and temporal trends in the areal distribution of geomorphic features. The mapping data represent channel conditions at discrete points in time, whereas estimates of geomorphic change represent the cumulative response to numerous controlling factors during each study period. We present estimates of cumulative geomorphic change, describe controlling factors, and assess the primary causal mechanisms that created geomorphic change during each of the five study periods. The areal extent of individual geomorphic features, summarized for each of the thirteen geomorphic reaches, is presented in [appendix A](#).

Spatial and Temporal Analysis of Geomorphic Change

When the areal extent of the riparian and channel environments were compared at the system-scale geomorphic change was not apparent because large riparian features dominated the landscape ([fig. 6A](#)). In particular, the riparian environment was dominated by the pre-dam floodplain. The active-channel margin represents the boundary between riparian and channel features. In [figures 6B to 6F](#), the change in active-channel area is shown for the five periods of interest. An increase in the active-channel area equated to an equal loss of riparian area, and likewise a decrease in the active-channel area equated to an equal increase in riparian area.

Excluding the pre-dam floodplain and focusing on smaller-scale lower-elevation features highlighted spatial and temporal changes in riparian diversity ([fig. 7](#)). In

1980, post-dam benches composed 94 percent of the lower elevation riparian environment ([fig. 7A](#)). By 2001, floodplain construction and bar stabilization increased riparian diversity, and the proportion of post-dam benches decreased to 86 percent ([fig. 7C](#)). By the end of the study period in 2011, the relative proportions of post-dam benches, constructed floodplains, stable bars, and riparian wetlands were 60, 27, 10 and 3 percent, respectively ([fig. 7F](#)).

The diversity of channel features was more variable than riparian features in space and time ([fig. 8](#)). In 1980, channel diversity was greatest in the upper and central river reaches and channel-complexity features, such as active bars and secondary water features (split-flow channels, side channels, alcoves, and aquatic wetlands), composed approximately 12 percent of the active-channel area ([fig. 8A](#)). From 1980 to 2001, the active-channel area increased by 20 percent ([fig. 6](#)). By 2001, there were relatively more channel complexity features in the upper and central river reaches ([fig. 8B](#)) and these features composed 17 percent of the active-channel area. From 2001 to 2011, the increase in active-channel area was about 5 percent. By 2011, channel complexity had increased in the upper river, but decreased in the lower river. By 2011, the channel-complexity features occupied 14 percent of the active-channel area ([fig. 8F](#)). During the longer (21 years) and relatively wetter pre-ROD period, increases in active-channel area and channel complexity were 20 and 70 percent, respectively. The post-ROD period was shorter (10 years) and relatively drier, with intensified management. During this later period, there were smaller, but measurable, increases in active-channel area of about 5 percent, and channel complexity decreased by 3 percent.

Spatial and temporal changes in geomorphic features are illustrated in greater detail in this section and are used to interpret trajectories and rates of geomorphic change during the five study periods. We present summary data for individual upland, riparian, or channel features in the context of the 13 geomorphic reaches and the upper, central, and lower river segments, as defined in [table 3](#). In each figure, panel A shows the cumulative area of each geomorphic feature summed in the downstream direction from Lewiston Dam to the confluence with the North Fork Trinity River; panel B shows cumulative change in feature area per year, where the slope of the line represents and annual rate of change; and panel C shows a time series of feature area scaled by reach length and illustrates trajectories of change. Note the differences in the scale of the y-axis in these figures.

Uplands showed little cumulative change during the study period ([fig. 9](#)), particularly when compared to changes in total riparian area ([fig. 10](#)) and individual riparian features ([figs. 11–14](#)). The exception to this generality was Reach 3 ([fig. 9B](#)), where uplands were converted to constructed floodplains by mechanical surface lowering from 2009 to 2011.

18 Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

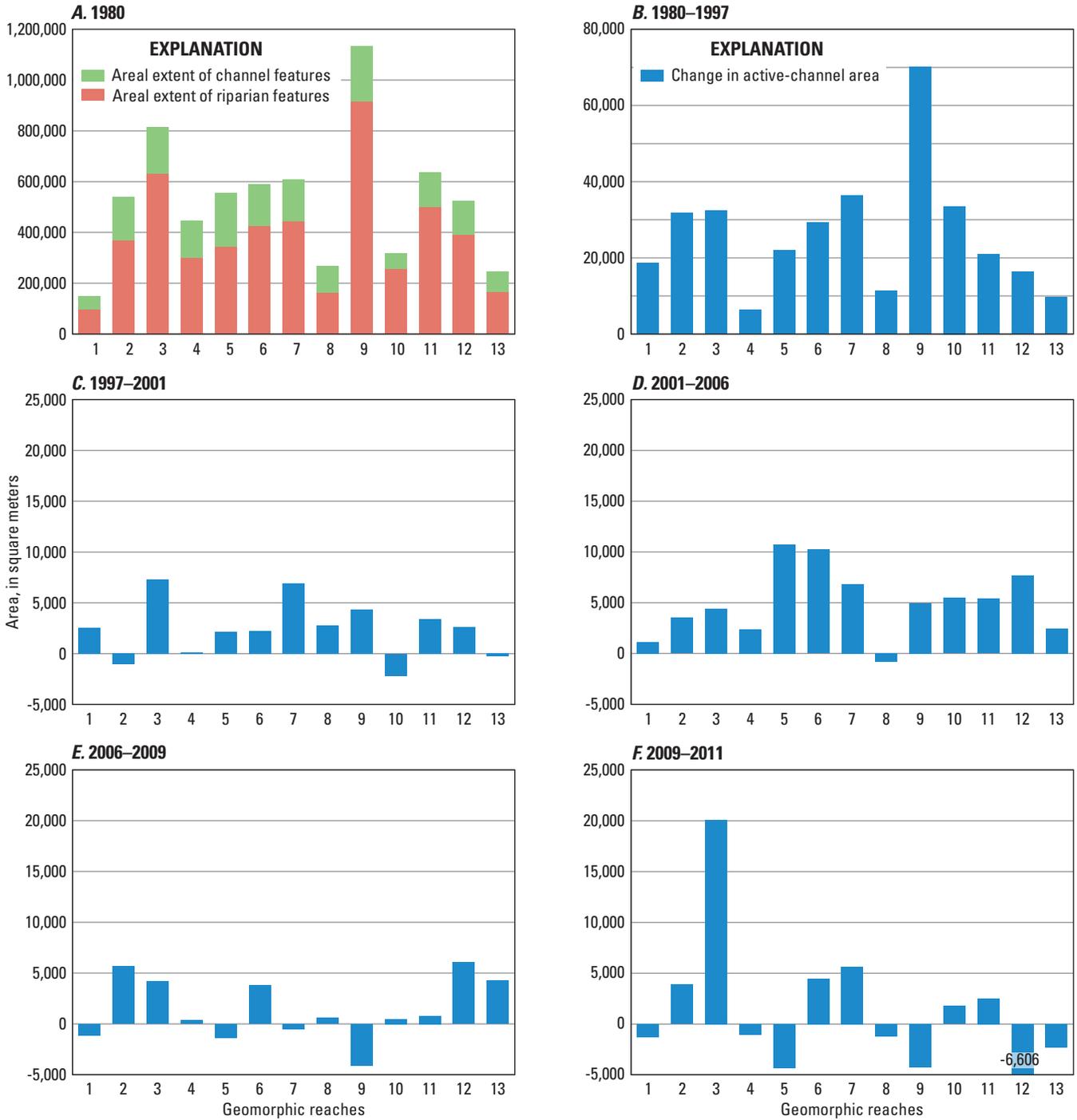


Figure 6. Areal extent of riparian and channel features along the Trinity River downstream from Lewiston Dam, California, A, in 1980, and change in active-channel area for five periods from 1980 to 2011: B, 1980 to 1997; C, 1997 to 2001; D, 2001 to 2006; E, 2006 to 2009; and F, 2009 to 2011. Note differences in y-axis scale among periods.

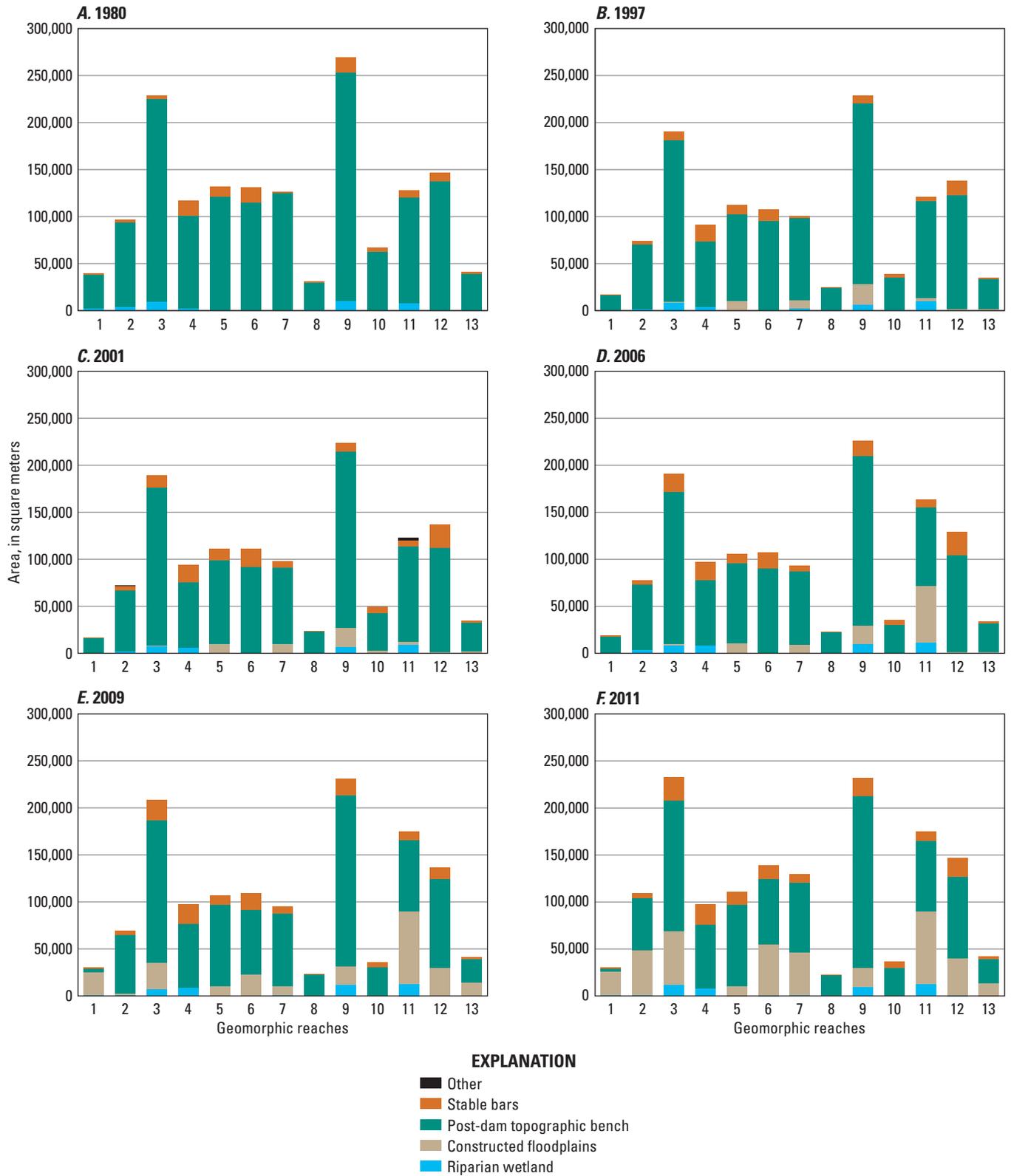


Figure 7. Areal extent of lower elevation riparian features along the Trinity River downstream from Lewiston Dam, California, in A, 1980; B, 1997; C, 2001; D, 2006; E, 2009; and F, 2011.

20 Assessing Geomorphic Change along the Trinity River Downstream from Lewiston Dam, California, 1980 to 2011

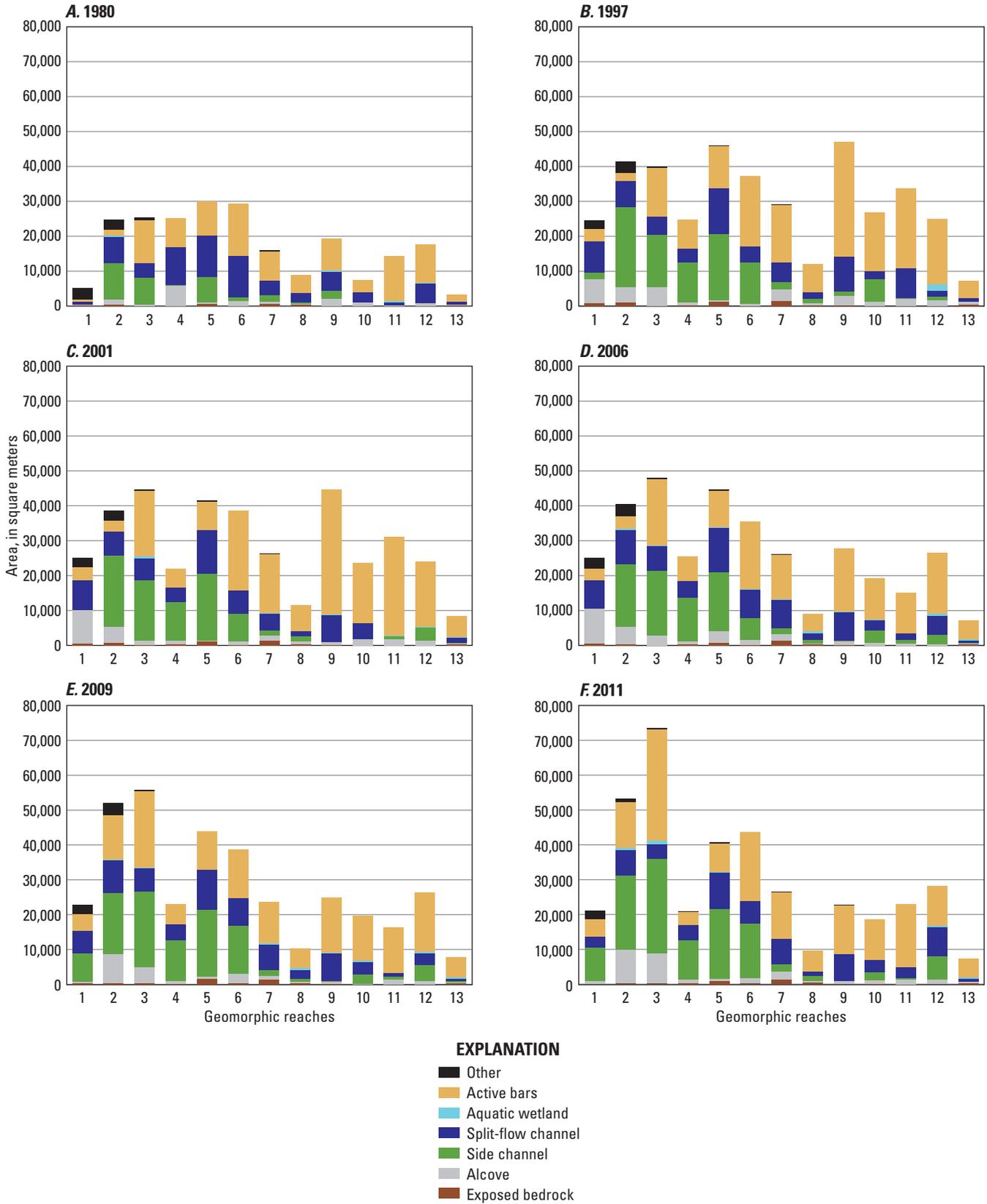


Figure 8. Areal extent of channel-complexity features within the active channel along the Trinity River downstream from Lewiston Dam, California, in A, 1980; B, 1997; C, 2001; D, 2006; E, 2009; and F, 2011.

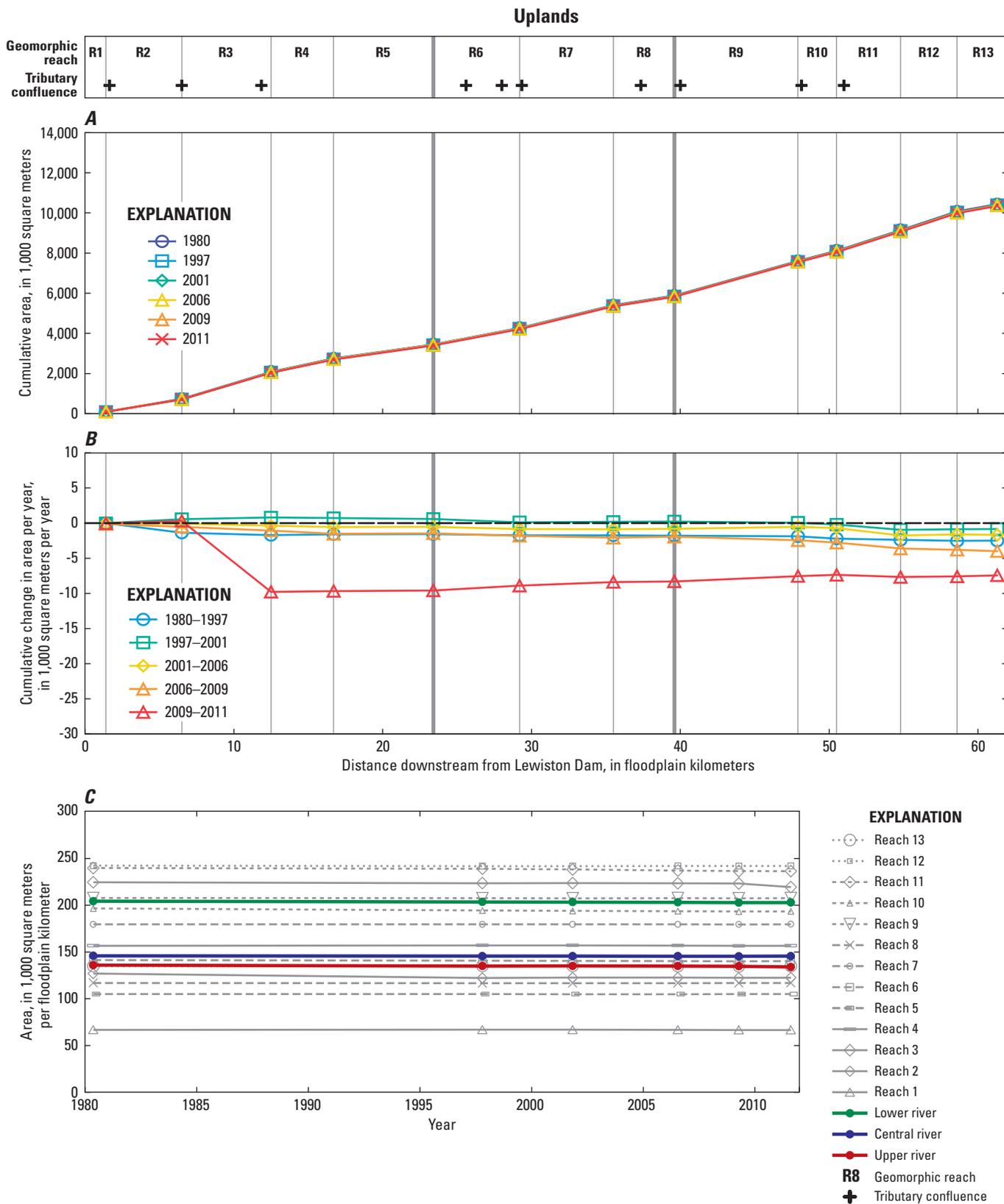


Figure 9. Area of uplands along the Trinity River downstream from Lewiston Dam, California, and change in upland area from 1980 to 2011: *A*, cumulative area by reach; *B*, cumulative change in area per year by reach; *C*, area by study reach and segments over time.

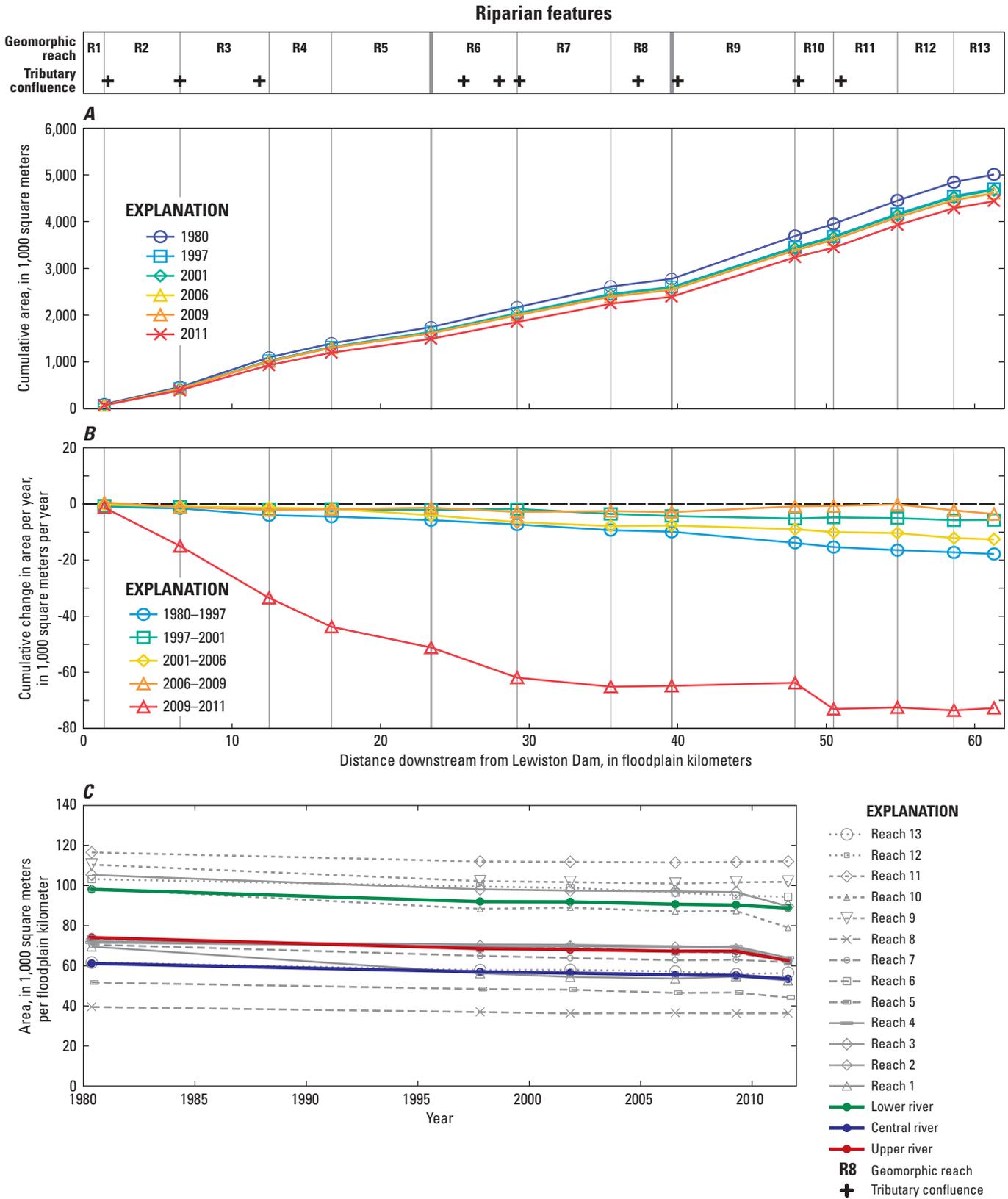


Figure 10. Area of riparian features along the Trinity River downstream from Lewiston Dam, California, and change in riparian area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and segments over time.

Riparian area generally decreased during the study period, but the decrease accelerated after 2009 (fig. 10B). The post-2009 decrease in riparian area was primarily caused by conversion of a large portion of pre-dam floodplain (fig. 11B) into a series of constructed floodplains by mechanical surface lowering. The area of post-dam benches also decreased during the study period, with the largest cumulative decreases from 1980 to 1997 (fig. 12A) caused by bank erosion and bar scour. Post-dam benches were also converted into constructed floodplains by vegetated berm removal and mechanical surface lowering. Floodplain construction accelerated during the post-ROD period, especially after 2006 (fig. 13).

Stable bars are transitional units, originally deposited in the active channel, but are part of the riparian environment when stabilized by vegetation and revert back to the active channel when scoured and remobilized. Bar stabilization accelerated from 1997 to 2001 (fig. 14A), and the area of stable bars continued to increase until the end of the study period in 2011 (fig. 14C). The exception to this generalization was a decrease in stable bar area from 2006 to 2009 in the lower river caused by the 2006 tributary-flow event.

The active-channel area generally increased during the study period as upland and riparian features were eroded or mechanically altered. The largest cumulative increase in active-channel area occurred from 1980 to 1997 (fig. 15A). When cumulative change is scaled by time (fig. 15B), the highest rate of change in the upper river was in Reach 3 during the relatively short period from 2009 to 2011. This period included the 2011 flow release, the largest since 1974 (Krause, 2012a), and several large scale TRRP bank rehabilitation projects. The cumulative change in active-channel area across the study area from 2009 to 2011 was slightly less than the rate estimated for the much longer and relatively wetter period from 1980 to 1997.

The largest cumulative increase in active-bar area occurred between 1997 and 2001, primarily downstream from Indian Creek (25.6 percent; fig. 16A). Post-2001 changes in active-bar area were variable across the study area. From 2001 to 2006, there was a slight increase in active-bar area in the upper river (fig. 16B). With the start of gravel augmentation by direct injection in 2008, active-bar area increased notably in the upper river between 2006 and 2011 (fig. 16C). From 2001 to 2009, active-bar area decreased in the central river, which was followed by an increase from 2009 to 2011. From 2001 to 2006, active bar area decreased notably in the lower river, then remained relatively stable from 2006 to 2009, and decreased slightly from 2009 to 2011 (fig. 16C).

We combined the area of secondary water features (split-flow channels, side channels, alcoves, and aquatic wetlands) into a single category for analysis because the

trajectories of change for these small features were highly variable. There were large increases in the area of secondary water features from 1980 to 1997 (fig. 17A), primarily in the upper river. The area of secondary water features remained fairly static after 1997 (fig. 17A), and there were minor decreases from 1997 to 2001, primarily in the central and lower river (fig. 17B). From 2001 to 2006 and 2006 to 2009, there were small increases in the area of secondary water features primarily in the central river, and from 2009 to 2011, there were larger increases in the area of secondary water features primarily in the lower river (fig. 17C). Trends in shoreline length were similar to those for secondary water features (fig. 18A).

From 1980 to 2006, average active-channel widths increased in all the study reaches (fig. 18B). In 1980, the active channel width was much greater in the upper river, but by 1997, active-channel widths in the upper and lower river were about equal and remained similar for the remainder of the study period. Channel widths continued to increase from 1997 to 2006, but remained stable from 2006 to 2009. From 2009 to 2011, channel widths decreased slightly in the upper and lower river and increased slightly in the central river.

Natural and Managed Drivers of Geomorphic Change

Sediment retention by upstream dams, flow diversion, and flow regulation led to diminished sediment supply and transport capacity, particularly in the reach that extends from Lewiston Dam downstream to Rush Creek (0–6.5 FPkm). Further downstream, sediment supply from Grass Valley Creek (11.85 FPkm) was effectively eliminated by sediment retention dams constructed in 1986 (Trinity River Taskforce, 1970). These retention ponds are actively maintained by dredging, under the present sediment-management program (Krause, 2012b). Although Deadwood Creek (1.65 FPkm) and Rush Creek (6.5 FPkm) contribute flow and sediment, transport capacity remains low downstream to Poker Bar Canyon, where channel confinement and transport capacity increase as the river flows through a confined bedrock canyon (16.7–23.4 FPkm).

Contributing drainage area, sediment supply, and flow increase in the central river as a result of tributary contributions from Indian Creek (25.6 FPkm), Weaver Creek (28.0 FPkm), and Reading Creek (29.4 FPkm) and localized bank erosion of legacy mine tailings. Further downstream, the central river flows through a second confined bedrock reach (35.5–39.6 FPkm), where transport capacity increases, but sediment supply diminishes.

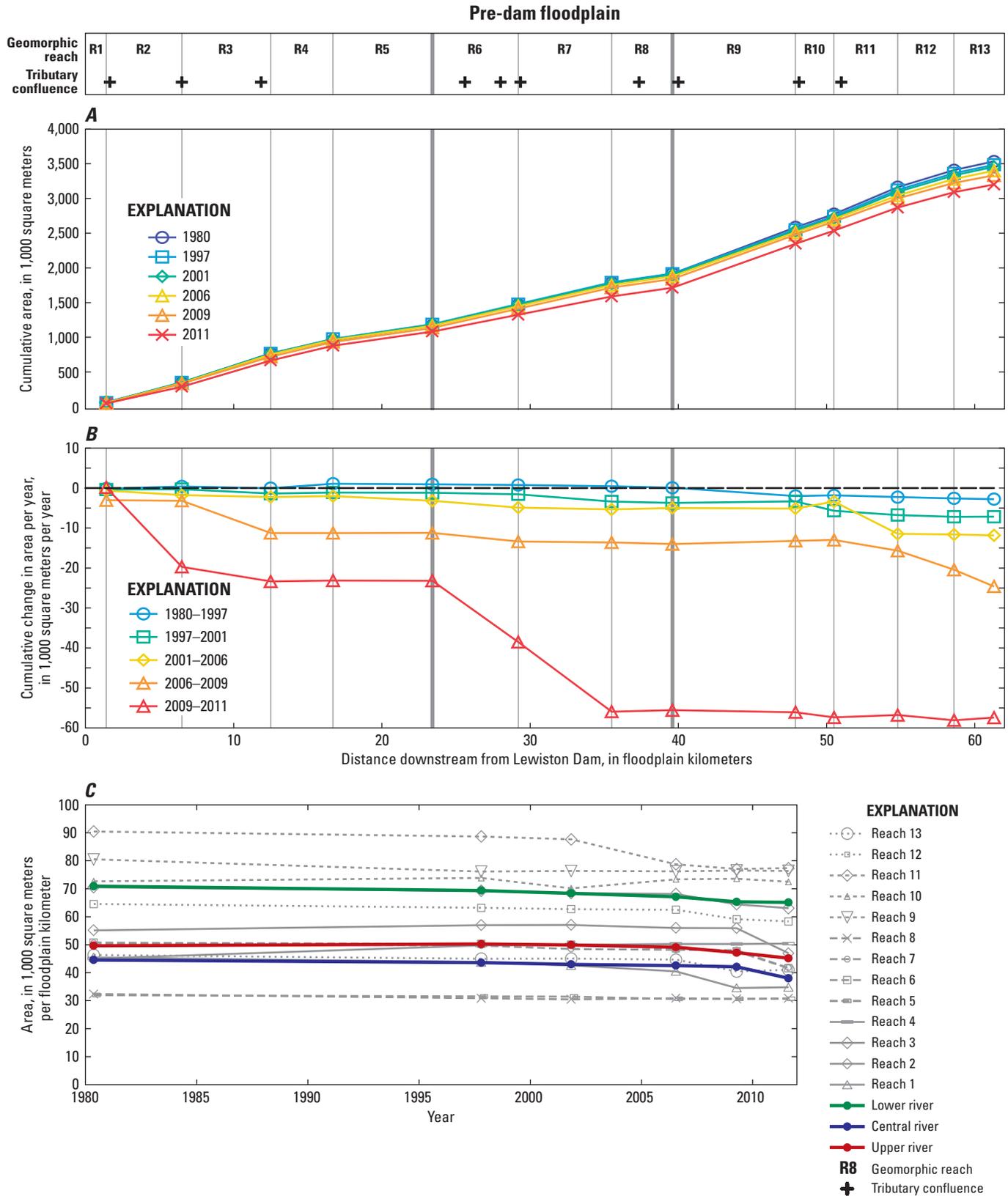


Figure 11. Area of the pre-dam floodplain along the Trinity River downstream from Lewiston Dam, California, and change in pre-dam floodplain area from 1980 to 2011: A, cumulative area by study reach; B, cumulative change in area per year by study reach; C, area by study reach and river segments over time.

Post-dam topographic benches

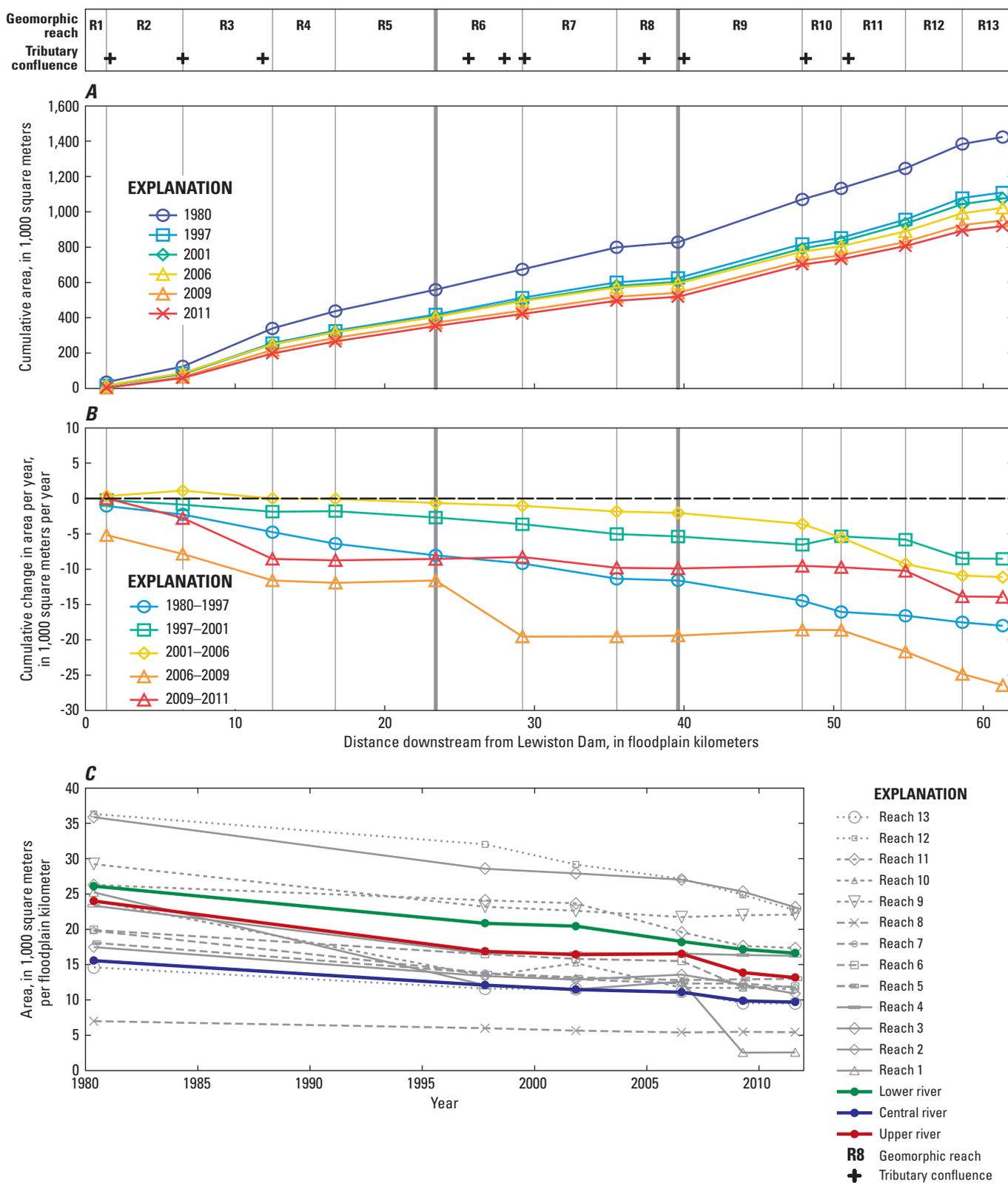


Figure 12. Area of post-dam benches along the Trinity River downstream from Lewiston Dam, California, and change in post-dam bench area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.

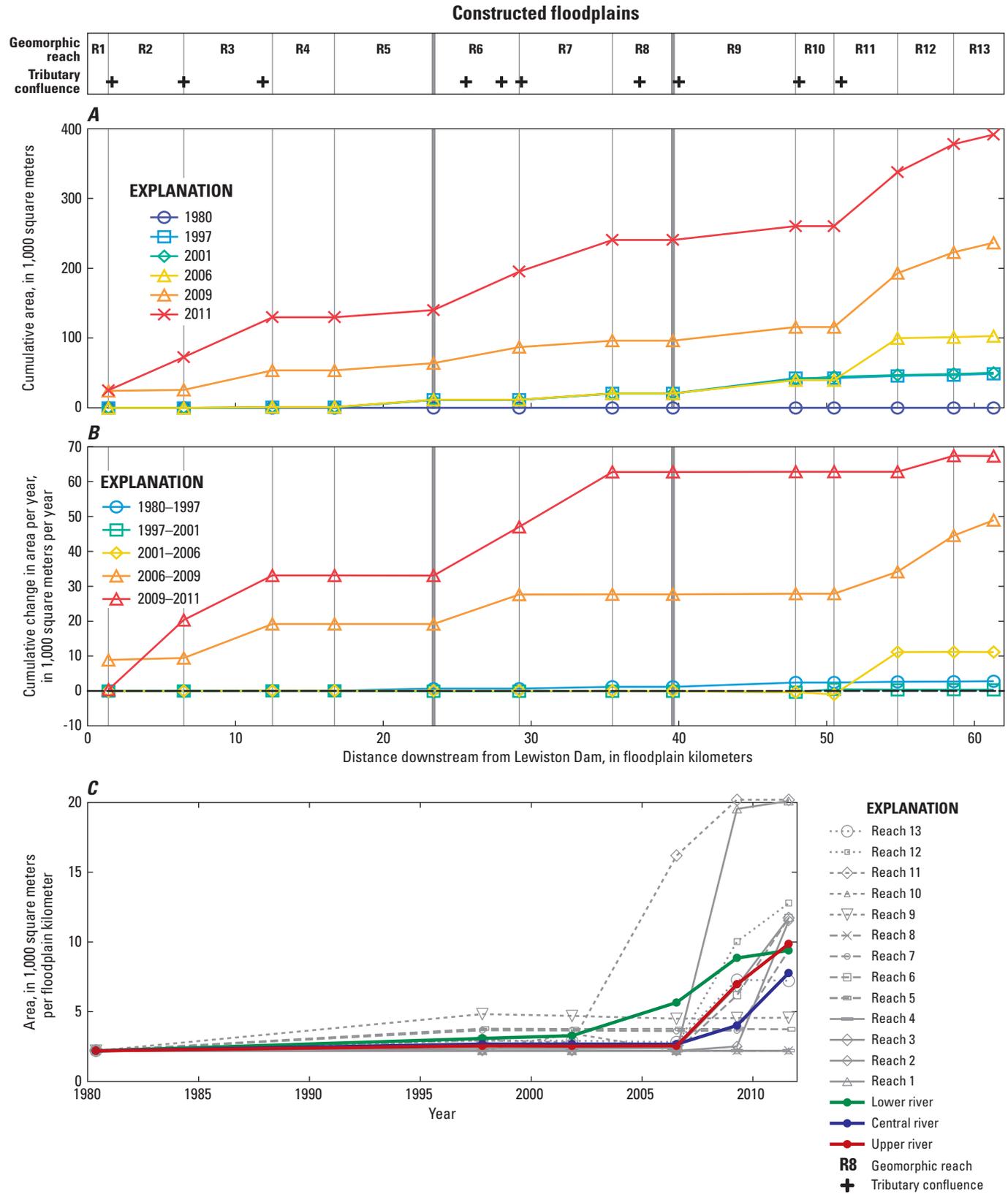


Figure 13. Area of constructed floodplains along the Trinity River downstream from Lewiston Dam, California, and change in constructed floodplain area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.

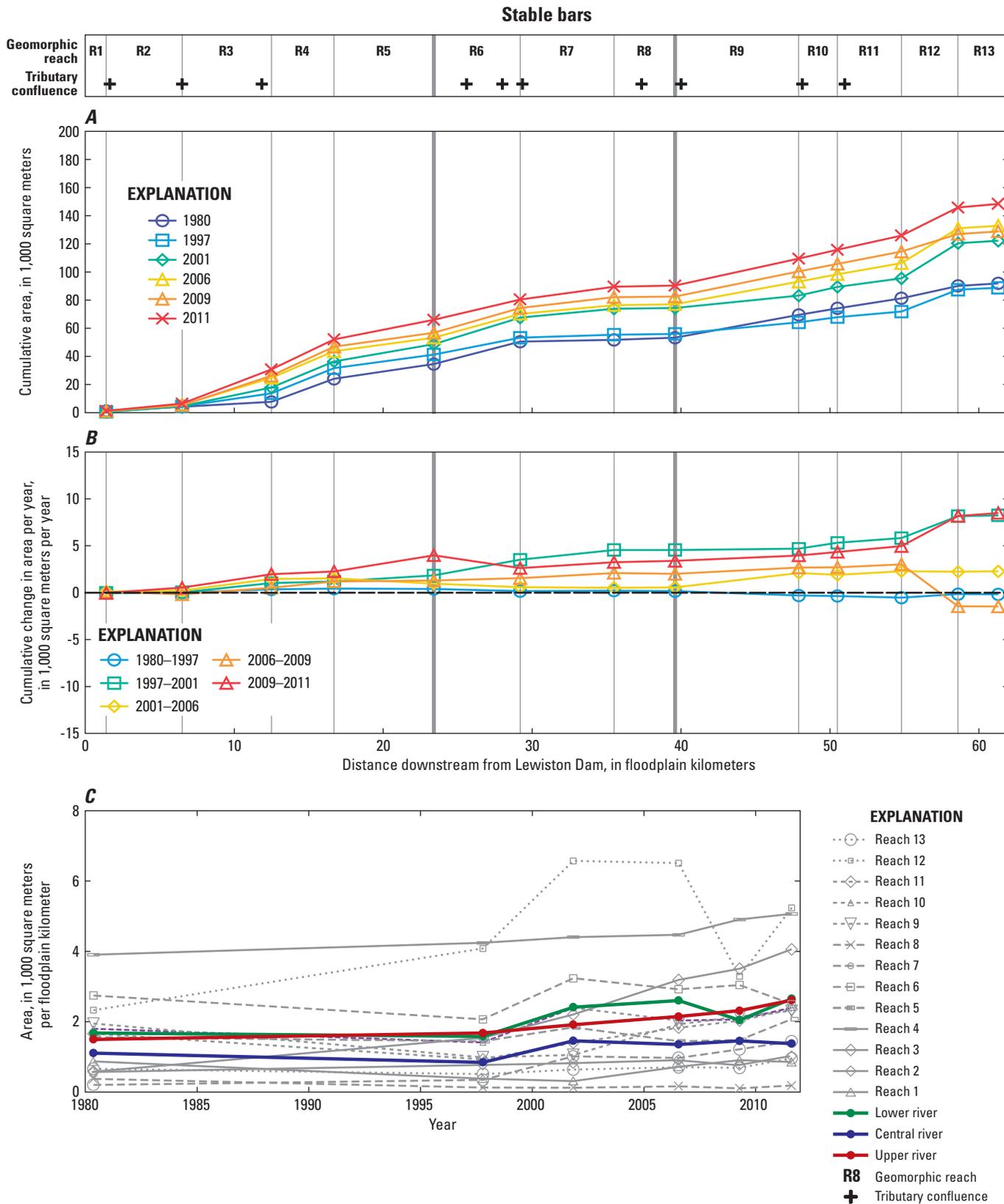


Figure 14. Area of stable bars along the Trinity River downstream from Lewiston Dam, California, and change in stable bar area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.

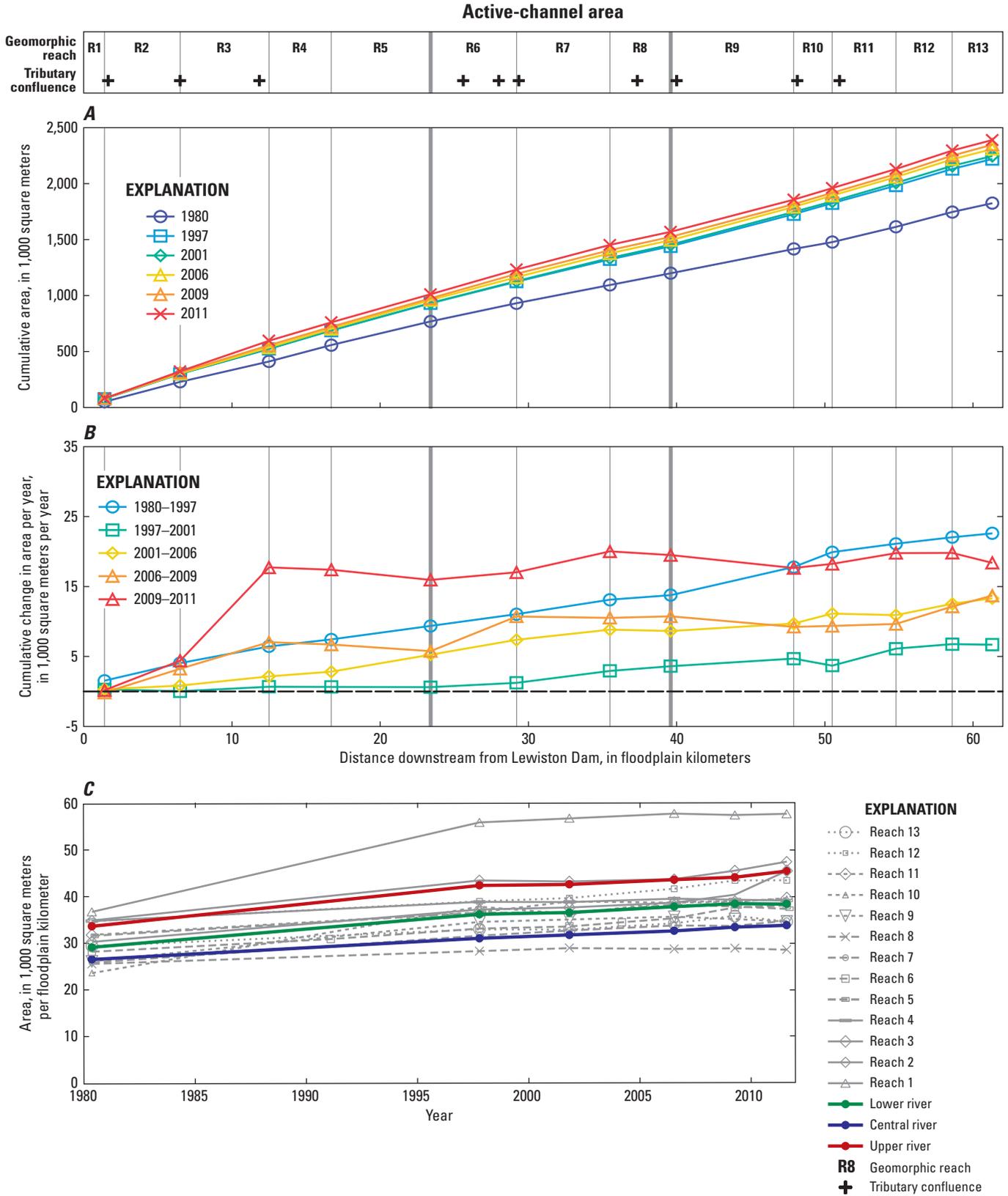


Figure 15. Area of the active channel along the Trinity River downstream from Lewiston Dam, California, and change in active channel area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.

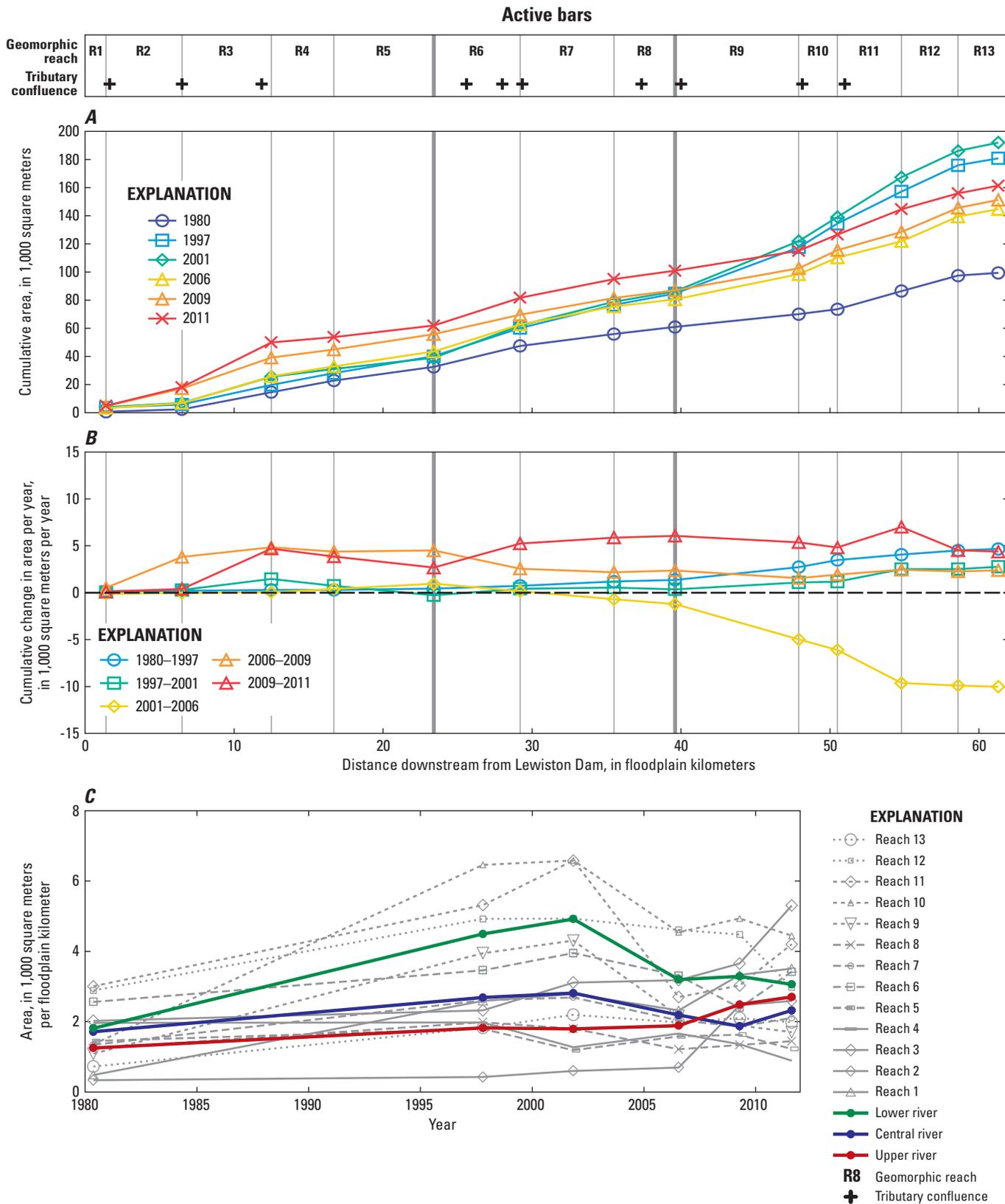


Figure 16. Area of active bars along the Trinity River downstream from Lewiston Dam, California, and change in active bar area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.

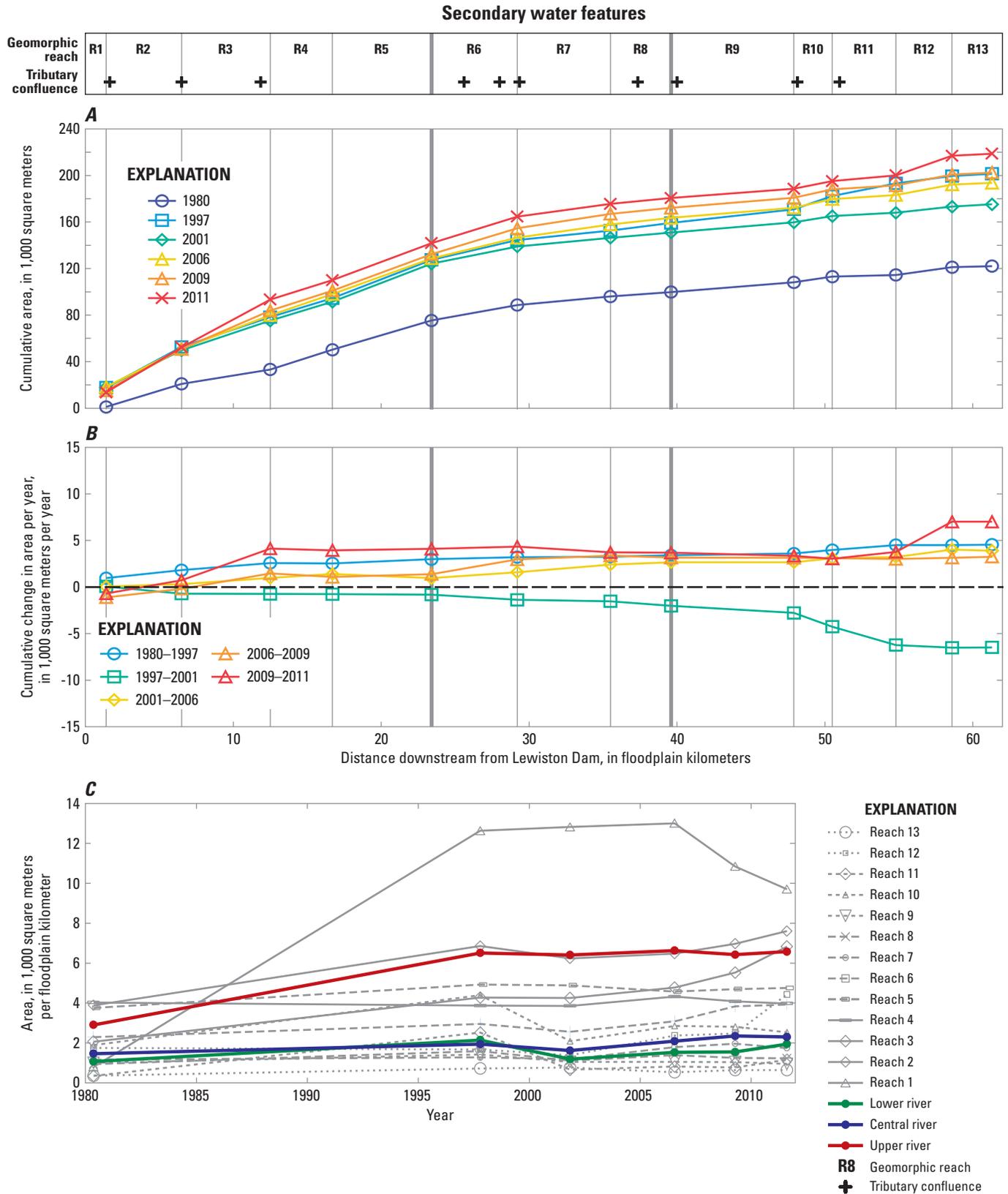


Figure 17. Area of secondary water features (split-flow channels, side channels, alcoves, and aquatic wetlands) along the Trinity River downstream from Lewiston Dam, California, and change in secondary water feature area from 1980 to 2011: *A*, cumulative area by study reach; *B*, cumulative change in area per year by study reach; *C*, area by study reach and river segments over time.

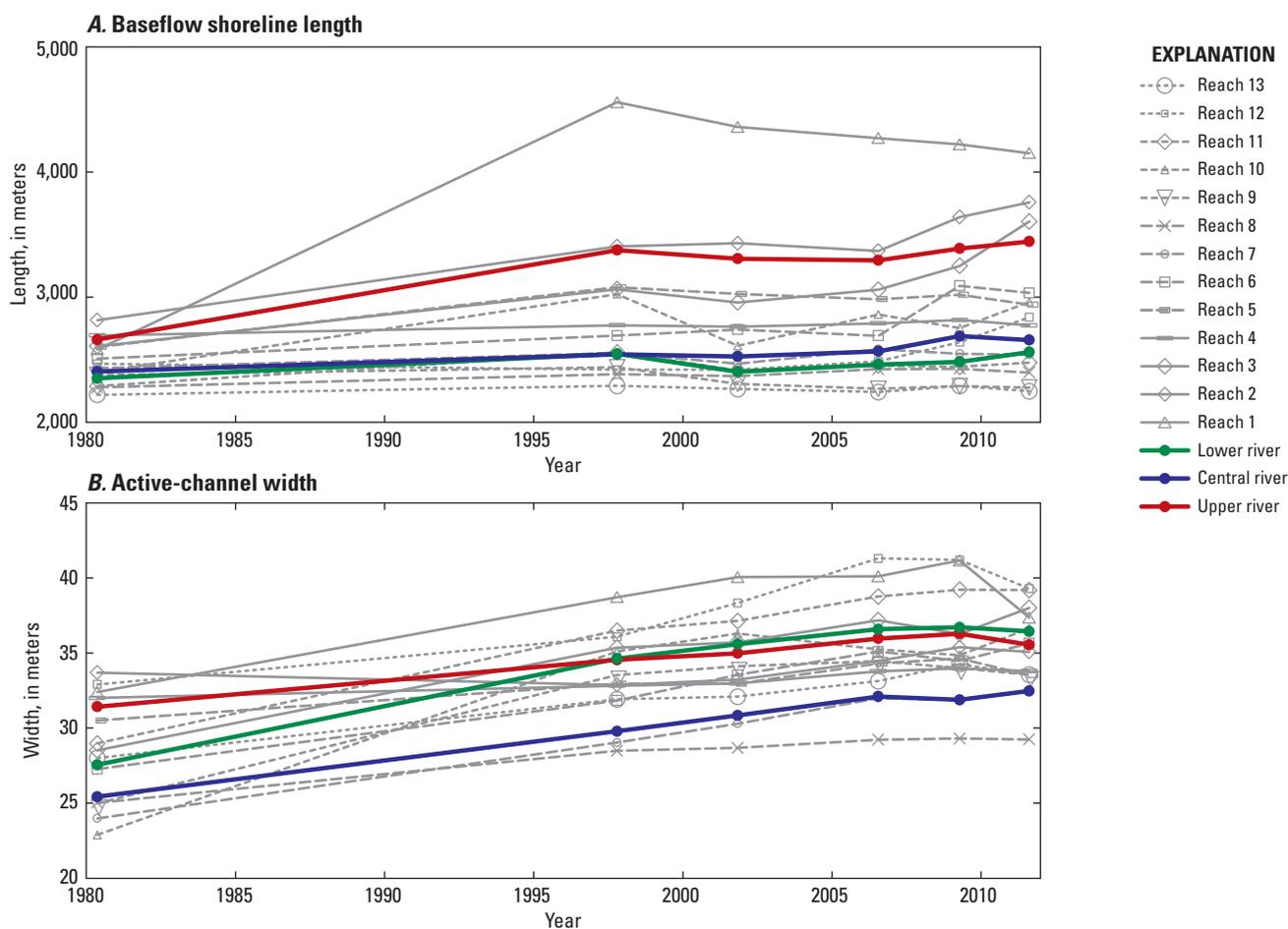


Figure 18. Temporal changes in the active-channel from 1980 to 2011 for the Trinity River downstream from Lewiston Dam, California: *A*, baseflow shoreline length; *B*, active-channel width.

At the upstream end of the lower river segment, the river flows through a wider reach (39.6–47.9 FPkm), where the local sediment supply increases as a result of bank erosion. Continuing downstream (47.9–54.8 FPkm), transport capacity and sediment supply increase again as a result of contributions from bank erosion, Canyon Creek (51.0 FPkm), and, to a lesser extent, Oregon Gulch (48.2 FPkm). Although there are no large local sediment sources at the bottom of the study reach (54.8–61.3 FPkm), upstream sources of flow and sediment maintain dynamic river processes.

Streamflow and Sediment Supply

To assess transport capacity in greater detail, we analyzed the size, frequency, and duration of flows at five USGS gaging stations along the mainstem Trinity River (fig. 2; table 5). Our analyses necessarily focused on the Lewiston gage, which is approximately 1.5 km downstream from Lewiston Dam. Flows at the Lewiston gage represented regulated conditions, but this was the only site with continuous daily flow data spanning the study period. The four downstream gages had partial records.

Mean daily flows at the Lewiston gage for the pre- and post-ROD periods were 700 ft³/s and 890 ft³/s, respectively. Analysis of local precipitation records indicated the increase in mean daily flows was caused by increases in post-ROD annual flow releases rather than increased precipitation. Monthly precipitation records from the National Weather Service station near Weaverville, California, indicated the long-term mean annual precipitation from 1911 to 2011 was 935 mm. Mean annual precipitation during the pre-ROD period (979 mm) was slightly greater than the long-term average, but the post-ROD mean annual precipitation (465 mm) was about 50 percent of the long-term average.

Figure 19 presents mean daily flows, annual peaks, and annual average flows for the Lewiston gage. During the relatively wetter pre-ROD period, there were three water years (1983, 1997, and 1998) classified as “extremely wet,” and one year (1995) classified as “wet” (table 1). The years 1983 and 1995 bracketed a decade of lower flows from 1985 to 1994. During the relatively drier post-ROD period, one year (2006) was classified as “extremely wet,” and two years (2004 and 2011) were classified as “wet.”

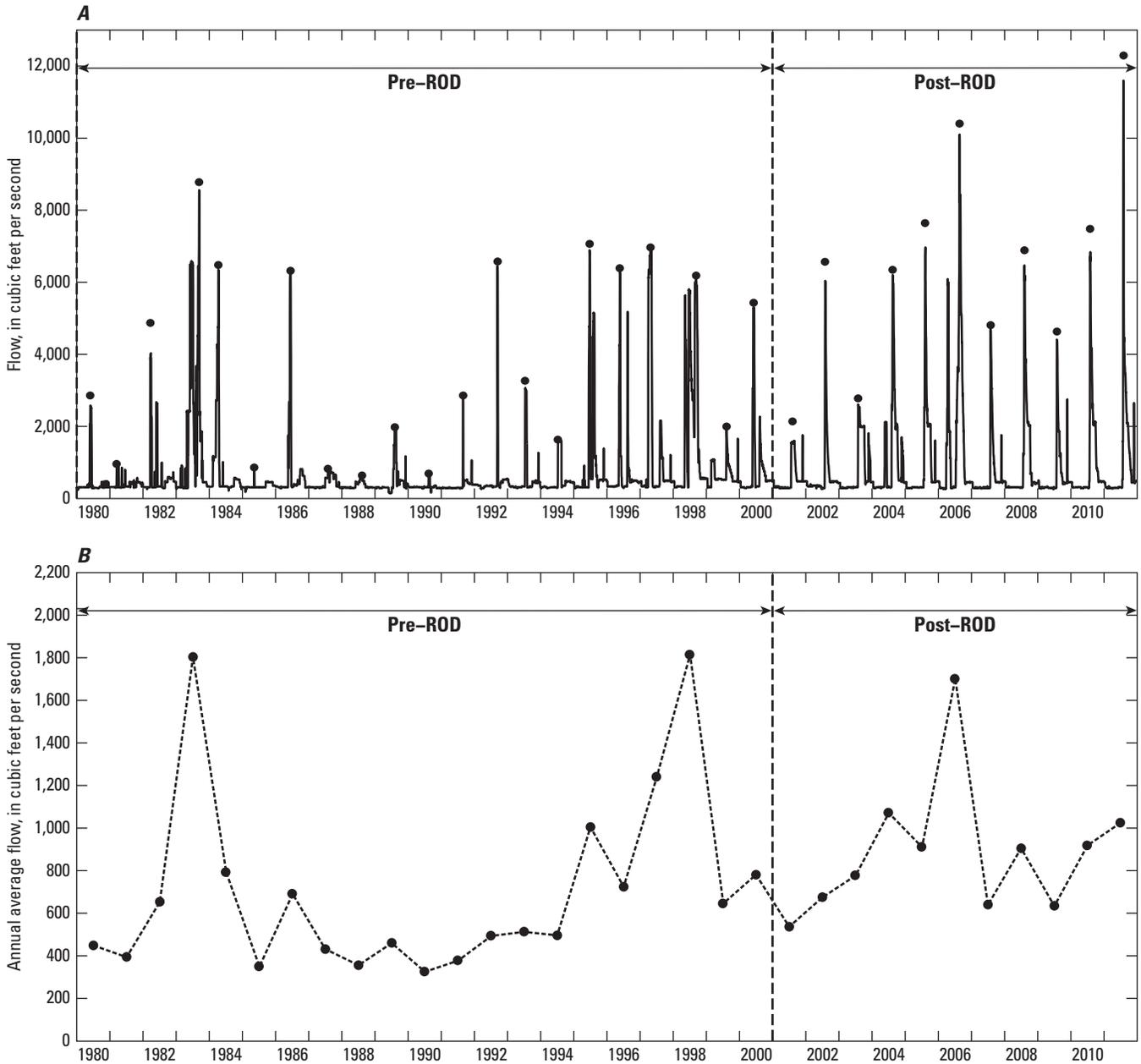


Figure 19. Streamflow measured at the Lewiston gage on the Trinity River, California, 1.5 km downstream from Lewiston Dam, from 1980 to 2011: *A*, mean daily and annual peak flows; *B*, annual average flows. ROD, Record of Decision.

The post-ROD flow regime altered the timing and variability of annual peak flows released from Lewiston Dam. Winter peak-flow releases were eliminated, and the peak release was shifted to the spring to mimic snowmelt conditions. Analysis of the monthly distribution of mean daily flows at the Lewiston gage indicated that annual peak-flow releases during the pre-ROD period were distributed from December to June, whereas the post-ROD peak-flow releases were larger in May and June (fig. 20). Notably, post-ROD flows from February to April were lower compared to pre-ROD flows.

Post-ROD flows were also evaluated by computing the number of exceedance days at the Lewiston gage for the prescriptive ROD-flow thresholds (table 1). Mean daily flows greater than 1,500 ft³/s occurred about three times more frequently during the post-ROD period compared to the pre-ROD-period, whereas the medium-range flow thresholds of 4,500 and 6,000 ft³/s were exceeded 90 and 60 percent more frequently, respectively, during the post-ROD period. Flows greater than 8,500 ft³/s were exceeded an average of about 1.7 days per year during the post-ROD period compared to 0.1 days per year during the pre-ROD period.

Tributary flows were important drivers of geomorphic change, particularly during wet periods. Unlike clear-water releases from Lewiston Dam, the amount of sediment delivered to the mainstem study reach from ungaged tributaries is unknown, but likely substantial (Ritter, 1968; Knox, 1974; Trinity River Taskforce, 1979; U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999; Graham Matthews and Associates, 2001). The contributing area upstream from Lewiston Dam (1,850 km²) represents 63 percent of the total contributing area upstream from the North Fork Trinity River (2,930 km²). Sediment supply from Grass Valley Creek (11.85 FPKm; fig. 2), which represents 3 percent (94 km²) of the contributing area, is detained by a series of retention ponds so that only 34 percent (986 km²) of the Trinity River watershed contributes bedload to the study reach (fig. 21). The contributing areas for the upper, central, and lower river reaches were 131, 550, and 305 km², representing 13, 56, and 31 percent, respectively. Indian, Weaver, and Redding Creek all flow into the central river upstream from the Douglas City gage (29.9 FPKm). A recent sediment-budget estimate of the study reach upstream from the Douglas City streamgage determined that the transition between sediment deficit and surplus conditions under present conditions is between the Douglas City and Limekiln Gulch gage (20.4 FPKm; Gaeuman and Krause, 2011), which is upstream from the central river reach's boundary (23.4 FPKm). Based on contributing area, sediment budget estimates, and active bar area, the transition from a sediment deficit to a sediment surplus condition is downstream from Indian Creek (25.6 FPKm).

Inconsistencies in the timing of tributary-flow events and mainstem flushing-flow releases influenced sediment dynamics in the study reach. Precipitation-driven tributary flows and the associated sediment delivery peaked during the winter and spring and did not coincide with the peak-flow releases. Peak-flow releases occurred from May to June, and from 2008 to 2011, these were accompanied by the direct injection of gravel. The delay of peak-flow releases results in interim channel aggradation.

Aggradation of tributary confluences has been a recurring problem (Ritter, 1968; Trinity River Taskforce, 1979; U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999) because it produces upstream slackwater conditions on the mainstem, where undesirable fine bed material (less than 8mm) accumulates. Wilcock and others (1995) recommended moderate peak-flow releases (4,500 to 6,000 ft³/s) to mobilize bed material and remove undesirable fine-grained bed material and higher peak flows (8,500 to 11,000 ft³/s) to produce deeper scour and greater transport.

The effects of tributary-flow contributions on mainstem transport capacity are illustrated in figure 22, which shows mean annual flows for the five mainstem gages from 1996 to 2011, the period in which multiple mainstem gages were in operation (table 5). During the relatively wetter 2006 and 2011 water years, mean annual flow at the North Fork gage was 70 to 80 percent greater than at the Lewiston gage. Again, we inferred, on the basis of previous investigations, that these tributary-flow events contributed large, but unknown, amounts of sediment.

Figure 23 illustrates mean daily flows for mainstem gages and highlights two pre-ROD water years (1997, 1998) and two post-ROD years (2006, 2011), which represent the four largest tributary-flow events during the study period. The influence of tributaries on mainstem flows was clear in December 1997, when mean daily flows increased from about 6,900 ft³/s at Lewiston to 10,200 ft³/s at Douglas City and to 27,000 ft³/s at Junction City. In February 1998, mean daily flows increased from about 5,600 ft³/s at Lewiston to 9,900 ft³/s at Douglas City and to 25,000 ft³/s at Junction City. Mean daily flows released in December of 2006 were about 1,500 ft³/s at Lewiston, but increased to 7,500 ft³/s at Douglas City, to 12,000 ft³/s at Junction City, and to nearly 20,000 ft³/s at the North Fork gage (fig. 23D). In comparison, mean daily flows in May 2011, during the largest flow release since 1974 (Krause, 2012a), lacked tributary contributions because the flow release did not coincide with tributary runoff. In May 2011, flow releases at Lewiston peaked at 12,000 ft³/s, compared to 12,500 ft³/s at Limekiln Gulch, 12,900 ft³/s at Douglas City, 13,700 ft³/s at Junction City, and 12,900 ft³/s at the North Fork gage (fig. 23E).

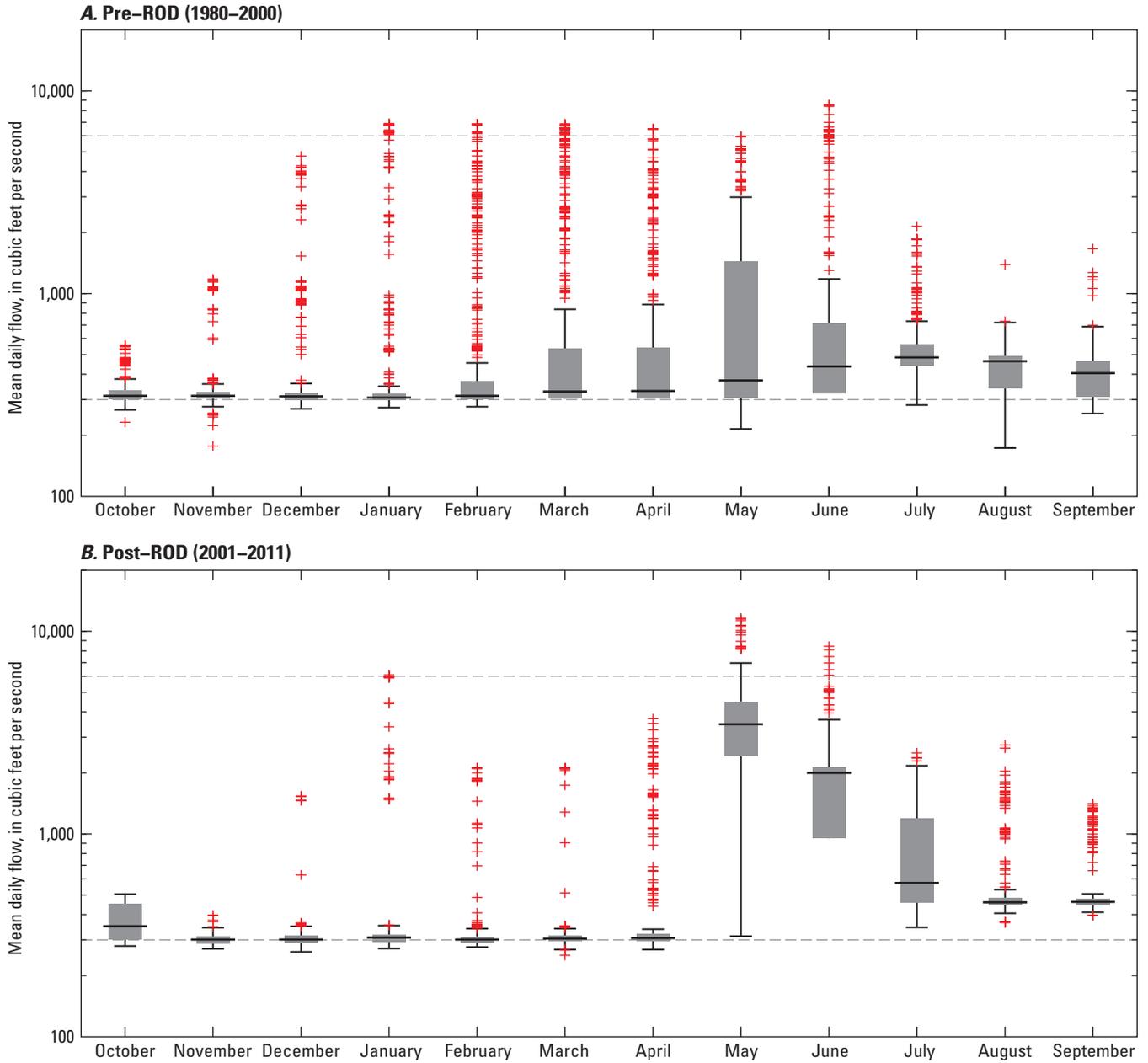


Figure 20. Mean daily flows from 1980 to 2011, grouped by month with minimum in-stream flow, for the Lewiston gage on the Trinity River, California: *A*, pre-ROD (Record of Decision) period; *B*, post-ROD period. The horizontal dashed lines indicate 300 cubic feet per second, which represents summer-baseflow conditions, and 6,000 cubic feet per second, which represents the post-ROD mean annual peak flow.

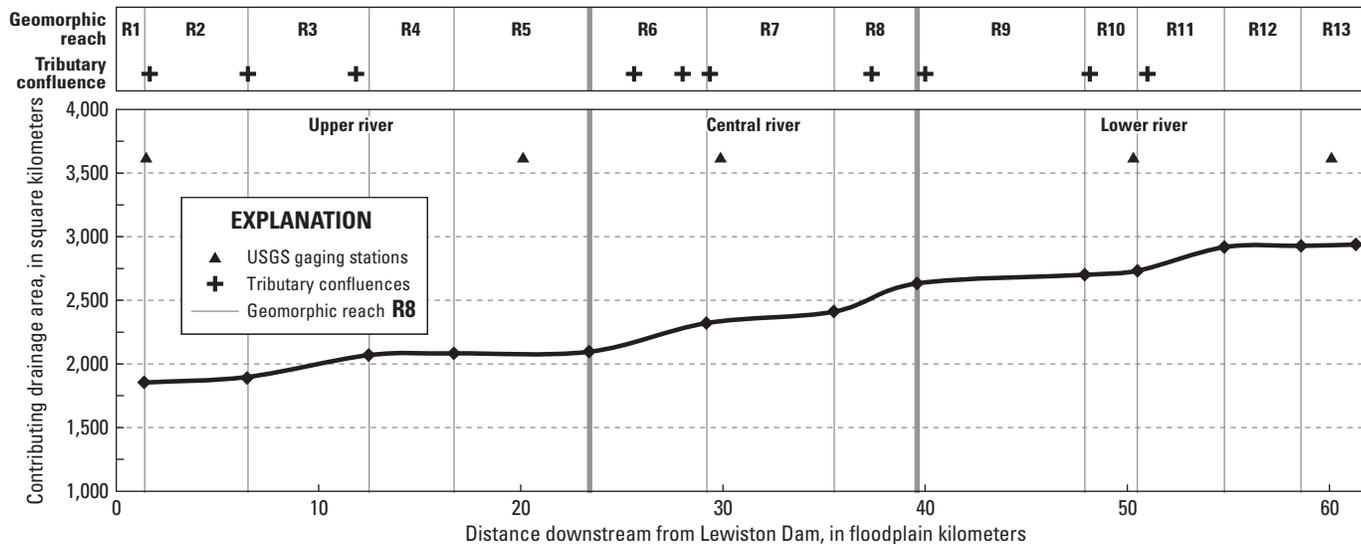


Figure 21. Contributing drainage area for 13 geomorphic reaches, delineated by vertical lines and described in table 2, along the Trinity River downstream from Lewiston Dam, California. USGS, U.S. Geological Survey.

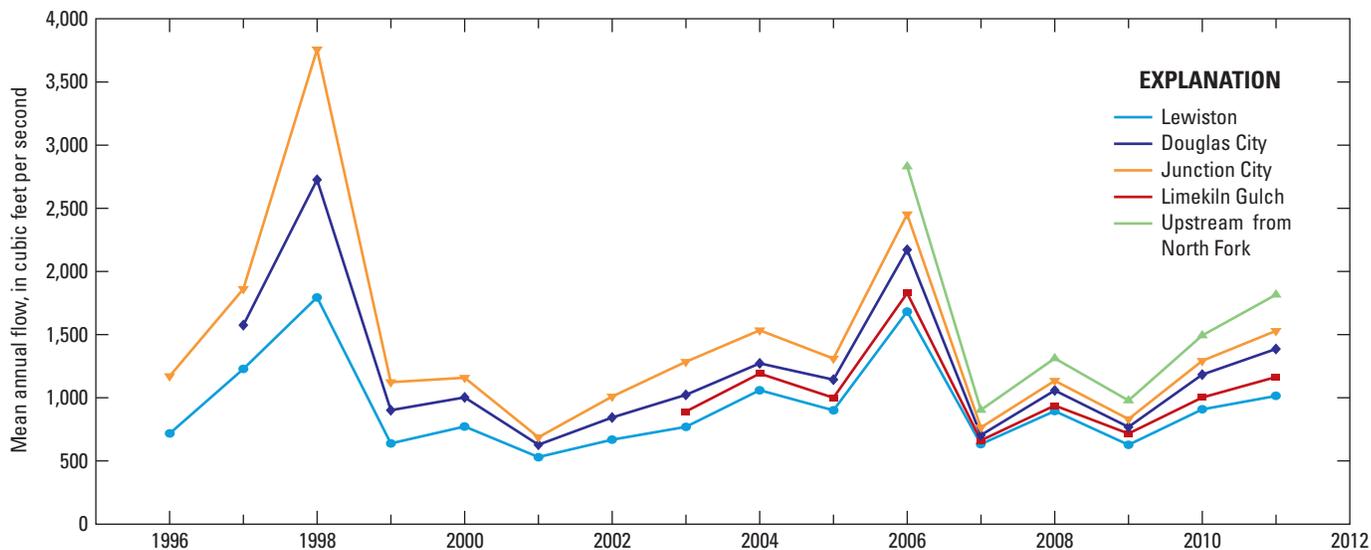


Figure 22. Mean annual flow measured at five mainstem gages on the Trinity River, California, downstream of Lewiston Dam, California, from 1996 to 2011.

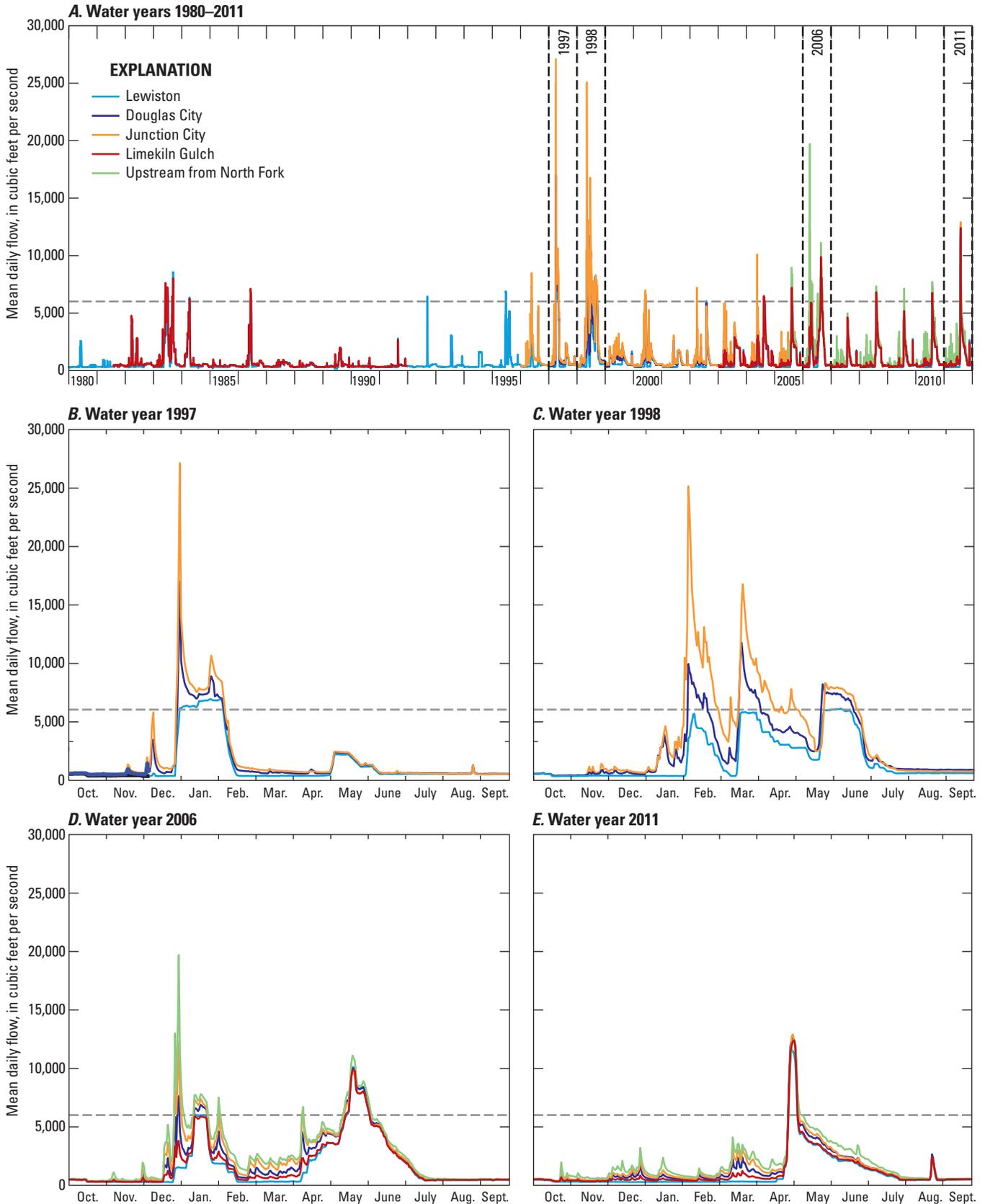


Figure 23. Mean daily flows measured at five mainstem gaging stations on the Trinity River, California, downstream from Lewiston Dam, from 1980 to 2011, and annual time series for four wettest years during the study period: *A*, 1997; *B*, 1998; *C*, 2006; *D*, 2011. Dashed horizontal line denotes 6,000 cubic feet per second, which represents the post-Record of Decision mean annual peak flow.

Sediment Management and Mechanical Channel Rehabilitation

The history of sediment management and mechanical channel rehabilitation were reviewed earlier in this report, and in this section we present pertinent details. Figure 24 provides a spatial and temporal summary of management actions in the project reach. Pre-ROD management was focused on restoring adult-holding and spawning habitat (Trinity River Taskforce, 1970). Adult salmonids require deep-water holding pools and spawning riffles free of fine bed material (less than 8 mm). Pre-ROD dredging of mainstem pools increased and maintained deep-water adult-holding habitat. Riffle and grade-control construction created spawning habitat, whereas upland watershed restoration and sediment-retention basins at the Grass Valley Creek confluence reduced the delivery of

undesirable fine-sediment (U.S. Bureau of Land Management, 1995; Graham Matthews and Associates, 2001).

Krause (2012a) provided a detailed history of sediment extraction and augmentation for the study reach, which is summarized in figure 25. Following dam closure, flow diversions, combined with elevated tributary sediment supply related to land use, caused significant aggradation of the channel bed with sand-sized bed material that filled pools and inundated spawning areas (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999). Sediment extraction, primarily by pool dredging, and to a lesser degree bar scalping, began in 1976 and continued until 1990. Extracted volumes of sediment were composed of approximately 15–25 percent coarse-grained sediment (greater than 16-mm in diameter) and about 75–85 percent finer grained material (less than 16 mm).

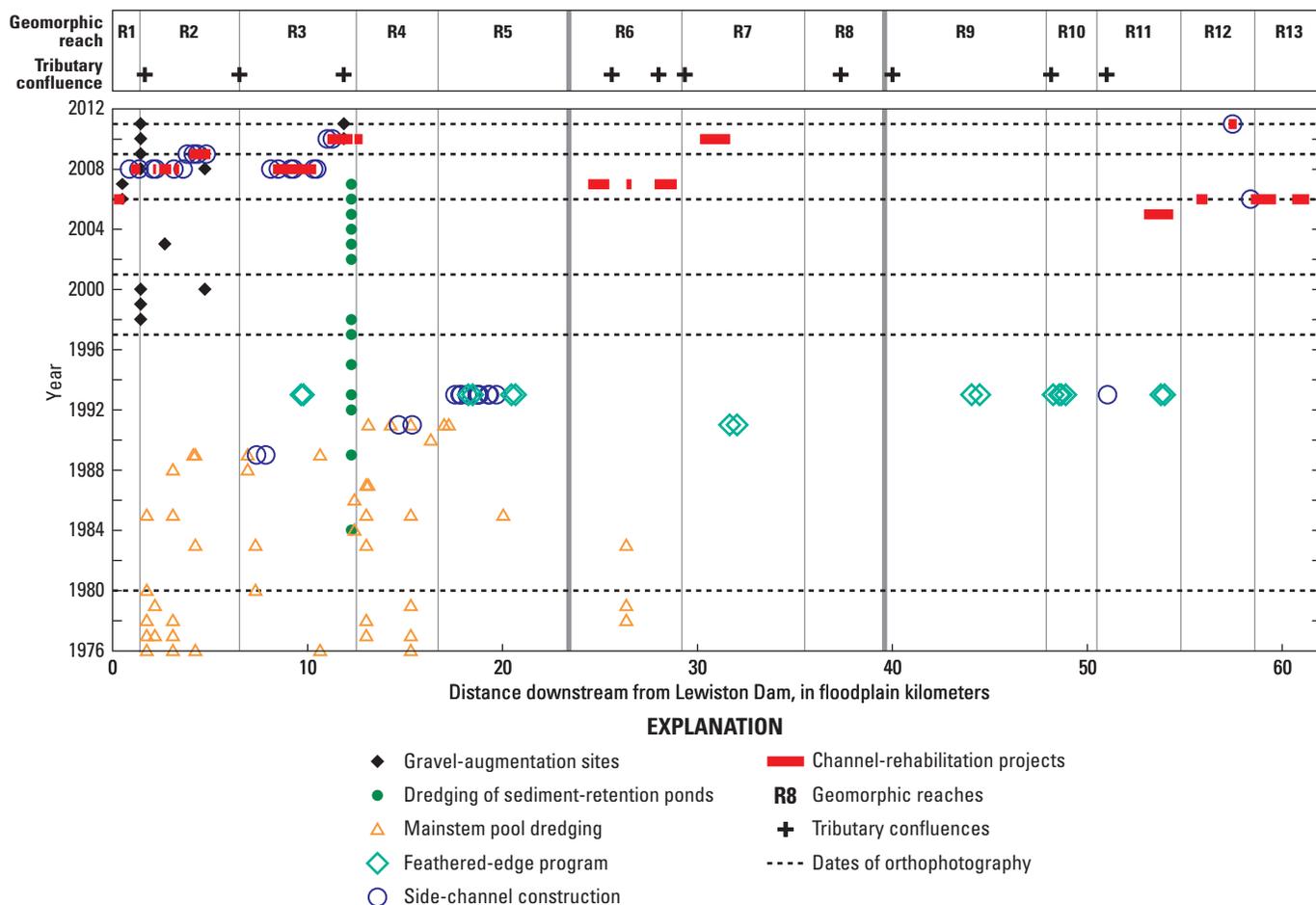


Figure 24. Summary of relevant management actions from 1976 to 2011 along the Trinity River downstream from Lewiston Dam, California.

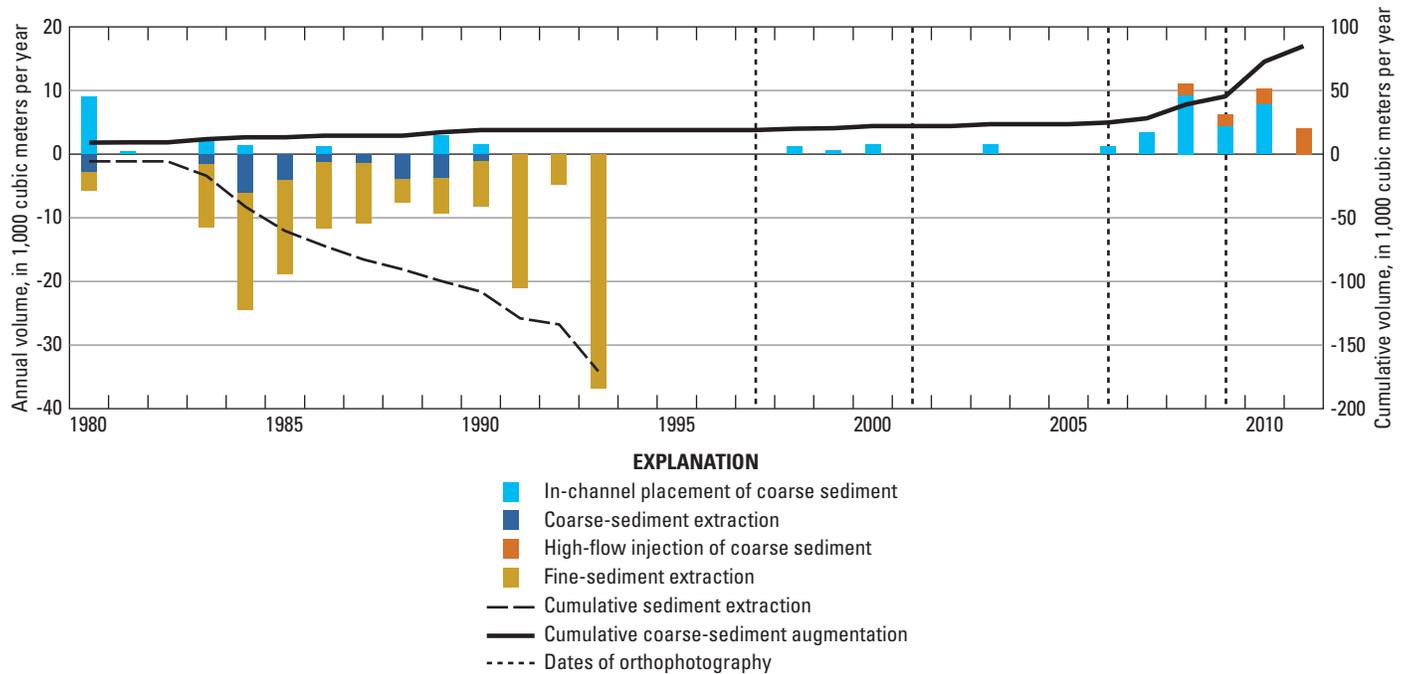


Figure 25. Annual and cumulative volumes of sediment extraction and augmentation for Trinity River downstream from Lewiston Dam, California, from 1980 to 2011 (Krause, 2012b).

A summary of constructed features is presented in figure 26. An emphasis on salmonid rearing habitat began in the 1990s (U.S. Fish and Wildlife Service, 1989), and a series of 18 side channels and 9 bank-rehabilitation projects, referred to as “feathered edges,” were constructed to create shallow-water rearing habitat (fig. 24; U.S. Fish and Wildlife Service, 1994). Side-channel construction increased shoreline length and low-velocity off-channel rearing habitat and also created large island features. The “feathered edge” program targeted overly steep channel margins where vegetation had encroached. Riparian vegetation and sediment berms were mechanically removed to create gently sloping, gravelly channel margins intended to function as mainstem rearing habitat.

In 1999, the TRFE determined the lack of rearing habitat continued to be a primary limiting factor for sustainable salmonid populations and made recommendations for prescriptive-flow management, channel rehabilitation, and augmentation of coarse bed-material-sized sediment adopted by the ROD in 2001. The TRFE identified 44 potential channel-rehabilitation sites and 3 potential side-channel sites. Construction of these projects began in 2005 under a phased approach to allow for monitoring and performance assessment (Trinity River Restoration Program and ESSA Technologies Ltd., 2009). From 2005 to 2011, 19 of the proposed rehabilitation projects were constructed (fig. 24).

The design of post-ROD channel-rehabilitation projects evolved over time. Early designs, constructed in 2005 and 2006, were relatively simple channel–floodplain connectivity projects designed to facilitate inundation of channel margins by vegetation removal, riparian berm recontouring,

and surface lowering of riparian features. These early projects were in the lower river, where ample in-channel and tributary sediment sources existed and where TRRP partners hypothesized the river would “rehabilitate itself.” A lack of geomorphic response at these early restoration sites (Hoopa Valley Tribe and others, 2011b) led to broader hypotheses and the evolution of project designs. More recent projects, constructed from 2006 to 2011, focused on enhancing channel–floodplain connectivity and utilized new design criteria (Hoopa Valley Tribe and others, 2011a) to mechanically increase the diversity and extent of salmonid habitat by incorporating channel complexity features into project designs.

Gravel augmentation to create and maintain spawning habitat in the upper river began in 1972 and continued into the post-ROD period. Gravel augmentation approaches evolved from the pre-ROD strategy of in-channel placement of static gravel features to provide spawning or rearing habitat to the post-ROD strategy of direct injection during the spring peak-flow release (Kondolf and Minear, 2004). In-channel placement of gravel to increase sediment supply and restore dynamic fluvial processes began in 1998. Direct injection during managed high-flow releases, by using front-end loaders or conveyor belts, began in 2008. Although the TRFE recommended gravel augmentation up to 51,000 cubic meters per year (m³/yr), the actual volumes placed each water year varied (fig. 25). At time of writing, recommendations for average annual-injection volumes, based on gravel transport rates and desired bed-surface textures, were about 5,400 m³/yr (Gaeuman, 2008).

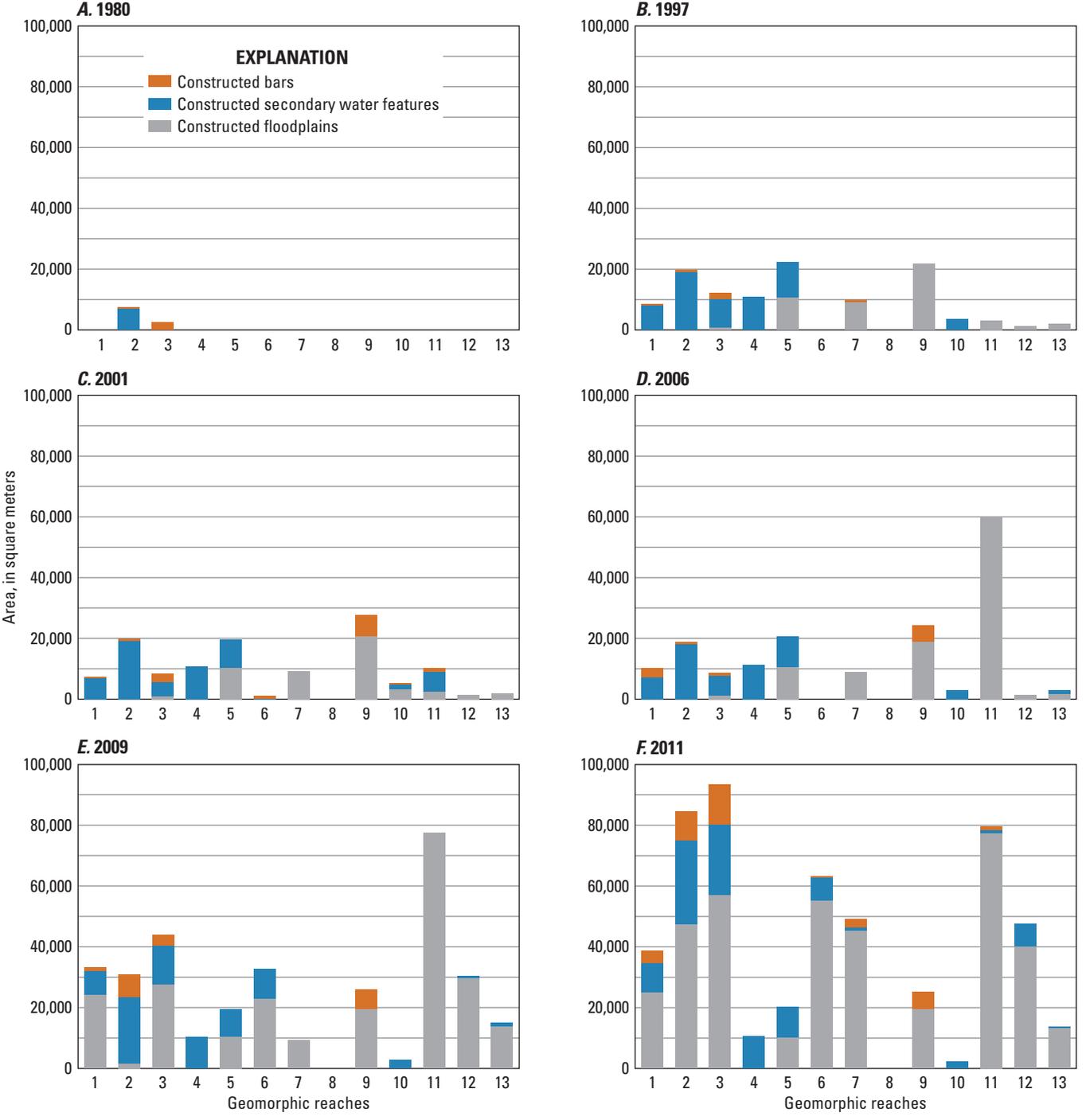


Figure 26. Bar graphs showing a summary of constructed riparian and channel features along the Trinity River downstream from Lewiston Dam, California, in 1980, 1997, 2001, 2006, 2009, and 2011.

Summary of Bar and Bank Processes

Lateral changes induced by bar and bank processes were characterized by summarizing change polygons in 1-km sub-reaches during the five periods of interest. We used conditional statements, as described previously, in a geographic information system (GIS) to estimate scour and accretion by quantifying changes in bar and bank spatial extents.

The first mapping interval, from 1980 to 1997, was dominated by channel widening; 24 percent of the active-channel area showed lateral bank changes compared to about 8 to 10 percent during subsequent periods (table 6). About 7 percent of the active channel showed a change in bar area compared to about 2 to 5 percent during subsequent periods. The combined effects of scour-inducing tributary floods, experimental flow releases, and “feathered-edge” construction resulted in the greatest bank-erosion rates of the study period (fig. 27). There was a small amount of bar accretion, primarily in the vicinity of tributary confluences (fig. 28), and in the lower river, there was scour of bar vegetation (fig. 29). A post-flood assessment (McBain and Trush, Inc., 2000) indicated much of the bank erosion during this period was caused by the 1997 tributary flood (fig. 23), and from 1980 to 1997, mean daily flows at the Lewiston

gage exceeded 6,000 ft³/s, the flow threshold designed to mobilize and scour channel features (table 1), for a total of 81 days. Additional management actions that contributed to bank and bar changes included pool dredging and side-channel construction (fig. 24).

The period from 1997 to 2001 was dominated by bar accretion (fig. 28) near Rush Creek (6.5 FPkm), Indian Creek (25.6 FPkm), and downstream from Oregon Gulch (50.5 FPkm). Bank erosion continued (fig. 27), although rates declined slightly (table 6), and bar stabilization by vegetation encroachment ensued throughout the study area (fig. 29). Compared to the previous period, a smaller proportion of the channel underwent bar and bank changes. About 4 percent of the active channel underwent bar scour or accretion, whereas about 10 percent underwent bank erosion or accretion (table 6). The rate of bar accretion was an order of magnitude higher (8,709 m²/yr) than during the previous period (772 m²/yr), but the bank erosion rate (0.24 m/yr) was similar to the previous period (0.3 m/yr). Although there was a large, long duration, tributary-flow event in 1998 (fig. 23), mean daily flows at the Lewiston gage exceeded 6,000 ft³/s for only 9 days. Management actions were confined to the upper river and included dredging of sediment-retention ponds (fig. 24) and small amounts of gravel augmentation (fig. 25).

Table 6. Summary of bar and bank changes during five study periods for the Trinity River, California, downstream from Lewiston Dam.

[Abbreviations: m/yr, meter per year; m²/m, square meter per meter; m²/yr, square meter per year]

Type of change	1980 to 1997	1997 to 2001	2001 to 2006	2006 to 2009	2009 to 2011
Bar change					
Net change in active-bar area per unit channel length ¹ (m ² /m)	0.20	0.54	-0.72	0.15	0.20
Rate of change in active-bar area (m ² /yr)	772	8,709	-9,324	3,267	6,505
Active-channel area experiencing bar scour or accretion (percent)	7.4	3.5	5.1	2.4	4.2
Bank change					
Net change in active-channel area per unit channel length ² (m ² /m)	5.05	0.95	1.13	0.25	0.53
Rate of change in active-channel width (m/yr)	0.30	0.24	0.23	0.08	0.27
Active-channel area experiencing bank erosion or accretion (percent)	24.4	10.2	10.9	8.4	8.7

¹Positive values indicate bar accretion, and negative values indicate bar scour. Data normalized by channel length estimated by using the centerline of baseflow channel.

²Positive values indicate channel widening and bank erosion, and negative values indicate channel narrowing and bank accretion and riparian vegetation encroachment. Data normalized by channel length estimated by using the centerline of baseflow channel.

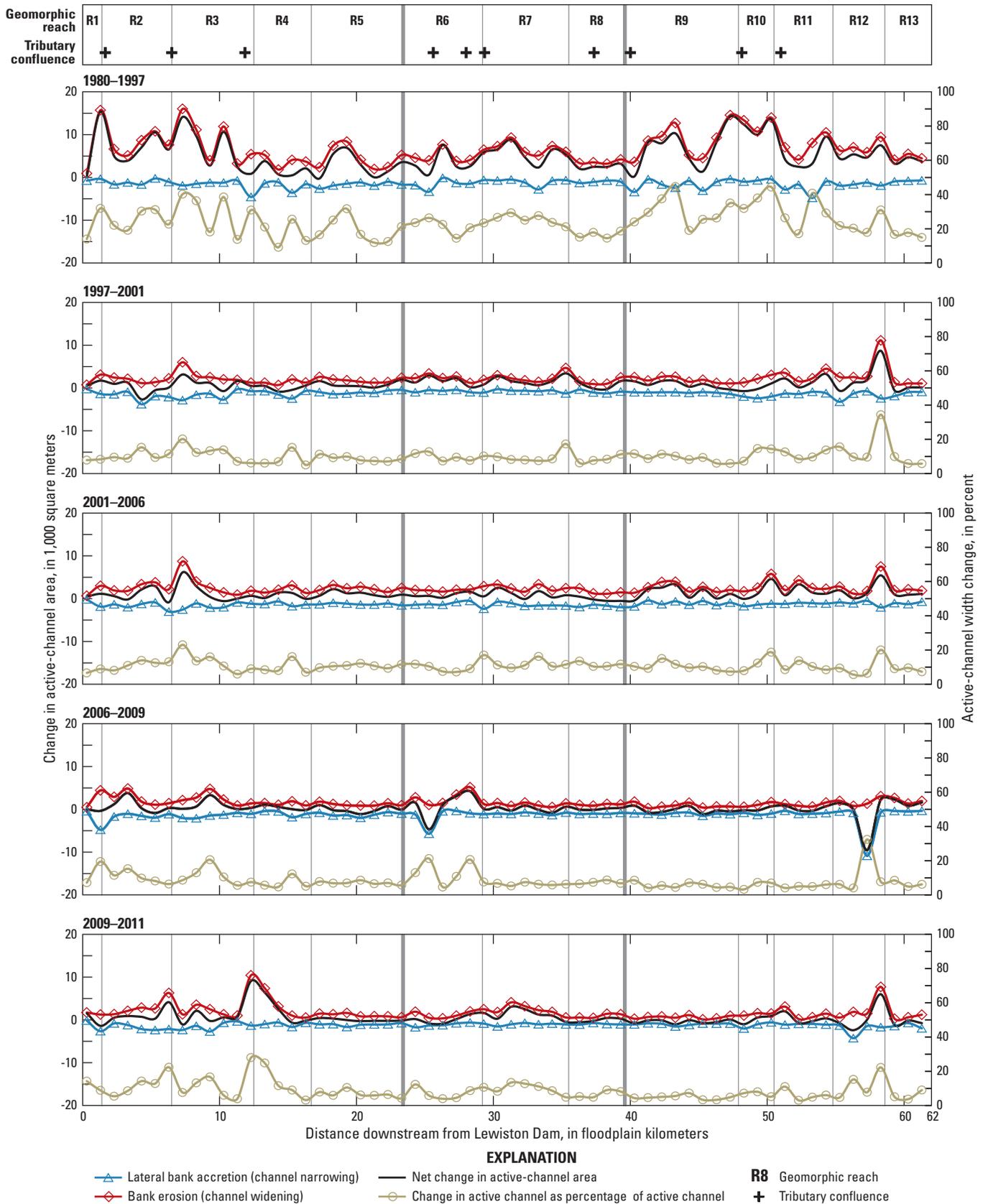


Figure 27. Changes in active-channel area due to bank erosion and accretion along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 2011.

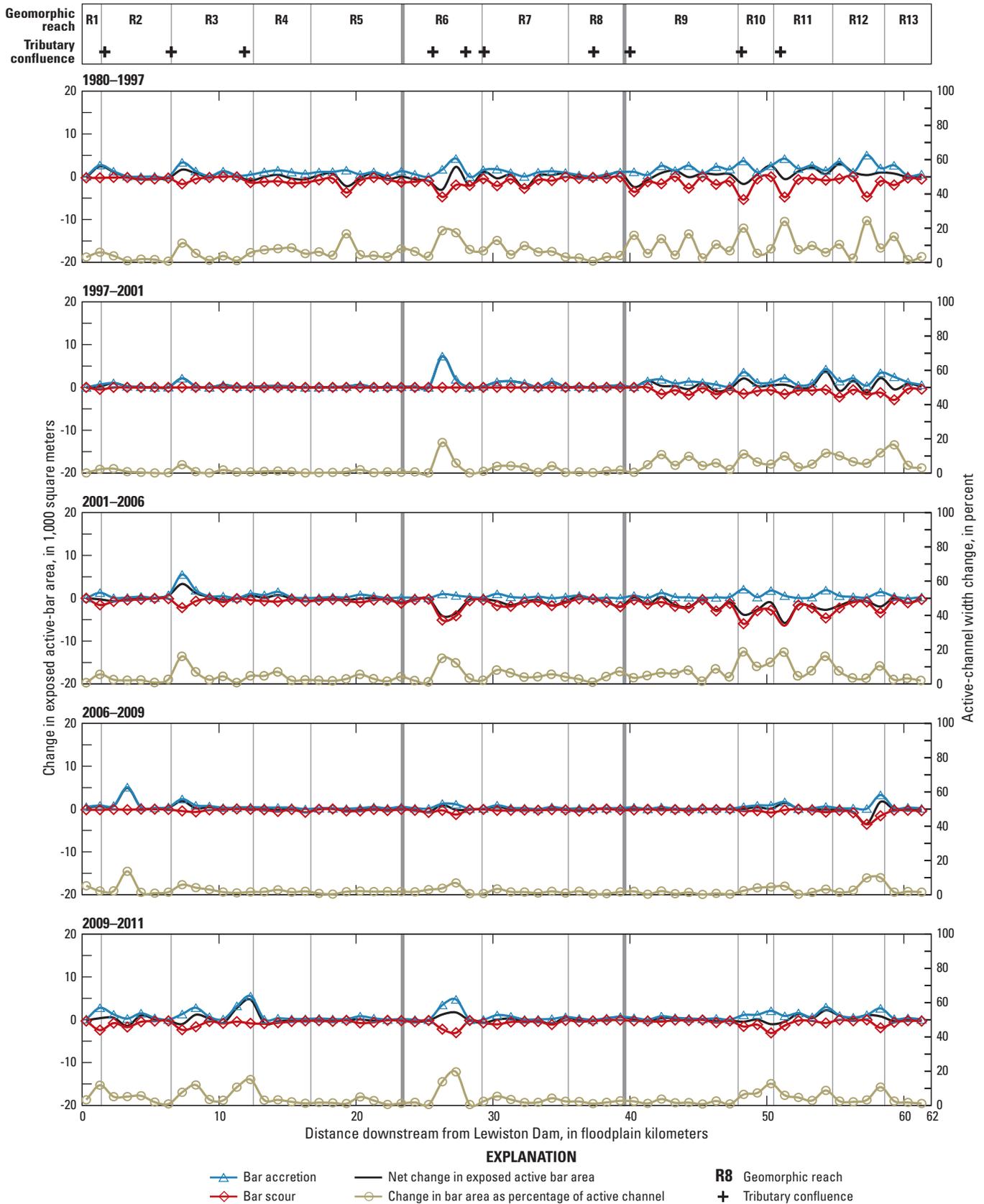


Figure 28. Changes in active-bar area due to bar scour and accretion along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 2011.

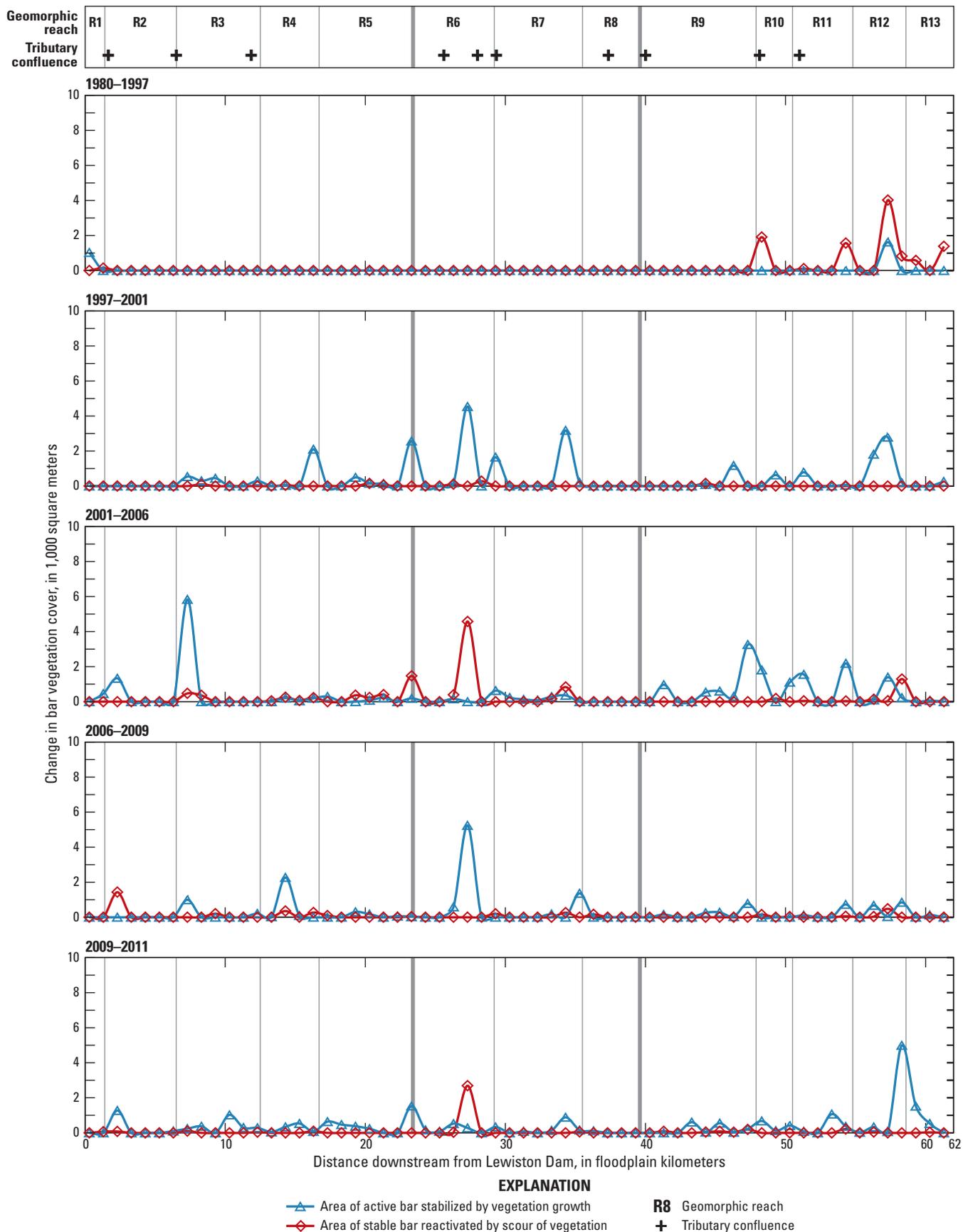


Figure 29. Changes in bar vegetation along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 2011.

The period from 2001 to 2006 was dominated by bar scour (fig. 28), and bar stabilization from encroachment of riparian vegetation continued in the upper and lower river (fig. 29). Bar accretion occurred in the upper river downstream of Rush Creek (6.5 FPkm), but bar scour dominated downstream of Indian Creek (25.6 FPkm). System wide, about 5 percent of the active channel showed bar scour or accretion, whereas about 11 percent showed bank change (table 6). Rates of bar scour (9,324 m²/yr) were slightly greater than bar accretion during the previous period, but the bank erosion rate (0.23 m/yr) was similar to the previous period (table 6). There was a significant tributary flood followed by a secondary spring flow release in 2006 (fig. 23), and there were 33 days with flows greater than 6,000 ft³/s measured at the Lewiston gage. Management activities included small amounts of gravel augmentation in the upper river (fig. 25) and construction of the first large-scale channel-rehabilitation project in the lower river that involved surface lowering and floodplain construction (fig. 24).

From a system-wide perspective, bar and bank changes from 2006 to 2009 were relatively small compared to previous periods (table 6), but stabilization of active bars as a result of vegetation encroachment continued throughout the study area (fig. 29). There was bank erosion in upper river (fig. 27), and the largest amount of bar accretion was near the Sawmill gravel-augmentation site (1.7 FPkm). In the lower river, the Lime Point reach (54.8 FPkm) was the only reach that had notable bar and bank changes. System wide, about 2 percent of the active channel showed bar scour or accretion, whereas about 8 percent of the active channel showed bank changes (table 6). There was net bar accretion (3,267 m²/yr), but bank-erosion rates decreased (0.08 m/yr) relative to the previous period (0.23 m/yr). Tributary flows were relatively low, and there were only 7 days with flows greater than 6,000 ft³/s at the Lewiston gage; however, larger volumes of gravel augmentation by direct injection began in 2008 (fig. 25), causing bar accretion in the upper river (fig. 28). Additional management actions included construction of 14 large-scale channel-rehabilitation projects in the study reach (fig. 24). Mechanical restoration included surface lowering to increase channel–floodplain connectivity and construction of channel complexity features.

Bar and bank changes increased from 2009 to 2011. In the upper river, bar accretion and bank erosion occurred near the Lowden Ranch gravel-augmentation site (11.5 FPkm). There was also net bar accretion near Indian Creek (25.6 FPkm) and downstream of Oregon Gulch (48.2 FPkm). The largest amount of bank erosion (fig. 27) was near Grass Valley Creek (11.9 FPkm) and Lime Point (58 FPkm), and stabilization of active bars by vegetation encroachment continued throughout the study area (fig. 29). System wide, about 4 percent of the active channel underwent bar scour or accretion, whereas about 9 percent of the active channel underwent bank erosion or accretion (table 6). The rate of bar accretion doubled (6,505 m²/yr) compared to the previous period (3,267 m²/y), and the bank erosion rate (0.27 m/yr)

increased and was comparable to estimates from 1980 to 2006 (table 6). A moderate tributary-flow event in 2011 was followed by the largest flow release since 1974 in May of 2011 (Krause, 2012a). At the Lewiston gage, there were 12 days with flows greater than 6,000 ft³/s and 3 days with flows greater than 11,000 ft³/s. Gravel augmentation by direct injection during the flow release increased active-bar area in the upper river (fig. 28), and four large-scale channel-rehabilitation projects were constructed (fig. 24). Mechanical rehabilitation included surface lowering to increase channel–floodplain connectivity and construction of channel-complexity features.

Discussion

Our assessment of the cumulative changes in active bar and active channel areas are summarized in figure 30, which shows pre-ROD increases in the active-channel area were well distributed downstream, whereas pre-ROD increases in the active-bar area were primarily downstream of Indian Creek (25.6 FPkm). Post-ROD increases in the area of the active-channel and active-bars were primarily in the upper river upstream of Indian Creek. These interpretations are consistent with our contributing area analysis (fig. 21) and a recent sediment budget estimate (Gaeuman and Krause, 2011), which indicated a transition to a sediment surplus condition downstream of Indian Creek (25.6FPkm). In the remainder of this report, we discuss pertinent controlling factors responsible for the documented geomorphic changes.

Channel Change Potential

The study reach is in an active zone of uplift that provided a tectonic mechanism over geologic time for river incision and development of a bedrock-channel network (Anderson, 2008). Active uplift zones tend to be drained by channels with high transport capacities and low volumes of stored sediment because of the confined setting (Gilbert, 1914; Montgomery and others, 1996; Brierley and others, 2002; Wallick and others, 2010). It follows that sediment storage is often transient and concentrated near point sources or in reaches with erodible channel margins; however, watershed disturbances can result in episodic aggradation and degradation, and such is the case for the Trinity River downstream from Lewiston Dam.

The combined effects caused by the influx of large-diameter mining tailings, dam construction, flow diversion, vegetation encroachment, and flood-induced confluence aggradation effectively trapped the modern channel, often against resistant bedrock valley margins, creating conditions that sustain static channel form and stable alluvial features. An unknown amount of historic channel aggradation between 1848 and 1970, as a result of gold-extraction activities, increased the sediment supply by several orders of magnitude

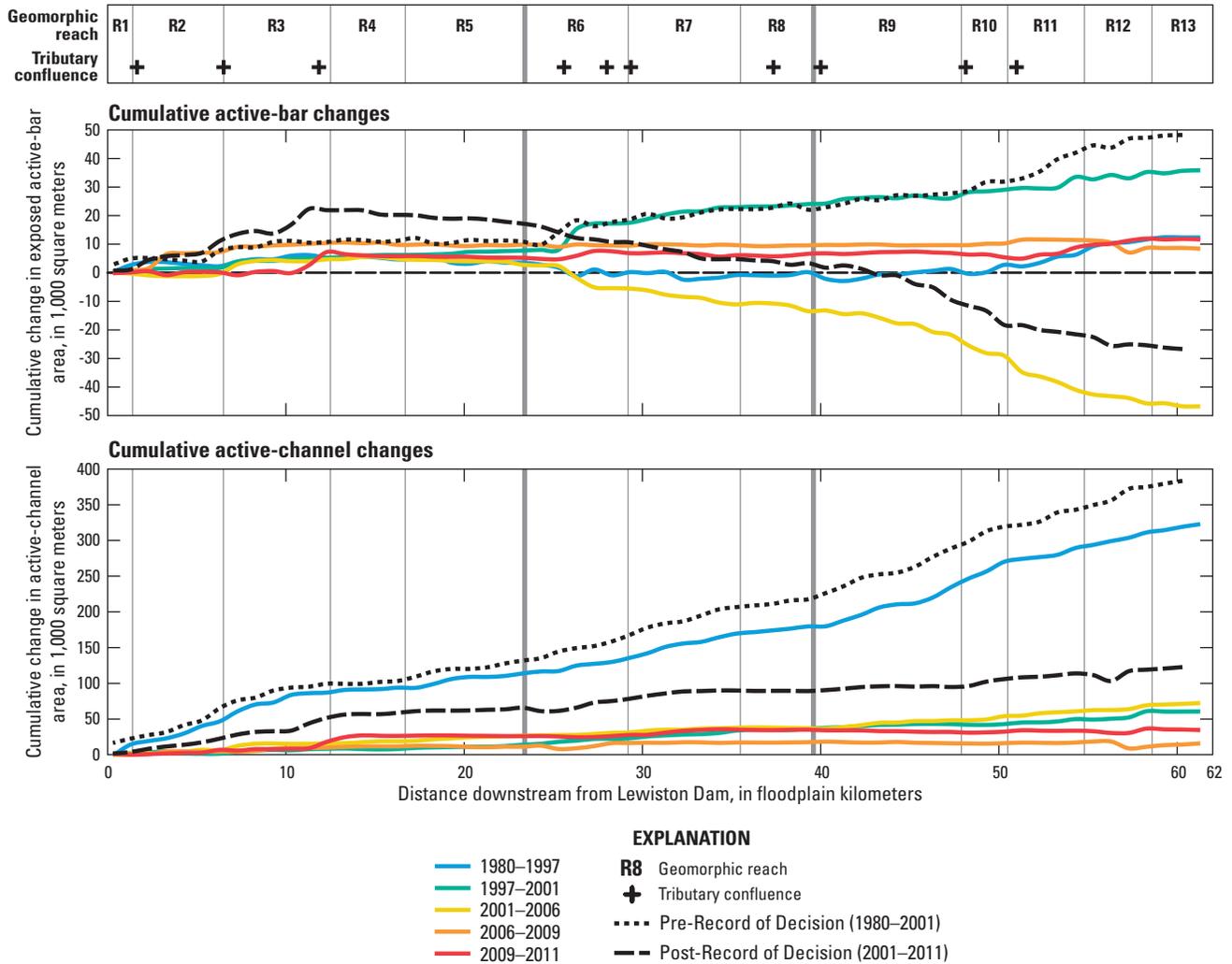


Figure 30. Cumulative downstream change in the areal extent of exposed active bars and of the active channel along the Trinity River downstream from Lewiston Dam, California, for five periods ending in 1997, 2001, 2006, 2009, and 2011.

(Krause and others, 2010; Krause, 2012b). Flow regulation and diversions that began in 1960 effectively decreased the river’s transport capacity (U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999) and enabled vegetation encroachment and stabilization of channel margins. In 1964, a massive regional flood initiated a new episode of aggradation at all major tributary confluences in the study reach (Ritter, 1968). The combined effects of these disturbances produced a narrower, partially confined, aggraded river. Although riparian encroachment continues to be an issue, the tendency toward a static channel form and stable alluvial features was disrupted by pre-ROD tributary floods and continues to be moderated by post-ROD tributary floods, increases in the size and duration of peak-flow releases, and upper-river gravel augmentation.

The upper river generally has a lower potential for dynamic geomorphic change because it lacks tributary contributions to flow and sediment supply. To resolve the lack of capacity for creating dynamic change, post-ROD channel rehabilitation, gravel augmentation, and alterations in flow management were implemented to increase and maintain active-channel areas and channel complexity. The post-2006 increases in gravel augmentation provided additional sediment supply, and regulated flows were increased to support transport capacity. Beginning in 2008, a new phase of channel-rehabilitation began to include channel complexity features, such as bars and secondary water features (split-flow channels, side channels, alcoves, and aquatic wetlands).

The potential of flow events to create channel change depends on antecedent channel conditions, transport capacity, and sediment supply. In terms of creating system-wide responses, the geomorphic effectiveness of ROD-flows is relatively low compared to tributary flows, which produce larger, longer duration flows with greater sediment delivery. Because the upper river lacked sufficient transport capacity and sediment supply, intensive post-ROD management was required to achieve the TRRP goal of promoting active alluvial processes that create and maintain the quantity and quality of available salmonid habitat. Our analyses indicated that geomorphic change induced by managed-flow releases, with concurrent gravel augmentation, tended to be spatially limited. Although the majority of the pre-2001 active bars were remobilized and scoured by the 2006 tributary flood, subsequent increases in bar vegetation indicated post-ROD flows were not sufficient to scour emergent bar vegetation and to maintain active-bar areas in reaches downstream of Indian Creek (25.6 FPkm). However, post-ROD gravel augmentation and flow management did successfully increase and maintain active-bar area in the upper river.

Trajectories of Geomorphic Response and Primary Controls

The general trajectory of change during the study period was the conversion of riparian features into channel features and an expansion of the active-channel system. During the pre-ROD period, channel widening dominated from 1980 to 1997, followed by bar accretion from 1997 to 2001. Although channel widening continued through the post-ROD period, 2001 to 2006 was characterized by bar scour, and there were relatively small geomorphic changes from 2006 to 2011 related to the implementation of ROD-mandated gravel augmentation, prescriptive flow releases, and channel rehabilitation.

The largest and longest duration tributary floods during the study period occurred in 1997 and 1998. The relatively wet period in the early 1980s likely initiated some of the channel changes between 1980 and 1997, but these effects were undocumented. Effects of the 1997 tributary flood were assessed (McBain and Trush, Inc., 2000), and results from the post-flood survey indicated the 1997 flow event effectively scoured channel margins downstream of the Rush Creek confluence (6.5 FPkm).

The 1980 to 1997 period was dominated by bank erosion and channel widening, and we inferred, on the basis of the post-flood reconnaissance, that much of the expansion of the active-channel area was induced by the 1997 flood. The greatest cumulative downstream increase in exposed

active-bar area during the study period was from 1997 to 2001 (fig. 30), primarily downstream of the Indian Creek confluence (25.6 FPkm).

The rapid rate of accretion (8,709 m²/yr; table 6) during the relatively short period from 1997 to 2001 was facilitated by decreased transport capacity and increased sediment supply. Channel widening from 1980 to 1997 altered the river's hydraulic geometry and effectively decreased available transport capacity. Local sediment supply likely increased after 1997 because of scour of riparian vegetation and bank destabilization. We also inferred that tributary sediment supplies increased during the relatively wetter 1998 water year, when there were two large tributary floods. Gravel augmentation accounted for a relatively small portion of the increase in sediment supply during this period. A total of 3,200 m³ of coarse gravel (fig. 25), or about 800 m³/yr, was added to the upper river at two locations (1.4 and 4.6 FPkm).

During the period from 2001 to 2006, the study area was dominated by bar scour, again, primarily downstream of the Indian Creek confluence (25.6 FPkm; fig. 30). Bar scour was most likely induced during a relatively wetter period that culminated in the 2006 tributary flood and a 10,400 ft³/s peak-flow release (fig. 23). Bar scour during this period was slightly greater (9,324 m²/yr) than bar accretion during the previous period (8,709 m²/yr; table 6).

Beginning in 2005, large-scale channel rehabilitation began (fig. 24), and there were concurrent increases in the frequency of flows inundating floodplains (fig. 19) and gravel augmentation (fig. 25). Intensified mechanical rehabilitation increased the connectivity of low-elevation riparian features (post-dam benches and constructed floodplains), and implementation of the post-ROD flow regime increased the frequency of floodplain inundation. Implementation of larger scale channel rehabilitation also increased channel complexity (fig. 8) in the form of exposed active-bar areas (fig. 16) and secondary water features (split-channels, side channels, alcoves, and aquatic wetlands; fig. 17) in the upper and central river.

During the remainder of the post-ROD period, 2006 to 2011, the active-channel area continued to increase (fig. 30), and bar changes were primarily confined to the upper river reaches that had gravel augmentation (1.4 FPkm and 11.5 FPkm) and downstream of the Canyon Creek confluence (51.0 FPkm). The cumulative results of intensive management in the upper river were increased channel complexity and floodplain connectivity that was maintained with managed-flow releases. Gravel augmentation was the primary factor leading to upper river increases in active-bar area, and the 2006 tributary flood was the primary factor that increased lower river active-bar area.

During the post-ROD period, large channel changes were spatially limited to reaches that had mechanical restoration or gravel augmentation and to reaches downstream of tributary confluences, where localized excess sediment supplies or transport capacity exist. This observation was supported by earlier studies (Ritter, 1968; Trinity Restoration Associates, Inc., 1993; Hoopa Valley Tribe and others, 2011b). The exception to this generalization was the Lime Point reach (54.8 to 58.2 FPkm). The Lime Point reach was one of the most dynamic reaches during the study period. Although there was a series of rehabilitation projects constructed in this reach in 2006 and 2010, dynamic channel changes were primarily in un-rehabilitated reaches. The greatest bar and bank changes were in the lowermost section of the Lime Point reach (58 FPkm), which is in an incised meander bend that has a relatively small radius of curvature, which produces large bed-shear stresses and high transport capacity.

We constructed a series of figures to show the cumulative pre- and post-ROD changes in representative reaches. [Figure 31](#) shows a portion of the primary spawning reach and the Sven Olbertson rehabilitation site (1.0 FPkm) in the upper river downstream from Lewiston Dam. Intensive management of this reach during pre- and post-ROD periods included gravel augmentation, mechanical restoration, and peak-flow releases that increased the active-channel area, channel complexity, and floodplain connectivity.

[Figures 32, 33, and 34](#) show a series of reaches in the lower river where there was dynamic channel change. [Figure 32](#) illustrates bank erosion and bar accretion near Junction City, Calif. (50.1 FPkm), upstream from the Canyon Creek confluence. Pre-ROD erosion of the left bank and deposition of lateral bars resulted in about 25 m of channel migration between 1980 and 2001. Post-ROD bank erosion continued to expand the active-channel area, and there was concurrent bar accretion, bar scour, and stabilization of a downstream lateral bar. Channel complexity also increased with the number of bars and secondary water features. [Figure 33](#) shows the upstream portion of the Conner Creek rehabilitation site (53.8 FPkm), where the deposition of large pre-ROD bars increased channel complexity and sinuosity. During the post-ROD period, there was bar scour, bar stabilization, and bank erosion that expanded the active-channel area, and rehabilitation of the channel margin increased riparian diversity with floodplain construction. [Figure 34](#) illustrates Lime Point (58.1 FPkm), where a pre-ROD channel avulsion was accompanied by bar scour and bar deposition, which increased channel complexity and the active-channel area. During the post-ROD period, a large medial bar was stabilized by vegetation encroachment, and the active channel area decreased, but the 1980-era channel continued to function as a side channel, and new bar features formed.

Geomorphology and Habitat Linkages

To support the TRRP adaptive management program, we evaluated the relative effectiveness of natural and managed controlling factors and the associated cumulative geomorphic response during the five study periods. We also assessed a set of performance measures (channel complexity, shoreline length, and channel-floodplain connectivity) identified by the TRRP as primary metrics for characterizing linkages between geomorphic structure and available salmonid habitat (Trinity River Restoration Program and ESSA Technologies Ltd., 2009).

Measures of channel complexity included exposed active-bar area ([fig. 16](#)) and secondary water features ([fig. 17](#)). There were greater increases in channel complexity during the pre-ROD period than during the post-ROD period. System-wide channel complexity increased markedly from 1980 to 1997 and then decreased slightly from 1997 to 2001. During the post-ROD period system-wide channel complexity decreased slightly, but there were smaller, yet measurable, increases in channel complexity in the upper river.

An integrated habitat assessment (U.S. Fish and Wildlife Service and others, 2011) of channel-rehabilitation projects constructed from 2005 to 2009 concluded that the only metric well correlated to fish use was the length of the wetted-channel edge, or shoreline length. During the study period, the largest increase in shoreline length ([fig. 18.4](#)) was during the pre-ROD period, primarily in the upper river, as a result of extensive side-channel construction and bar accretion. There were smaller, but measurable, increases in shoreline length during the post-ROD period, primarily after 2006, related to channel rehabilitation.

Increases in channel–floodplain connectivity were inferred from the areal extent of constructed floodplains and by increases in the size and frequency of post-ROD flow releases. During the pre-ROD period in the early 1990s, small-scale riparian berm removal and feathered-edge construction increased floodplain connectivity ([fig. 24](#)). Extensive scour of riparian vegetation during the 1997 tributary flood resulted in additional increases in floodplain connectivity, primarily downstream from Indian Creek (25.6 FPkm; [fig. 29](#)). During the post-ROD period, riparian vegetation was scoured near tributary confluences from 2001 to 2006 ([fig. 29](#)), and there was a relatively large increase in constructed floodplain area from 2005 to 2011 ([fig. 25](#)). Post-ROD increases in the areal extent of lower-elevation floodplains, inundated by flows greater than about 4,500 ft³/s, and concurrent increases in the frequency of exceedance ([table 1](#)) indicated a larger proportion of riparian features were inundated annually during the post-ROD period.

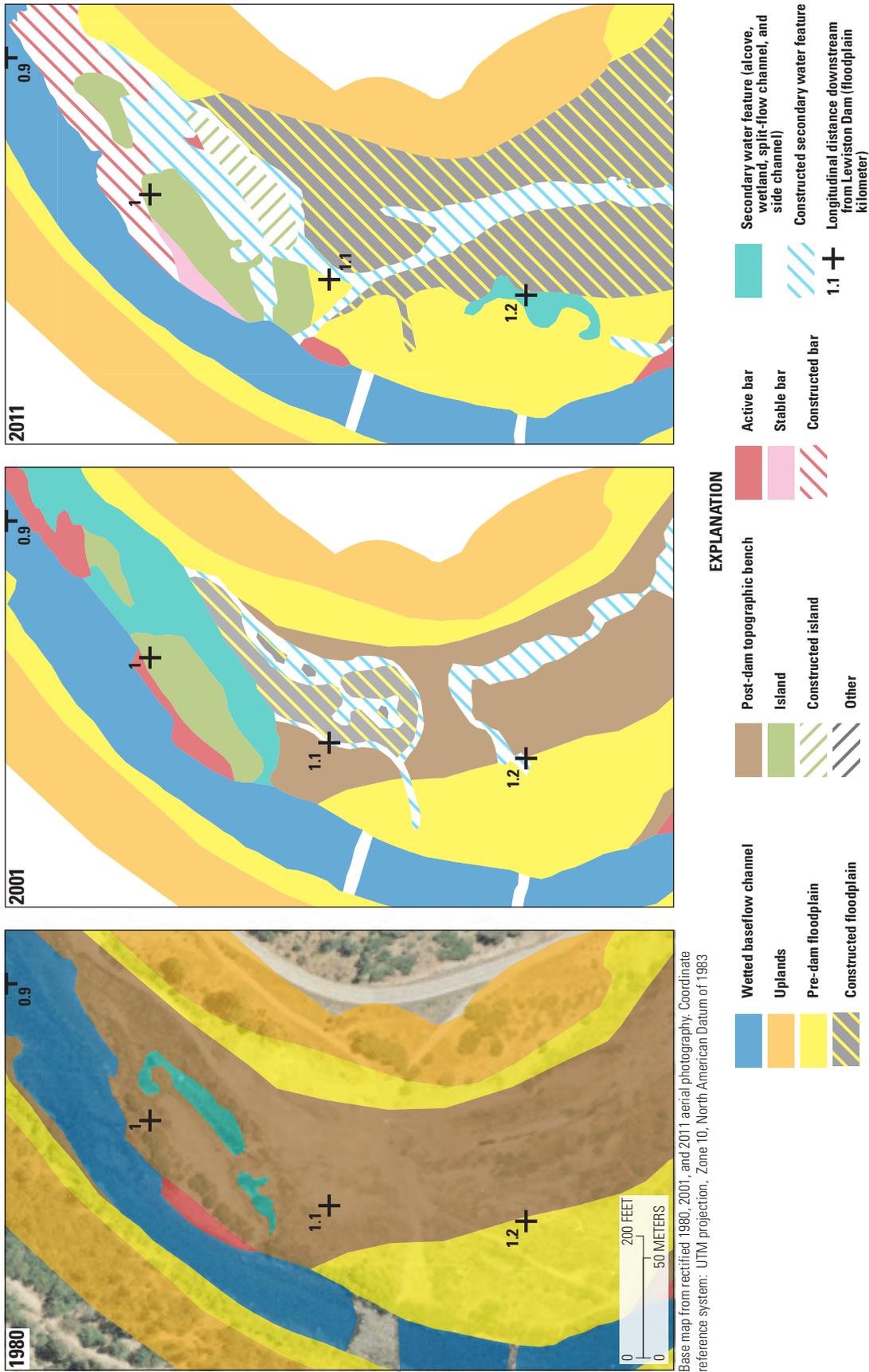


Figure 31. Geomorphic feature maps for the Sven Olbertson Rehabilitation Site on the Trinity River, California, 1.0 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.

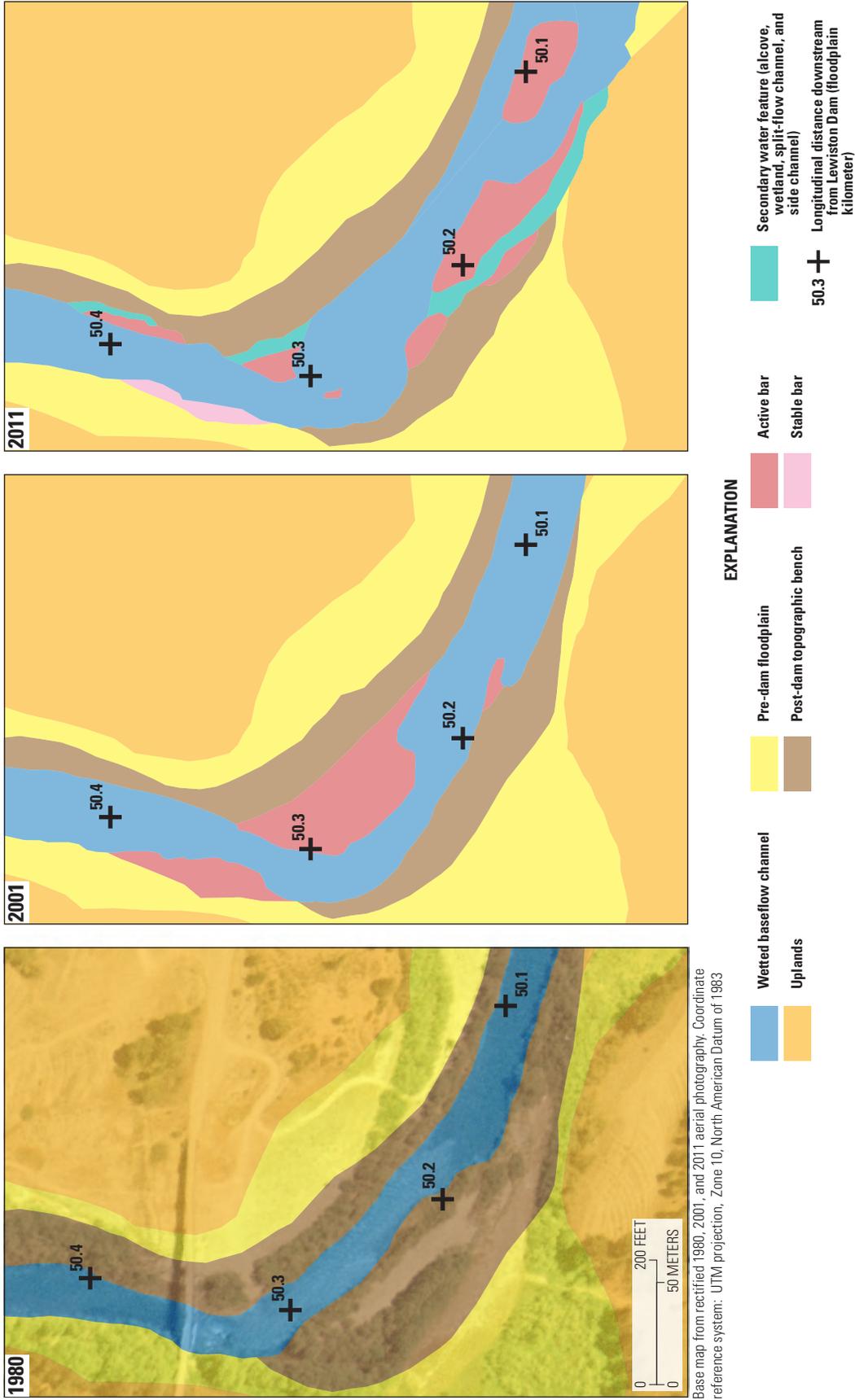


Figure 32. Geomorphic feature maps near Junction City on the Trinity River, California, 50.1 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.

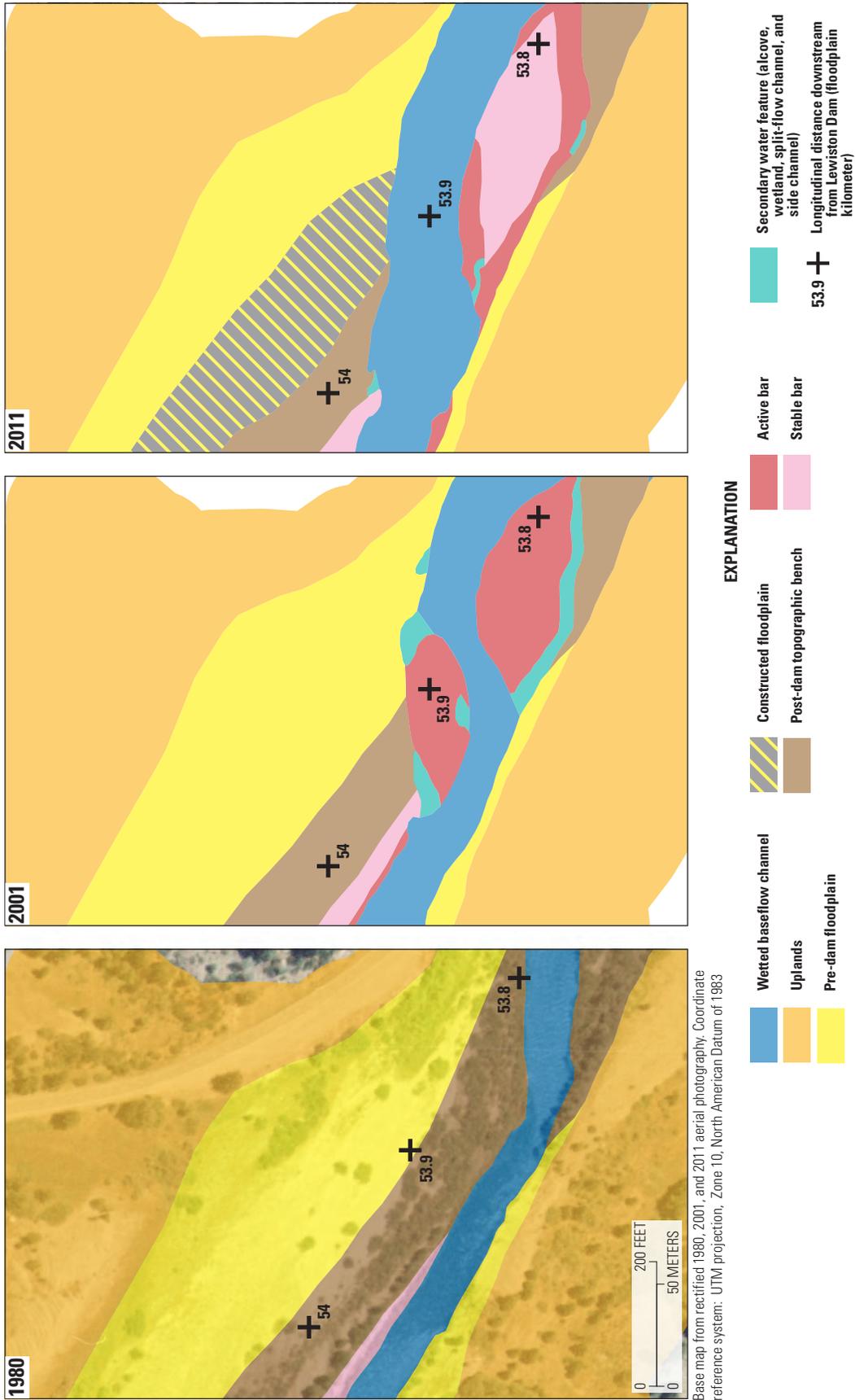


Figure 33. Geomorphic feature maps for Conner Creek Rehabilitation Site on the Trinity River, California, 53.8 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.

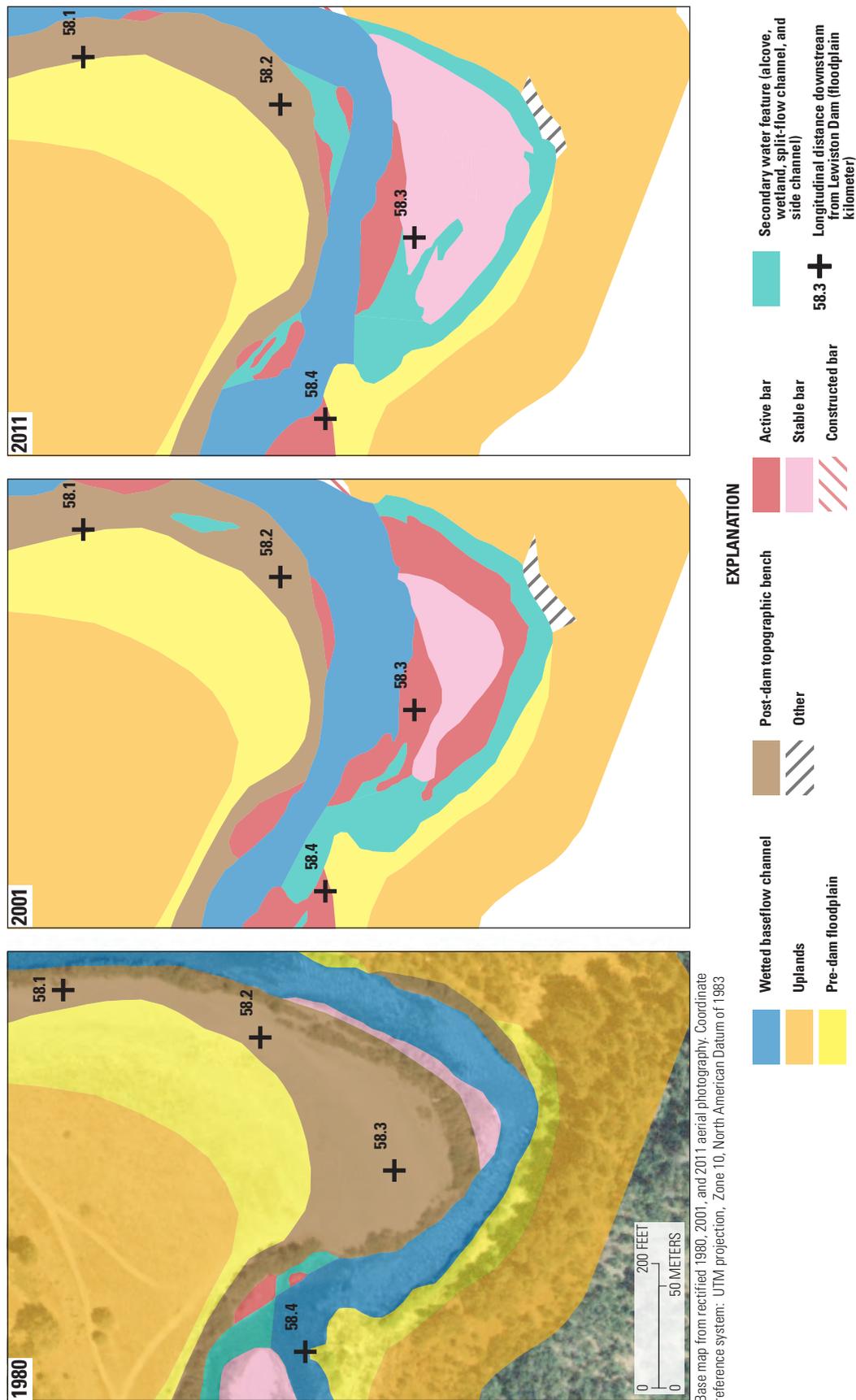


Figure 34. Geomorphic feature maps at Lime Point on the Trinity River, California, 58.1 floodplain kilometers downstream from Lewiston Dam, in 1980, 2001, and 2011.

Conclusions

This report documents a geomorphic assessment of a 65-km study reach along the Trinity River, California, downstream of Lewiston Dam. A series of geomorphic maps were used to characterize trajectories of geomorphic change and to investigate the evolution of geomorphic features and alluvial processes for one of the nation's largest adaptively managed river restoration programs. The maps illustrate a system-wide perspective of evolving geomorphic features governed by natural processes and management actions from 1980 to 2011. The 1980 to 1997 period was dominated by channel widening, primarily induced by the 1997 tributary flood, and accompanied by smaller increases in active-bar area. This period of channel widening was followed by extensive bar accretion, primarily downstream of Indian Creek, from 1997 to 2001. Bar and channel margins, scoured by large tributary floods in 1997 and 1998, were recolonized by vegetation as early as 2001. The beginning of the post-ROD period, from 2001 to 2006, was characterized by bar scour slightly greater than bar accretion during the previous period, again, primarily downstream from Indian Creek. From 2006 to 2011, there were smaller, but measurable geomorphic changes, but these were generally limited to gravel-augmentation sites in the upper river, mechanical channel-rehabilitation sites, tributary confluences, and lower river reaches that had sufficient transport capacity and sediment supply.

The general trajectory of change from 1980 to 2011 was a system-wide increase in riparian diversity and conversion of riparian features to channel features, such that the active-channel area and channel complexity increased. During the longer (21 years) and relatively wetter pre-ROD period, increases in active-channel area and channel complexity were 20 and 70 percent, respectively. In 1980, the pre-dam floodplain and post-dam benches were the primary riparian features. Pre-ROD changes in riparian diversity included an increase in constructed floodplain and stable bar areas. The post-ROD period was shorter (10 years), relatively drier, had intensified management, and there were small, but measurable, increases in active-channel area (5 percent) and decreases in channel complexity (3 percent). Post-ROD changes in riparian diversity included large increases in constructed floodplain area and smaller increases in stable bar area.

Parsing out responses to individual causal mechanisms is exceedingly complex with numerous and concurrent natural and managed controlling factors operating at the watershed to reach scale. We determined the primary drivers of change during the wetter pre-ROD period were sequential tributary floods in 1997 and 1998 that produced channel widening (1997) following by bar accretion (1998). During the relatively drier post-ROD period, there were measurable increases in channel complexity, shoreline length, riparian

diversity, and channel–floodplain connectivity, which can be attributed to the 2006 tributary flood, mechanical restoration, gravel augmentation, and managed flow increases. Since 2006, restoration efforts successfully increased exposed active-bar areas by using gravel augmentation in the upper river, and these active-bars were maintained with managed-flow releases. System-wide riparian diversity and floodplain connectivity peaked in 2011, and constructed floodplains were inundated for the first time by the 2011 peak-flow release. Channel complexity peaked in the central and lower river in 2001 and subsequently decreased as a result of natural scour and bar stabilization by vegetation encroachment. In the upper river, channel complexity peaked in 2011 as a result of gravel augmentation and construction of channel-complexity features.

Our analysis of tributary floods and managed peak-flow releases indicated tributary floods have the potential to initiate larger and more extensive geomorphic change than managed peak-flow releases. During the study period, tributary-flows in 1997, 1998, and 2006 delivered an unknown, yet presumably large, amount of flow and sediment to the mainstem study reach. We inferred that increases in transport capacity and sediment supply during these tributary floods resulted in the greatest channel changes during the study period.

The regulated-flow strategy in use at the time of writing largely decouples mainstem flows from tributary flows in terms of timing. The annual peak flow releases from Lewiston Dam begin in May, whereas tributary contributions are distributed through the winter and spring. An alternative strategy for inducing system-wide dynamic bar and bank processes would be to coordinate managed-flow releases from Lewiston Dam to coincide with tributary flooding. Also, the muted and spatially limited physical response to flow releases during the post-ROD period highlights the need for continued monitoring and assessment of the magnitude, duration, and timing of prescriptive flows and associated geomorphic response.

Channel widening from 1980 to 1997 represented a threshold disturbance resulting in a system-wide decrease in transport capacity, which was likely a primary factor governing active-bar deposition from 1997 to 2001. Bed-mobility studies in the mid-1990s determined that 80 percent of the low-flow channel margin was mobilized at 6,000 ft³/s (Trinity Restoration Associates, Inc., 1993; Wilcock and others, 1995; McBain and Trush, Inc., 1997). After 1997, studies showed that 6,000 ft³/s did not produce the expected scour, mobility, or channel maintenance targets (Hoopa Valley Tribe and others, 2011b). These observations indicate that pre-ROD channel widening could have altered channel hydraulics, such that flows required to produce targeted geomorphic objectives need to be increased. Achieving the TRRP goal of a downscaled dynamic river could come with the unexpected consequence of a larger active-channel area that requires periodic higher maintenance flows.

Expansion of the geomorphic feature database (Curtis and Guerrero, 2015; <http://dx.doi.org/10.5066/F7TT4P04>) to include additional study periods and additional physical attributes would support disturbance–response analyses, interpretation of the linkages between geomorphology and physical habitat, and could be used to refine conceptual models and test hypotheses highlighted as a fundamental component of adaptive management (Trinity River Restoration Program and ESSA Technologies Ltd, 2009). Rectified orthophotography from 1944, 1960, and 1975 exists. Expanding the retrospective mapping to include the pre-1980 orthophotography would enable assessment of legacy influences related to hydraulic and dredge mining and the 1955, 1964, and 1974 floods. More detailed mapping of the type and density of riparian vegetation within the framework of the existing geomorphic feature maps would enable refinement of the active-channel boundary and bar-stability classification. This study used a relatively simple bar classification that included lateral and medial bars. For the more recent periods, the bar classification could be expanded to include additional morphologic and topographic attributes and to include additional field reconnaissance and mapping of hydraulic controls to support the assessment of bar-forcing mechanisms.

Geomorphic change was strongly influenced by the relation between transport capacity and sediment supply, which varied in space and time. The lack of spatially distributed estimates of transport capacity and sediment supply severely hindered the controlling factor analysis. A series of physical models that link tributaries and the mainstem study reach, and characterize flow and sediment flux, would be useful for interpreting the spatial distribution of transport capacity and sediment supply and for developing testable hypotheses regarding potential geomorphic changes under present and future conditions. Spatially distributed estimates of transport capacity and sediment supply would also support a more detailed disturbance–response analysis and assessment of the effectiveness of channel-maintenance flows, gravel-augmentation prescriptions, and channel-rehabilitation design criteria.

References Cited

- Anderson, K.T., 2008, Inferring bedrock uplift in the Klamath Mountains Province, from river profile analysis and digital topography, Master's Thesis, Texas Tech University, Tex., 314 p.
- Brierley, G.J., Fryirs, K., Outhet, D., Massey, C., 2002, Application of the river styles framework as a basis for river management in New South Wales, Australia: *Applied Geography* v. 22 no. 1, p. 91–122. [http://dx.doi.org/10.1016/S0143-6228\(01\)00016-9](http://dx.doi.org/10.1016/S0143-6228(01)00016-9).
- California Department of Water Resources Northern District, 2007, Trinity River Hydraulic Flow Study North Fork Trinity to Lewiston Dam: Sacramento, California, 85 p., http://odp.trrp.net/FileDatabase/Documents/DWR_HydraulicFlowStudyReport_forTRRP_Final_2007071.pdf.
- Church, M., 2002, Geomorphic thresholds in riverine landscapes: *Freshwater Biology*, v. 47, p. 541–557. DOI: 10.1046/j.1365-2427.2002.00919.x.
- Curtis, J.A., and Guerrero, T.M. 2015, Geomorphic mapping to support river restoration on the Trinity River downstream from Lewiston Dam, California, 1980–2011: U.S. Geological Survey Open File Report, OFR-5046, xp.
- Diller, J.S., 1902, Topographic development of the Klamath Mountains: Washington, D.C., U.S. Geological Survey Bulletin, v. 196, p. 69. <http://pubs.usgs.gov/bul/0196/report.pdf>.
- Draut, A.E., Logan, J.B., McCoy, R.E., McHenry, M., and Warrick, J.A., 2008, Channel evolution on the lower Elwha River, Washington, 1939–2006: U.S. Geological Survey, Scientific Investigations Report 2008–5127, 26 p., <http://pubs.usgs.gov/sir/2008/5127/>.
- Draut, A.E., Logan, J.B., and Mastin, M.C., 2011, Channel evolution on the dammed Elwha River, Washington, USA: *Geomorphology*, v. 127, p. 71–87, doi:10.1016/j.geomorph.2010.12.008.
- Gaeuman, D., 2008, Recommended quantities and gradation for long-term coarse sediment augmentation downstream from Lewiston Dam: Weaverville, Calif., Trinity River Restoration Program, Technical Report TM-TRRP-2008-2, 16 p. http://odp.trrp.net/FileDatabase/Documents/TM-TRRP-2008_21.pdf.
- Gaeuman, D., and Krause, A.F., 2011, 2010 Bed-material sediment budget update, Trinity River, Lewiston Dam to Douglas City, California: Trinity River Restoration Program Technical Report TM-TRRP-2011-2: Weaverville, Calif., 24 p. http://odp.trrp.net/FileDatabase/Documents/Gaeuman%20Krause%20%282011%29%202010%20Bed-material%20sediment%20budget%20update...TR-TRRP-2011_21.pdf.
- Gallagher, S.P, 1995, Evaluation of the feathered edge restoration projects on the Trinity River: fish use and physical habitat: Sacramento, Calif., U.S. Fish and Wildlife Service, Division of Ecological Services, In-stream Flow Branch, 28 p.
- Gilbert, G.K., 1914, The transport of debris by running water: U.S. Geological Survey Professional Paper 86, 263 p. <http://pubs.usgs.gov/pp/0086/report.pdf>.

- Graham Matthews and Associates, 2001, Sediment source analysis for the mainstem Trinity River, Trinity County, California, Final Report to Tetra Tech, Inc.: Fairfax, Va., 190 p. http://www.krisweb.com/biblio/trinity_tetrattech_gma_2001_sediment.pdf.
- Graham Matthews and Associates, 2012, Trinity River WY2011 sediment transport monitoring final report, Prepared for the Trinity River Restoration Program: Weaverville, Calif., 144 p. <http://odp.trrp.net/FileDatabase/Documents/GMA%20%282012%29%20Trinity%20River%20WY2011%20Sediment%20Transport%20Monitoring1.pdf>.
- Grams, P.E., and Schmidt, J.C. 2002, Streamflow regulation and multi-level flood plain formation: channel narrowing on the aggrading Green River in the eastern Uinta Mountains, Colorado and Utah: *Geomorphology*, v. 44, p. 337–360. [http://dx.doi.org/10.1016/S0169-555X\(01\)00182-9](http://dx.doi.org/10.1016/S0169-555X(01)00182-9).
- Grant, G. E. and Swanson, F. J., 1995, Morphology and Processes of Valley Floors in Mountain Streams, Western Cascades, Oregon, *in* Costa, J.E., Miller, A.J., Potter, K.W., and Wilcock P.R., eds., *Natural and Anthropogenic Influences in Fluvial Geomorphology*: Washington, D. C., American Geophysical Union. doi: 10.1029/GM089p0083.
- Hoopa Valley Tribe, McBain & Trush, Inc., and Northern Hydrology and Engineering, 2011a, Channel rehabilitation design guidelines for the mainstem Trinity River: Prepared for the Trinity River Restoration Program, Hoopa, Calif., 338 p. <http://odp.trrp.net/FileDatabase/Documents/Trinity%20River%20Channel%20Design%20Guide%201-21-11%20reduced2.pdf>.
- Hoopa Valley Tribe, U.S. Fish and Wildlife Service, and Yurok Tribe, 2011b, Integrated habitat assessment of the Upper Trinity River, 2009: Draft Report: Prepared for the Trinity River Restoration Program, Hoopa, Calif., 336 p.
- Hughes, M.L., McDowell, P.F., and Marcus, W.A., 2006, Accuracy assessment of georectified aerial photographs—Implications for measuring lateral channel movement in GIS: *Geomorphology*, v. 74, p. 1–16. <http://dx.doi.org/10.1016/j.geomorph.2005.07.001>.
- Ingersoll, R.V., and Schweickert, R.A., 1986, A plate-tectonic model for Late Jurassic Ophiolite Genesis, Nevadan orogeny and forearc initiation, northern California: *Tectonics*, v. 5, no. 6, p. 901–912. doi:10.1029/TC005i006p00901.
- Irwin, W., 1972, Terranes of the western Paleozoic and Triassic belt in the southern Klamath Mountains, California: U.S. Geological Survey Professional Paper 800–C, p. 103–111. <http://pubs.usgs.gov/pp/0800c/report.pdf>.
- Irwin, W.P., 1981, Tectonic accretion of the Klamath Mountains, *in* Ernst, W.G., ed., *The geotectonic development of California (Rubey Volume 1)*: Prentice-Hall, Englewood Cliffs, N.J., p. 29–49.
- Irwin, W.P., 1994, Geologic map of the Klamath Mountains, California and Oregon: U.S. Geological Survey Miscellaneous Investigations Series Map I–2148, scale 1:500,000. <http://pubs.er.usgs.gov/publication/i2148>.
- Knott, J.M., 1974, Sediment discharge in the Trinity River Basin, California: U.S. Geological Survey Water Resources Investigation 73–49, 56 p. <http://pubs.er.usgs.gov/publication/wri7349>.
- Kondolf, G.M., and Minear, J.T., 2004, Coarse sediment augmentation on the Trinity River below Lewiston Dam: Geomorphic Perspectives and Review of Past Projects, Report to the Trinity River Restoration Program, 67 p. <http://odp.trrp.net/FileDatabase/Documents/Kondolf,%20G%20and%20Minear,%20J%20%282004%29%20Coarse%20sediment%20augmentation%20on%20the%20Trinity%20River...2.pdf>.
- Krause, A.F., 2012a, Flow releases and diversions and the Trinity River, CA: Water Year 2011: Weaverville, Calif., Bureau of Reclamation, Trinity River Restoration Program, Technical Report, TR-TRRP-2012-1. <http://odp.trrp.net/FileDatabase/Documents/Krause%202012%20Flow%20Releases%20and%20Diversion%20on%20the%20Trinity%20River%20WY2011.pdf>.
- Krause, A.F., 2012b, History of mechanical sediment augmentation and extraction on the Trinity River, California, 1912–2011: Trinity River Restoration Program Technical Report, TR-TRRP-2012-2, 49 p. [http://odp.trrp.net/FileDatabase/Documents/Krause%20\(2012\)%20History%20of%20mechanical%20sediment%20augmentation%20and%20extraction%201912%20-%202011.Revised1.pdf](http://odp.trrp.net/FileDatabase/Documents/Krause%20(2012)%20History%20of%20mechanical%20sediment%20augmentation%20and%20extraction%201912%20-%202011.Revised1.pdf).
- Krause, A.F., Wilcock, P.R., Gaeuman, D., 2010, One hundred and fifty years of sediment manipulation on the Trinity River, Calif.: *In* Proceedings of the 9th Joint Federal Interagency Conference on Sedimentation and Hydrologic Modeling, Las Vegas, Nev., June 27, 2010–July 1, 2010. http://acwi.gov/sos/pubs/2ndJFIC/Contents/3D_Krause_3_1_10.pdf.
- McBain & Trush, Inc., 1997, Trinity River maintenance flow study—Final report: Arcata, Calif., prepared for the Hoopa Valley Tribe, McBain and Trush, Inc., 482 p. <http://odp.trrp.net/FileDatabase/Documents/Trinity%20Maintenance%20Flow%20Study%20-%20November%201997.pdf>.

- McBain & Trush, Inc., 2000, Evaluation of 1997 flood impacts on Riparian Berms along the Trinity River, California— Final Report: Arcata, Calif., prepared for the Hoopa Valley Tribe, McBain and Trush, Inc., 27 p. <http://odp.trrp.net/FileDatabase/Documents/MT%20%282000%29%20Evaluation%20of%201997%20Flood%20Impacts%20on%20Riparian%20Berms1.pdf>.
- Micheli, E.R., Kirchner, J.W., and Larsen, E.W., 2004, Quantifying the effect of riparian forest versus agricultural vegetation on river meander migration rates, Central Sacramento River, California, U.S.A.: *River Research and Applications*, v. 20, no. 5, p. 537–548. doi: 10.1002/rra.756.
- Montgomery, D.R., and Buffington, J.M. 1998, Channel processes, classification, and response, chapter 2 in Naiman, R., and Bilby, R., eds., *River Ecology and Management*: New York, N.Y., Springer-Verlag Inc., p. 13–42.
- Montgomery, D.R., Abbe, T.B., Buffington, J.M., Peterson, N.P., Schmidt, K.M., and Stock, J.D., 1996, Distribution of bedrock and alluvial channel in forested mountain drainage basins: *Nature*, v. 381, p. 587–589. doi:10.1038/381587a0 http://www.fs.fed.us/rm/boise/publications/watershed/rmrs_1998_montgomery001.pdf.
- Mount, N.J., and Louis, J., 2005, Estimation and propagation of error in the measurement of river channel movement from aerial imagery: *Earth Surface Processes and Landforms*, v. 30, no. 5, p. 635–643. DOI: 10.1002/esp.1172.
- O'Connor, J.E., Jones, M.A., Haluska, T.L., 2003, Flood plain and channel dynamics of the Quinault and Queets Rivers, Washington, USA: *Geomorphology* v. 51, p. 31–59. [http://dx.doi.org/10.1016/S0169-555X\(02\)00324-0](http://dx.doi.org/10.1016/S0169-555X(02)00324-0).
- Pitlick, J. and Wilcock, P.R., 2001, Relations between Streamflow, Sediment Transport, and Aquatic Habitat in Regulated Rivers, in Dorava, J.M., Montgomery, D.R., Palcsak, B.B, and Fitzpatrick, F. A., eds, *Geomorphic Processes and Riverine Habitat*: Washington, D. C., American Geophysical Union, p. 185–198. doi: 10.1029/WS004p0185.
- Schmidt, J.C., and Wilcock, P.R., 2008, Metrics for assessing the downstream effects of dams: *Water Resources Research*, W04404. doi:10.1029/2006WR005092.
- Schmidt, J.C., Grams, P.E., and Leschin, M.F., 1999, Variation in the magnitude and style of deposition and erosion in three long (8–12 km) reaches as determined by photographic analysis, in Webb, R.H., Schmidt, J.C., Valdez, R.A., and Marzolf, G.R., eds., *The Controlled Flood in Grand Canyon*: Washington, D.C., American Geophysical Union, p. 185–203. doi: 10.1029/GM110p0185.
- Stearns, J.G., 1969, Task force report on sediment problems in the Trinity River near Lewiston, State of California: Sacramento, California Resources Agency, 159 p. <http://odp.trrp.net/FileDatabase/Documents/Sediment%20Problems%20in%20the%20Trinity%20River,%20Near%20Lewiston%2019691.pdf>.
- Trinity Restoration Associates, Inc., 1993, Trinity River maintenance flow report: evaluation of the 6,000 cfs release: Report to Hoopa Valley Indian Tribe Fisheries Department, 140 p. http://www.fws.gov/arcata/fisheries/reports/technical/Trinity_River_Channel_Maintenance_Flow_Study_Final_Report.pdf.
- Trinity River Restoration Program and ESSA Technologies Ltd, 2009, Integrated Assessment Plan, Version 1.0–September 2009: Draft report prepared for the Trinity River Restoration Program, Weaverville, Calif., 285 p. http://odp.trrp.net/FileDatabase/Documents/IAP_1.01.pdf.
- Trinity River Taskforce, 1970, Task force findings and recommendations on sediment problems in the Trinity River near Lewiston and a summary of the watershed investigation: California Resources Agency, 29 p.
- Trinity River Taskforce, 1979, Delta formations at the mouths of tributary streams: California Resources Agency, 6 p.
- U.S. Bureau of Land Management, 1995, Mainstem Trinity River watershed analysis: Redding Resource Area, 74 p. http://www.fs.usda.gov/Internet/FSE_DOCUMENTS/stelprdb5380151.pdf.
- U.S. Department of the Interior, 2000, Record of Decision, Trinity River mainstem fishery restoration, Final Environmental Impact Statement/Environmental Impact Report, 43p. <http://odp.trrp.net/FileDatabase/Documents/Trinity%20River%20Record%20of%20Decision%2012-19-00.pdf>.
- U.S. Fish and Wildlife Service, 1980, Environmental impact statement on the management of river flows to mitigate the loss of the anadromous fishery of the Trinity River, California, Volume I: Sacramento, California, 229 p. <http://odp.trrp.net/FileDatabase/Documents/Enviro%20Impact%20Statement%20Vol.%201%201980b1.pdf>.
- U.S. Fish and Wildlife Service, 1989, Annual report, Klamath River fisheries assessment program juvenile salmonid production monitoring, 1988: Report No. AFF-FAO-89-12: Arcata, Calif., U.S. Fish and Wildlife Service, 19 p. http://odp.trrp.net/FileDatabase/Documents/Juvenile_Salmonid_Monitoring_on_the_Klamath_and_Trinity_Rivers_-_19881.pdf.

- U.S. Fish and Wildlife Service, 1994, Restoration of the mainstem Trinity River background report, Trinity River Restoration Program: Weaverville, Calif., U.S. Fish and Wildlife Service, 14 p. <http://odp.trrp.net/FileDatabase/Documents/Restoration%20of%20the%20Mainstem%20TR%20Background%20Report%2019941.pdf>.
- U.S. Fish and Wildlife Service and Hoopa Valley Tribe, 1999, Trinity River Flow Evaluation Study: Final Report, 310 p. [http://odp.trrp.net/FileDatabase/Documents/USFWS%20HVT%201999%20\(June%20FINAL%20-%20locked\)%20Trinity%20River%20Flow%20Evaluation%20Final%20Report1.pdf](http://odp.trrp.net/FileDatabase/Documents/USFWS%20HVT%201999%20(June%20FINAL%20-%20locked)%20Trinity%20River%20Flow%20Evaluation%20Final%20Report1.pdf).
- Wallick, J.R., Anderson, S.W., Cannon, Charles, and O'Connor, J.E., 2010, Channel change and bed-material transport in the lower Chetco River, Oregon: U.S. Geological Survey Scientific Investigations Report 2010-5065, 68 p. <http://pubs.usgs.gov/sir/2010/5065/pdf/sir20105065.pdf>.
- Wallick, J.R., O'Connor, J.E., Anderson, S., Keith, M., Cannon, C., and Risley, J.C., 2011, Channel change and bed-material transport in the Umpqua River basin, Oregon: U.S. Geological Survey Scientific Investigations Report 2011-5041, 112 p. <http://pubs.usgs.gov/sir/2011/5041/pdf/sir20115041.pdf>.
- Wilcock, P.R., Kondolf, G.M., Barta, A.F., Matthews, W.V.G., and Shea, C.C., 1995, Spawning gravel flushing during trial reservoir releases on the Trinity River: Field observations and recommendations for sediment maintenance flushing flows: Prepared for the U.S. Fish Wildlife Service, Sacramento, Calif., Cooperative Agreements 14-16-0001-91514 and 14-16-0001-91515, 96 p. http://www.fws.gov/arcata/fisheries/reports/technical/Spawning_Gravel_Flushing_During_Trial_Reservoir_Releases_on_the_Trinity_River_Field_Observations_and_Recommendations_for_Sediment_Maintenance_Flushing_Flows.pdf.
- Woolpert, Inc., 2010, Trinity River bathymetry, airborne laser data and photogrammetric DTM merging, verification and certification: Report prepared for Trinity River Restoration Program, U.S. Bureau of Reclamation Task Order R10PD40022, 41 p. http://odp.trrp.net/FileDatabase/Documents/TRRP_2009_DTM&ORTHO1.pdf.
- Zilliani, L. and Surian N., 2012, Evolutionary trajectory of channel morphology and controlling factors in a large gravel-bed river: *Geomorphology*, v. 173-174, p. 104-117. doi:10.1016/j.geomorph.2012.06.001.

Appendix A

Table A1. Summary of the areal extent of geomorphic features estimated in 1980, Trinity River downstream from Lewiston Dam in California.

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Lewiston (reach 1) (m ²)	Sawmill (reach 2) (m ²)	Rush Creek (reach 3) (m ²)	Stott (reach 4) (m ²)	Poker Bar Canyon (reach 5) (m ²)	Vitzhum (reach 6) (m ²)	Reading Creek (reach 7) (m ²)	Dutton Creek (reach 8) (m ²)
Uplands	93,491	647,047	1,347,078	658,070	703,090	819,531	1,131,225	479,288
Riparian	97,436	368,627	632,002	300,784	345,756	425,715	444,294	161,774
Island	0	33,603	24,113	1,858	17,664	2,411	2,342	0
Pre-dam floodplain	58,092	238,509	379,402	181,717	196,437	291,897	315,534	130,427
Constructed floodplain	0	0	0	0	0	0	0	0
Post-dam topographic bench	35,326	89,074	215,249	97,980	121,210	115,473	124,726	28,689
Stable bars	1,223	2,919	3,494	16,398	10,446	15,934	1,301	1,542
Riparian wetland	2,796	4,522	9,744	2,832	0	0	392	1,114
Other	0	0	0	0	0	0	0	0
Active channel	51,386	170,623	181,626	145,929	211,395	163,236	162,999	104,778
Baseflow wetted channel	46,227	145,914	156,354	120,763	181,457	133,955	147,053	96,019
Exposed bedrock	186	439	0	0	651	53	570	496
Alcove	183	1,416	447	5,910	306	1,392	746	102
Side channel	0	10,356	7,651	212	7,494	1,157	1,857	508
Split-flow channel	932	7,654	4,278	10,777	11,763	11,813	4,081	2,581
Aquatic wetland	0	380	0	0	0	0	0	0
Constructed secondary water features	0	7,161	0	0	0	0	0	0
Active bars	680	1,726	12,155	8,266	9,723	14,866	8,471	5,072
Other	3,179	2,736	741	0	0	0	221	0
Lateral bar	1,660	3,638	13,335	20,654	14,755	19,143	8,672	6,078
Medial bar	243	1,007	2,314	4,010	5,414	11,658	1,099	536
Constructed bar	0	293	2,495	0	0	0	0	0
Additional channel attributes								
Baseflow-channel length	1,586	5,276	6,369	4,559	6,929	5,986	6,794	4,187
Shoreline length	3,613	14,359	15,643	11,312	17,425	14,550	15,314	9,341
Mean baseflow-channel width	29.1	27.7	24.5	26.5	26.2	22.4	21.6	22.9
Mean active-channel width	32.4	32.3	28.5	32.0	30.5	27.3	24.0	25.0

Table A1. Summary of the areal extent of geomorphic features estimated in 1980, Trinity River downstream from Lewiston Dam in California.—Continued

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Dutch Creek (reach 9) (m ²)	Oregon Gulch (reach 10) (m ²)	Canyon Creek (reach 11) (m ²)	Lime Point (reach 12) (m ²)	Pear Tree (reach 13) (m ²)	Summary		
						Study reach (m ²)	Proportion of total (percent)	Relative proportion (percent)
Uplands	1,723,956	511,038	1,031,079	921,186	364,453	10,430,532	60.4	—
Riparian	916,591	256,145	501,117	392,207	166,376	5,008,825	29.0	—
Island	14,459	2,160	0	0	0	98,610	—	2.0
Pre-dam floodplain	632,919	186,786	372,951	245,322	125,144	3,355,138	—	67.0
Constructed floodplain	0	0	0	0	0	0	—	0.0
Post-dam topographic bench	242,608	62,515	113,012	138,037	39,441	1,423,338	—	28.4
Stable bars	16,179	4,684	7,141	8,848	1,791	91,900	—	1.8
Riparian wetland	10,426	0	8,014	0	0	39,839	—	0.8
Other	0	0	0	0	0	0	—	0.0
Active channel	216,776	61,350	136,630	131,820	79,371	1,817,918	10.5	—
Baseflow wetted channel	197,449	53,826	122,219	114,195	76,113	1,591,545	—	87.5
Exposed bedrock	77	0	0	0	342	2,814	—	0.2
Alcove	1,987	1,066	289	717	79	14,640	—	0.8
Side channel	2,295	0	0	195	0	31,725	—	1.7
Split-flow channel	5,470	2,920	848	5,630	878	69,627	—	3.8
Aquatic wetland	460	0	347	114	0	1,301	—	0.1
Constructed secondary water features	0	0	0	0	0	7,161	—	0.4
Active bars	9,037	3,538	12,927	10,969	1,959	99,389	—	5.5
Other	0	0	0	0	0	6,877	—	0.4
Lateral bar	23,518	3,433	14,995	9,023	3,561	142,464	—	7.8
Medial bar	1,699	4,789	5,073	10,794	190	48,826	—	2.7
Constructed bar	0	0	0	0	0	2,789	—	0.2
Additional channel attributes								
Baseflow-channel length	8,679	2,680	4,714	4,006	2,834	64,599	—	—
Shoreline length	19,726	6,243	9,843	9,375	5,991	152,736	—	—
Mean baseflow-channel width	22.8	20.1	25.9	28.5	27.2	25.0	—	—
Mean active-channel width	25.0	22.9	29.0	32.9	28.0	28.4	—	—

Table A2. Summary of the areal extent of geomorphic features estimated in 1997, Trinity River downstream from Lewiston Dam in California.[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Lewiston (reach 1) (m ²)	Sawmill (reach 2) (m ²)	Rush Creek (reach 3) (m ²)	Stott (reach 4) (m ²)	Poker Bar Canyon (reach 5) (m ²)	Vizhum (reach 6) (m ²)	Reating Creek (reach 7) (m ²)	Dutton Creek (reach 8) (m ²)
Uplands	93,608	623,198	1,341,307	660,063	703,295	816,500	1,131,285	478,180
Riparian	78,701	360,596	588,401	292,450	323,602	399,224	409,184	151,584
Island	5,125	57,845	37,106	25,694	26,812	10,735	1,612	1,059
Pre-dam floodplain	56,096	228,427	360,925	175,645	184,264	280,898	306,883	125,413
Constructed floodplain	0	0	891	0	10,640	0	9,254	0
Post-dam topographic bench	16,941	68,212	171,503	69,539	92,157	95,598	87,085	24,587
Stable bars	538	3,936	9,275	17,813	9,694	11,993	2,184	524
Riparian wetland	0	2,176	8,701	3,759	35	0	2,166	0
Other	0	0	0	0	0	0	0	0
Active channel	70,005	202,481	214,037	152,269	233,344	192,508	199,276	116,059
Baseflow wetted channel	45,514	161,146	174,055	127,409	187,261	155,202	170,256	103,977
Exposed bedrock	859	975	53	283	1,300	197	1,493	331
Alcove	7,025	4,533	5,349	917	489	416	3,402	484
Side channel	1,726	22,838	15,071	11,315	18,795	12,009	2,162	1,454
Split-flow channel	8,929	7,510	5,202	4,030	13,264	4,491	5,470	1,673
Aquatic wetland	0	76	0	0	0	109	0	0
Constructed secondary water features	8,234	19,210	9,285	10,919	11,592	0	0	0
Active bars	3,624	2,182	13,920	8,316	12,036	20,085	16,439	8,139
Other	2,327	3,222	388	0	199	0	55	0
Lateral bar	1,332	4,627	11,913	21,451	7,948	22,842	16,834	6,029
Medial bar	2,831	1,491	11,281	4,678	13,782	9,236	1,789	2,635
Constructed bar	448	590	1,869	0	0	0	587	0
Additional channel attributes								
Baseflow-channel length	1,586	5,276	6,369	4,559	6,929	5,986	6,794	4,187
Shoreline length	6,379	17,369	18,375	11,651	20,626	15,616	16,083	9,771
Mean baseflow-channel width	36.5	32.5	30.0	30.0	31.2	28.4	26.5	26.0
Mean active-channel width	38.7	32.9	35.3	32.8	33.0	31.8	29.0	28.5

Table A2. Summary of the areal extent of geomorphic features estimated in 1997, Trinity River downstream from Lewiston Dam in California.—Continued

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Dutch Creek (reach 9) (m ²)	Oregon Gulch (reach 10) (m ²)	Canyon Creek (reach 11) (m ²)	Lime Point (reach 12) (m ²)	Pear Tree (reach 13) (m ²)	Summary		
						Study reach (m ²)	Proportion of total (percent)	Relative proportion (percent)
Uplands	1,722,563	505,425	1,027,867	918,801	364,941	10,387,034	60.2	—
Riparian	847,880	229,782	481,825	378,284	156,179	4,697,692	27.2	—
Island	0	17,439	904	0	0	184,332	—	3.9
Pre-dam floodplain	619,005	173,264	359,810	239,678	121,465	3,231,774	—	68.8
Constructed floodplain	21,784	0	3,163	1,190	2,011	48,935	—	1.0
Post-dam topographic bench	192,476	34,764	103,673	121,691	31,314	1,109,540	—	23.6
Stable bars	8,215	3,676	4,001	15,513	1,389	88,752	—	1.9
Riparian wetland	6,399	640	10,273	212	0	34,360	—	0.7
Other	0	0	0	0	0	0	—	0.0
Active channel	286,937	94,876	157,611	148,128	89,080	2,156,612	12.5	—
Baseflow wetted channel	239,904	68,006	123,924	123,060	81,781	1,761,495	—	81.7
Exposed bedrock	229	0	0	0	422	6,141	—	0.3
Alcove	2,760	1,418	2,034	1,726	828	31,382	—	1.5
Side channel	1,096	6,283	395	1,043	0	94,186	—	4.4
Split-flow channel	10,188	2,265	8,402	1,692	1,011	74,128	—	3.4
Aquatic wetland	0	106	0	1,900	102	2,292	—	0.1
Constructed secondary water features	0	3,460	0	0	0	62,700	—	2.9
Active bars	32,760	16,798	22,857	18,706	4,936	180,797	—	8.4
Other	0	0	0	0	0	6,191	—	0.3
Lateral bar	32,419	11,205	24,202	31,841	6,325	198,968	—	9.2
Medial bar	8,556	9,268	2,656	2,378	0	70,581	—	3.3
Constructed bar	0	0	0	0	0	3,493	—	0.2
Additional channel attributes								
Baseflow-channel length	8,679	2,680	4,714	4,006	2,834	64,599	—	—
Shoreline length	20,239	7,861	11,003	9,196	6,186	170,354	—	—
Mean baseflow-channel width	29.8	29.0	31.4	31.5	30.2	30.2	—	—
Mean active-channel width	33.5	35.1	36.5	36.1	31.9	33.5	—	—

Table A3. Summary of the areal extent of geomorphic features estimated in 2001, Trinity River downstream from Lewiston Dam in California.

[Abbreviations: m², square meter; —, no data]

Geomorphic Reach	Lewiston (reach 1) (m ²)	Sawmill (reach 2) (m ²)	Rush Creek (reach 3) (m ²)	Stott (reach 4) (m ²)	Poker Bar Canyon (reach 5) (m ²)	Vizhum (reach 6) (m ²)	Reading Creek (reach 7) (m ²)	Dutton Creek (reach 8) (m ²)
Uplands	93,595	625,515	1,342,284	659,740	702,753	814,607	1,131,561	478,335
Riparian	76,169	359,213	584,947	292,682	321,992	400,674	402,091	148,628
Island	4,899	58,490	36,112	25,833	26,250	9,108	1,045	1,054
Pre-dam floodplain	54,734	228,963	359,569	172,801	184,556	281,024	303,525	123,893
Constructed floodplain	0	0	952	0	10,394	0	9,175	0
Post-dam topographic bench	16,094	65,586	167,455	69,858	88,463	91,776	81,458	23,171
Stable bars	443	4,185	13,239	18,503	12,329	18,766	6,405	511
Riparian wetland	0	1,799	7,621	5,688	0	0	482	0
Other	0	190	0	0	0	0	0	0
Active channel	72,549	201,466	221,378	152,360	235,496	194,765	206,178	118,793
Baseflow wetted channel	47,452	162,887	176,786	130,451	194,087	156,081	179,930	107,210
Exposed bedrock	667	888	39	355	1,088	199	1,427	411
Alcove	9,405	4,597	1,412	1,068	385	1,104	1,508	772
Side channel	0	20,242	17,129	11,092	18,980	7,765	1,349	1,430
Split-flow channel	8,541	6,945	6,444	4,032	12,698	6,709	4,844	1,592
Aquatic wetland	0	0	523	0	0	0	121	0
Constructed secondary water features	6,919	19,125	4,580	10,718	9,290	280	0	0
Active bars	3,898	3,066	18,681	5,363	7,964	22,907	16,938	7,379
Other	2,586	2,840	364	0	294	0	61	0
Lateral bar	1,375	5,765	26,092	19,795	8,080	27,687	21,475	5,690
Medial bar	2,965	1,486	5,828	4,070	12,213	13,986	1,869	2,201
Constructed bar	417	584	2,773	0	0	861	0	0
Additional channel attributes								
Baseflow-channel length	1,586	5,276	6,369	4,559	6,929	5,986	6,794	4,187
Shoreline length	6,103	17,491	17,740	11,605	20,266	15,892	15,539	9,714
Mean baseflow-channel width	37.6	32.7	29.7	30.5	31.8	29.6	27.7	26.6
Mean active-channel width	40.1	33.2	35.7	33.0	33.0	33.5	30.3	28.7

Table A3. Summary of the areal extent of geomorphic features estimated in 2001, Trinity River downstream from Lewiston Dam in California.—Continued

[Abbreviations: m², square meter; —, no data]

Geomorphic Reach	Summary							
	Dutch Creek (reach 9) (m ²)	Oregon Gulch (reach 10) (m ²)	Canyon Creek (reach 11) (m ²)	Lime Point (reach 12) (m ²)	Pear Tree (reach 13) (m ²)	Study reach (m ²)	Proportion of total (percent)	Relative proportion (percent)
Uplands	1,721,904	504,326	1,024,853	919,134	365,065	10,383,672	60.2	—
Riparian	844,159	231,460	480,820	375,344	156,342	4,674,523	27.1	—
Island	0	0	0	0	0	162,790	—	3.5
Pre-dam floodplain	620,349	182,438	357,810	238,006	121,553	3,229,220	—	69.1
Constructed floodplain	20,719	3,216	2,611	1,323	1,910	50,300	—	1.1
Post-dam topographic bench	187,707	39,581	101,791	110,878	31,146	1,074,962	—	23.0
Stable bars	8,791	6,225	6,034	24,968	1,733	122,133	—	2.6
Riparian wetland	6,593	0	9,533	169	0	31,886	—	0.7
Other	0	0	3,042	0	0	3,232	—	0.1
Active channel	291,267	92,683	160,988	150,736	88,793	2,187,452	12.7	—
Baseflow wetted channel	246,691	69,027	129,867	126,761	80,392	1,807,622	—	82.6
Exposed bedrock	220	0	0	0	395	5,689	—	0.3
Alcove	694	1,799	1,866	1,295	162	26,065	—	1.2
Side channel	0	0	744	3,892	74	82,697	—	3.8
Split-flow channel	7,887	4,631	0	0	1,666	65,989	—	3.0
Aquatic wetland	52	107	209	61	170	1,241	—	0.1
Constructed secondary water features	0	1,656	6,431	0	0	58,997	—	2.7
Active bars	35,724	17,120	28,303	18,726	5,935	192,004	—	8.8
Other	0	0	0	0	0	6,145	—	0.3
Lateral bar	39,292	16,861	30,942	38,840	7,524	249,418	—	11.4
Medial bar	5,223	6,483	3,395	4,855	144	64,719	—	3.0
Constructed bar	6,893	438	1,151	0	0	13,115	—	0.6
Additional channel attributes								
Baseflow-channel length	8,679	2,680	4,714	4,006	2,834	64,599	—	—
Shoreline length	19,148	6,787	10,379	9,196	6,116	165,976	—	—
Mean baseflow-channel width	30.0	29.9	30.9	33.6	30.0	30.8	—	—
Mean active-channel width	34.1	36.3	37.1	38.3	32.1	34.3	—	—

Table A4. Summary of the areal extent of geomorphic features estimated in 2006, Trinity River downstream from Lewiston Dam in California.

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Lewiston (reach 1) (m ²)	Sawmill (reach 2) (m ²)	Rush Creek (reach 3) (m ²)	Stott (reach 4) (m ²)	Poker Bar Canyon (reach 5) (m ²)	Vitzhum (reach 6) (m ²)	Reading Creek (reach 7) (m ²)	Dutton Creek (reach 8) (m ²)
Uplands	93,560	625,205	1,340,891	658,894	702,875	813,123	1,131,437	478,610
Riparian	75,092	355,981	582,693	291,163	311,115	389,163	395,585	149,411
Island	2,283	52,729	34,463	23,878	21,990	9,910	1,111	437
Pre-dam floodplain	53,847	225,754	357,206	170,662	183,195	272,323	301,360	126,072
Constructed floodplain	0	0	1,177	0	10,519	0	8,897	0
Post-dam topographic bench	17,671	69,289	162,196	69,561	85,730	89,967	77,639	22,171
Stable bars	1,011	4,644	19,141	18,780	9,681	16,963	6,136	683
Riparian wetland	279	3,566	8,511	8,281	0	0	442	48
Other	0	0	0	0	0	0	0	0
Active channel	73,662	204,976	225,768	154,726	246,252	205,004	213,033	117,981
Baseflow wetted channel	48,594	164,457	177,734	129,343	201,591	169,551	186,894	108,836
Exposed bedrock	515	428	50	262	854	248	1,338	390
Alcove	10,142	4,983	2,924	940	3,280	1,399	2,048	110
Side channel	0	17,826	18,352	12,494	16,809	6,309	1,497	1,038
Split-flow channel	8,070	9,912	7,169	4,711	12,869	8,019	8,189	2,028
Aquatic wetland	0	305	192	0	23	276	200	597
Constructed secondary water features	7,257	18,155	6,444	11,418	10,084	0	0	0
Active bars	3,254	3,560	19,080	6,975	10,596	19,202	12,827	4,981
Other	3,088	3,504	267	0	230	0	41	0
Lateral bar	1,284	5,533	25,365	20,042	10,002	23,740	13,531	3,134
Medial bar	2,981	2,671	12,855	5,713	10,275	12,425	5,432	2,530
Constructed bar	3,078	688	1,013	0	0	0	0	0
Additional channel attributes								
Baseflow-channel length	1,581	5,242	6,323	4,547	6,902	5,982	6,768	4,160
Shoreline length	5,977	17,183	18,353	11,715	19,981	15,608	16,277	9,939
Mean baseflow-channel width	38.0	33.8	31.3	30.8	32.8	31.9	29.8	27.4
Mean active-channel width	40.1	34.5	37.2	33.8	34.3	35.1	32.0	29.2

Table A4. Summary of the areal extent of geomorphic features estimated in 2006, Trinity River downstream from Lewiston Dam in California.—Continued

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Summary									
	Dutch Creek (reach 9) (m ²)	Oregon Gulch (reach 10) (m ²)	Canyon Creek (reach 11) (m ²)	Lime Point (reach 12) (m ²)	Pear Tree (reach 13) (m ²)	Study reach (m ²)	Proportion of total (percent)	Relative proportion (percent)		
Uplands	1,723,242	503,565	1,019,735	919,929	364,683	10,375,749	60.2	—		
Riparian	837,908	226,454	479,394	366,877	154,279	4,615,115	26.8	—		
Island	0	18,599	0	482	0	165,881	—	3.6		
Pre-dam floodplain	612,217	172,032	315,728	237,094	120,577	3,148,067	—	68.2		
Constructed floodplain	19,045	0	60,142	1,441	1,675	102,895	—	2.2		
Post-dam topographic bench	180,311	30,442	84,190	103,134	30,115	1,022,418	—	22.2		
Stable bars	16,015	5,297	7,875	24,727	1,911	132,864	—	2.9		
Riparian wetland	10,321	83	11,459	0	0	42,991	—	0.9		
Other	0	0	0	0	0	0	—	0.0		
Active channel	296,201	98,157	166,379	158,407	91,238	2,251,783	13.1	—		
Baseflow wetted channel	268,495	78,995	151,253	131,868	84,095	1,901,707	—	84.5		
Exposed bedrock	198	0	0	0	375	4,659	—	0.2		
Alcove	946	876	636	420	256	28,959	—	1.3		
Side channel	227	3,440	982	2,649	93	81,717	—	3.6		
Split-flow channel	8,164	2,978	1,899	5,472	744	80,224	—	3.6		
Aquatic wetland	225	56	0	475	337	2,686	—	0.1		
Constructed secondary water features	0	2,895	0	0	1,294	57,547	—	2.6		
Active bars	17,946	11,812	11,610	17,523	5,338	144,703	—	6.4		
Other	0	0	0	0	0	7,130	—	0.3		
Lateral bar	30,659	14,643	14,539	36,022	7,250	205,744	—	9.1		
Medial bar	3,302	2,467	4,945	6,227	0	71,823	—	3.2		
Constructed bar	5,399	0	0	0	0	10,177	—	0.5		
Additional channel attributes										
Baseflow-channel length	8,666	2,753	4,666	3,985	2,825	64,401	—	—		
Shoreline length	18,818	7,436	10,548	9,446	6,051	167,333	—	—		
Mean baseflow-channel width	32.4	30.9	36.1	36.9	31.2	32.6	—	—		
Mean active-channel width	34.5	35.2	38.8	41.3	33.1	35.3	—	—		

Table A5. Summary of the areal extent of geomorphic features estimated in 2009, Trinity River downstream from Lewiston Dam in California.[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Lewiston (reach 1) (m ²)	Sawmill (reach 2) (m ²)	Rush Creek (reach 3) (m ²)	Stott (reach 4) (m ²)	Poker Bar Canyon (reach 5) (m ²)	Vizthum (reach 6) (m ²)	Reading Creek (reach 7) (m ²)	Dutton Creek (reach 8) (m ²)
Uplands	93,253	624,100	1,339,419	657,647	703,078	812,104	1,130,735	478,994
Riparian	76,524	351,357	580,028	292,074	312,265	385,277	396,403	148,408
Island	3,847	58,173	39,082	24,365	22,094	21,442	1,141	427
Pre-dam floodplain	42,684	224,356	332,654	170,218	183,212	254,756	299,903	125,059
Constructed floodplain	24,257	1,571	27,786	0	10,418	23,051	9,166	0
Post-dam topographic bench	3,558	61,974	151,994	68,644	86,603	68,296	77,708	22,485
Stable bars	1,271	3,908	21,042	20,607	9,938	17,659	7,653	437
Riparian wetland	906	1,376	7,469	8,241	0	73	833	0
Other	0	0	0	0	0	0	0	0
Active channel	72,536	210,664	229,973	155,061	244,898	208,769	212,501	118,570
Baseflow wetted channel	49,886	158,703	174,161	132,057	201,106	170,100	188,775	108,287
Exposed bedrock	292	425	420	169	1,629	263	1,361	465
Alcove	513	8,326	4,579	769	544	2,831	1,020	224
Side channel	8,065	17,400	21,558	11,739	19,325	13,745	1,736	922
Split-flow channel	6,601	9,535	6,826	4,623	11,376	7,921	7,393	2,449
Aquatic wetland	0	277	166	0	0	0	420	731
Constructed secondary water features	7,923	21,788	12,600	10,180	8,882	9,739	0	0
Active bars	4,659	12,555	21,911	5,705	10,918	13,910	11,795	5,491
Other	2,520	3,442	351	0	0	0	0	0
Lateral bar	2,177	11,070	35,599	20,468	7,427	18,431	13,345	3,736
Medial bar	3,754	5,393	7,354	5,843	13,429	13,138	6,103	2,192
Constructed bar	1,104	7,512	3,444	0	0	0	0	0
Additional channel attributes								
Baseflow-channel length	1,586	5,276	6,369	4,559	6,929	5,986	6,794	4,187
Shoreline length	5,907	18,559	19,492	11,828	20,222	17,919	16,047	9,949
Mean baseflow-channel width	38.2	33.0	29.9	31.3	33.1	32.1	30.1	27.2
Mean active-channel width	41.2	35.4	36.3	34.0	34.6	34.5	31.9	29.3

Table A5. Summary of the areal extent of geomorphic features estimated in 2009, Trinity River downstream from Lewiston Dam in California.—Continued

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Dutch Creek (reach 9) (m ²)	Oregon Gulch (reach 10) (m ²)	Canyon Creek (reach 11) (m ²)	Lime Point (reach 12) (m ²)	Pear Tree (reach 13) (m ²)	Summary		
						Study reach (m ²)	Proportion of total (percent)	
Relative proportion (percent)								
Uplands	1,721,861	502,653	1,017,454	919,435	364,147	10,364,880	60.1	—
Riparian	843,387	227,031	480,700	361,294	150,537	4,605,284	26.7	—
Island	0	18,978	0	584	0	190,134	—	4.1
Pre-dam floodplain	611,970	172,203	306,312	223,873	109,171	3,056,371	—	66.4
Constructed floodplain	19,484	0	77,343	29,730	13,732	236,537	—	5.1
Post-dam topographic bench	182,536	30,378	75,809	94,536	25,768	950,289	—	20.6
Stable bars	17,840	5,369	8,737	12,507	1,865	128,833	—	2.8
Riparian wetland	11,557	103	12,498	65	0	43,121	—	0.9
Other	0	0	0	0	0	0	—	0.0
Active channel	292,120	98,630	167,157	164,484	95,516	2,270,878	13.2	—
Baseflow wetted channel	267,211	78,859	150,830	138,085	87,774	1,905,833	—	83.9
Exposed bedrock	78	0	0	0	332	5,433	—	0.2
Alcove	683	307	1,389	1,036	295	22,517	—	1.0
Side channel	154	2,507	762	4,529	263	102,706	—	4.5
Split-flow channel	8,019	3,491	1,143	3,443	743	73,564	—	3.2
Aquatic wetland	257	635	0	370	426	3,283	—	0.1
Constructed secondary water features	0	2,745	0	698	1,299	75,854	—	3.3
Active bars	15,719	12,831	13,032	17,020	5,684	151,230	—	6.7
Other	0	0	0	0	0	6,313	—	0.3
Lateral bar	30,316	17,085	16,232	27,110	7,549	210,546	—	9.3
Medial bar	3,243	1,114	5,537	2,417	0	69,516	—	3.1
Constructed bar	6,383	0	0	0	0	18,443	—	0.8
Additional channel attributes								
Baseflow-channel length	8,679	2,680	4,714	4,006	2,834	64,599	—	—
Shoreline length	18,996	7,155	10,505	10,030	6,181	172,789	—	—
Mean baseflow-channel width	32.2	30.2	36.2	36.9	32.3	32.5	—	—
Mean active-channel width	34.0	34.9	39.2	41.2	34.3	35.4	—	—

Table A6. Summary of the areal extent of geomorphic features estimated in 2011, Trinity River downstream from Lewiston Dam in California.

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Lewiston (reach 1) (m ²)	Sawmill (reach 2) (m ²)	Rush Creek (reach 3) (m ²)	Stott (reach 4) (m ²)	Poker Bar Canyon (reach 5) (m ²)	Vizthum (reach 6) (m ²)	Reading Creek (reach 7) (m ²)	Dutton Creek (reach 8) (m ²)
Uplands	93,171	624,917	1,316,188	657,913	703,261	813,700	1,131,927	479,191
Riparian	77,863	346,649	586,145	292,870	316,440	379,657	390,107	149,400
Island	4,223	26,913	48,684	24,433	21,083	19,073	1,134	332
Pre-dam floodplain	43,067	210,161	304,952	170,751	184,135	221,791	259,215	126,018
Constructed floodplain	25,062	47,573	57,125	0	10,316	55,168	45,366	0
Post-dam topographic bench	3,600	55,557	138,706	68,202	87,018	68,980	74,154	22,289
Stable bars	1,199	5,212	24,350	21,279	13,888	14,519	9,105	761
Riparian wetland	712	1,234	12,327	8,205	0	126	1,134	0
Other	0	0	0	0	0	0	0	0
Active channel	71,279	214,564	250,085	154,000	240,539	213,255	218,156	117,355
Baseflow wetted channel	50,089	161,272	176,684	133,202	199,874	169,494	191,718	107,782
Exposed bedrock	186	339	376	290	914	335	1,366	566
Alcove	714	9,663	8,454	1,116	603	1,450	2,275	331
Side channel	9,560	21,248	27,186	11,218	20,147	15,583	2,134	1,532
Split-flow channel	3,311	7,317	4,235	4,354	10,525	6,573	7,379	1,221
Aquatic wetland	0	562	1,104	0	46	0	0	0
Constructed secondary water features	9,566	27,636	23,128	10,502	9,893	7,715	1,240	0
Active bars	680	1,726	12,155	8,266	9,723	14,866	8,471	5,072
Other	2,499	964	223	66	229	0	39	0
Lateral bar	5,569	14,841	43,878	19,095	10,749	18,153	16,614	3,840
Medial bar	550	3,571	12,294	5,938	11,340	16,186	5,735	2,843
Constructed bar	3,997	9,414	13,036	0	0	483	2,670	0
Additional channel attributes								
Baseflow-channel length	1,586	5,276	6,369	4,559	6,929	5,986	6,794	4,187
Shoreline length	5,810	19,160	21,622	11,649	19,686	17,591	16,003	9,828
Mean baseflow-channel width	34.2	32.6	30.5	31.6	32.3	32.3	30.5	27.1
Mean active-channel width	37.4	35.1	38.0	33.8	33.5	35.6	32.5	29.2

Table A6. Summary of the areal extent of geomorphic features estimated in 2011, Trinity River downstream from Lewiston Dam in California.—Continued

[Abbreviations: m², square meter; —, no data]

Geomorphic reach	Summary						Relative proportion (percent)
	Dutch Creek (reach 9) (m ²)	Oregon Gulch (reach 10) (m ²)	Canyon Creek (reach 11) (m ²)	Lime Point (reach 12) (m ²)	Pear Tree (reach 13) (m ²)	Study reach (m ²)	
Uplands	1,723,568	503,078	1,016,755	919,619	364,493	10,347,782	60.0
Riparian	845,908	224,622	481,982	367,717	152,463	4,611,824	26.7
Island	0	19,053	0	8,855	0	173,783	3.8
Pre-dam floodplain	613,625	169,371	307,041	212,330	110,703	2,933,161	63.6
Constructed floodplain	19,645	0	77,351	40,233	13,534	391,373	8.5
Post-dam topographic bench	183,363	29,954	74,623	86,186	25,630	918,261	19.9
Stable bars	19,154	6,245	10,154	19,910	2,596	148,369	3.2
Riparian wetland	10,121	0	12,814	204	0	46,877	1.0
Other	0	0	0	0	0	0	0.0
Active channel	287,855	100,419	169,659	157,878	93,244	2,288,289	13.3
Baseflow wetted channel	265,027	81,879	146,608	129,733	85,873	1,899,233	83.0
Exposed bedrock	202	30	0	0	297	4,902	0.2
Alcove	845	1,212	1,322	1,481	383	29,850	1.3
Side channel	0	2,331	344	6,678	101	118,062	5.2
Split-flow channel	7,585	3,412	3,272	8,219	779	68,182	3.0
Aquatic wetland	0	0	46	460	461	2,678	0.1
Constructed secondary water features	0	2,331	1,065	7,356	305	100,737	4.4
Active bars	9,037	3,538	18,068	10,969	1,959	104,530	4.6
Other	78	0	0	0	0	4,098	0.2
Lateral bar	30,332	14,468	22,763	24,482	7,946	232,731	10.2
Medial bar	2,941	3,331	5,459	6,090	0	76,278	3.3
Constructed bar	5,520	0	1,190	0	0	36,310	1.6
Additional channel attributes							
Baseflow-channel length	8,679	2,680	4,714	4,006	2,834	64,599	—
Shoreline length	18,901	7,700	10,649	10,787	6,070	175,456	—
Mean baseflow-channel width	31.9	32.4	35.3	36.4	31.7	32.2	—
Mean active-channel width	33.5	36.6	39.2	39.3	33.5	35.2	—

Publishing support provided by the U.S. Geological Survey
Science Publishing Network, Sacramento and Tacoma Publishing Service Centers

For more information concerning the research in this report, contact the

Director, California Water Science Center
U.S. Geological Survey
6000 J Street, Placer Hall
Sacramento, California 95819
<http://ca.water.usgs.gov>

