

57K
592

Unclassified.

ELECTRICAL PROPERTIES OF SANDSTONES
OF THE MORRISON FORMATION

By George V. Keller



Trace Elements Investigation Report 592

UNITED STATES DEPARTMENT OF THE INTERIOR

✓ U.S. GEOLOGICAL SURVEY

(592)
67 n
10.592

Geology and Mineralogy

UNITED STATES DEPARTMENT OF THE INTERIOR

✓ U.S. GEOLOGICAL SURVEY

ELECTRICAL PROPERTIES OF SANDSTONES
OF THE MORRISON FORMATION*

By

George V. Keller

March 1957

Trace Elements Investigations Report 592

This preliminary report is distributed without editorial and technical review for conformity with official standards and nomenclature. It is not for public inspection or quotation.

*This report concerns work done on behalf of the Division of Raw Materials of the U. S. Atomic Energy Commission.

USGS - TEI-592

GEOLOGY AND MINERALOGY

| <u>Distribution</u> | <u>No. of copies</u> |
|---|----------------------|
| Division of Raw Materials, Albuquerque..... | 1 |
| Division of Raw Materials, Austin..... | 1 |
| Division of Raw Materials, Casper..... | 1 |
| Division of Raw Materials, Denver..... | 1 |
| Division of Raw Materials, Rapid City..... | 1 |
| Division of Raw Materials, Salt Lake City..... | 1 |
| Division of Raw Materials, Spokane..... | 1 |
| Division of Raw Materials, Washington..... | 3 |
| Exploration Division, Grand Junction Operations Office..... | 6 |
| Grand Junction Operations Office..... | 1 |
| Technical Information Service Extension, Oak Ridge..... | 6 |
| U. S. Geological Survey: | |
| Foreign Geology Branch, Washington..... | 1 |
| Fuels Branch, Washington..... | 1 |
| Geochemistry and Petrology Branch, Washington..... | 1 |
| Geophysics Branch, Washington..... | 6 |
| Mineral Deposits Branch, Washington..... | 2 |
| D. E. White, Menlo Park..... | 1 |
| A. L. Brokaw, Grand Junction..... | 2 |
| N. M. Denson, Denver..... | 1 |
| R. L. Griggs, Albuquerque..... | 1 |
| W. R. Keefer, Laramie..... | 1 |
| E. M. MacKevett, Menlo Park..... | 1 |
| L. R. Page, Washington..... | 1 |
| F. K. Sims, Denver..... | 1 |
| Q. D. Singewald, Beltsville..... | 1 |
| A. E. Weissenborn, Spokane..... | 1 |
| TEPCO, Denver..... | 2 |
| TEPCO, Washington (including master)..... | 2 |

CONTENTS

| | Page |
|---|------|
| Abstract..... | 5 |
| Introduction..... | 5 |
| Acknowledgments..... | 7 |
| Electric logging..... | 8 |
| Equipment and techniques..... | 10 |
| Results..... | 11 |
| Laboratory measurements..... | 18 |
| Nature of rock resistivity..... | 18 |
| Resistivity measurements on cores..... | 24 |
| Spontaneous potential measurements..... | 37 |
| Correlation of laboratory and field data..... | 47 |
| Quantitative interpretation of logs..... | 57 |
| Use of electric logging in exploration..... | 60 |
| References cited..... | 63 |

ILLUSTRATIONS

| | |
|---|----|
| Figure 1. Index map of the Colorado Plateau showing locations of areas discussed in this report..... | 9 |
| 2. Cumulative frequency curves of the resistivity of sandstone in drill holes in favorable and unfavorable ground..... | 13 |
| 3. Electric, radioactivity, and core logs in drill holes through mineralized ground..... | 14 |
| 4. Map of the Spud Patch area showing contours of the product of resistivity and the thickness of the ore-bearing member of the Morrison formation..... | 17 |
| 5. Idealized diagram of a single pore structure showing the features which control the resistivity of a rock..... | 20 |
| 6. Device used in measuring resistivity of cores..... | 25 |
| 7. Formation factor as function of porosity..... | 29 |
| 8. Resistivity index as function of water saturation..... | 32 |
| 9. Variations of formation factor caused by variations in water salinity..... | 36 |

| | |
|---|----|
| Figure 10. Device used in measuring the diffusion potentials of cores..... | 42 |
| 11. Ion concentration immobilized in double-layer as function of porosity..... | 44 |
| 12. Schematic representation of the sources of potential variations measured in electric logging..... | 45 |
| 13. Calculated relationship between spontaneous potential and connate water salinity for logging conditions in the Spud Patch area, Colorado..... | 48 |
| 14. Correlation of the laboratory measurements on cores with electric log data..... | 51 |
| 15. Summary of data on the inch-to-inch variations of porosity in sandstone cores..... | 54 |
| 16. Empirical relationship between porosity, electric log resistivity and spontaneous potential deflection..... | 56 |

TABLES

| | |
|--|----|
| Table 1. Quality of logging water..... | 11 |
| 2. Apparent salinities associated with clay conductance..... | 37 |
| 3. Results of the quantitative interpretations of electric logs..... | 59 |

ELECTRICAL PROPERTIES OF SANDSTONES
OF THE MORRISON FORMATION

By George V. Keller

ABSTRACT

The electrical properties of the Morrison formation in the Uravan mineral belt of the Colorado Plateau have been studied to determine if there are anomalous variations in these properties in and near zones of uranium-vanadium minerals which might serve as a target for geophysical prospecting. Measurements of electrical properties of the Morrison formation in place were obtained by the electric logging of 147 drill holes, and measurements were made of the resistivity and porosity of 440 drill cores in the laboratory to aid in the interpretation of the electric logs. The resistivity of the sandstone members of the Morrison formation is highest in areas that are the most favorable for the occurrence of ore. This increase in resistivity is probably due to a lower water saturation or a lower salinity of the water in the favorable areas.

INTRODUCTION

Uranium- and vanadium-bearing sandstones are widely distributed in the Colorado Plateau province, which covers parts of the four states of Colorado, Utah, New Mexico, and Arizona. Deposits have been found in many formations in the area; many of the important deposits are in the Morrison formation, particularly in an area of west central and southwest Colorado called the Uravan mineral belt. The deposits are usually small in extent, ranging from a few tons to

some thousands of tons of ore. The ore bodies form irregularly tabular masses that tend to be parallel to the bedding, but they do not follow the beds in detail (Fischer, 1942).

In southwestern Colorado, the Morrison formation is comprised of two recognized members, the Brushy Basin and the Salt Wash. The Brushy Basin member consists predominantly of mudstones which may be gray, red, green, purple, and brown. The Brushy Basin also contains several thin sandstones and limestones. Locally, there are thick lenses of conglomerate.

The lower member, the Salt Wash, consists of massive lenses of medium- to coarse-grained sandstones interbedded with red and blue-gray mudstones. Much of the ore is in sandstones in the upper part of the Salt Wash member but usually in the lower parts of the individual sandstone lenses. The Salt Wash is not sharply separated from the Brushy Basin, particularly where there are sandstone lenses in the lower part of the Brushy Basin.

In general, the localization of the ore seems to be related to certain geologic features that can serve as guides to the presence of ore. Such guides are the tendency of the ore to occur in the thicker central parts of sandstone lenses, the association of ore with medium-grained pale yellow to light brown sandstone, the association of ore with the thicker parts of mudstone that have been altered from red to gray or gray-green, and the association of ore with an abundance of carbonaceous material.

In hopes of delineating favorable areas and locating ore more rapidly and at less expense, various geophysical exploration methods were tested on the Colorado Plateau beginning in 1949. Electrical

resistivity surveys were tried in several areas, and in several known ore deposits, higher resistivities were noted over the ore zones. However, the exact interpretation of these surveys proved difficult, particularly when the ore-bearing member was at a depth of several hundred feet.

In order to determine the possibilities and limitations of surface resistivity surveys, a program of measurements of the electrical properties of the Morrison formation was undertaken. The program consisted of two parts: the measurement of the resistivity of the Morrison formation in place and the measurement of resistivity and associated properties of drill cores with restored water saturations.

Acknowledgments

Both field and laboratory studies described in this report were made as part of a program carried on by the Geological Survey on behalf of the Division of Raw Materials of the Atomic Energy Commission.

ELECTRIC LOGGING

Measurements in place, consisting of electrical well logs, were made in 147 drill holes (fig. 1) in four areas where surface resistivity surveys had been made previously to determine whether there are any pronounced differences in the electrical properties of the Morrison formation in these areas. In the Spud Patch area of San Miguel County, Colo., 103 measurements were made so that it was possible to determine the areal variation of electrical properties. A smaller number of drill holes, 23 in all, were logged in the Gramlich group of claims at La Sal Creek, Montrose County, Colo. A few holes were also logged at Long Park in Montrose County, Colo., and at Yellow Cat, Grand County, Utah.

The electric logs taken on the Colorado Plateau were of three types, natural potential measurements, resistivity measurements with a normal electrode arrangement, and resistance measurements with a single point electrode arrangement. Natural potential logs are made by recording the voltage between a moving electrode in the drill hole and a reference electrode, usually placed on the ground surface near the drill hole. In the work reported here, resistivity logs with radii of investigation of 4, 8 and 24 inches were taken in each drill hole; single-point resistance logs were made to provide sufficient data to determine rock resistivity. By comparing the apparent resistivities measured with these several electrode arrangements, it is possible to estimate the true resistivity more accurately than can be done with a single measurement.

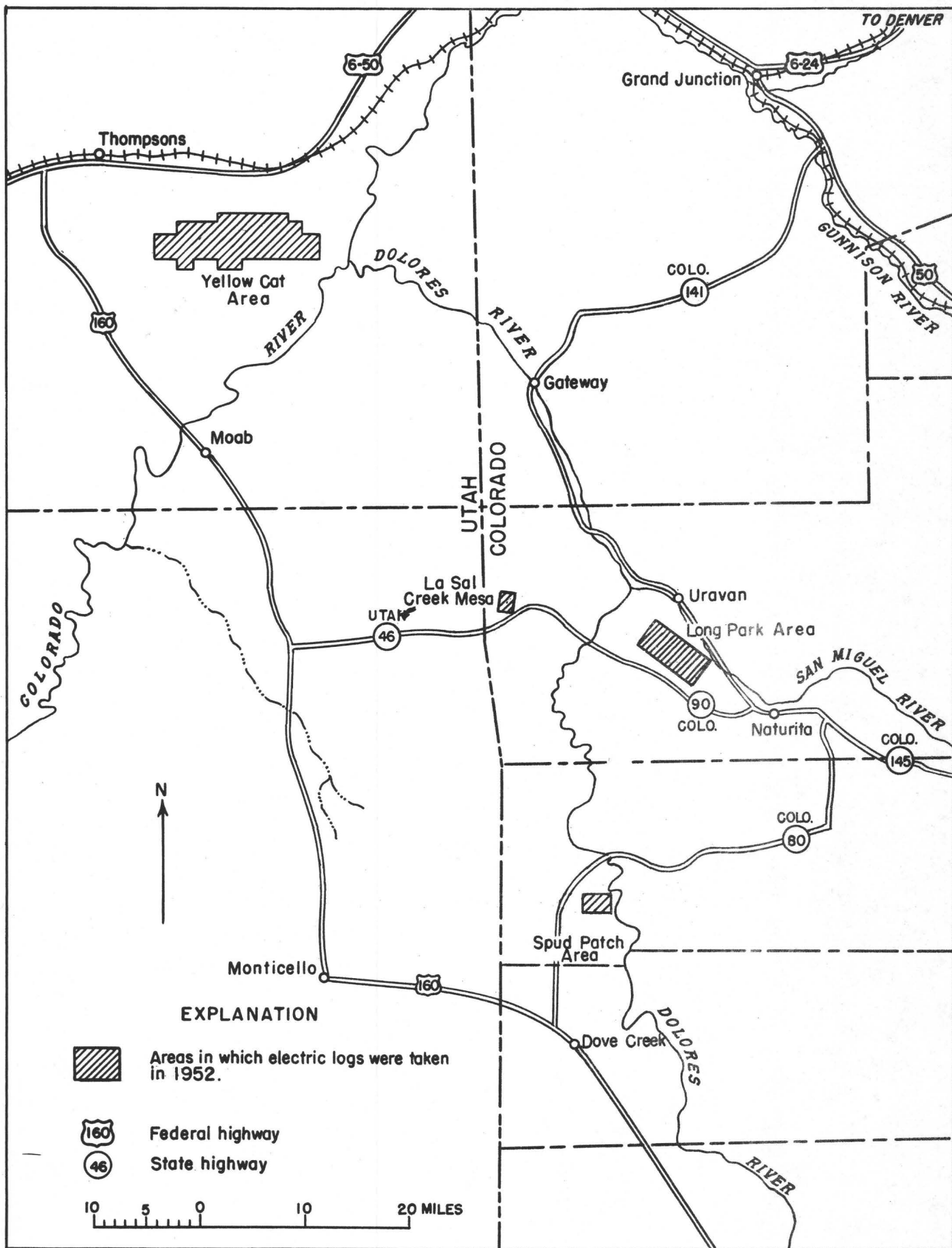


Figure 1: Index map of the Colorado Plateau showing locations of areas discussed in this report.

Equipment and techniques

The electric logging unit used for this work consisted of a three-conductor cable and an electric hoist to raise the electrode sonde through the drill hole. The current to the electrodes was provided by dry batteries, regulated with a servomechanical regulator, and commutated at a frequency of 21 cycles per second. The voltage between pick-up electrodes was rectified with a set of commutator rings coupled mechanically to the current commutator, as in the Gish-Rooney system. This rectified current was recorded on one channel of a modified servomechanical recorder, calibrated in ohm-meters.

The spontaneous potential, present as a d-c voltage between the pick-up electrodes, was separated from the 21-cycle resistivity logging current by means of a blocking condenser and recorded simultaneously on the other channel of the recorder, calibrated in millivolts.

The chart drive of the recorder was controlled by a selsyn motor coupled to a selsyn generator on a calibrated sheave over the drill hole. The logging cable passed over this sheave as it was lowered or raised in the drill hole, so that the paper in the recorder was driven forwards or backwards through the recorder. Paper drive ratios of one inch to 20, 50, and 100 feet of electrode movement were used.

Because most of the drill holes on the Colorado Plateau are dry, it was necessary to haul water to fill the drill holes in order that contact could be made between the in-hole electrodes and the rock.

Obtaining water for logging proved to be one of the biggest handicaps to logging on the Colorado Plateau. In all the areas logged, surface drainage either from springs or from reservoirs was used to fill the drill holes. The water sources and their qualities are listed in table 1.

Table 1.--Quality of logging water

| <u>Logging area</u> | <u>Water source</u> | <u>Resistivity at 50 C.</u> | <u>Equivalent salinity, ppm NaCl</u> |
|---------------------|-------------------------------|---------------------------------|--|
| Spud Patch | Bell Canyon Reservoir | 6,500 ohm-cms | 130 |
| Spud Patch | Water standing in D. H. 19 | 1,780 ohm-cms | 430 |
| Gramlich Group | Lion Creek Spring | 3,230 ohm-cms | 240 |
| Long Park | Eagle Canyon Reservoir | 4,200 ohm-cms | 185 |

Results

Analysis of the electric logs showed that the resistivity of the different members of the Morrison formation in the drill holes that were logged ranged from a low of 8 ohm-meters to a maximum of 2,000 ohm-meters. The resistivity of the mudstone members ranged from 8 ohm-meters to 35 ohm-meters, and the average resistivity did not change greatly from drill hole to drill hole.

The average resistivity of the sandstone members of the Morrison formation within any one drill hole showed a greater variation, ranging from 130 ohm-meters to 430 ohm-meters. Moreover, the resistivity of the sandstone within any one drill hole showed wide variations about the average.

An apparent correlation was noted between resistivity of the sandstone and favorability for occurrence of ore as determined by geologic guides. This apparent correlation was studied in more detail by a statistical analysis of the resistivity logs of 35 drill holes in which the complete section of the ore-bearing member had been logged. Of these 35 drill holes, 20 had been classed as favorable with respect to geologic guides, and 15 were considered to be semifavorable or unfavorable. The logs were studied by taking resistivity intervals of progressively larger size: 56 to 80 ohm-meters, 80 to 115 ohm-meters, and so on up to the interval 1,400 to 2,000 ohm-meters. The number of feet of sandstone in each of these classes in each group of drill holes was then measured. These data are presented on a cumulative frequency graph in figure 2. The shape of the curves indicates that the number of feet of sandstone of a given resistivity is a statistically normal variable when the resistivity is considered logarithmically. The curve for favorable sandstones is significantly different than the curve for semifavorable and unfavorable sandstones; the median of the curve of resistivity in favorable sandstone is 50 percent higher than that in the less favorable sandstones.

In addition to the generally higher resistivities found in the drill holes in more favorable ground, especially high resistivities were found in drill holes through mineralized ground at approximately the depth of mineralized area. Figure 3 shows the electric logs, the core log, and the radioactivity log of seven typical drill holes through mineralized ground.

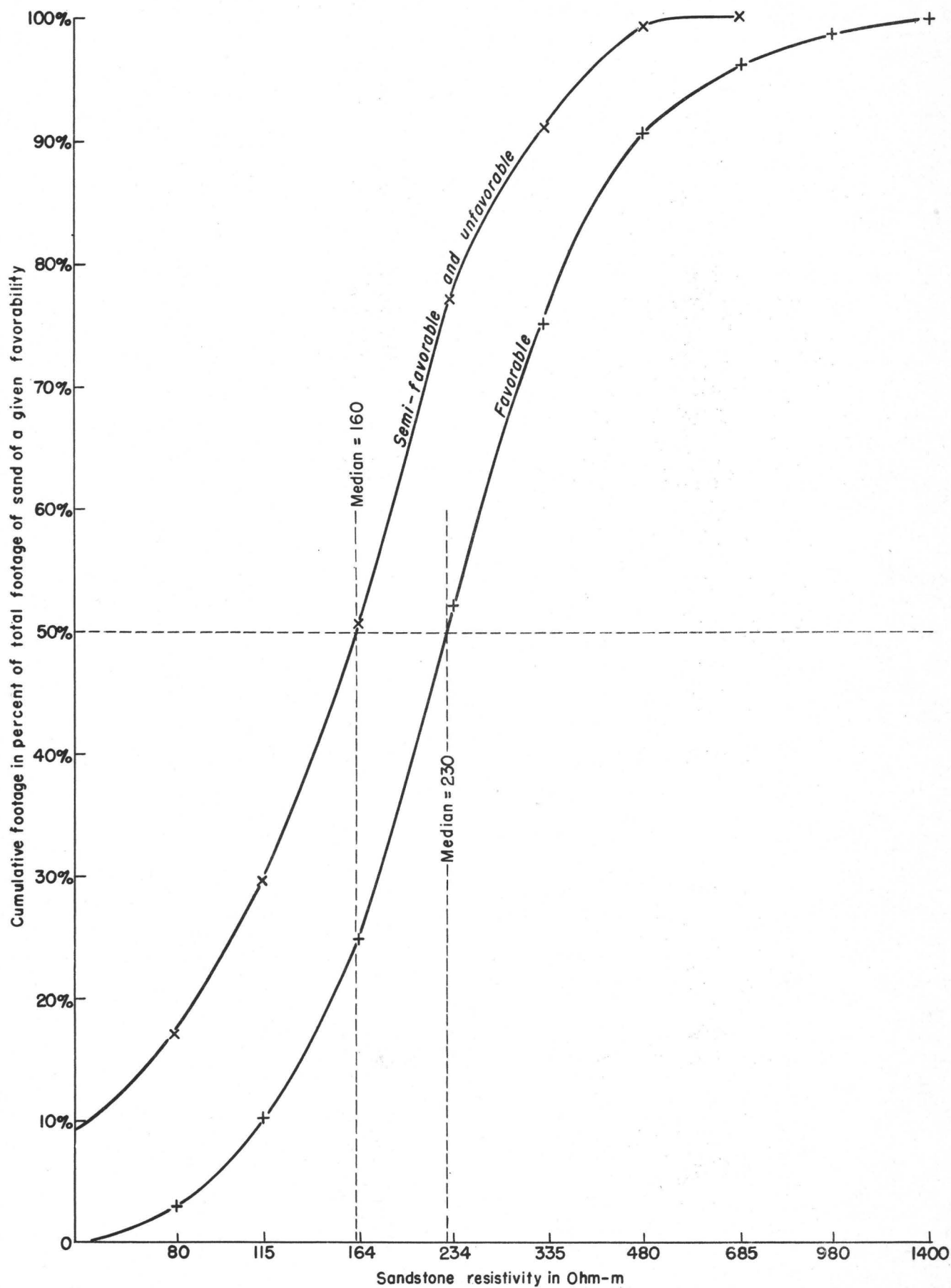
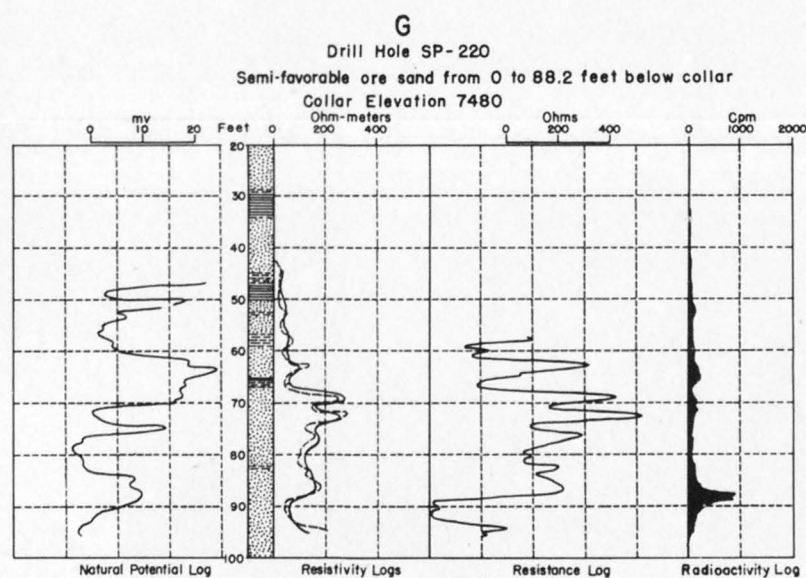
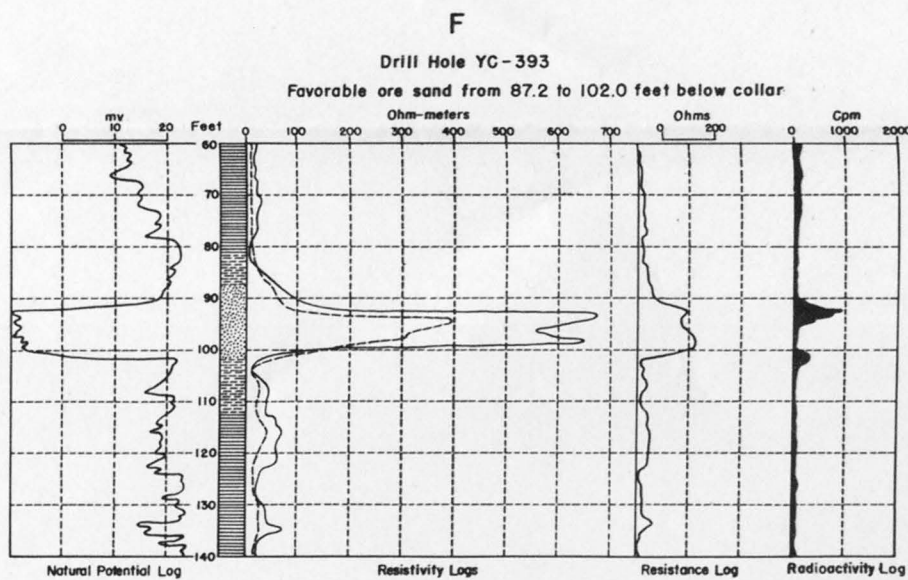
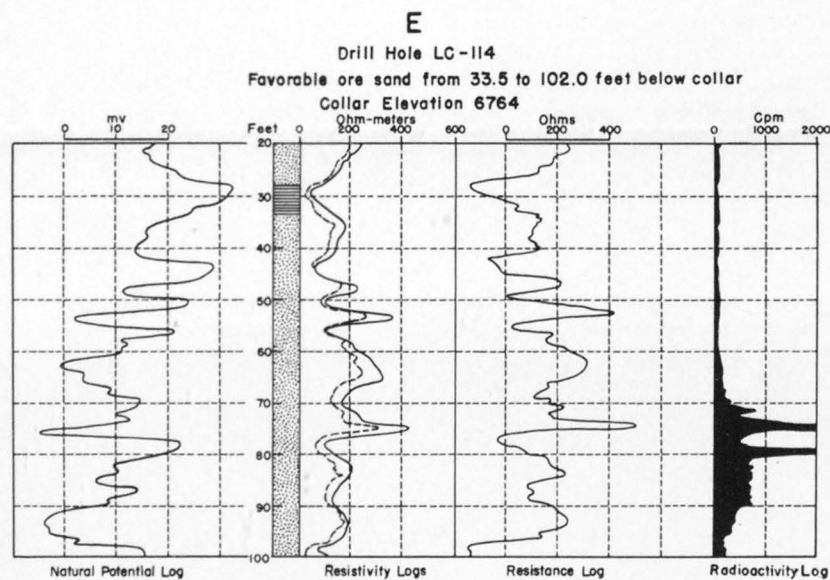
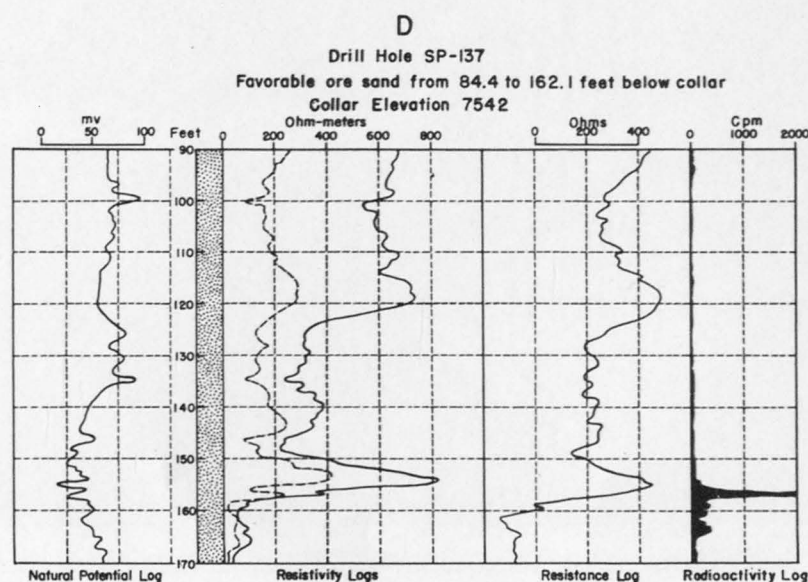
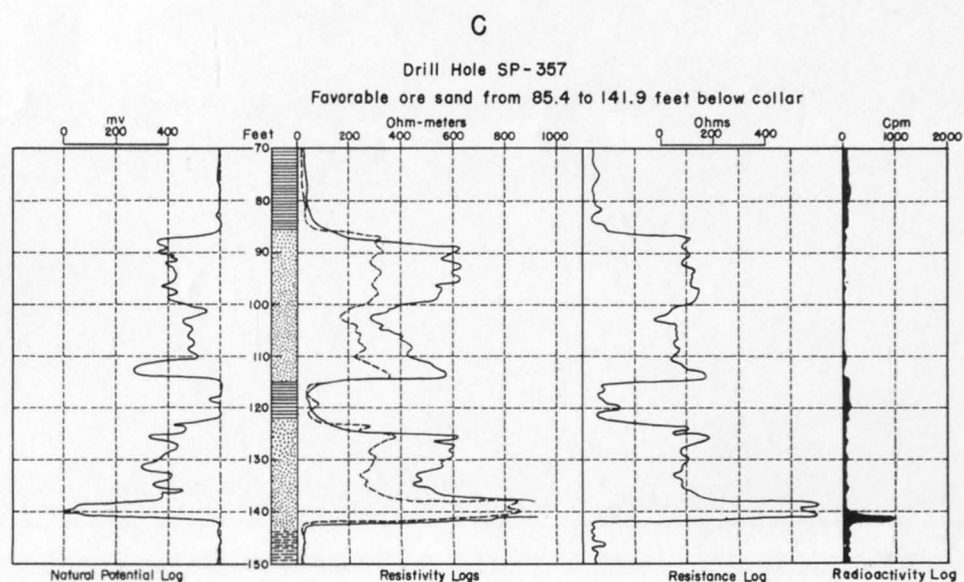
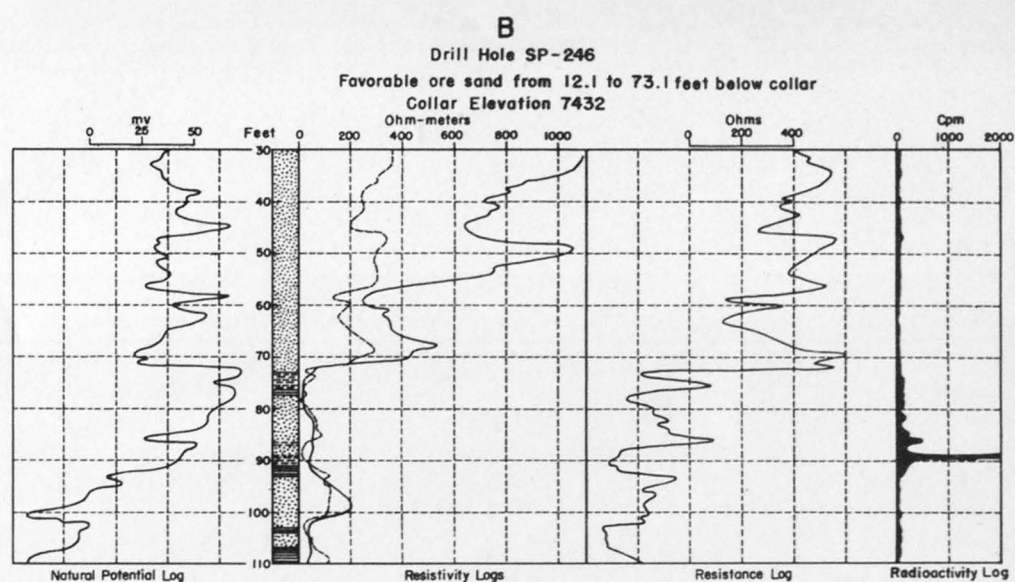
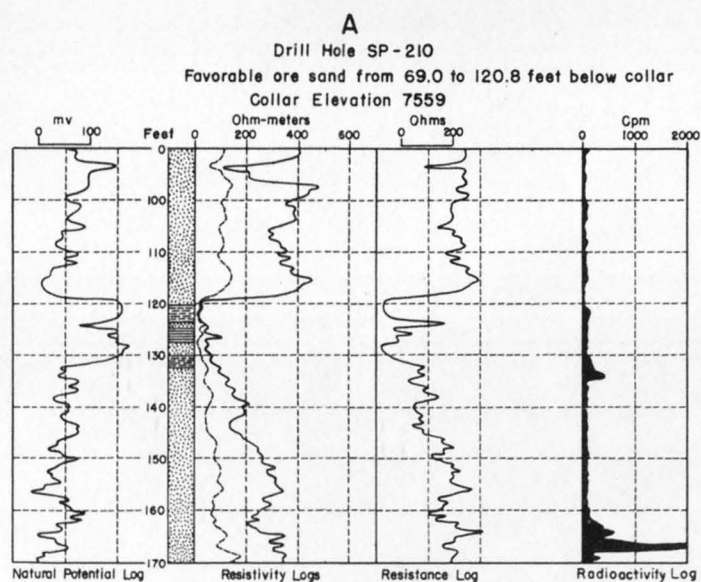


Figure 2: Cumulative frequency curves of the resistivity of sandstone in drillholes in favorable and unfavorable ground.



EXPLANATION

- Sandstone
- Gray-green mudstone
- Red-brown mudstone
- Resistivity measured with a normal 24 inch electrode spacing
- Resistivity measured with a normal 4 inch electrode spacing

Figure 3: Electric, radioactivity, and core logs in drill holes through mineralized ground.

With one exception, a thin layer of high resistivity is found near the depth of the radioactivity anomaly. The one exception is drill hole SP 210 (fig. 3A), in which there is a small increase in resistivity at the depth of the mineralized ground. In other holes, (figs. 3C and 3F), the high resistivity layer is the most striking feature of the log. In the remaining examples, the resistivity of the ore zone is one of the highest recorded on the log but is not so large as to be outstanding.

The resistivity anomaly occurs in the upper part of the radioactivity anomaly or is offset up the hole by one or two feet. This offset indicates that the anomaly is not directly associated with mineralized ground but may be caused by some other factor. The combination of high resistivity and high natural potential deflection shown by the logs in figure 3 indicates that the anomalous layer has a low saturation of water of high salinity. This relation in turn implies that the layer has been subject to an extreme amount of evaporation, as if it had high permeability. The mineralized layer seems to be covered by a desaturated cap rock that gives rise to a resistivity anomaly.

One of the geologic guides to ore is the association of ore with the thicker Salt Wash sandstone. Because of this association and the observation that the resistivity of the sandstones in drill holes through mineralized ground is generally higher than the resistivity in drill holes in unfavorable ground, it was believed that a combined measure of sandstone thickness and resistivity would be a sensitive index to the favorability of a drill hole. To check this, the area under the 8-inch normal resistivity logs was planimetered for the

drill holes in which logs were obtained for 60 percent or more of the ore-bearing sandstone. None of the sandstones in the overlying Brushy Basin were included in these measurements. When a log did not cover the entire thickness of ore-bearing sandstone, it was assumed that the average resistivity in the unlogged section was the same as in the logged section, and the resistivity integral was extrapolated to include the unlogged section of the sandstone.

The 8-inch normal curve was used in these studies as no correction is necessary for the influence of mud resistivity and hole diameter. In all holes, the mud resistivity was 65 ohm-meters within an accuracy of 20 percent. The diameters of the holes were 3 inches. Corrections for these conditions are less than 10 percent for all resistivities less than 2,500 ohm-meters and for beds thicker than 3 feet according to Schlumberger departure curves. Corrections may be made for thinner beds, but such corrections usually are no more accurate than the original data.

These measurements were made for 58 drill holes of the Spud Patch area; the resulting integral ranged from 3,800 to 29,600 ohm-meter-feet. A contour map (fig. 4) of these data shows six pronounced features, three highs and three lows. The highs include all but one of the drill holes through mineralized ground and many of the drill holes through favorable ground. One drill hole through mineralized ground occurs in a low, but this drill hole was classed as unfavorable according to geologic guides. The low areas include all the drill holes in unfavorable ground and a majority of the drill holes in semi-favorable ground.

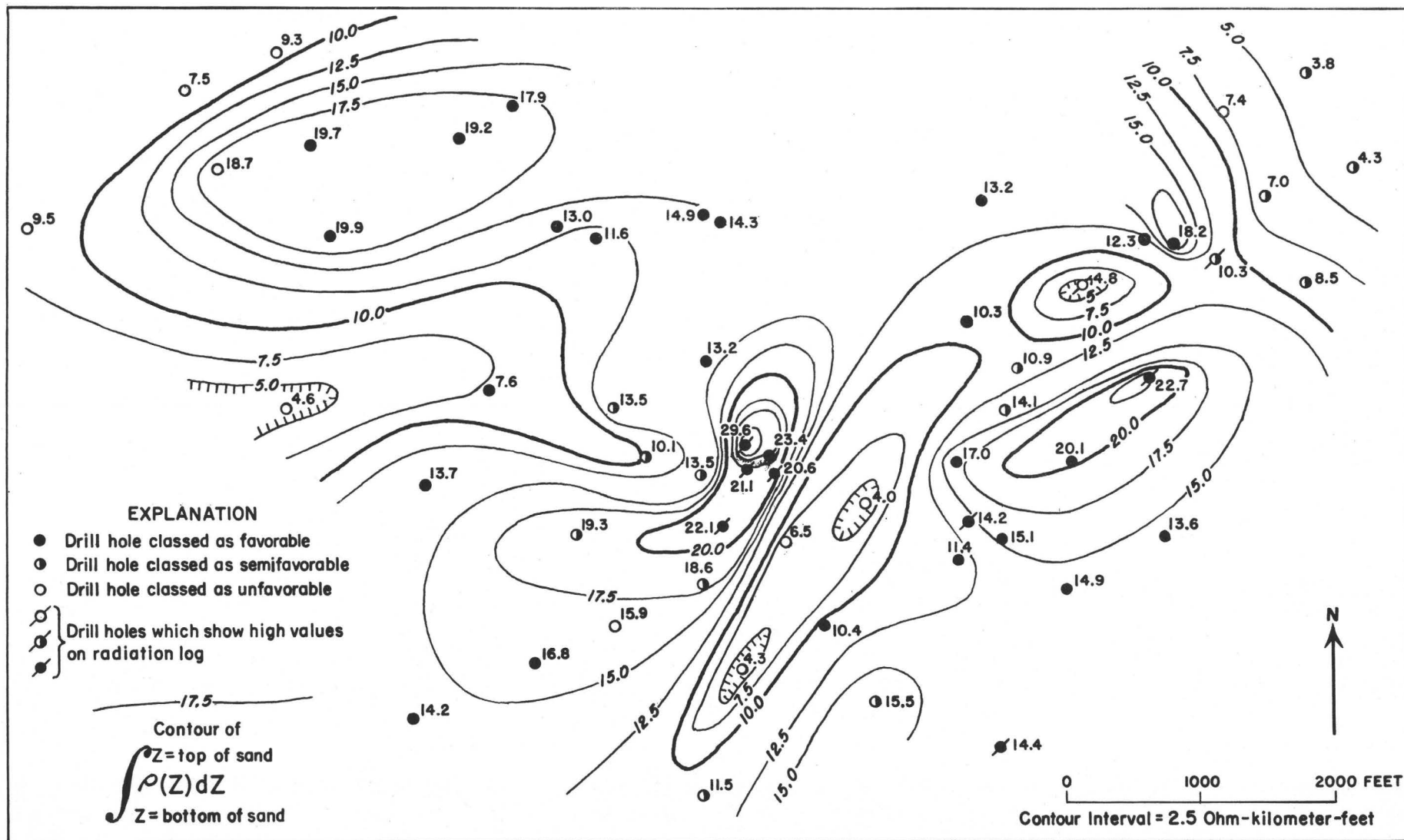


Figure 4: Map of the Spud Patch area showing contours of the product of resistivity and the thickness of the ore-bearing member of the Morrison formation.

LABORATORY MEASUREMENTS

To interpret the logs quantitatively in terms of texture and composition it is necessary to have detailed information on the properties of the rock, such as can be obtained by the physical analysis of cores. Usually this additional information is obtained from resistivity measurements on cores taken from a typical drill hole. These measurements are designed to determine how rock resistivity depends upon the rock texture and the composition of the contained water. The results are then extrapolated to drill holes from which no cores have been studied.

Nature of rock resistivity

The electrical conductivity of sedimentary rocks such as those which comprise the Morrison formation is readily shown to be a consequence of the presence of small amounts of water in the rock. If a sedimentary rock is dried completely, it is an insulator. However, if even a small amount of water is present, a rock exhibits an appreciable ability to conduct electrical currents. Because the conduction is ionic, rather than electronic as in metals, the nature of the conductivity of the rock and water combination is more complex than if the conduction were metallic.

Current conduction in sedimentary rocks can be understood by considering what happens in a small portion of the pore structure. Clastic detrital rocks, such as the sandstones and mudstones which constitute the Morrison formation, consist of a network of void space separating the solid grains. This void space, or porosity,

can be classified into two general types of pores. Most of the void space is comprised of relatively large, more or less equidimensional pores that make up the storage capacity of the rock. The rest of the void space consists of small elongated channels that connect the larger voids. These channels are only a small part of the total porosity, but they are the primary factor in controlling current conduction because of their small cross-sectional area. To aid in visualizing this, the concept of the ideal porelet (fig. 5) is useful. The porelet consists of a spherical body, or storage chamber, with small tubular extensions that connect with other porelets. Clay particles are shown lining this porelet, particularly in the small connecting pores, where the clays tend to occur. A porous, isotropic rock can be thought of as consisting of a large number of these porelets, randomly oriented and connected to each other in a geometrically complicated manner.

If such a rock were fully saturated with a brine solution, the resistance presented to an electrical current would depend on the length of the connecting pores, their cross-sectional area, the average angle that the porelets make with the overall direction of current flow, and the total number of porelets per unit area.

In the study of the resistivity of porous materials, it has become customary to use a quantity called the "formation factor," which is the resistivity of the bulk material, such as the rock, divided by the resistivity of the conductive material in it, such as the brine. In simple ohmic conduction, the formation factor would be a constant for a given rock, and would represent the geometric distribution of the porelets as described above. The formation

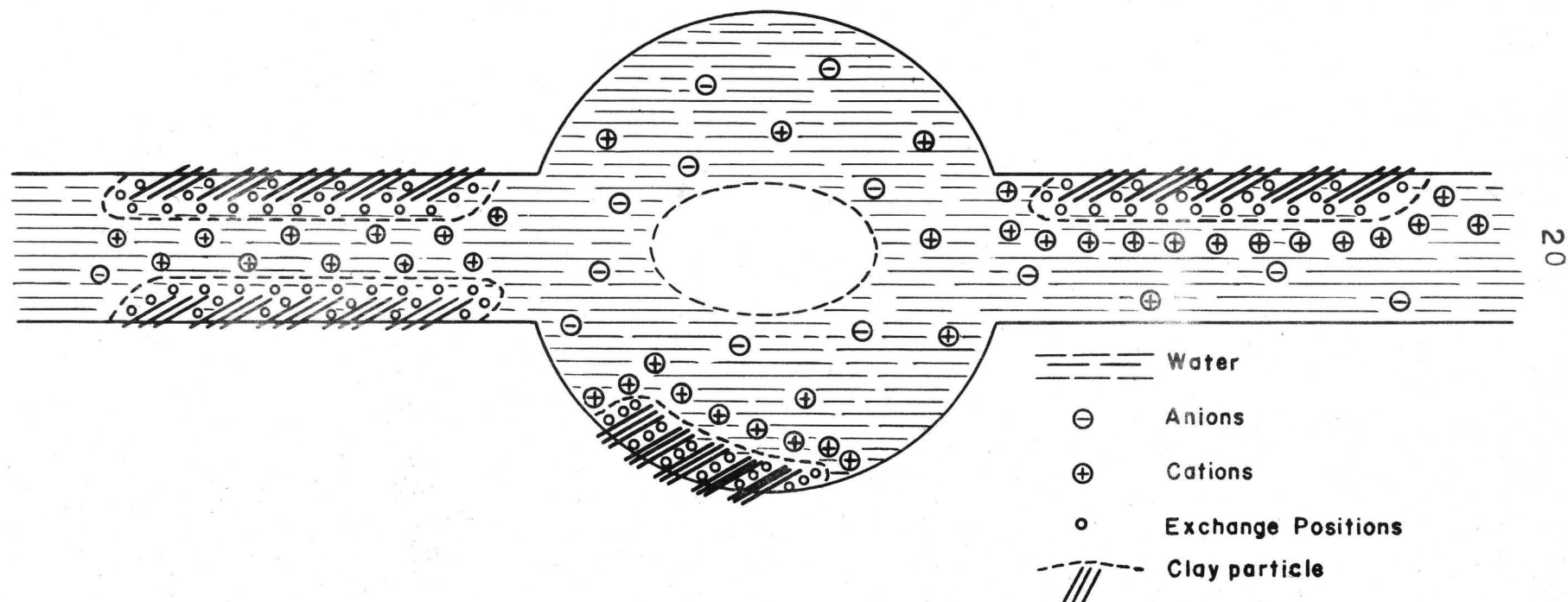


Figure 5: Idealized diagram of a single pore structure showing the features which control the resistivity of a rock.

factor would decrease as the volume of conductive material, or number of porelets, increased. Similarly, as the degree of consolidation of the rock increased and the size of the connecting tubes was reduced by the deposition of cement, the formation factor should increase. The relationship between electrical resistivity and porosity has been determined empirically as:

$$F = c\phi^k \quad (1)$$

where F is the formation factor as defined above,

ϕ is the porosity, and

c and k are constants determined by the various dimensions of the porelets.

This equation implies that the resistivity of the brine within the pores is known or can be measured. Generally it is assumed that the conductivity of the brine in the pores is due solely to the presence of ionized salts and is the same as the conductivity of a similar brine outside the rock. This is not always true. If a rock contains any surface-active material, such as clay, there may be a reaction between the water and the rock that tends to increase the conductivity of the rock. This effect is known as double-layer conductivity, because it is related to the presence of a Helmholtz double layer of charge on the surfaces of the clay particles (Winsauer, and McCardell, 1952).

Many different phenomena can occur when water comes in contact with these clays in the rock. Many clays, such as montmorillonite and illite, are colloidal electrolytes. These clays have a number of cations in their crystal structure that are free to leave the clay particle and go into a state resembling ionic solution. The number

of these cations and the ease with which they may leave the clay particle depend on the type of clay, the type of ion that is in the exchange position, and the nature of the brine in contact with the clay. The exchangeable cations that leave the clay add to the ability of the water to conduct current, but the mobility of these ions may not be the same as in true ionization because of the presence of the charged clay particle or micelle.

More complex reactions may occur also. Over certain ranges in salinity of the external solution, the plates of the clay particle become separated as water molecules are attracted between them by the unsatisfied electrical charges of the exchange positions. In these conditions, the clay will swell to many times its original size, the viscosity of the clay-water mixture will be increased and the cross section available for current conduction will be reduced.

As the salinity of the water in the pores is increased, the relative effect of the ions added by cation exchange becomes small. As a result, resistivity measurements made with a high-salinity brine saturating the rock generally approach the constant formation factor expectable if the clay were not present.

In nature, the pore space in most rocks is only partly filled with water. As a result, the rock has a higher resistivity than if it were completely saturated. In studying the effect of saturation on resistivity, it is common practice to use a quantity called the "resistivity index." This index is the resistivity of a rock partly saturated by water divided by the resistivity of the same rock fully saturated with a brine of the same composition.

As the water saturation of a rock is reduced, water is first removed from the centers of large voids (fig. 5), because the water is held in the smaller pores by capillary tension. The removal of water from these larger pores increases the distance that the current has to flow through the pore and decreases the cross-sectional area available for current conduction. In an ideal case the process continues until all the water is removed from the pores with the exception of a uniform coating over the pore walls. If there is further reduction in water content, the water film in a pore becomes discontinuous; and the remaining water in that pore is unavailable for current conduction. The result is a rapid increase in resistivity as the water content is reduced beneath the critical saturation. It has been found (Keller, 1953) that the relationship between resistivity and saturation generally takes the form:

$$I = S_w^{-n_1} \cdot S_w > S_{wc} \quad (2)$$

$$I = aS_w^{-n_2} \cdot S_w < S_{wc}$$

where I is the resistivity index defined above,

S_w is the water saturation, expressed as a fraction of the total pore space,

n_1 is the saturation exponent at high-water saturation,

n_2 is the saturation exponent at low-water saturations,

S_{wc} is a critical water saturation separating high- and low-water saturations, and a is a constant that enters the equation at low-water saturations.

As this discussion indicates, in order to specify the resistivity of a rock from measurable quantities, it is necessary to know the influence of the water saturation, porosity, and clay

content individually on resistivity. To determine these, a series of measurements were made on cores from six Spud Patch drill holes. Three groups of resistivity data and one group of natural potential data were obtained.

Resistivity measurements on cores

To study the relation between resistivity and porosity, a group of 346 cores was selected. These cores were taken at intervals of one to two feet through the sandstone members penetrated in the six drill holes. The cores as they came from the coring bit were 1-3/16 inches in diameter and a few inches to several feet long. The cores at the selected depths were faced with a diamond cut-off wheel to a length of 1 inch. The flat faces of these cores were then coated with Silver Print, a conductive silver paint used in printed electronic circuits.

The cores were saturated with tap water and permitted to soak in tap water for two weeks; the water was changed daily in order to remove any salt remaining from the original water saturation. At the end of the soaking period, the electrical resistance between the silver-coated faces of the cores was measured by placing the core in a clamp consisting of two lead-plated brass plates in contact with the ends of a core (fig. 6). The resistance between these brass plates and through the core was measured with a Wheatstone bridge circuit. A 20-cycle-per-second current was caused to flow through the bridge and regulated so that a constant 5 milliamperes of current flowed through the core. The null position of the Wheatstone bridge was detected with an oscilloscope.

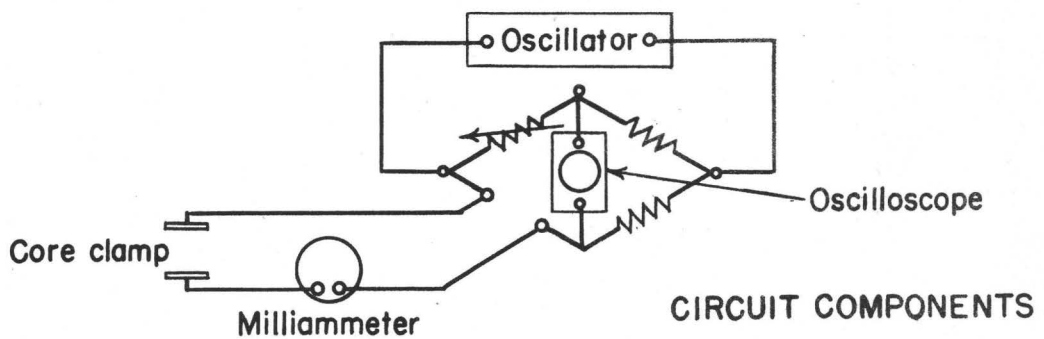
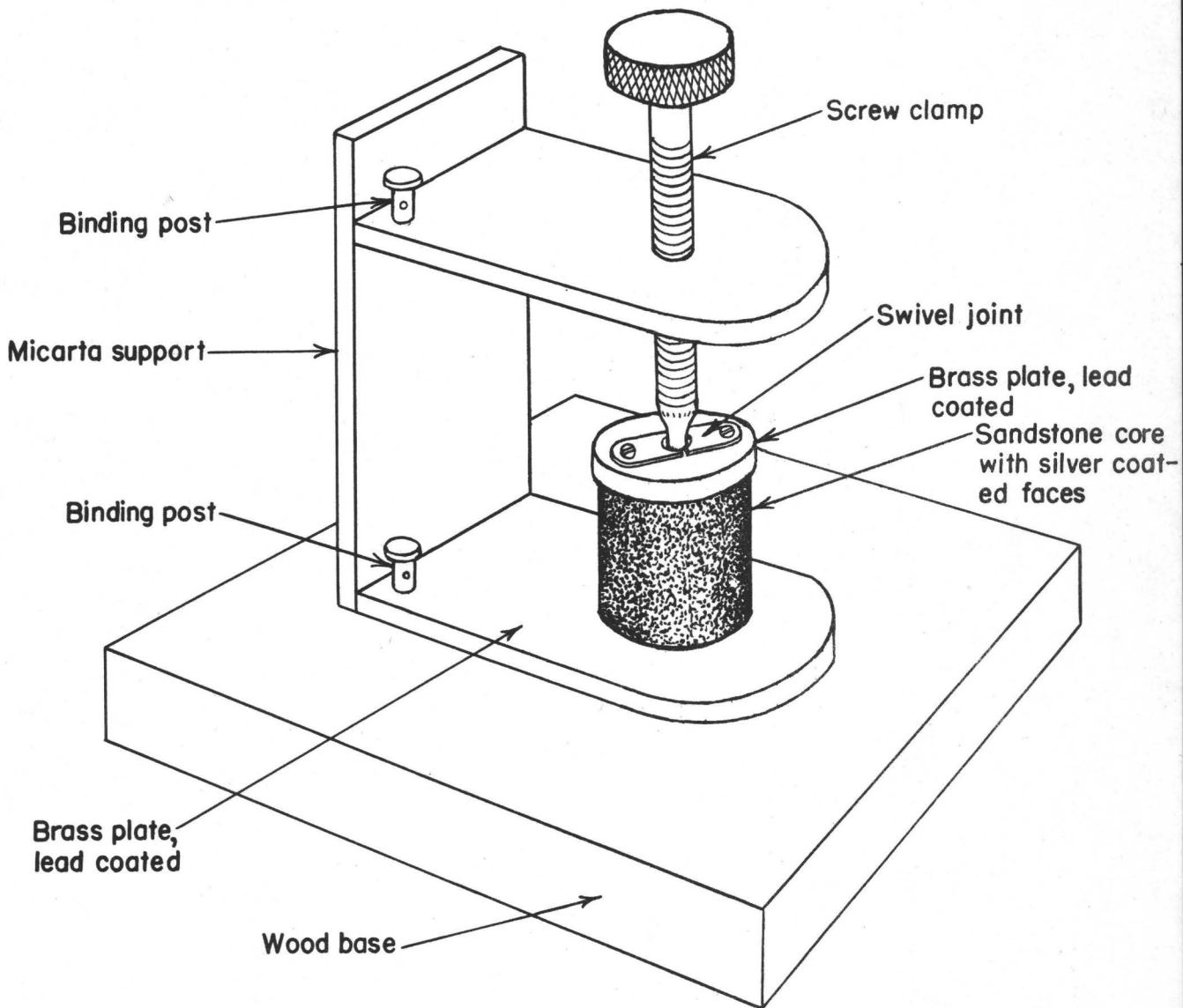


Figure 6: Device used in measuring the resistivity of cores

After the resistances had been measured, the cores were dried for six hours at 105° C. The dried cores were then weighed and placed in a vacuum dessicator. The pressure was reduced to a few millimeters of mercury for a period of two to four hours.

When the air had been removed from the cores, a deaerated brine containing a known amount of sodium chloride in solution was introduced into the dessicator. The cores were covered with this brine and subjected to atmospheric pressure, forcing the brine into the pore spaces of the cores. The cores were reweighed, and the resistance between silvered faces was measured as before. The volumes of the cores were determined by weighing them while they were suspended in a brine of the same composition as the one with which they were saturated.

The resistivity of the brine, which contained 30,000 ppm sodium chloride, was determined from tables and checked with a calibrated dip cell.

The volume of the brine in the cores was calculated from the following equation:

$$\phi_w = \frac{W_2 - W_1}{W_2 - W_3} \quad (3)$$

where ϕ_w is the fraction of the total volume of the core occupied by brine,

W_1 is the weight of the dry core,

W_2 is the weight of the core saturated with brine, and

W_3 is the weight of the core suspended in brine.

The quantity ϕ_w is the effective porosity to water, which should be only slightly smaller than the total porosity because of the method by which the cores were saturated.

The resistivity of the cores was readily determined from:

$$\rho = \frac{2\pi r^2}{l} \frac{R_1 R_2}{R_1 - R_2} \quad (4)$$

where r is the radius of the core,

l is the length of a core

R_1 is the resistance of a core saturated with tap water, and

R_2 is the resistance of a core saturated with brine.

Resistivity at very high brine salinities should be approximated by this formula because the conductivity of the core saturated with tap water is considered to be in parallel with the conductivity of the brine when the core is saturated with brine, and the error caused by the action of clay and the presence of an unknown amount of salt from the original connate water is approximately corrected. Inasmuch as this correction does not exceed 10 percent the assumption that the two conductances are parallel is accurate within 1 percent.

The formation factor was determined for each core by dividing resistivity of the rock by the resistivity of the brine used to saturate the cores.

Because of the large number of measurements, it was possible to determine an empirical relation between formation factor and porosity by a statistical method. The data were grouped into 11 classes or ranges of porosity: that is, 14.01 percent to 15.00 percent, 15.01 percent to 16.00 percent, and so on. Then it was assumed that the logarithms of the formation factors in each group were normally distributed about some mean. This mean of the logarithm of formation factor was calculated for each of the 11 intervals, and a standard deviation was calculated for each group by the formula:

$$\sigma_F = \frac{\sum (\log F - \overline{\log F})^2}{N} \quad (5)$$

where σ_F is the standard deviation of $\log F$,

N is the number of cores in any one porosity class, and

$\overline{\log F}$ is the average value of $\log F$.

The standard deviation of the mean value of the logarithm of the formation factor was also computed from the equation:

$$\sigma_{\mu_F} = \frac{\sigma_F}{\sqrt{N-1}} \quad (6)$$

where σ_{μ_F} is the standard deviation of the average value of $\log F$.

In figure 7, the mean values of formation factor have been plotted as a function of the mean values of porosities in each class. The table from which this graph was plotted is given below:

| <u>Number of cores</u> | <u>Average porosity</u> | <u>Average formation factor</u> |
|----------------------------|-----------------------------|-------------------------------------|
| 44 | 21.7 | 16.8 |
| 29 | 19.5 | 20.7 |
| 39 | 18.4 | 23.6 |
| 44 | 17.5 | 26.1 |
| 37 | 16.5 | 29.9 |
| 34 | 15.5 | 31.6 |
| 16 | 14.3 | 39.8 |
| 34 | 13.1 | 40.8 |
| 25 | 11.0 | 60.1 |
| 22 | 7.2 | 101.0 |
| 22 | 2.6 | 296.0 |

The 95 percent confidence limits of the means are indicated by the length of the bar through each point, and the 95 percent confidence limits of the individual datum points are indicated by the dashed lines.

The equation of the form of equation 1 that best fits these data between porosities of 14 percent and 23 percent is:

$$F = 0.62 \phi_w^{-2.10} \quad (7)$$

The data for lower porosities are probably unreliable because of

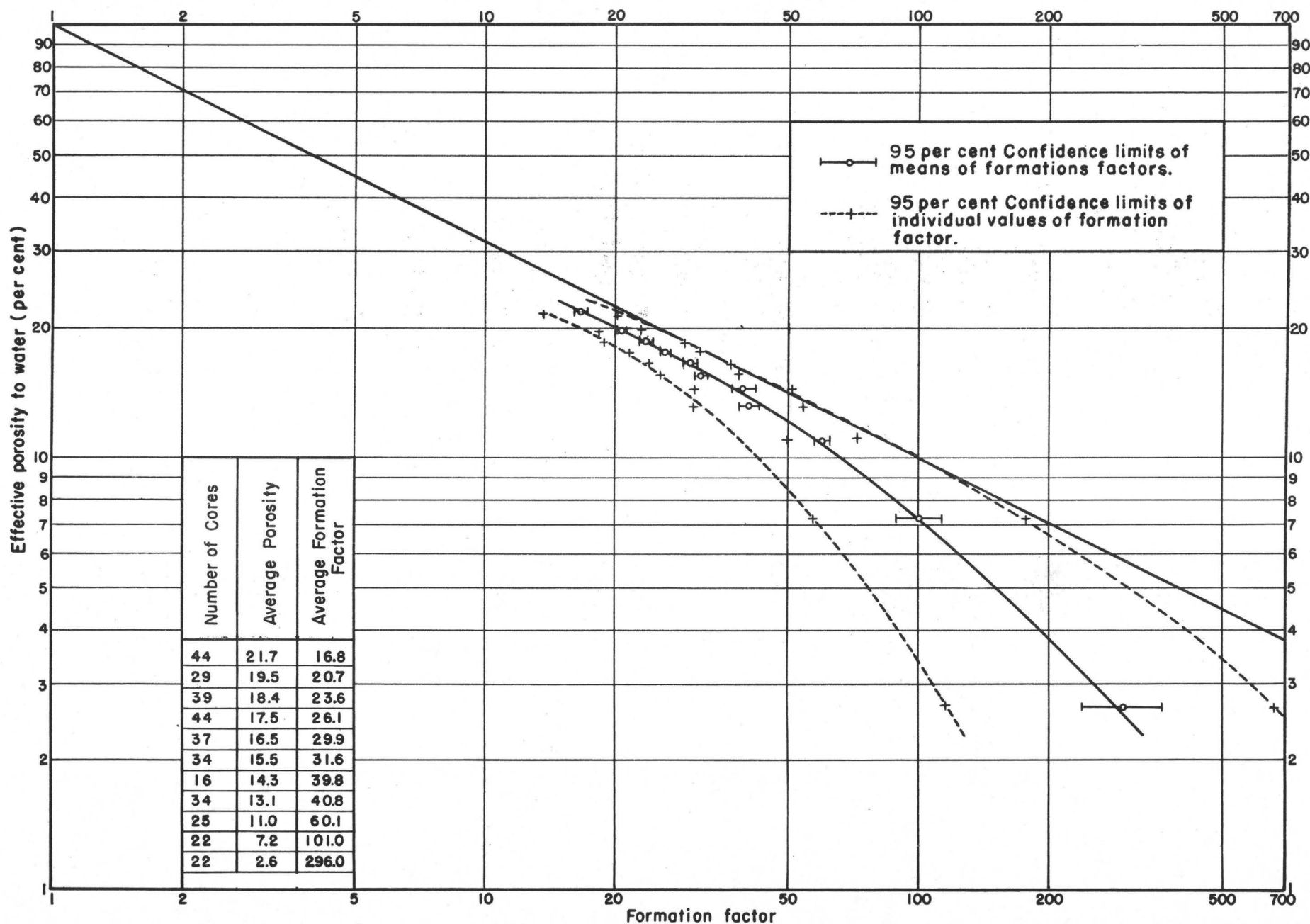


Figure 7: Formation factor as function of porosity.

the difficulty of obtaining uniform saturation in cores with low porosity and poor permeability.

A smaller group of cores, 45 in all, was selected for study of resistivity as a function of water saturation. These cores were prepared in the same manner as those used in the study of formation factor. The cores were leached in tap water, weighed, dried, and saturated with a brine containing 7,500 ppm sodium chloride. The porosity and formation factor of these fully saturated cores were determined as before.

In order to reduce the water content of the cores to partial saturations, groups of these cores were permitted to dry slowly in air. As evaporation progressed, the weights and resistances of the cores were measured at intervals of approximately 30 minutes. The resistivity was then calculated as in the previous experiments. The instantaneous water saturation of a core was determined from the equation:

$$S_w = \frac{W_1 - (W_1 + s)}{W_2 - (W_1 + s)} \quad (8)$$

where S_w is the water saturation expressed as a fraction of its maximum value,

W_1 is the instantaneous weight of a core during evaporation,

s is the weight of sodium chloride in the core and

W_1 and W_2 are the weights of the dry core and core saturated with brine.

The amount of salt in a core is constant, so that as the water evaporates from the core, the salinity of the remaining water increases. Thus the resistivity of the water decreases as the saturation decreases. In order to calculate the resistivity index,

it is necessary to determine the instantaneous resistivity of the saturating water from tables. Then the resistivity index can be computed from the equation:

$$I = \frac{\rho_i}{\rho_{w_i}} \frac{\rho_w}{\rho_{100}} \quad (9)$$

where ρ_i is the instantaneous value of the core resistivity at the water saturation S_w ,

ρ_{w_i} is the instantaneous value of water resistivity at the saturation S_w ,

ρ_w is the water resistivity before evaporation and

ρ_{100} is the resistivity of the core at 100 percent water saturation.

A total of 387 measurements of I and S_w were made on the 45 cores. The results of these measurements are summarized graphically in the table below and in figure 8. These data were treated

| <u>Number of measurements</u> | <u>Average water saturation</u> | <u>Average resistivity index</u> |
|-----------------------------------|-------------------------------------|--------------------------------------|
| 25 | 11.0 | 117.0 |
| 39 | 18.5 | 30.7 |
| 44 | 25.9 | 13.2 |
| 50 | 34.2 | 7.46 |
| 38 | 45.0 | 4.36 |
| 39 | 54.5 | 3.33 |
| 46 | 65.8 | 2.31 |
| 57 | 79.4 | 1.67 |
| 49 | 91.4 | 1.26 |

statistically in the same manner as the data on formation factors.

The data were divided into groups according to class intervals of water saturation. It was then assumed that in each class the values of the logarithm of resistivity index are distributed normally about some mean value. The mean values were calculated and are shown in figure 8. The standard deviation and confidence limits of the data

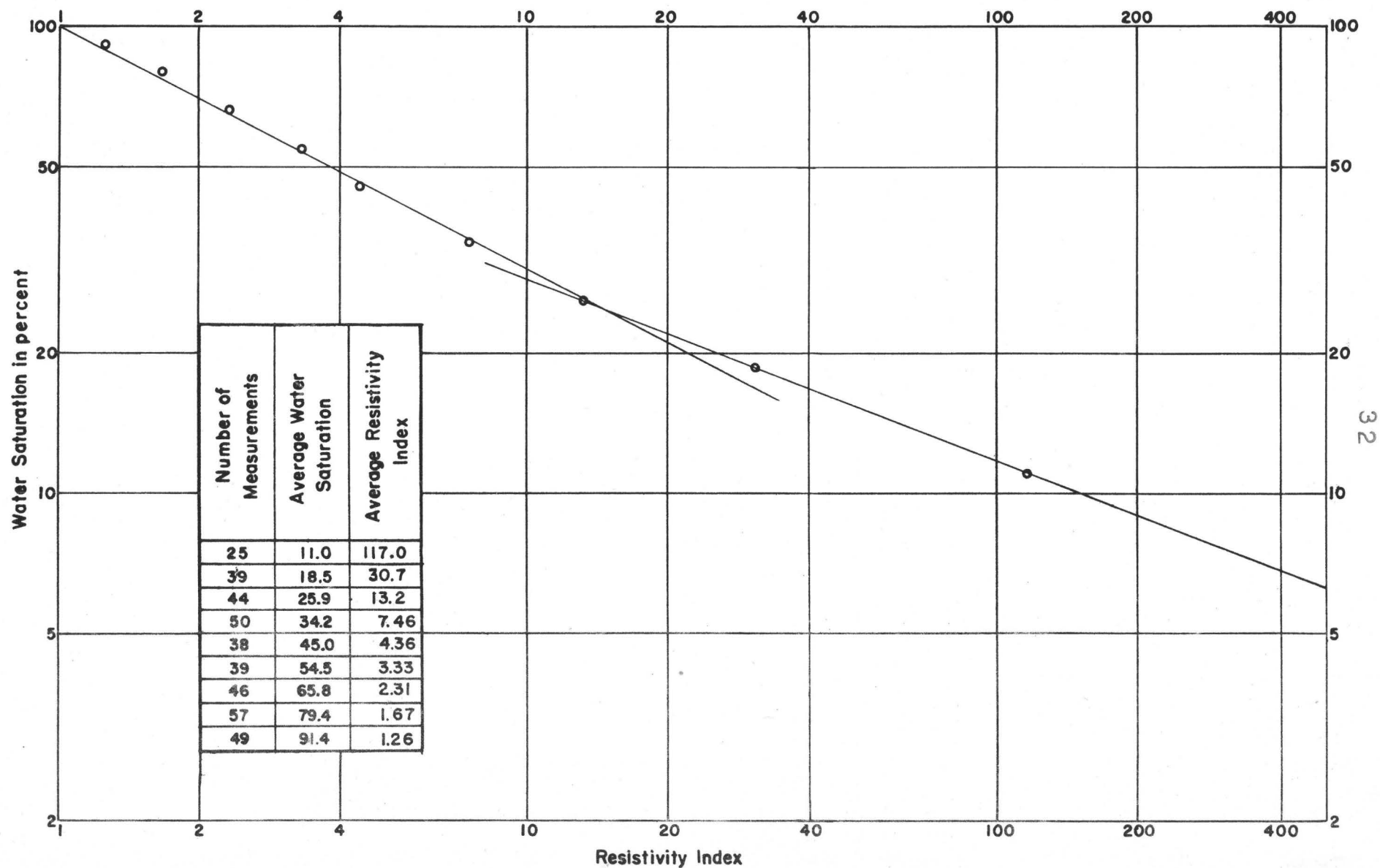


Figure 8: Resistivity index as function of water saturation.

were also computed; but, because the data showed only negligible scatter, these computations are not shown on the graph.

The data fit equation 2 with the following constants:

$$\begin{aligned} I &= S_w^{-1.92}; S_w > 0.245 \\ I &= 0.4S_w^{-2.57}; S_w < 0.245 \end{aligned} \quad (10)$$

This equation agrees well with the results that have been obtained from measurements on a number of water-wetted oil reservoir sandstones.

The influence of clay on resistivity was studied in a third group of 45 cores by measuring formation factors at several different water salinities. Because some of these salinities were quite low, it was deemed necessary to remove the salt remaining in the cores from their original connate water content more completely than was possible by the diffusion method. The cores were electro-dialyzed to remove their ion content.

In electrodialysis, the cores are saturated with distilled water and placed in a tray containing distilled water. A direct current is then passed through the cores for a long period of time, in this experiment 96 hours. This current causes ions in the cores to migrate to the oppositely charged electrode. The electrodes were carbon rods so that they themselves could not supply ions for current conduction. The electrodes were placed in porous alundum cups so that the water around the electrodes could be changed frequently, and the migrating ions prevented from reaching an equilibrium stage in which the potential due to their concentration gradient stopped further migration.

Resistivity measurements on these cores after electrodialysis indicated that their ion concentrations had been reduced to the range of 100 to 500 ppm equivalent sodium chloride salinity. This concentration was believed to be the lowest that could be obtained, as any clay present in the cores would account for that much conduction.

These cores were then saturated with a deaerated brine containing 1,875 ppm sodium chloride, using the same procedure. The volume of water taken by the cores and their resistances were measured. Following this, the cores were dried and saturated a second time with a brine of 1,875 ppm sodium chloride. The cores were saturated for only a short period, about 30 minutes, so that the salt remaining in a core from the first saturation would not have a chance to diffuse into the external brine. In this way, the second brine when it entered the cores would take up the salt from the first saturation into solution, and result in a brine with a salinity of 3,750 ppm sodium chloride. This process was repeated to obtain saturations with brines of 7,500, 15,000, 30,000, 60,000 and 120,000 ppm sodium chloride. Each time the cores were weighed dry and saturated and the resistances measured.

Resistivities were calculated from the resistance measurements, and these were used to determine apparent values of the formation factor corresponding to each water salinity. It was found that as the salinity of the saturating water increased, the formation factor increased to a maximum and then decreased slightly at very high salinities.

The data were treated statistically as before by dividing the cores into two groups: those with high porosities and those with low porosities. The percentages that the formation factor at a given salinity deviated from the formation factor of the same core at the highest salinity was calculated by the formula:

$$\text{percent deviation} = 100 (F_0 - F) / F_0 \quad (11)$$

where F_0 is the formation factor of a core saturated with a brine of 120,000 parts per million sodium chloride, and F is the formation factor at any other salinity. It was then assumed that these deviations were normally distributed about some average value for each water salinity and for each porosity group. The average values were computed, as well as the 92 percent confidence limits of these averages; the results of the measurements and computations are shown in the table below and in figure 9. The deviations for the low-porosity

| Brine resistivity | Mean $(1 - \frac{T}{T_0})$ of 12 cores in group I | Mean $(1 - \frac{T}{T_0})$ of 33 cores in group II |
|----------------------|--|---|
| 6.7 | 0.000 | 0.000 |
| 11.4 | -0.006 | -0.018 |
| 20.0 | -0.044 | -0.030 |
| 38.0 | -0.050 | -0.045 |
| 80.0 | -0.193 | -0.065 |
| 158.0 | -0.321 | -0.204 |
| 285.0 | 0.545 | 0.424 |

cores are higher than those for the high porosity cores, as expected. The negative deviations shown in figure 9 are unexpected, but possibly arise from an increase in the viscosity of the brine-clay mixture in the cores over that range of salinity, or possibly from progressive errors in the brine salinities during the repeated saturations.

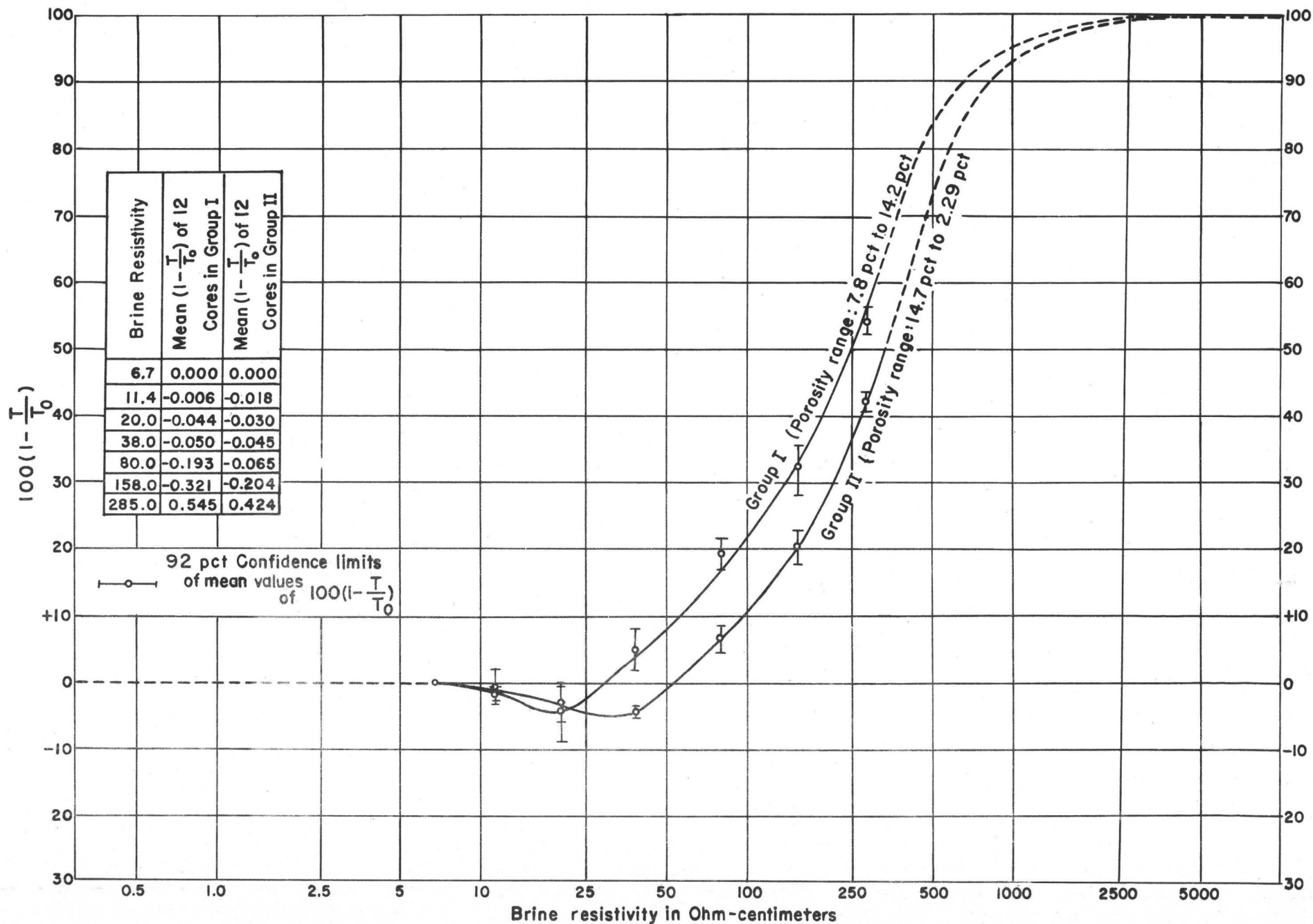


Figure 9: Variations of formation factor caused by variations in water salinity

It is evident that the data do not precisely fit the concept of the clay (or double-layer) conductivity electrically in parallel with the brine conductivity. The apparent salinity added to the brine in the core was calculated for several salinities and the results are given in table 2.

Table 2.--Apparent salinities associated with clay conductance

| <u>Salinity of the saturating brine</u> | <u>Equivalent salinity of clay</u> | |
|---|------------------------------------|-----------------------------------|
| | <u>Group 1</u> (low porosity) | <u>Group 2</u> (high porosity) |
| 1,875 ppm | 3,700 ppm | 1,900 ppm |
| 3,750 | 2,800 | 1,300 |
| 7,500 | 2,500 | 500 |
| 15,000 | 2,000 | -300 |
| 30,000 | -1,000 | -200 |

Spontaneous potential measurements

The measurement of the natural potentials existing in a fluid-filled drill hole was first described by the Schlumbergers and Doll (Schlumberger, C. and M., and Doll, H. G., 1934). They attributed the differences in potential that could be measured between adjacent sand and shale beds in a drill hole to a combination of diffusion and electrokinetic potentials. The diffusion potential was said to arise from a difference in ion concentrations between the fluid in the drill hole and the fluid in the rock and to obey Nernst's equation:

$$E.M.F. = K \log \frac{\rho_m}{\rho_w} \quad (12)$$

where K is a constant dependent on ion mobilities,

ρ_m is the resistivity of the water in the drill hole, and

ρ_w is the resistivity of the water contained in the rock around the drill hole.

The electrokinetic potential was attributed to the flow of the electrolyte from the drill hole past the solid surfaces of the sand grains as water is forced from the drill hole into the rock around it. This flow would give rise to an electrokinetic potential given by the equation (Wyllie, 1951):

$$\text{E.M.F.} = k PY \quad (13)$$

where P is the pressure differential between the drill hole and the rock, and k and y are constants dependent on the nature of the moving fluid and the properties of the solid surface along which the fluid is moving.

Unfortunately, even when this streaming potential can be taken into account, the remaining potential is usually too large to be explained by the Nernst equation. Only recently has a satisfactory explanation been given for the mechanism involved in the generation of the diffusion potential in clay-bearing rocks. McCardell, Winsauer and Williams (1953) have studied the diffusion potential arising when there is a concentration gradient in the presence of a distributed surface charge, or when there is a gradient in the distributed charge itself.

In an idealized pore, the clay particles lining the pore have a negative charge (represented by the small circles in figure 5) in the clay lattice positions vacated by cations during dissociation. This negative charge on the clay particle attracts an equal number of

positive ions in the surrounding solution. As a result, when there is an equilibrium distribution of charge, there are more cations than anions in solution in the vicinity of the clay.

If there is a large amount of clay, then the brine throughout the pore will be richer in cations than in anions by a number equal to the charge of the clay.

When such a clay-bearing rock is in contact with an external solution, there is a difference of cation concentration between the brine in the rock and the external brine. This gives rise to a phase-boundary potential, the magnitude of which is given by the equation (McCardell, Winsauer, and Williams, 1953):

$$E_p = -\frac{kT}{\epsilon} \ln \left[\frac{n_0}{2n} + \sqrt{1 - \left(\frac{n_0}{2n}\right)^2} \right] \quad (14)$$

where k is Boltzmann's constant, T is the absolute temperature,

ϵ is the ionic charge (one for sodium chloride),

n_0 is the ion concentration in equilibrium with the clay charge, and

n is the ion concentration in the free solution at some distance from the clay.

In addition to this phase-boundary potential that exists when the anion concentration is the same in the internal and external solutions, there is a diffusion potential when there is an actual difference in salinity of the internal and external solutions. This potential is given by an equation similar to that of Nernst (McCardell, Winsauer, and Williams, 1953):

$$E_d = -\frac{kT}{\epsilon} \frac{\mu_1 - \mu_2}{\mu_1 + \mu_2} \ln \left[\frac{\left(\frac{\mu_1}{\mu_2} + 1\right) \frac{n_B}{n_0} - 1}{\left(\frac{\mu_1}{\mu_2} + 1\right) \frac{n_A}{n_0} - 1} \right] \quad (15)$$

where μ_1 is the cation mobility,

μ_2 is the anion mobility,

n_B is the concentration of the concentrated electrolyte, and

n_A is the concentration of the dilute electrolyte.

In practice, the quantity n_0 will be large for shales or mudstones, in which all of the pores are clay lined, and small for sandstones with little or no clay. As a result, the phase and diffusion potentials will differ between sandstones and mudstones. This difference in potential will cause current to flow along the drill hole, and the ohmic drop in potential due to this current flow is recorded as a deflection on the spontaneous potential log as the inhole electrode passes a sandstone-mudstone contact.

Under ideal logging conditions, the spontaneous potential deflection between sandstones and mudstones should be a function of only three variables: the salinity of the water in the drill hole, the salinity of the connate water, and the equivalent salinity immobilized by the clay. The salinity of the water in the drill hole is a readily measurable quantity, so the spontaneous potential log can be used to calculate the connate water salinity when n_0 is known or can be estimated.

With this possibility in mind, the potentials across cores in contact with brines of two different salinities were measured. The cores used in these measurements were prepared in the same manner as those used in the resistivity experiments, and the porosities and formation factors were determined. The cores were then saturated with a brine consisting of 60,000 ppm sodium chloride.

These cores were coated with paraffin to prevent evaporation of their water content during the experiments. Two small holes in the coating on opposite sides of the cores permitted access of the external brine solutions. To make a measurement, a core was placed in the clamp (fig. 10), from which tubes extended to two brine reservoirs containing lead-lead chloride electrodes, so that the brines could be brought in contact with opposite sides of the core. A brine with a salinity of 60,000 ppm was placed in one reservoir, and a brine with a salinity of 600 ppm was placed in the other. The potential between the two lead-lead chloride electrodes was amplified with a d-c amplifier that had an input resistance of 10 megohms. The output of this amplifier was registered on a d-c voltmeter, and the recording system was calibrated at frequent intervals with a known voltage.

The potential developed in the cell was observed for a period of 30 minutes to 2 hours in order that an equilibrium value might be determined. It was observed that the potential had a non-zero value as the brines were first brought in contact with a core, and that within a few seconds the potential reached a maximum; the saline solution was negative with respect to the dilute solution. Following this, the potential changed sign and approached a positive value asymptotically over a period of approximately one hour. For very porous cores, the potential approached a positive maximum and then decreased, probably because of a change in the salinity of the brines in the reservoirs by rapid diffusion.

In order to eliminate the effects of electrode polarization at the two lead electrodes, the potential across an aluminum membrane

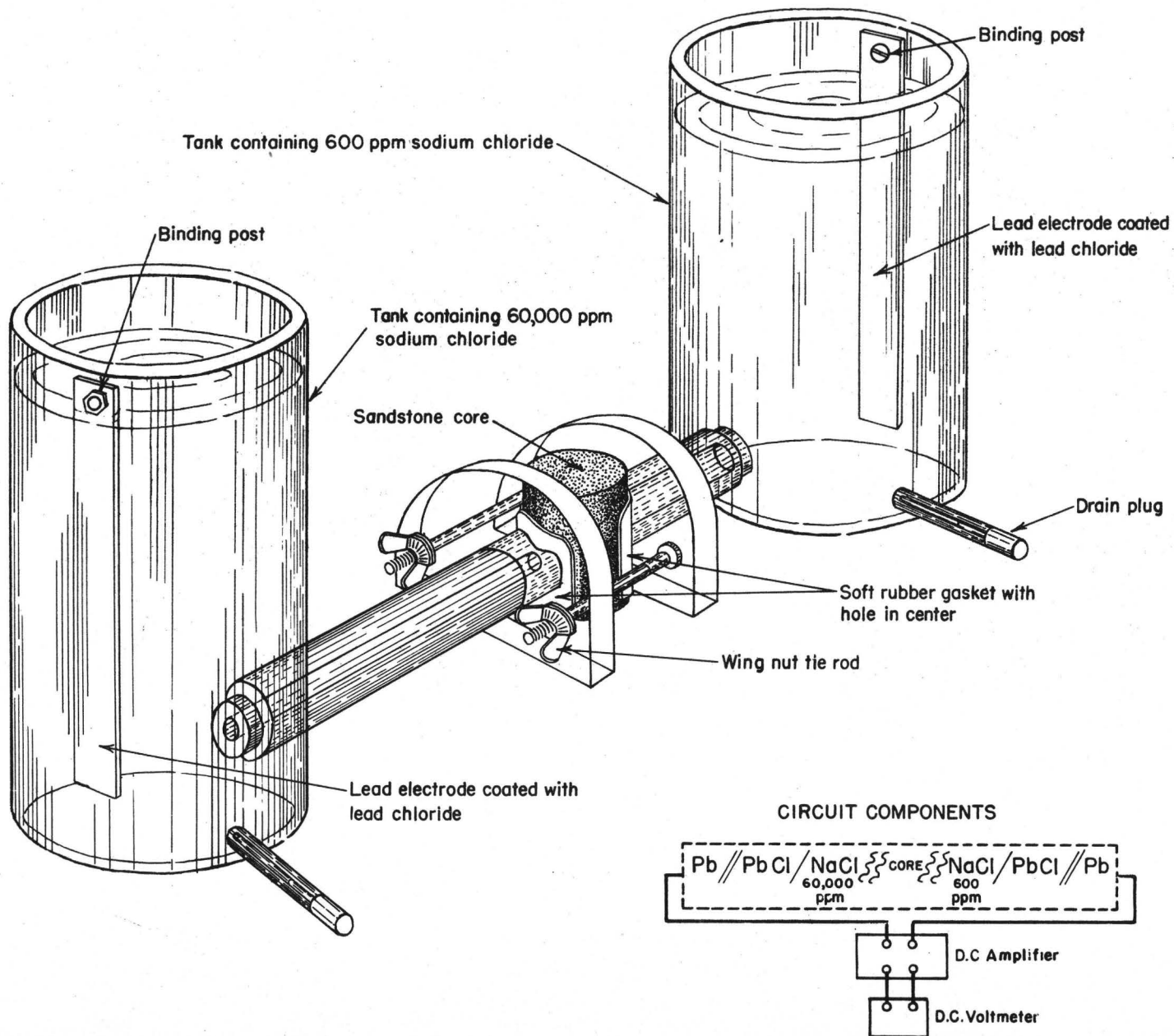


Figure 10: Device used in measuring the diffusion potentials of cores

was measured. The difference between this potential and the theoretical potential for the experimental conditions was subtracted from each of the other measurements.

The asymptotic value of potential was then used to calculate apparent values of the immobilized double-layer concentration according to equations 14 and 15. The results of these measurements and computations are presented in figure 11 in which n_0 has been plotted as a function of porosity.

These data show that n_0 varies from 40 to 56,000 ppm for the cores studied, all sandstone specimens. There is no pronounced relation between n_0 and porosity, except at low porosities. At porosities greater than 10 percent an average value for n_0 is 1,500 ppm. These values of n_0 were then used to determine the relation between the deflection recorded on the spontaneous potential logs taken in the Spud Patch area and the connate water salinity.

In spontaneous potential logging, a single electrode is raised through the drill hole, and its potential is measured with respect to a reference electrode at the surface. In interpretation, the deflection of this curve between a sandstone at depth A and a mudstone at depth B is measured. This deflection is equivalent to the voltage that would be measured between a pair of electrodes at A and B. The voltage is caused by the current flowing through the three media: the water in the drill hole, the sandstone, and the mudstone. The current arises from three phase-boundary potentials and two diffusion potentials, if it is assumed that there is no diffusion between the sandstone and the mudstone. A current tube, idealized to a considerable extent, is shown in figure 12 to indicate where each of

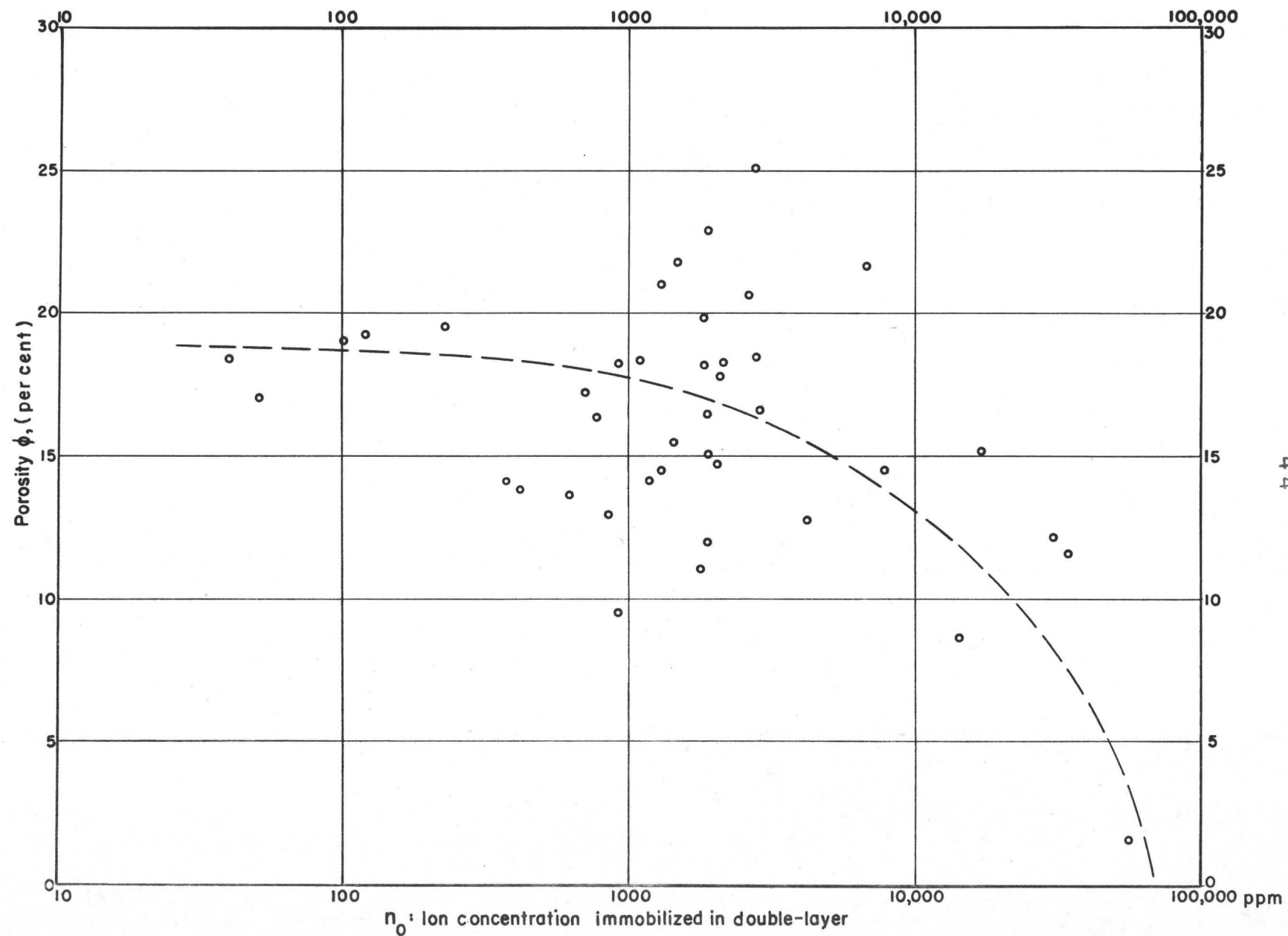


Figure II: Ion concentration immobilized in double-layer as function of porosity

these

/five potentials exists. The sum of the five is given by:

$$SP = {}_{12}E_P + {}_{12}E_d + {}_{23}E_P + {}_{31}E_P + {}_{31}E_d \quad (16)$$

where E_d and E_P are the diffusion and phase potentials respectively between the pairs of media represented by the numerical prescripts.

In terms of ion concentrations, these potentials would be:

$$SP = -\frac{kT}{e} \left\{ \left(\frac{\mu_1 - \mu_2}{\mu_1 + \mu_2} \right) \left[\ln \frac{\left(\frac{\mu_1}{\mu_2} + 1 \right) \frac{n_1}{on_3} - 1}{\left(\frac{\mu_1}{\mu_2} + 1 \right) \frac{n_2}{on_3} - 1} - \ln \frac{\left(\frac{\mu_1}{\mu_2} + 1 \right) \frac{n_1}{on_2} - 1}{\left(\frac{\mu_1}{\mu_2} + 1 \right) \frac{n_2}{on_2} - 1} \right] \right. \\ \left. + \ln \frac{\left(\frac{on_3}{2n_1} + \sqrt{1 - \left(\frac{on_3}{2n_1} \right)^2} \right) \left(\frac{on_2}{2n_3} + \sqrt{1 - \left(\frac{on_2}{2n_3} \right)^2} \right)}{\left(\frac{on_3}{2n_1} + \sqrt{1 - \left(\frac{on_2}{2n_1} \right)^2} \right) \left(\frac{on_3}{2n_1} + \sqrt{1 - \left(\frac{on_2}{2n_1} \right)^2} \right)} \right\} \quad (17)$$

where n_1 is the concentration of the anions in the internal electrolyte of the sandstone and mudstone,

on_3 is the mobilized ion concentration in the mudstone.

on_2 is the immobilized ion concentration in the sandstone,

and

n_2 is the ion concentration in the external solution filling the drill hole.

This equation was evaluated for the two extreme ranges of conditions to be expected for the logging conditions at Spud Patch:

a. Salinity of the water in the drill hole, n_1 , was assumed to be approximately 150 ppm, close to the salinity determined by resistivity measurements on a sample of water from Bell Canyon Reservoir.

b. The immobilized concentration in the sandstone, on_2 , was assumed to be between the limits of zero and 1,500 ppm.

c. The immobilized concentration in the mudstone, ϕ_{n3} , was assumed to be between the limits of 150,000 and 75,000 ppm.

d. A range in connate-water salinity from 1,000 to 240,000 ppm was considered.

The spontaneous potential deflections that would be recorded for this range in conditions are included as the shaded area in figure 13. On the basis of present information, the best estimate of the relation between spontaneous potential and connate-water salinity may be that given by the dashed line on this graph. This line was drawn on the assumption that the largest recorded spontaneous potentials would probably be associated with the most porous sandstones, which had undergone the most evaporation, and in which the salinity of the connate water would be high and the amount of clay low.

CORRELATION OF LABORATORY AND FIELD DATA

The measurements on the cores were made to provide a basis for the quantitative interpretation of electric logs in terms of porosity and water content. If we assume that the constants in the empirical equations obtained in these experiments are generally valid and that the effect of clay on resistivity and spontaneous potential can be ignored, or estimated, then there remain three unknown variable quantities: porosity, water saturation, and water salinity. Only two measurements are available in the field data for the determination of these three factors, so that the problem would seem to be indeterminate.

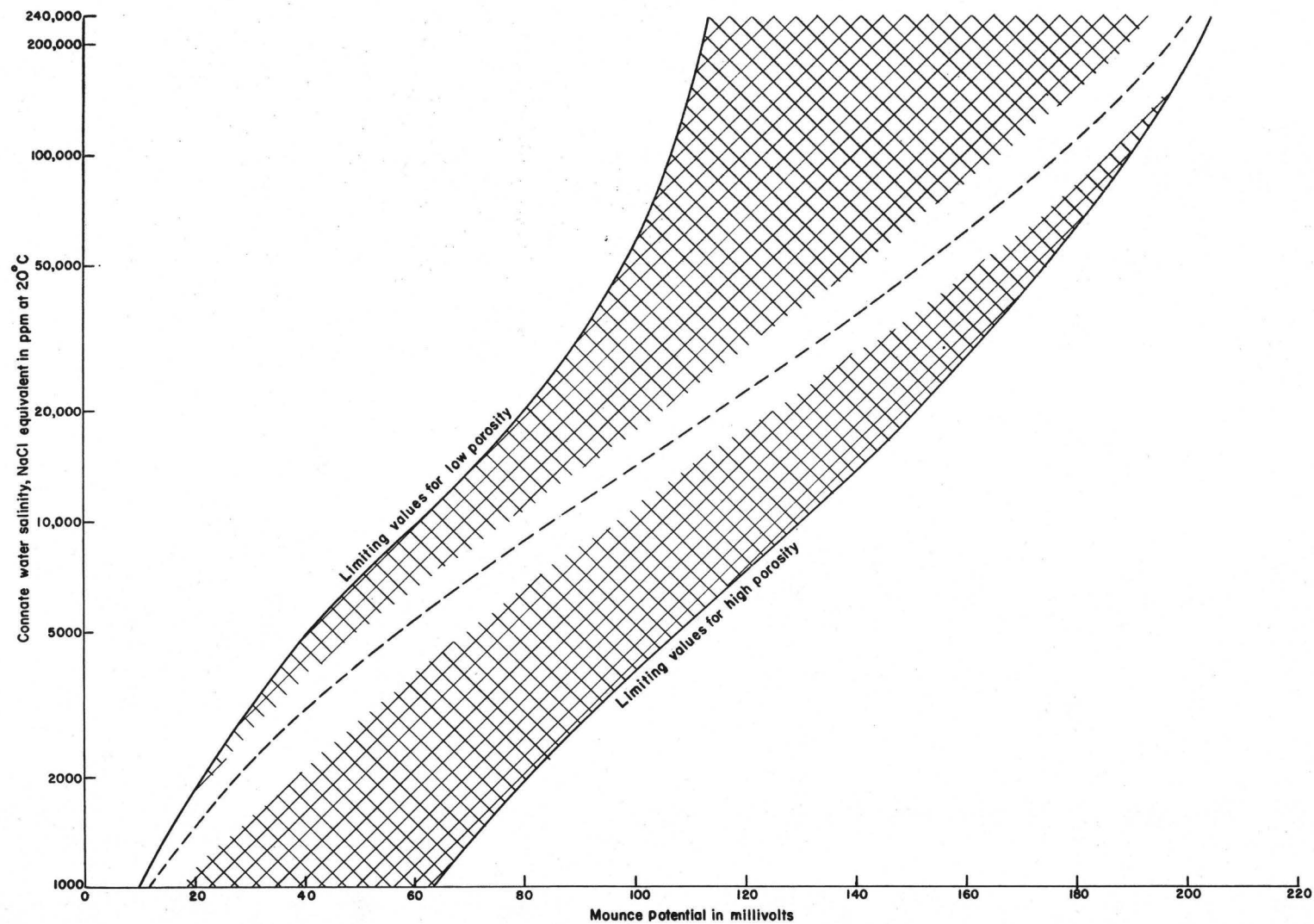


Figure 13: Calculated relationship between spontaneous potential and connate water salinity for logging conditions in the Spud Patch area, Colorado.

26653

One hope of determining these quantities from the field data lies in the possibility of finding a natural relationship between them: that is, to find that they are not independent variables. In the present case, it is possible that the sandstone members of the Morrison formation were at one time saturated with a connate water of uniform salinity. It is likely that the Morrison formation has been dehydrated to some extent in the areas in which these studies were carried out, because it is close to the surface and frequently crops out on mesa rims. The present values of water saturation, resistivity, and natural potential of the sandstone should be interrelated.

The resistivity of the sandstone around a drill hole at the time of electric logging is:

$$\rho_r = 0.62 \rho_{w_r} \phi^{-2.10} S_w^{-1.92} \quad (18)$$

where ρ_{w_r} is the resistivity of the connate water at the time of logging, S_w is the water saturation, and ϕ is the porosity, restricted to the limits 14 percent to 25 percent and with S_w greater than 25 percent.

If the present connate water is a remnant of an original connate water of resistivity ρ_{w_1} that has evaporated without the removal or addition of salt, then the present water resistivity is a function of the present water saturation and the original water resistivity:

$$S_w = \left(\frac{\rho_{w_r}}{\rho_{w_1}} \right)^{1.05} \quad (19)$$

This relationship is valid for a temperature of 20° C and is accurate within 5 percent over the range from 100 to 100,000 ppm.

By using this relationship, one unknown quantity can be eliminated from equation 18, and

$$\rho_r = 0.62 \rho_{w1}^{2.02} \rho_{wr}^{-1.02} \phi^{-2.10} \quad (20)$$

This can be written as:

$$\frac{\text{Constant}}{\rho_r \phi^{2.10}} = (\rho_{wr})^{1.02} \quad (21)$$

In addition, the resistivity of the connate water is related to the spontaneous potential by equation 17, which may be expressed simply as:

$$\text{S.P.} = -K \log (\rho_m / \rho_{wr}) \quad (22)$$

where ρ_m is the resistivity of the water in the drill hole and K varies from 35 for low porosities to 70 for high porosities and salinities, and represents the influence of the various factors involved in equation 17. By combining equation 21 with equation 22, the following is obtained:

$$\log \text{constant} - \log \rho_r \phi^{2.10} = 1.02 \left(\frac{\text{S.P.}}{K} + \log \rho_m \right) \quad (23)$$

Thus, the equation for the resistivity of the sandstone members of the Morrison formation has been reduced to a form in which there are only two quantities not measurable in normal logging routine: the porosity and the spontaneous potential coefficient, K. However, the coefficient K can be predicted within reasonable limits, as indicated by figure 13. This means that porosity is determinable from electric log data if the initial assumptions of a constant water salinity and consequent evaporation are correct.

To test this hypothesis, the quantity $\rho_r \phi^2$, determined from the resistivity log and core analysis, was plotted as a function of the spontaneous potential deflection for each of the six drill holes from which cores were studied (fig. 14). In all six cases, there is

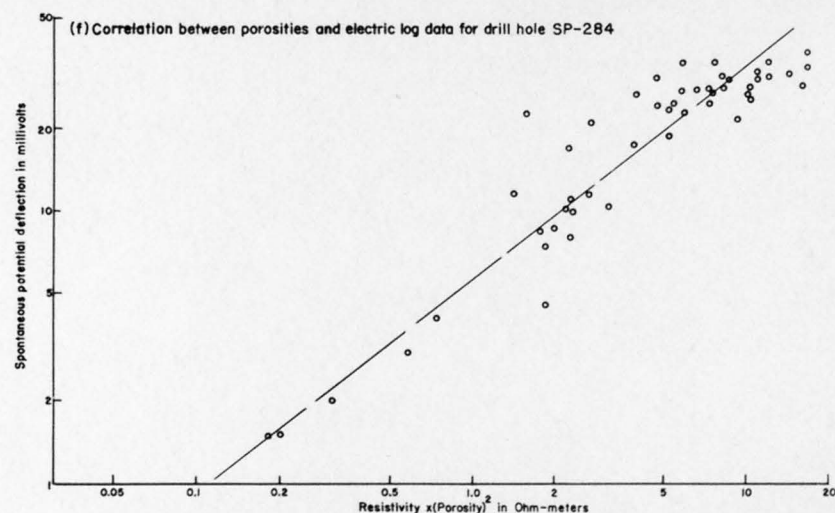
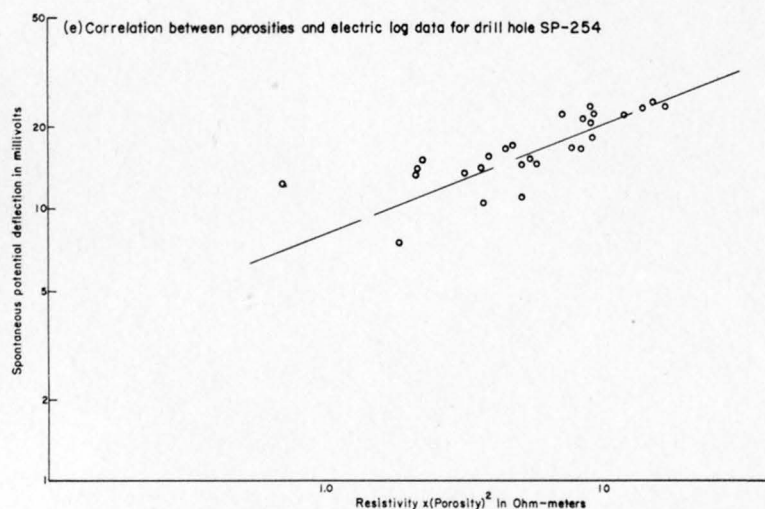
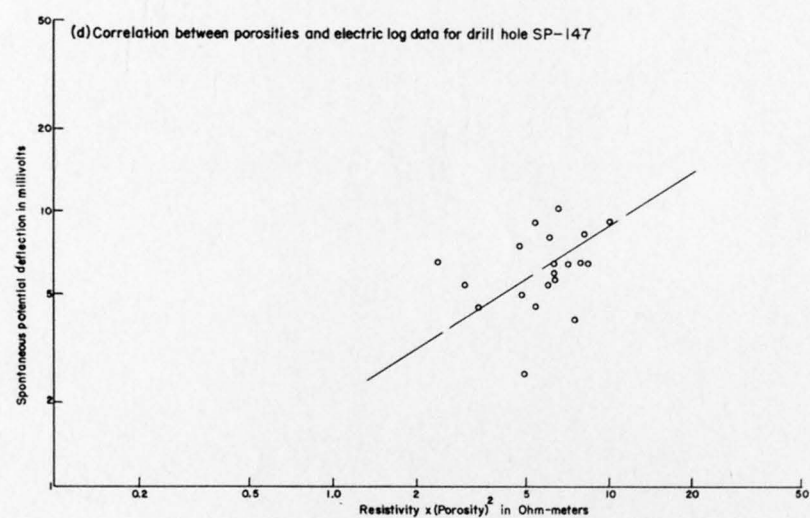
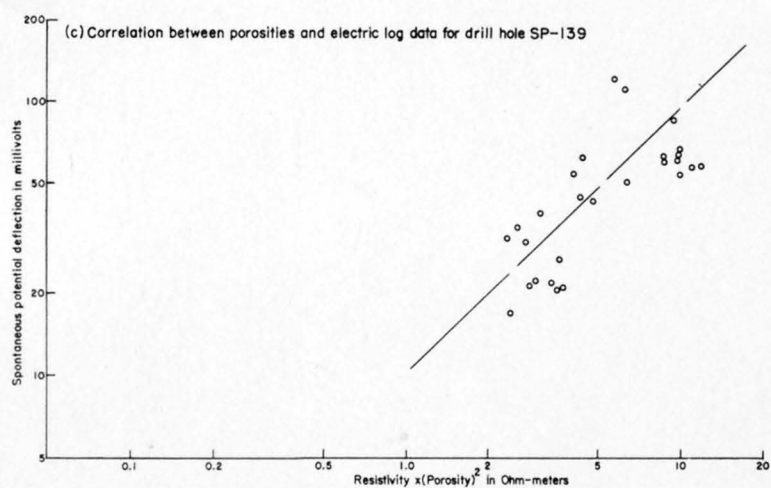
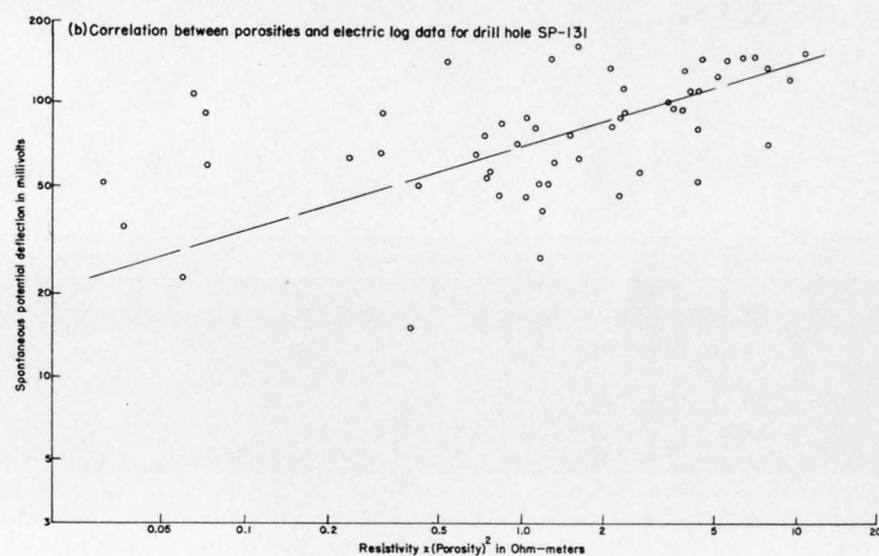
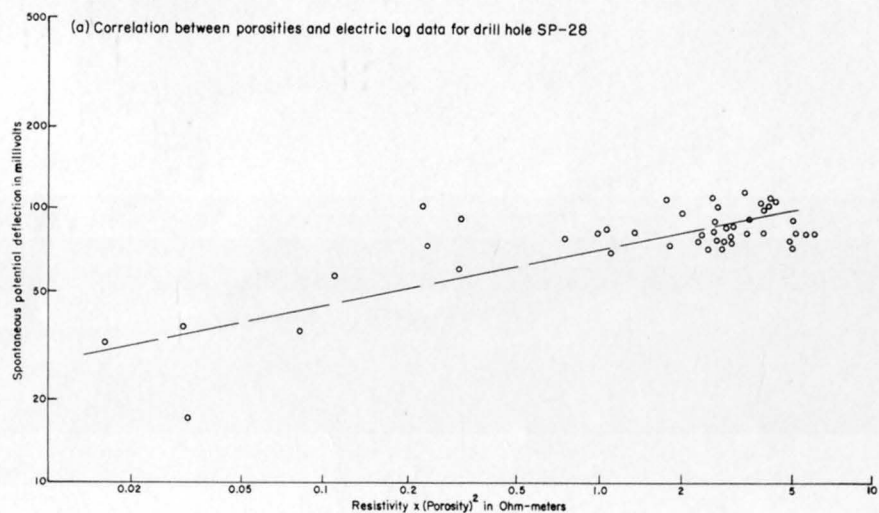


Figure 14: Correlation of laboratory measurements on cores with electric log data.

a trend recognizable in the data that indicates that there is at least some truth in the original assumptions.

The considerable scatter apparent in these data is probably not all caused by the shortcomings of the original hypothesis. There are other sources of error that almost certainly contribute considerable deviations. Among these is the error involved in matching the core depths with depths on the electric log, so that the correct values of resistivity and spontaneous potential can be read.

Another major source of error is the inability of determining accurately the resistivity of thin layers by any logging arrangement. The apparent resistivity recorded on the log may be larger or smaller than the true resistivity, depending on the resistivities of the adjoining strata. The single-point log was the most sensitive device used, but it was also the most subject to errors from variations in the resistivity of the water in the drill hole. Single-point logs of adequate quality for use in these correlations were available for only two of the six wells under consideration: SP-131 and SP-284. For the other four drill holes, the 8-inch normal spacing resistivity log was used because it was a compromise of the large disturbing effects of the water in the drill hole on the log with 4-inch spacing and the large disturbing effect of bed thickness on the log with 24-inch spacing.

There may also be errors because the properties measured on the individual core are not representative of the material around the drill hole that controls the response of the electric logs. The laboratory measurements were made on a specimen of core approximately one cubic inch in size, but the resistivity measured in the electric

logs is the average resistivity of a minimum of one cubic foot of material around a drill hole. The degree to which this difference is the source of the scatter in the correlation diagrams of figure 14 is a measure of the inch-to-inch variation of the physical properties of sandstone.

In a number of cases, four samples had been cut from cores over a six inch depth interval. Measurements of porosity and formation factor had been made on all these cores, and the data were used to compute the variance of the averages for each group. The variance for any one group is given by the equation:

$$\sigma^2 = 1/3 \left(\sum_{i=1}^4 \phi_i^2 - \frac{1}{4} \left(\sum_{i=1}^4 \phi_i \right)^2 \right) \quad (24)$$

where σ is the variance or square of the standard deviation. The value computed from this equation is not the variance of the actual data, but a best estimate of the variance of the population from which the data are a subsample. Forty-one values of this best estimate of variance were computed; the highest values were those for the groups of cores of low average porosity. The results of these computations are shown in figure 15 in which the standard deviation is expressed as a percentage of the average porosity. This graph shows for a given porosity how closely a single value of porosity measured on a core represents the average porosity of the bed from which it came. It is obvious that the limits of error are quite wide.

Because of the magnitude of these different sources of error, it is likely that the correlations indicated in figure 14 are considerably better than the scatter of the data would lead one to believe. In order to find the relationship indicated by these correlations, it is necessary to use the same statistical approach used earlier on the core data.

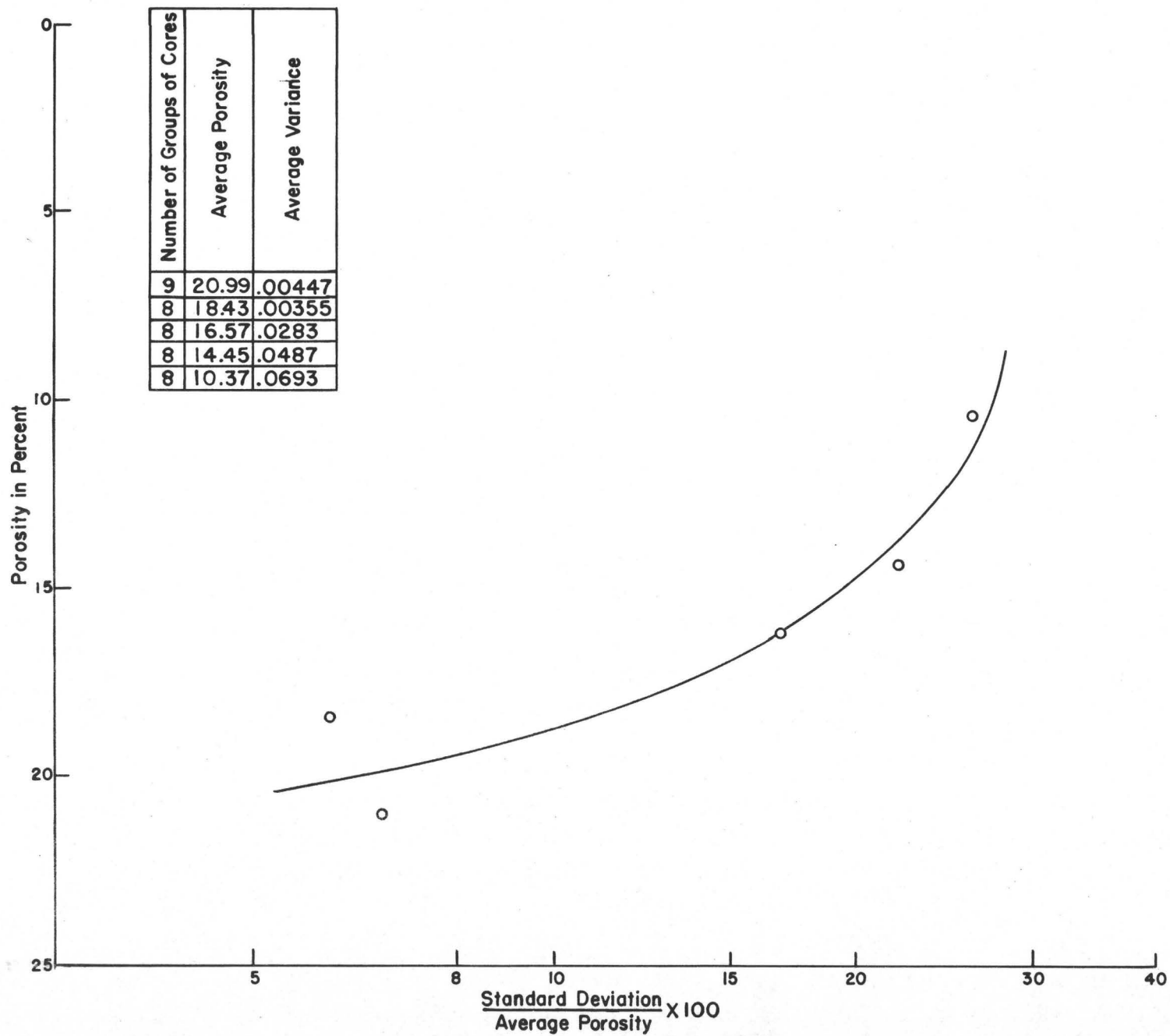


Figure 15: Summary of data on the inch-to-inch variations of porosity in sandstone cores.

The absolute range of the variables plotted in figure 14 varies considerably from drill hole to drill hole, so that the data from the several drill holes cannot be compared directly. In order to normalize the data from all of the drill holes to the same scale, the variables S.P. and $\rho\phi^2$ were expressed as percentages of their maximum values in each drill hole.

The data were grouped in classes according to the value of the quantity ($\rho\phi^2/\max \rho\phi^2$), and it was assumed that for each class the values of S.P./Maximum S.P. are normally distributed about a mean. The average was computed, and the standard deviation of the values of S.P./Maximum S.P. for each class of $\rho\phi^2/\max \rho\phi^2$ determined. The 65 percent confidence limits were calculated for both individual values of the data and for the mean values of S.P./Maximum S.P. The results are shown in figure 16 in which the horizontal scale is logarithmic and the vertical scale is doubly logarithmic.

The data are also presented in tabular form on figure 16 and with the standard deviation of the average porosity corresponding to each plotted mean is listed. This standard deviation indicates the minimum part of the scatter of the data that can be attributed to nonrepresentative values of porosity.

The conclusion is that there is a significant correlation between the electric log data and the core data, and this correlation supports the hypothesis that sandstones of the Morrison formation were originally fully saturated with a brine of uniform salinity and that the present salinity of the connate water is a result of the evaporation of this original brine without removal of salt by circulating ground waters.

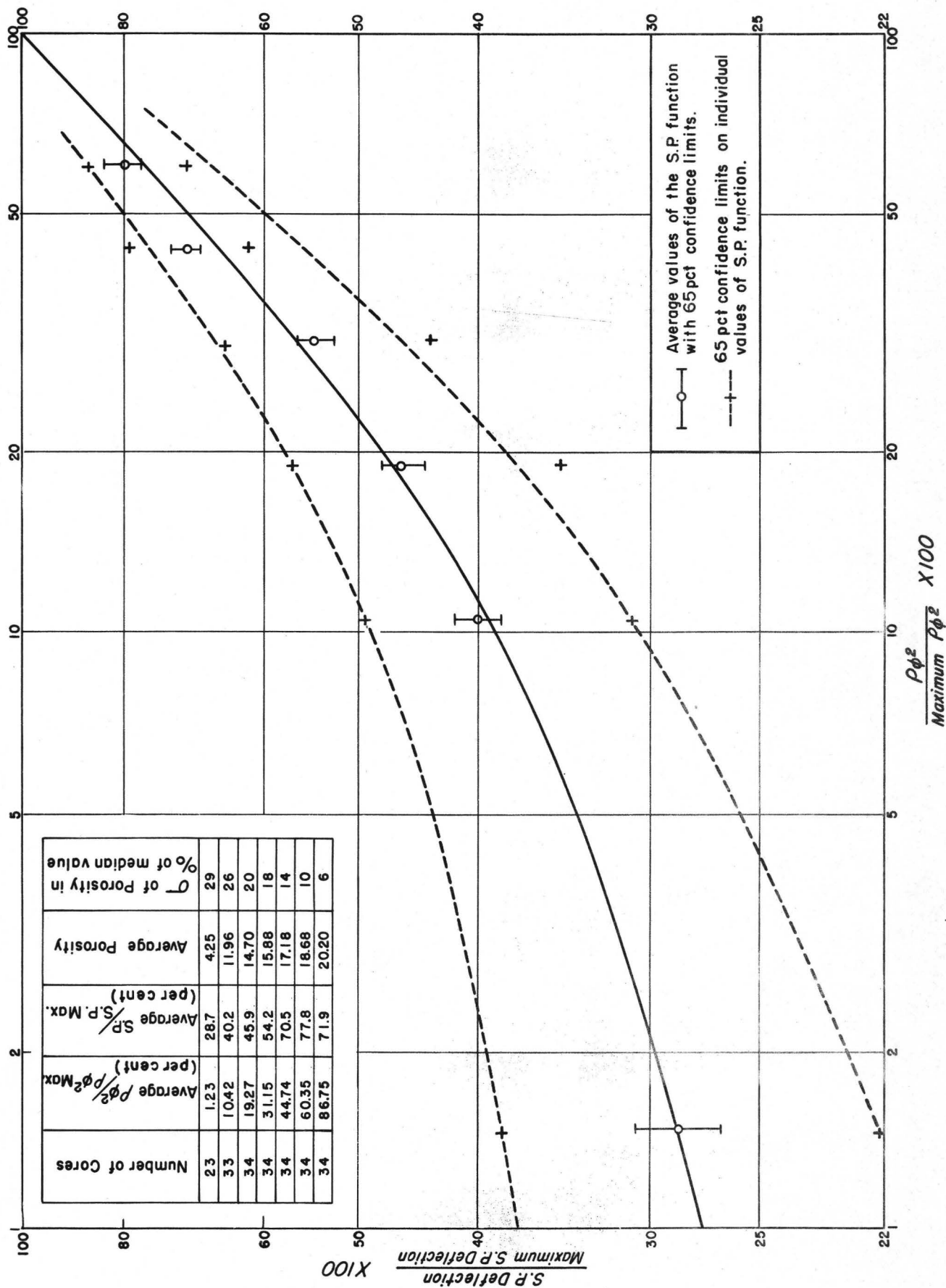


Figure 16: Empirical relationship between porosity, electric log resistivity, and spontaneous potential deflection.

QUANTITATIVE INTERPRETATION OF LOGS

The correlation of the core data with the electric log data indicates that porosity can be determined directly from electric log data. Once porosity is determined and the salinity of the water is found from the spontaneous potential log, it is possible to calculate the water saturation from the resistivity log.

Such an interpretation was attempted on logs of the Salt Wash member of the Morrison formation in 44 drill holes in the Spud Patch area. The procedure was as follows:

- (1) The maximum values of resistivity and spontaneous potential were read directly from the logs;
- (2) The average values of resistivity and spontaneous potential were determined by planimetering the areas between the respective logs and their base lines. These areas were divided by the thickness of the logged section to give average values;
- (3) The average porosity was determined by forming the ratio $S.P./\text{maximum } S.P.$ and determining the corresponding value of $\rho/\rho^2/\text{max } \rho/\rho^2$ from figure 16. The average porosity was determined by assuming a maximum porosity of 22 percent corresponding to the maximum resistivity;
- (4) The average connate water salinity was determined from the average spontaneous potential, by using figure 13;
- (5) The average water saturation was determined by dividing the average resistivity from the electric log by the resistivity of connate water determined above. This

average salinity was corrected for the influence of clay by using the data in figure 9. The water saturation was then computed from equation 18.

- (6) The apparent salinity of the original brine saturating the sandstone was estimated by calculating the dilution of the average water salinity necessary to fill the pore space completely.

The results of these interpretations are presented in table 3 as average values for the several classes of favorability to which the drill holes belonged.

Table 3 gives an idea of the physical properties associated with favorability that result in the apparent correlation of resistivity with occurrence of ore. There is no correlation between spontaneous potential and favorability or ore occurrence. Large- and small-amplitude spontaneous potential curves are obtained in drill holes in both favorable and unfavorable ground, and the spontaneous potential measurements are the same for favorable and unfavorable holes, as shown in table 3.

The salinities that were calculated from these spontaneous potential measurements are in terms of sodium chloride as the ionized salt. It is likely that the salinity is due to some other salt, such as calcium bicarbonate. If this is so, the equivalent sodium chloride salinity is not the same as the actual salinity in a different salt. If that salt is calcium bicarbonate, then the equivalent sodium chloride salinity is about one-half the actual salinity.

Table 3.--Results of the quantitative interpretation of electric logs

| <u>Favorability class</u> | <u>Favorable</u> | <u>Semi-favorable</u> | <u>Unfavorable</u> |
|---|------------------|-----------------------|--------------------|
| Number of drill holes: | 24 | 12 | 8 |
| Maximum S.P. (mv.) average for drill holes of each class: | 66.4 | 28.6 | 64.4 |
| Corresponding water salinity (ppm): | 6400 | 2100 | 6100 |
| Average S.P. (mv.) average for drill holes of each class: | 38.9 | 16.7 | 36.2 |
| Corresponding water salinity (ppm): | 3050 | 1300 | 2730 |
| Maximum resistivity (ohm-m), average for drill holes for each class: | 423 | 385 | 338 |
| Average resistivity (ohm-m), average for drill holes of each class: | 230 | 203 | 180 |
| Average porosity (percent): | 19.1 | 18.2 | 18.1 |
| Average water saturation (percent): | 43 | 57 | 53 |
| Minimum water saturation (percent) average for drill holes of each class: | 21 | 32 | 32 |
| Original water salinity before evaporation (ppm): | 1310 | 740 | 1450 |
| Product of sandstone thick- ness and average resis- tivity (ohm-m-ft.): | 16400 | 13300 | 7710 |

The calculated average porosities seem to vary with favorability, as evidenced by the decrease in porosity for the less favorable drill holes. The saturations, however, show a more pronounced variation from drill holes in favorable ground to those in unfavorable ground. Saturation seems to be the property which causes the correlation of resistivity with favorability: that is, the saturation seems to be reduced most in the drill holes that are most favorable for the occurrence of ore.

When the salinities are calculated on the assumption that the connate water is diluted to 100 percent of the pore space in all but three of the drill holes, they fall in the range 650 to 1,800 ppm equivalent sodium chloride. The three exceptions fall far out of this range being between 3,500 and 6,500 ppm.

USE OF ELECTRIC LOGGING IN EXPLORATION

Studies of the magnitude and extent of electrical anomalies that may be associated with occurrence of ore on the Colorado Plateau have shown that there is an increase in the average sandstone resistivity and a large increase in the product of resistivity and sandstone thickness in the areas that are most favorable for ore occurrence. Anomalously high resistivities are apparent in many drill holes in mineralized ground, but in general these anomalies are too small in extent to be detectable by surface resistivity measurements.

A contour map of the product of resistivity and sandstone thickness has indicated that the dimensions of favorable areas are of the order of one to several thousand feet, at least in the area studied.

If this is so generally, it would be expected that even with ideal conditions in the overlying beds, the variations in resistivity of the ore-bearing member at depths of 500 feet, would not be detectable by surface resistivity measurements, as Wenner electrode spacings of 1,000 feet and more would be required, and with these large spacings, no single resistivity sounding could be made with the electrode arrangement entirely within the favorable area.

Electric logs, however, are capable of giving much of the information that is obtained by visual examination of cores. The electric log is particularly suited to the differentiation of sandstone from mudstone and should give a more reliable distinction between the two than is possible from core inspection.

Mudstone exhibits a minimum on the resistivity log and a maximum (deflection to the right) on the spontaneous potential log. These minimum and maximum deflections are referred to as the "shale base line" by convention.

Because the Morrison formation is composed of mudstones and sandstones, any deflection to the right of the resistivity base line accompanied by a deflection to the left of the spontaneous potential base line can be attributed to the presence of a sandstone at that depth. Small deflections correspond to shaley sandstone and large deflections correspond to relatively pure sandstone. Deflections of only one curve from its base line are usually caused by changes in the salinity of the water in the drill hole rather than by lithologic changes.

The identification of mudstone and sandstone from the electric log is usually the same as that from visual examination of the core.

However, there may be some disagreement where there is a gradational contact between sandstone and mudstone, when it is difficult to separate the two visually. Under these conditions, the electric log may be superior to the actual examination of the core, as it provides a physical basis for the division between the two strata.

On the other hand, the electric log cannot give information on color and the presence of vanadium minerals or of certain accessory minerals that are factors used by the geologist in determining favorability. However, the electric log may be able to provide an index of favorability which is comparable in reliability determined by geologic guides to ore.

The advantage of electric logging is that when combined with radioactivity logging, it will give most of the information necessary in the exploration for ore at a lower cost than coring and examination of cores. In addition to reduced drilling costs, the time required to interpret a group of electric logs in the office would be much less than the time required to examine core at a group of drill holes, with resulting economy.

The utility of the electric log is not limited to the determination of information now obtained from cores; it is also capable of giving additional information such as porosity and water saturation which may be of value in the future. If production from the deeper Morrison deposits should become practical, it would be necessary to know porosities and water saturations for proper production practice. It has been found in oil-field practice that the determination of such properties from the electric log is more reliable than core analysis, as electric log data give an average value representative

of the rock in place. Core analysis is subject to the errors caused by the inch-to-inch variation in physical properties described in this report.

In the petroleum industry, the electric log has become an indispensable tool for the determination of the textural properties of the rock in place in a drill hole. There is reason to believe that the electric log may be valuable in the evaluation of the strata penetrated by exploratory drill holes here also.

The electric logs can be used not only to identify different lithologic units but to correlate such units between neighboring drill holes. Correlation of very small sandstone units is possible where drill holes are on a 50-foot spacing. Correlation between more widely spaced drill holes must necessarily be less detailed.

REFERENCES CITED

- Fischer, R. P., 1942, Vanadium deposits of Colorado and Utah, a preliminary report: U. S. Geol. Survey Bull. 936-P, p. 363-394.
- Keller, G. V., 1953, The role of wettability in the electrical resistivity of sands: Oil and Gas Jour., v. 51, no. 35, p. 62-65.
- McCardell, W. M., Winsauer, W. O., and Williams, M., 1953, Origin of the electric potential observed in wells: Am. Inst. Min. Metall. Engineers Trans., v. 198, p. 41-51.
- Schlumberger, C., Schlumberger, M., and Doll, H. G., 1934, A new contribution to subsurface studies by means of electrical measurements in drill holes: Am. Inst. Min. Metall. Engineers Trans., v. 110, p. 273-289.
- Weir, D. B., 1952, Geologic guides to prospecting for carnotite deposits on the Colorado Plateau: U. S. Geol. Survey Bull. 988-B, p. 15-27.

Winsauer, W. O., and McCardell, W. M., Ionic double layer conductivity in reservoir rock: Paper presented at the Los Angeles meeting, Petr. Branch, Am. Inst. Min. Metall. Engineers, October, 1952.

Winsauer, W. O., Shearin, H. M., Masson, P. H., and Williams, M., 1952, Resistivity of brine saturated sands in relation to pore geometry: Am. Assoc. Petroleum Geologists Bull., v. 36, p. 253-277.

Wyllie, M. R. J., 1951, An investigation of the electrokinetic component of the self potential curve: Am. Inst. Min. Metall. Engineers Trans., v. 192, p. 1-18.