

Appendix 12. Model Archive Summary for Suspended-Sediment Concentration at U.S. Geological Survey Site 07182510, Neosho River at Burlington, Kansas, during January 1, 2010, through December 31, 2019

This model archive summary summarizes the suspended-sediment concentration (SSC) model developed to compute hourly or daily SSC during January 1, 2010, through December 31, 2019. This model is used concomitantly with other models during this period to calculate concentrations when other explanatory variables are not available for the purposes of load and concentration model calculations. The methods used follow U.S. Geological Survey (USGS) guidance as referenced in relevant Office of Surface Water/Office of Water Quality Technical Memoranda and USGS Techniques and Methods, book 3, chapter C4 (Rasmussen and others, 2009; U.S. Geological Survey, 2016), and other standard USGS methods (Sauer and Turnipseed, 2010; Turnipseed and Sauer, 2010).

Site and Model Information

Site number: 07182510

Site name: Neosho River at Burlington, Kansas

Location: Lat 38°11'40", long 95°44'06" referenced to North American Datum of 1927, in NE 1/4 SW 1/4 sec.26, T.21 S., R.15 E., Coffey County, Kans., hydrologic unit 11070204, on right bank at upstream side of county highway bridge at Burlington, 0.3 mile upstream from Rock Creek, and at mile 338.4.

Equipment: Sutron Satlink data collection platform (DCP), Design Analysis H-350 pressure transducer. Primary gage is the pressure sensor, which is set to agree with the wire-weight readings. The connection to the stream is a standard open-end orifice buried under riprap directly streamward from the gage shelter. Reference gage is a Type-A wire-weight attached to the upstream side of the bridge rail about mid-stream. Check-bar elevation is 41.479 feet above gage datum.

Date model was developed: January 16, 2020

Model calibration data period: March 26, 2007, through March 15, 2019

Model Data

All data were collected using USGS protocols (Wagner and others, 2006; Sauer and Turnipseed, 2010; Turnipseed and Sauer, 2010; U.S. Geological Survey, variously dated) and are stored in the National Water Information System (NWIS) database (<https://doi.org/10.5066/F7P55KJN>; U.S. Geological Survey, 2020). Explanatory variables were

evaluated individually and in combination. Potential explanatory variables included streamflow, water temperature, specific conductance, and turbidity. Seasonal components (sine and cosine variables) were also evaluated as explanatory variables.

The regression model is based on 52 concurrent measurements of discretely collected SSC samples and continuously measured streamflow during March 26, 2007, through March 15, 2019. Discrete samples were collected over a range of streamflows. No samples had concentrations below laboratory detection limits. Identification of potential outliers included any values that exceeded the Cook's D test (Cook, 1977) and any point for which the studentized residual was greater than 3 or less than -3. None of the samples in this dataset were deemed outliers or removed from the model calibration dataset.

Suspended-Sediment Sampling Details

Discrete samples were collected from the downstream side of the bridge or instream within 1,000 feet of the bridge using equal-width-increment, multiple vertical, single vertical, or grab-dip methods following U.S. Geological Survey (2006) and Rasmussen and others (2014). Discrete samples were collected on a semifixed to event-based schedule ranging from one to nine samples per year with a Federal Interagency Sedimentation Project U.S. DH-75P, DH-76 TM, DH-95, or D-95 with a Teflon bottle, cap, and nozzle depth-integrating sampler, a D-96 bag sampler, a weighted-bottle sampler, an open mouth bottle, a DH-81 with a Teflon bottle, cap, and nozzle hand sampler, DH-48, or a grab sample with a Teflon bottle depending on sample location. Samples were analyzed for SSC, loss on ignition, and occasionally 5-point grain size by the USGS Sediment Laboratory in Iowa City, Iowa.

Continuous Data

Streamflow was measured using a nonsubmersible pressure transducer during December 31, 2006, through March 15, 2019 (U.S. Geological Survey, 2018). The continuous streamflow data used were time interpolated values from the continuous time series. If the continuous data were not available, the sample was not included in the dataset. The range of continuous streamflow data (in cubic feet per second) was as follows: maximum 36,500; minimum 5.00; mean 1,710; median 336.

Model Development

Ordinary least squares regression analysis was done using R programming language (R Core Team, 2019) to relate discretely collected SSC to streamflow and other continuously measured data. The distribution of residuals was examined for normality and plots of residuals (the difference between the measured and model calculated values) compared to model calculated SSC were examined for homoscedasticity (departures from zero did not change substantially over the range of model calculated values).

When the SSC and turbidity model could not be applied the streamflow model was selected instead as a good predictor of logarithm base 10 (\log_{10}) (SSC) based on residual plots, relatively high coefficient of determination (R^2), and relatively low model standard percentage error (MSPE).

Model Summary

Summary of final SSC regression analysis at site 07182510:
SSC-based model:

$$\text{Log}_{10}(\text{SSC}) = 0.333 \times \text{Log}_{10}(Q) + 0.806$$

where

SSC = suspended-sediment concentration, in milligrams per liter, and

Q = streamflow, in cubic feet per second.

The log-transformed model may be retransformed to the original units to calculate SSC directly. A bias is introduced in the calculated constituent during retransformation and may be corrected using the Duan's bias correction factor (BCF; Duan, 1983). The calculated BCF is 1.25 for this model and the formula for the retransformed model accounting for BCF is as follows:

$$\text{SSC} = 8.00 \times Q^{0.333}$$

Previously Published Model

No previously published model.

Model Statistics, Data, and Plots

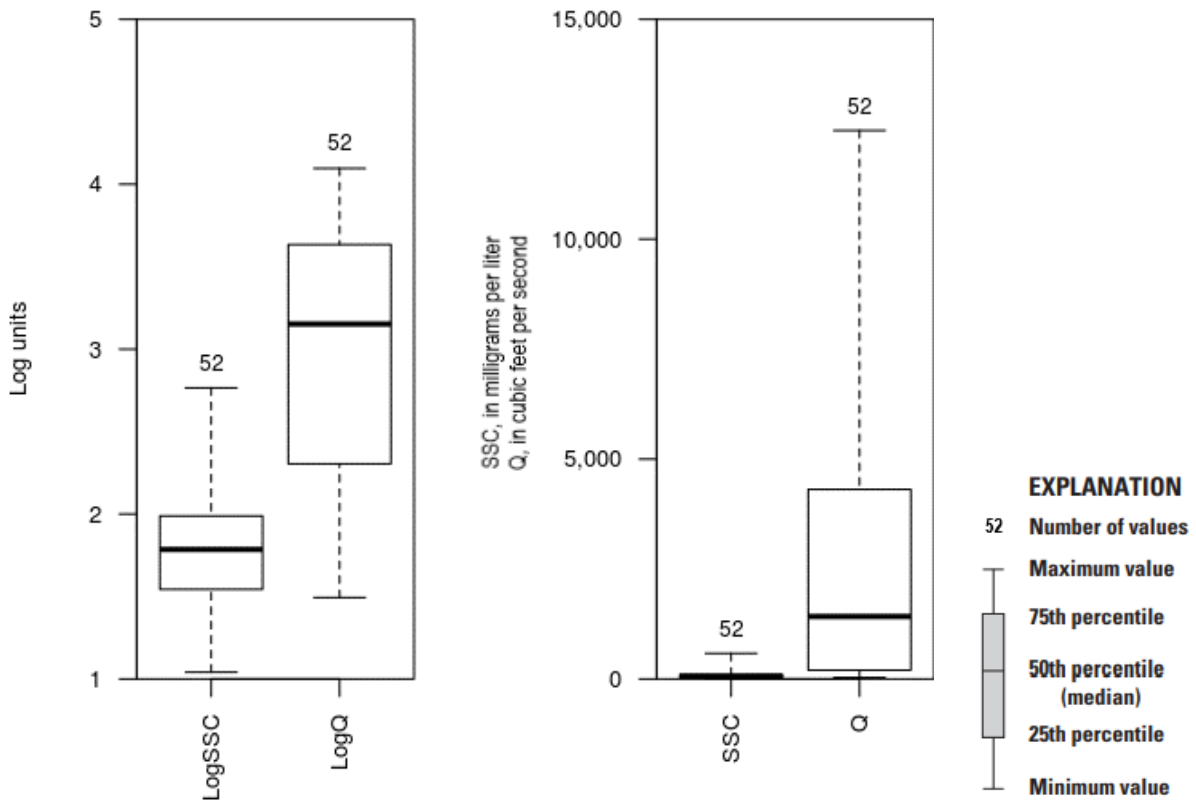
Model

$$\text{Log}(\text{SSC}) = + 0.333 * \text{Log}(Q) + 0.806$$

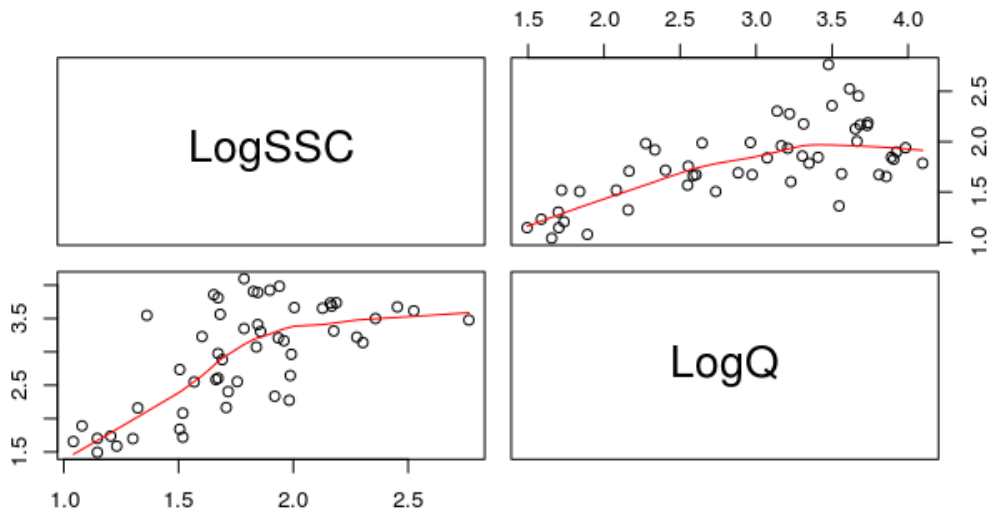
Variable Summary Statistics

	LogSSC	SSC	LogQ	Q
Minimum	1.04	11.0	1.49	31.2
1st Quartile	1.54	35.0	2.30	202.0
Median	1.79	61.0	3.15	1420.0
Mean	1.79	90.0	2.94	2530.0
3d Quartile	1.99	97.5	3.63	4310.0
Maximum	2.76	582.0	4.10	12500.0

Box Plots



Exploratory Plots



Basic Model Statistics

Number of Observations	52
Standard error (RMSE)	0.284
Average Model standard percentage error (MSPE)	70.2
Coefficient of determination (R^2)	0.457
Adjusted Coefficient of Determination (Adj. R^2)	0.446
Bias Correction Factor (BCF)	1.25

Explanatory Variables

	Coefficients	Standard Error	t value	Pr(> t)
(Intercept)	0.806	0.1560	5.17	4.16e-06
LogQ	0.333	0.0513	6.48	3.85e-08

Correlation Matrix

	Intercept	E.vars
Intercept	1.000	-0.968
E.vars	-0.968	1.000

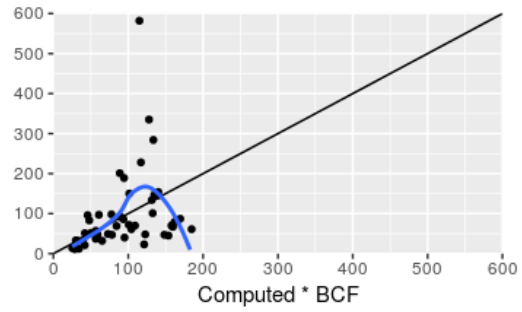
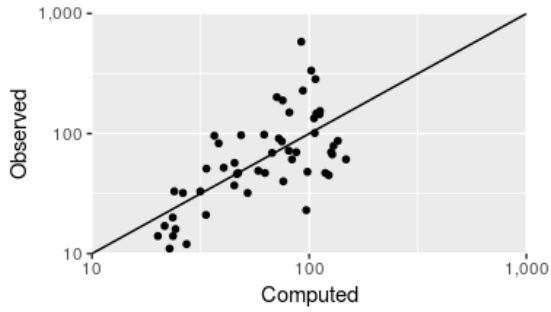
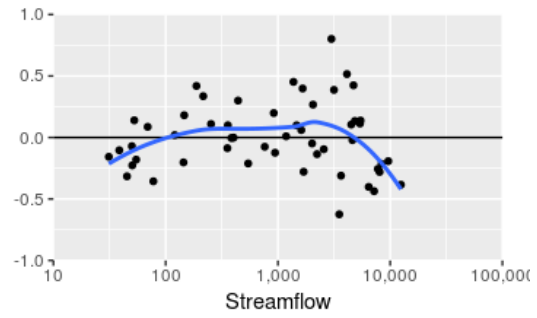
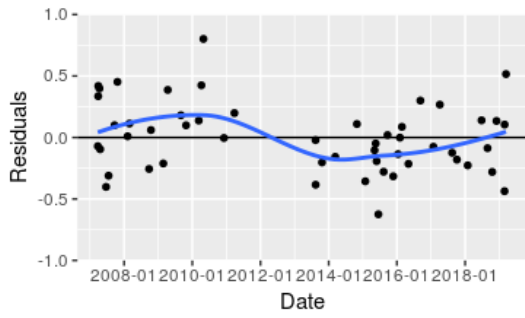
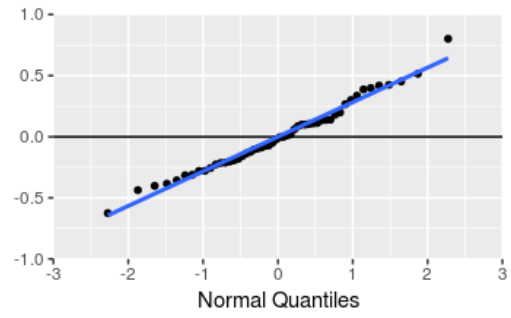
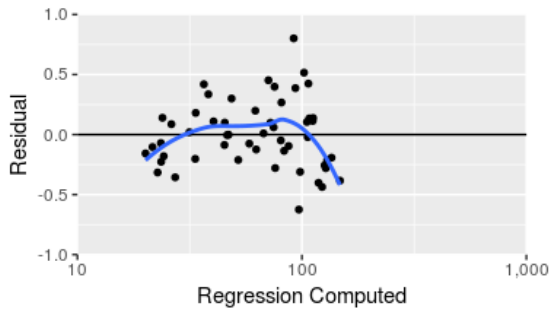
Outlier Test Criteria

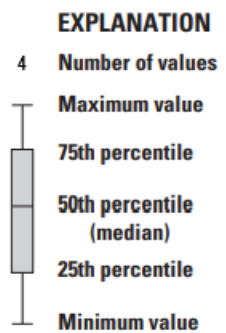
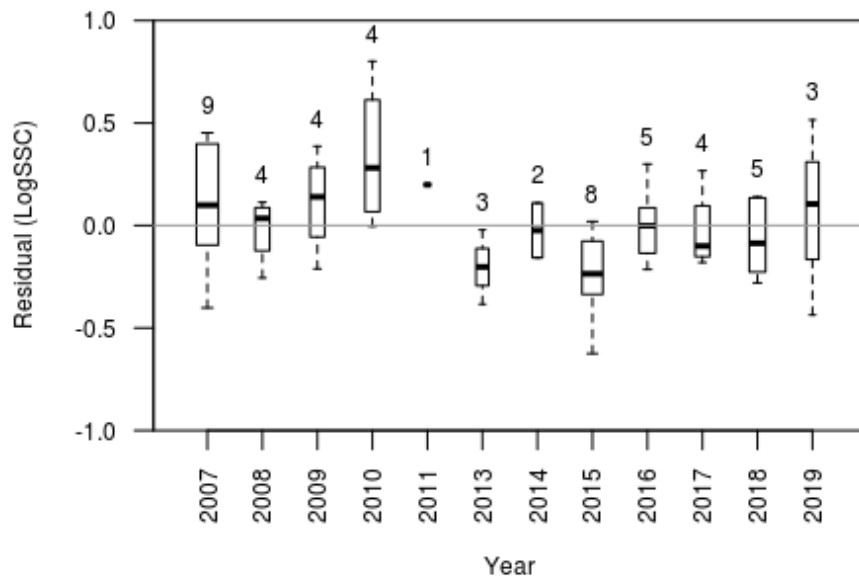
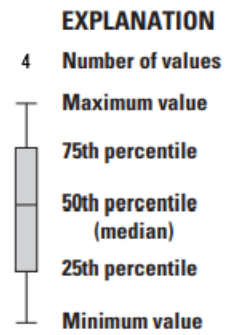
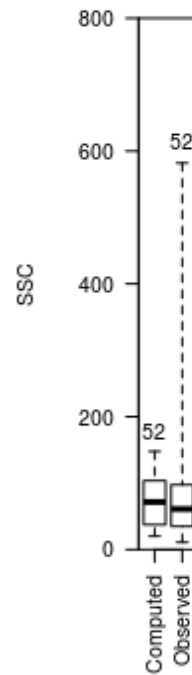
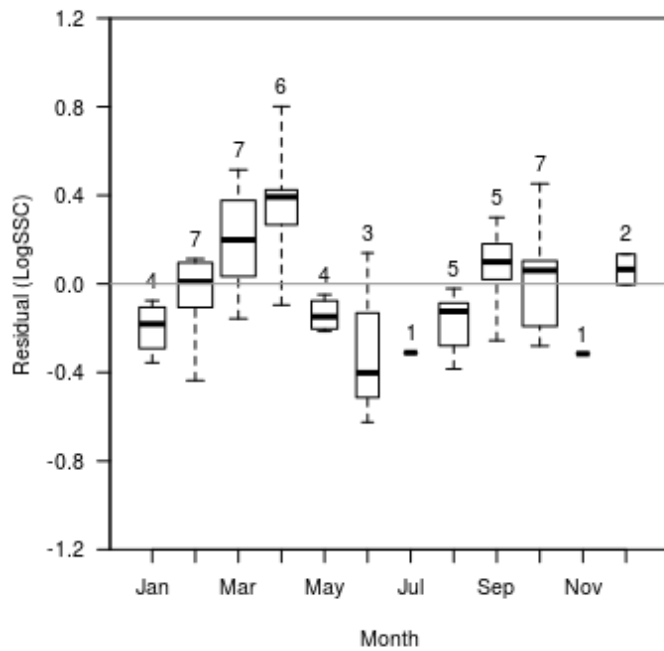
Leverage	Cook's D	DFFITS
0.115	0.194	0.392

Flagged Observations

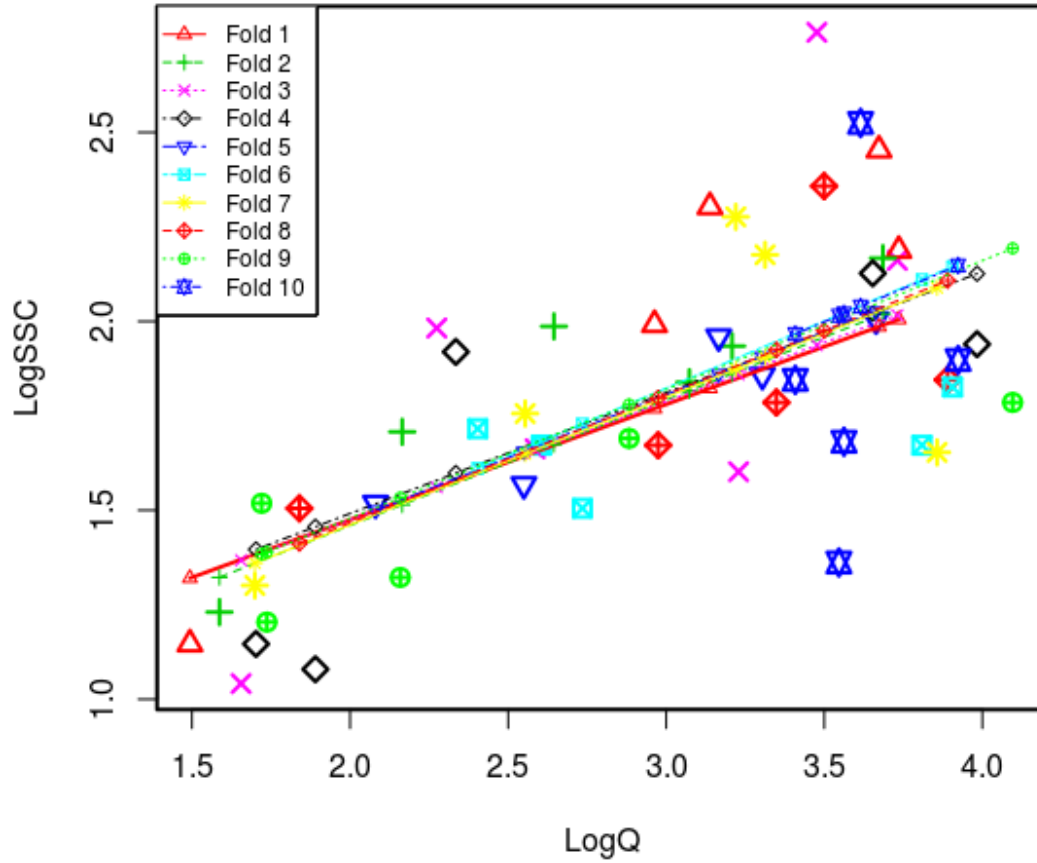
	LogSSC	Estimate	Residual	Standard Residual	Studentized Residual	Leverage	Cook's D	DFFITS
4/30/2010 11:15	2.76	1.96	0.802	2.86	3.10	0.0286	0.1210	0.532
6/17/2015 13:20	1.36	1.99	-0.625	-2.23	-2.33	0.0312	0.0804	-0.418

Statistical Plots

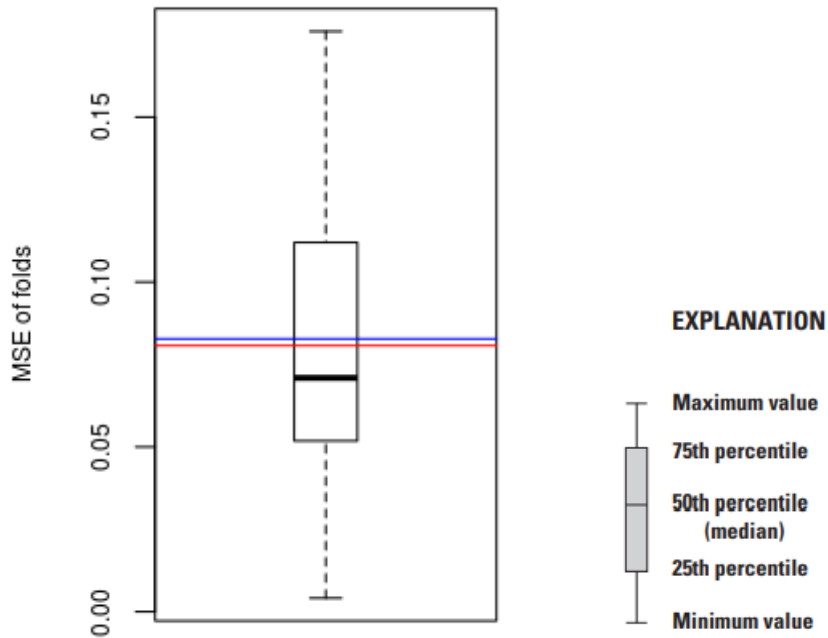




Cross Validation



Minimum mean squared error (MSE) of folds: 0.00412
Mean MSE of folds: 0.08280
Median MSE of folds: 0.07090
Maximum MSE of folds: 0.17600
(Mean MSE of folds) / (Model MSE): 1.03000



Red line - Model MSE
 Blue line - Mean MSE of folds

Model-Calibration Dataset

	Date	LogSSC	LogQ	SSC	Q	Computed LogSSC	Computed SSC	Residual	Normal Quantiles	Censored Values
0										
1	2007-03-26	1.3	1.7	20	50	1.37	29.4	-0.0707	-0.12	--
2	2007-03-30	1.92	2.33	83	216	1.58	47.9	0.336	1.06	--
3	2007-03-31	1.98	2.27	96	188	1.56	45.7	0.419	1.35	--
4	2007-04-12	2.28	3.22	189	1660	1.88	94.4	0.398	1.24	--
5	2007-04-20	1.85	3.41	70	2560	1.94	109	-0.0955	-0.267	--
6	2007-06-22	1.67	3.81	47	6440	2.07	148	-0.402	-1.65	--
7	2007-07-19	1.68	3.56	48	3650	1.99	123	-0.311	-1.14	--
8	2007-09-21	1.76	2.55	57	358	1.66	56.6	0.0996	0.368	--
9	2007-10-22	2.3	3.14	201	1380	1.85	88.7	0.452	1.65	--
10	2008-02-08	1.84	3.07	69	1180	1.83	84.3	0.00977	0.12	--
11	2008-02-28	2.16	3.73	145	5380	2.05	140	0.113	0.528	--
12	2008-09-25	1.85	3.89	70	7760	2.1	158	-0.256	-0.901	--
13	2008-10-15	1.93	3.21	86	1620	1.87	93.5	0.0605	0.218	--
14	2009-02-24	1.51	2.73	32	543	1.72	65.1	-0.211	-0.702	--
15	2009-04-13	2.36	3.5	228	3160	1.97	117	0.387	1.14	--
16	2009-09-01	1.71	2.16	51	146	1.53	42	0.181	0.765	--
17	2009-10-26	1.96	3.17	91	1470	1.86	90.6	0.099	0.317	--
18	2010-03-11	2.19	3.74	154	5440	2.05	140	0.138	0.642	--
19	2010-04-08	2.45	3.67	284	4710	2.03	134	0.425	1.48	--
20	2010-04-30	2.76	3.48	582	3000	1.96	115	0.802	2.27	--

21	2010-12-06	1.66	2.59	46	385	1.67	58	-0.00401	0.024	--
22	2011-03-28	1.99	2.96	98	918	1.79	77.5	0.199	0.831	--
23	2013-08-13	2	3.66	101	4610	2.03	133	-0.0213	-0.024	--
24	2013-08-14	1.79	4.1	61	12500	2.17	185	-0.384	-1.48	--
25	2013-10-21	1.32	2.16	21	144	1.52	41.8	-0.203	-0.642	--
26	2014-03-12	1.15	1.49	14	31.2	1.3	25.1	-0.157	-0.473	--
27	2014-10-30	1.72	2.4	52	254	1.61	50.5	0.11	0.473	--
28	2015-01-28	1.08	1.89	12	77.7	1.44	34.1	-0.356	-1.35	--
29	2015-05-07	1.23	1.59	17	38.6	1.33	27	-0.104	-0.317	--
30	2015-05-19	1.86	3.3	72	2010	1.91	101	-0.0487	-0.0721	--
31	2015-06-17	1.36	3.55	23	3520	1.99	121	-0.625	-2.27	--
32	2015-05-29	1.94	3.98	87	9620	2.13	169	-0.192	-0.584	--
33	2015-08-12	1.6	3.23	40	1690	1.88	95	-0.279	-0.975	--
34	2015-09-23	1.52	2.08	33	120	1.5	39.4	0.0198	0.169	--
35	2015-11-23	1.04	1.66	11	45.2	1.36	28.4	-0.316	-1.24	--
36	2016-01-14	1.79	3.35	61	2230	1.92	104	-0.135	-0.42	--
37	2016-02-03	1.67	2.6	47	403	1.67	58.9	-0.00116	0.0721	--
38	2016-02-24	1.51	1.84	32	69.1	1.42	32.8	0.0866	0.267	--
39	2016-05-04	1.9	3.92	79	8380	2.11	162	-0.214	-0.765	--
40	2016-09-09	1.99	2.64	97	441	1.69	60.7	0.3	0.975	--
41	2017-01-26	1.69	2.88	49	763	1.77	72.9	-0.0754	-0.169	--
42	2017-04-05	2.18	3.31	150	2050	1.91	101	0.267	0.901	--
43	2017-08-15	1.67	2.97	47	943	1.8	78.2	-0.124	-0.368	--
44	2017-10-05	1.2	1.74	16	54.6	1.38	30.3	-0.18	-0.528	--
45	2018-01-29	1.15	1.7	14	50.4	1.37	29.5	-0.227	-0.831	--
46	2018-06-26	1.52	1.72	33	52.5	1.38	29.9	0.14	0.702	--
47	2018-08-29	1.57	2.55	37	355	1.65	56.5	-0.0867	-0.218	--
48	2018-10-18	1.83	3.91	67	8050	2.11	160	-0.28	-1.06	--
49	2018-12-03	2.17	3.69	147	4850	2.03	135	0.134	0.584	--
50	2019-02-27	1.65	3.86	45	7190	2.09	154	-0.437	-1.87	--
51	2019-02-28	2.13	3.65	134	4500	2.02	132	0.105	0.42	--
52	2019-03-15	2.53	3.61	335	4120	2.01	128	0.516	1.87	--

Definitions

Adj R²: Adjusted coefficient of determination

BCF: Bias correction factor

DFFITS: Studentized difference in fits

Log: logarithm base 10

MSE: Mean squared error

MSPE: Model standard percentage error

R²: Coefficient of determination

RMSE: Root mean square error

SSC: Suspended-sediment concentration, in milligrams per liter (80154)

Q: Streamflow, mean daily, in cubic feet per second (00060)

Any use of trade, firm, or product names is for descriptive purposes only and does not imply endorsement by the U.S. Government.

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