

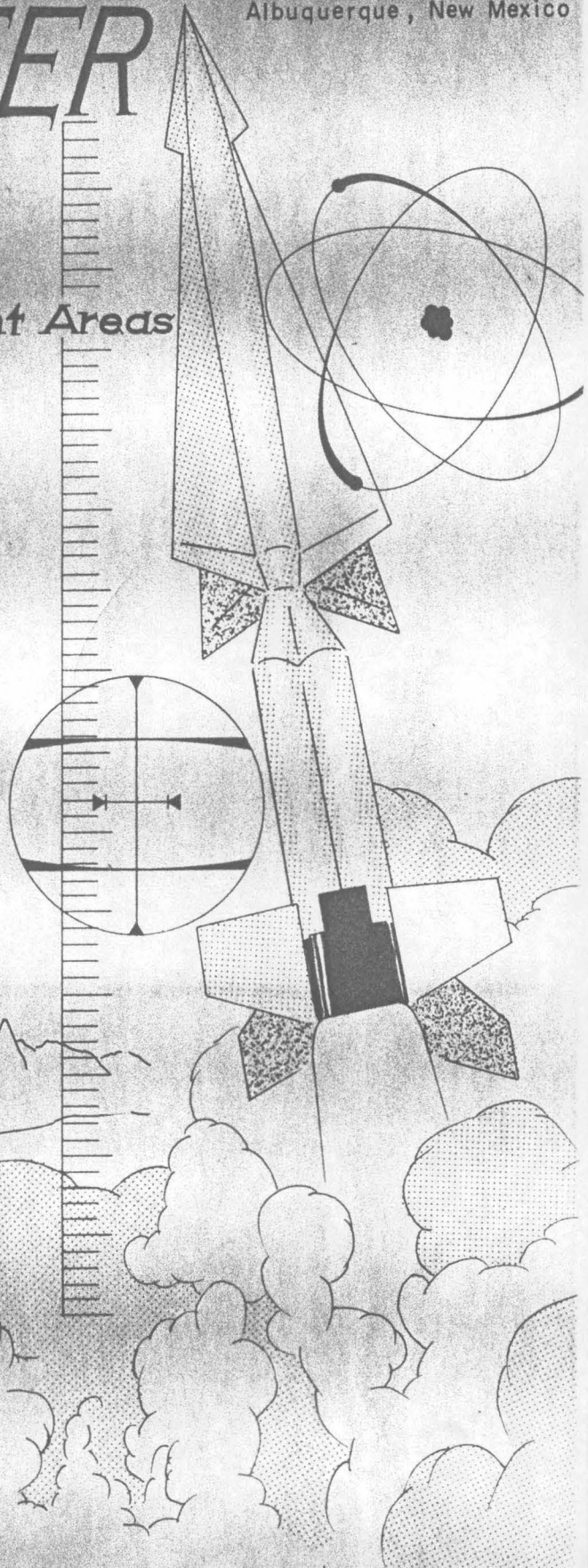
T. C. KELLY

SUMMARY OF GROUND-WATER DATA

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
Albuquerque, New Mexico

Post Headquarters & Adjacent Areas
White Sands Missile Range

by
T. E. Kelly



Open-file report
Prepared by the U.S. Geological Survey,
in cooperation with White Sands Missile Range
March 1973

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CONTENTS

	Page
ABSTRACT -----	6
INTRODUCTION -----	7
PURPOSE -----	10
HYDROLOGIC DATA -----	11
SUMMARY -----	53
BIBLIOGRAPHY -----	54

ILLUSTRATIONS

	Page
Figure 1.--Index map -----	8
2-3.--Map showing:	
2.--Percentage of sand between 500 and 1,000 feet ---	20
3.--Location of rain gages and surface-water stations -----	21
4-11.--Hydrograph of:	
4.--Main Gate well and monthly pumpage figures for well field -----	23
5.--Test wells T-4, T-5, and T-6 -----	25
6.--Test wells T-7 and T-8 -----	26
7.--Test wells T-9, T-10, and T-11 -----	27
8.--Test wells T-12, T-13, and T-14 -----	28
9.--Test wells T-15, T-16, T-17, and T-18 -----	29
10.--Test wells SMR-2, SMR-3, and SMR-4 -----	30
11.--Gregg well and HTA windmill -----	31
12-20.--Graph showing:	
12.--Annual pumpage and hydrograph of supply well 10A-	32
13.--Annual pumpage and hydrograph of supply well 11 -	33
14.--Annual pumpage and hydrograph of supply well 13 -	34
15.--Annual pumpage and hydrograph of supply well 15 -	35
16.--Annual pumpage and hydrograph of supply well 16 -	36
17.--Annual pumpage and hydrograph of supply well 17 -	37
18.--Annual pumpage and hydrograph of supply well 18 -	38

ILLUSTRATIONS - Concluded

	Page
Figure 19.--Annual pumpage and hydrograph of supply well 19 -	39
20.--Annual pumpage and hydrograph of supply well 20 -	40
21.--Hydrograph of supply wells HTA-1 and SMR-1 -----	41
22.--Hydrograph of old supply wells 12 and 14 -----	42
23.--Contour map of water table, 1949 -----	44
24.--Contour map of water table, 1964 -----	45
25.--Map showing water-level change between	
1949 and 1964 -----	46
26.--Contour map of water table in Post Headquarters	
area, July 1972 -----	47
27.--Map showing water-level change between	
1964 and 1972 -----	48
28.--Map showing water-level change between	
1949 and 1972 -----	50
29.--Cross sections of the Post Headquarters area ----	51
30.--Map showing configuration of base of aquifer ----	In pocket
31.--Map showing thickness of fresh water -----	In pocket
32.--Contour map of water table, July 1972 -----	In pocket
33.--Map showing chemical quality of water samples	
from selected wells -----	In pocket

TABLES

	Page
Table 1.--Record of wells and test holes in	
Post Headquarters and adjacent areas -----	12
2.--Hydrologic characteristics of the aquifer in the	
vicinity of the supply and test wells -----	15
3.--Specific capacity of supply wells -----	18

SUMMARY OF GROUND-WATER DATA, POST HEADQUARTERS AND
ADJACENT AREAS, WHITE SANDS MISSILE RANGE

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ABSTRACT

Geohydrologic data have been obtained from more than 100 wells and test holes that have been drilled in the Post Headquarters and adjacent areas of White Sands Missile Range. Observation-well data show that, in general, a continuous decline of the water table has occurred in the vicinity of the well field since production began in 1949. Approximately 40,000 acre-feet of water has been produced from the aquifer to date (1972).

A series of maps are presented which show the changes that have occurred in the well field as the result of development.

INTRODUCTION

Since 1953 a nearly continuous program of water-resources investigations has been conducted on White Sands Missile Range by the U.S. Geological Survey through the cooperation of the Facilities Engineering Directorate, White Sands Missile Range. These investigations have aided in the development and utilization of the ground-water resources, as well as contributing to the general knowledge of the geologic and hydrologic environment of the Missile Range.

White Sands Missile Range is located in the Tularosa Basin, about 25 miles east of Las Cruces, N. Mex., and approximately 40 miles north of El Paso, Tex. (fig. 1). The area included in this study encompasses approximately 300 square miles and includes the Post Headquarters and adjacent areas. The Post Headquarters is situated in a reentrant formed by the junction of the San Andres, San Augustin, and Organ Mountains (fig. 1). The eastern limit of the study area was arbitrarily set at approximately 15 miles east of the mountain axis. Where data were available, the area of investigation was extended to make optimum use of the data.

The central part of the Tularosa Basin east of the Post Headquarters contains saline water. Of particular significance to the ground-water resources of the area is the reentrant of the basin in the bordering mountain front. Seemingly this reentrant has entrapped a larger quantity of fresh water than commonly occurs along the linear mountain front, and it is here that the major water development has occurred.

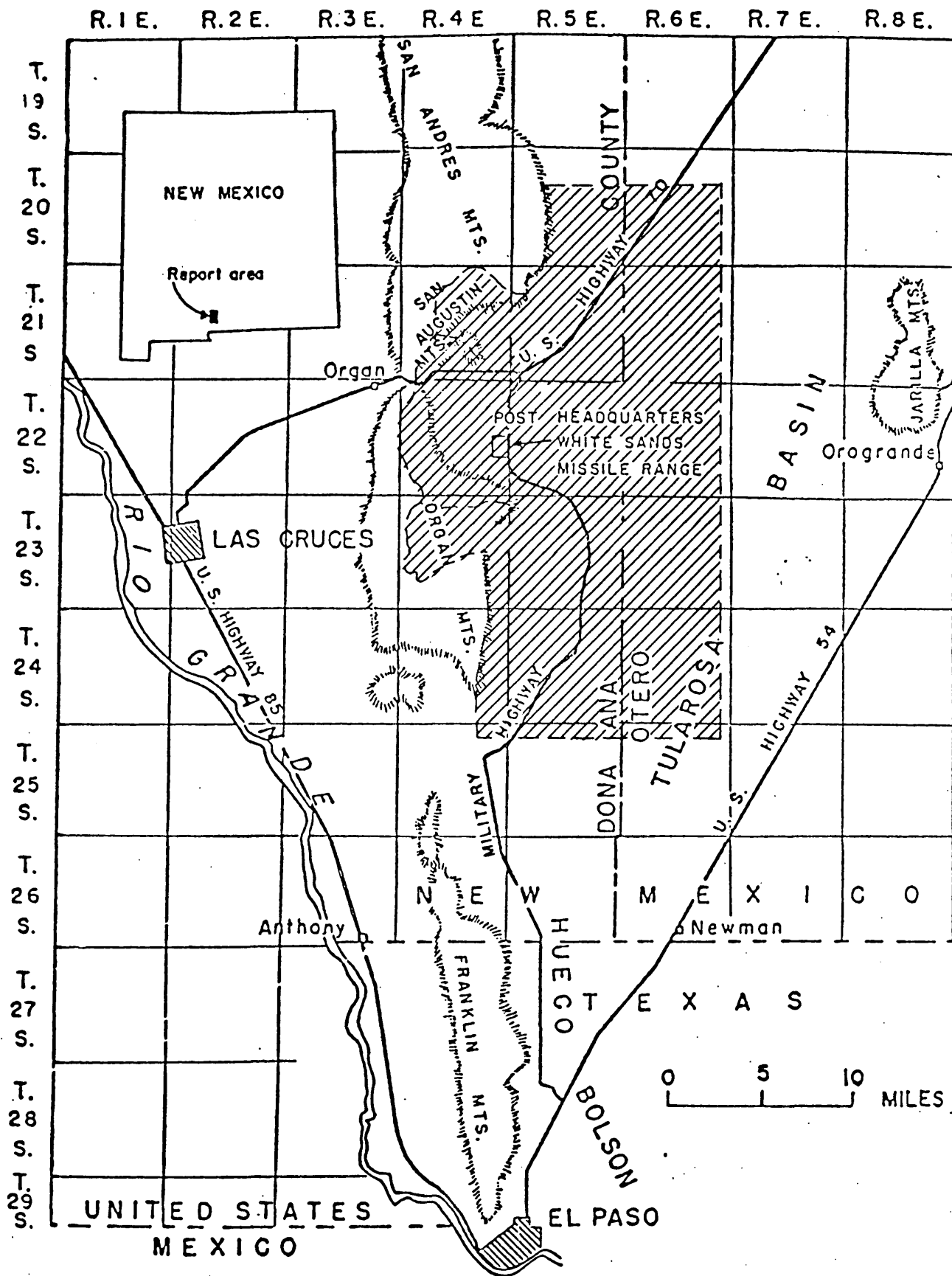


Figure 1.--Index map.

With the exception of a few domestic and stock wells drilled by ranchers before establishment of the Missile Range, no groundwater had been developed in the area prior to the mid-1940's.

By 1948, nine supply wells had been drilled approximately 2 miles southeast of the Post Headquarters. All but one of these wells were less than 400 feet deep; the principal water-bearing deposit was very fine sand. These wells were grouped in a tight cluster, which probably resulted in significant well interference. Consequently, this well field proved unsatisfactory and all wells were abandoned by 1953.

Well 10 was the first supply well drilled in the Post Headquarters area; this well was completed in August 1948. Currently (1972) the total production for White Sands Missile Range is withdrawn from nine wells, excluding a few small-capacity wells that are located in outlying areas.

Eighteen test holes have been drilled in the Post Headquarters area. These were completed as observation wells to monitor water-level changes and water quality. In addition, five exploratory holes were drilled in the Small Missile Range north of the Post Headquarters. One of these wells (SMR-1) was completed as a supply well; three are used as observation wells. SMR-5 failed to penetrate potable water and was abandoned. Two wells were drilled in the Hazardous Test Area.

A drilling program was started in 1971 to furnish additional control for mapping the water table and water quality. A total of 57 boreholes were drilled and logged. Water-level measurements were made in each borehole and water samples were collected for chemical analysis. Approximately 15 of these boreholes are being monitored to supplement the existing observation-well network.

PURPOSE

A large number of geologic and (or) hydrologic investigations have been made in the vicinity of White Sands Missile Range. Although each of these studies contributed to the geohydrologic knowledge of the region, little has been done to combine these data. These reports are listed in the bibliography of this report.

The possibility of saline-water encroachment from the central part of the Tularosa Basin into the Post Headquarters well field has long been recognized as a major threat to the water supply. To date, no significant change has been noted in the chemical quality of the water in any of the wells. Continued water use may result in deterioration of water quality. The purpose of this report is to summarize geohydrologic data available in the Post Headquarters and adjacent areas so that these data can be used in a forthcoming report which will evaluate the effects of ground-water withdrawal from the fresh-water unit. Of primary concern is the need for reasonable estimates of future pumpage from the system and a long range plan for economical, systematic development of these natural resources.

HYDROLOGIC DATA

More than 100 wells and test holes have been drilled within the project area (table 1). These wells provide the data necessary to evaluate the water resources. Water-level measurements have been made in most of the wells. Field specific-conductance measurements of the water from many wells have been obtained.

The hydrologic characteristics of many of these wells are given in table 2. These data show a wide range in values, which may be due to well construction, or to variations in lithologic characteristics of the aquifer. Specific capacity of the supply wells, which is a function of well production, is given in table 3. These data may be more useful in appraising the aquifer than the transmissivities listed in table 2. In general, the transmissivity is based on a one-well aquifer test made immediately after construction of the well; the specific capacities, though somewhat variable, are based on prolonged intervals of pumping after the well had been developed to its fullest capacity.

Table 1.—Record of wells and test holes in Post Headquarters and adjacent areas

Location	Well no.	Date drilled (month-year)	Depth drilled (feet)	Total depth (feet)	Per- forations (Depth in- terval, in feet)	Water level		Specific conductance (micromhos at 25°C)	Altitude		Remarks
						Depth below surface (feet)	Date of measure- ment		Land surface (feet)	Water level (feet)	
T. 20 S., R. 3 E.											
SW1/4 sec. 23	B-30	5-71	225	199	182-191	89.23	3- 8-72	+8,000	3,938.6	3,849.35	-
SW1/4 sec. 34	SHR-3	1-61	1,010	1,000	330-990	298.36	6- 6-72	884	4,177.9	3,879.54	-
SW1/4 sec. 35	B-29	5-71	310	132	150-184	dry	-	-	3,985.2	-	-
T. 20 S., R. 6 E.											
SW1/4 sec. 11	B-38	5-71	225	211	185-200	129.33	4-19-72	+8,000	3,984.0	3,854.67	-
SW1/4 sec. 29	B-31	5-71	240	220	170-190 220-240	122.95	4-19-72	+8,000	3,964.0	3,841.05	-
T. 21 S., R. 4 E.											
SW1/4 sec. 11	Windmill	-	-	-	-	44.94	6- 7-72	-	5,350	5,503.06	-
SW1/4 sec. 23	HTA-1	10-60	130	130	-	78.69	12-16-69	870	5,520	5,441.31	-
T. 21 S., R. 5 E.											
SW1/4 sec. 1	B-34	1-72	200	181	-	125.94	3- 8-72	790	3,974	3,848.06	-
SW1/4 sec. 2	B-28	5-71	225	214	125-145 165-190	139.51	3- 8-72	770	3,977.8	3,838.29	-
SW1/4 sec. 14	SHR-3	12-67	666	666	249-666	108.6	12-24-72	2,200	3,950	-	Plugged & abandoned
SW1/4 sec. 16	SHR-1	6-60	600	473	286-473	287.58	2-28-72	775	4,200.0	3,912.42	-
SW1/4 sec. 17	SHR-2	6-60	765	747	295-588 608-715	311.30	3-20-72	781	4,140	3,828.70	-
SW1/4 sec. 20	B-33	5-71	305	-	260-290	dry	-	-	4,411.8	-	Plugged & abandoned
SW1/4 sec. 20	SHR-4	12-67	1,016	580	470-570	278.67	6- 7-72	917	4,190	3,811.33	-
SW1/4 sec. 23	B-18	5-71	260	218	180-220	104.15	4-19-72	3,500	3,940.0	3,835.85	-
SW1/4 sec. 27	B-46	1-72	250	245	220-250	133.58	3- 8-72	650	3,990	3,856.42	-
SW1/4 sec. 30	B-32	5-72	399	399	357-397	dry	-	-	4,343.2	-	-
SW1/4 sec. 32	T-13	5-67	1,110	710	285-702	209.26	6- 7-72	490	4,056.6	3,847.34	-
SW1/4 sec. 33	B-17	5-71	284	243	230-275	109.19	3- 8-72	600	3,947.0	3,837.81	-
SW1/4 sec. 34	B-16	4-71	320	237	235-245	107.49	3- 8-72	860	3,943.6	3,836.11	-
T. 21 S., R. 6 E.											
SW1/4 sec. 2	B-39	5-71	230	217	157-177	156.15	4-19-72	+8,000	3,985	3,828.85	-
SW1/4 sec. 17	B-27	4-71	200	174	163-167	120.07	4-19-72	+8,000	3,945.8	3,825.73	-
SW1/4 sec. 26	B-40	5-71	237	223	158-165 183-194	dry	-	-	4,002	-	-
SW1/4 sec. 32	B-26	4-71	210	189	180-185	139.95	4-19-72	5,000	3,959.6	3,819.65	-
T. 22 S., R. 4 E.											
SW1/4 sec. 1	B-36	1-72	240	239	210-240	215.36	3- 8-72	610	4,478	4,262.64	-
SW1/4 sec. 1	T-9	8-66	598	598	538-595	389.50	6- 8-72	822	4,410.3	4,020.80	-
SW1/4 sec. 1	T-1	6-53	1,004	450	350-450	399.23	7-31-53	409	4,320	3,920.77	Abandoned 1-62
SW1/4 sec. 11	T-8	7-66	1,896	1,060	574-1,040	571.84	6- 8-72	700	4,441.7	3,869.86	-
SW1/4 sec. 11	B-37	1-72	540	521	510-540	418.42	3- 8-72	460	4,443	4,024.58	-
SW1/4 sec. 11	B-22	1-72	300	289	270-300	242.40	3- 8-72	560	4,477	4,234.60	Destroyed 6-72
SW1/4 sec. 11	B-42	1-72	520	513	490-520	384.14	3- 8-72	383	4,375	3,990.86	-
SW1/4 sec. 12	SW-20	1-65	842	842	462-838	501.73	1-27-72	400	4,354	3,852.27	-
SW1/4 sec. 12	SW-19	6-65	903	800	400-800	441.05	1-27-72	358	4,294	3,852.95	-
SW1/4 sec. 12	SW-18	5-64	800	800	400-800	417.52	1-27-72	382	4,264	3,846.48	-
SW1/4 sec. 13	SW-17	6-60	900	900	436-886	431.85	1-27-72	372	4,260	3,828.15	-
SW1/4 sec. 13	SW-13	8-51	534	534	373-393 470-534	312	1-27-72	331	4,330.3	4,018.3	-
SW1/4 sec. 13	T-2	5-53	1,000	400	300-400	337.98	5-29-53	505	4,262.6	3,924.62	Abandoned 3-60
SW1/4 sec. 13	SW-14	3-53	1,005	810	370-810	396.20	9- 9-71	321	4,290.3	3,894.10	Plugged
SW1/4 sec. 13	SW-15	2-54	1,010	820	350-820	421	1-27-72	325	4,261.3	3,840.3	-
SW1/4 sec. 13	SW-16	7-54	1,020	890	370-886	433	1-27-72	337	4,270	3,837.0	-
SW1/4 sec. 14	T-6	11-60	515	515	285-409	208.18	6- 8-72	437	4,507	4,298.82	-
SW1/4 sec. 14	B-20	5-71	447	426	410-440	335.69	3- 8-72	460	4,446	4,112.31	-
SW1/4 sec. 14	T-3	5-53	875	450	350-450	381.25	6- 6-53	610	4,442.4	4,061.15	Abandoned 1-61

Table 1.--Record of wells and test holes in Post Headquarters and adjacent areas - Continued

Location	Well no.	Date drilled (month-year)	Depth drilled (feet)	Total depth (feet)	Per- forations (Depth in- terval, in feet)	Water level		Specific conductance (micromhos at 25°C)	Altitude		Remarks
						Depth below surface (feet)	Date of measure- ment		Land surface (feet)	Water level (feet)	
T. 22 S., R. 4 E. - Concluded NE 1/4 SW 1/4 sec. 23	B-21b	1-72	195	184	164-184	dry	-	-	4,417	-	-
NE 1/4 SW 1/4 sec. 23	B-21a	5-71	394	-	278-298 328-338	dry	-	-	-	-	Plugged & abandoned
SE 1/4 SE 1/4 sec. 23	T-12	3-67	2,000	1,820	1,430-1,810	211.19	6- 8-72	410	4,334.6	4,123.41	Bridged at 220 ft by vandals
NE 1/4 NW 1/4 sec. 24	SW-11	5-50	523	500	380-490	219	1-27-72	327	4,333	4,042	-
NE 1/4 NW 1/4 sec. 24	SW-10	8-48	505	494	264-294	358	8-12-53	337	4,271.3	3,913.3	Abandoned 7-63
NE 1/4 NW 1/4 sec. 24	SW-10A	7-63	825	805	405-805	420.70	1-27-72	321	4,273	3,852.30	-
NE 1/4 NE 1/4 sec. 24	Main Gate	6-59	440	431	388-438	405.71	6- 8-72	347	4,252.9	3,847.19	-
T. 22 S., R. 5 E. NE 1/4 SW 1/4 sec. 3	B-14	5-71	265	209	180-220 240-258	110.94	3- 8-72	800	3,942.5	3,831.56	-
NE 1/4 SW 1/4 sec. 5	B-15	4-71	255	225	200-220	168.15	3- 9-72	500	4,037	-	-
SW 1/4 SW 1/4 sec. 5	T-10	9-66	1,365	555	370-545	260.49	6- 7-72	605	4,159.8	3,898.31	-
SE 1/4 SW 1/4 sec. 6	B-24	4-71	260	253	180-260	dry	-	-	4,337.7	-	-
SW 1/4 SW 1/4 sec. 6	B-25	4-71	280	264	260-270	dry	-	-	4,253.8	-	-
NE 1/4 NE 1/4 sec. 6	B-53	12-71	400	400	370-400	391.41	3- 9-72	420	4,260	3,868.59	-
NE 1/4 SE 1/4 sec. 7	B-50	12-71	350	349	320-350	293.10	3- 8-72	440	4,170	3,876.90	-
NE 1/4 SE 1/4 sec. 7	T-7	8-63	1,000	1,000	326-966	362.49	6- 6-72	376	4,185	3,822.51	-
NE 1/4 SE 1/4 sec. 8	B-13	4-71	315	287	250-285	233.44	3- 8-72	400	4,101	3,867.56	-
SE 1/4 SW 1/4 sec. 8	B-47	12-71	350	338	320-350	267.60	3- 8-72	355	4,114	3,846.40	-
SW 1/4 NW 1/4 sec. 9	B-49	12-71	200	200	170-200	196.32	3- 8-72	-	4,040	3,843.68	Cluster 1
SW 1/4 NW 1/4 sec. 9	B-52	12-71	350	336	320-350	207.15	3- 8-72	355	4,041	3,833.85	Do.
SW 1/4 NW 1/4 sec. 9	B-55	1-72	500	473	470-500	212.85	3- 8-72	320	4,040	3,827.15	Do.
NE 1/4 NE 1/4 sec. 15	T-14	10-67	6,015	370	210-360	133.15	6- 6-72	883	3,950	3,826.85	-
NE 1/4 NW 1/4 sec. 16	B-23	12-71	250	250	220-250	222.95	3- 8-72	370	4,050	3,827.05	Cluster 2
NE 1/4 NW 1/4 sec. 16	B-35	12-71	400	388	370-400	216.42	3- 8-72	340	4,046	3,829.58	Do.
NE 1/4 NW 1/4 sec. 16	B-54	12-71	500	437	470-500	228.90	3- 8-72	295	4,047	3,818.10	Do.
NE 1/4 NW 1/4 sec. 16	T-4	6-53	1,000	400	300-400	225.32	6- 7-72	573	4,051.3	3,825.98	-
NE 1/4 SE 1/4 sec. 18	B-12	4-71	408	309	355-365	283.96	3- 9-72	-	4,152.6	3,868.64	-
SE 1/4 SE 1/4 sec. 19	B-10	4-71	420	385	370-375 390-395	300.19	3- 9-72	405	4,169.8	3,869.61	-
NE 1/4 NW 1/4 sec. 20	T-5	7-53	1,000	400	300-400	274.02	6- 6-72	379	4,149.8	3,875.78	-
NE 1/4 NW 1/4 sec. 21	B-9	3-71	280	254	240-250	226.60	3- 9-72	380	4,036.2	3,809.60	-
NE 1/4 SE 1/4 sec. 23	B-7	3-71	235	205	195-215	175.42	9- 9-71	480	3,976.6	3,801.18	-
NE 1/4 SE 1/4 sec. 23	B-8	4-71	338	291	290-295	176.25	3- 9-72	480	3,976.6	3,800.35	-
NE 1/4 SE 1/4 sec. 26	B-51	2-72	400	312	370-400	141.90	3- 9-72	340	3,946	3,804.10	-
NE 1/4 NW 1/4 sec. 28	B-1	3-71	259	248	210-250	193.54	3- 8-72	-	4,015.0	3,821.46	-
SE 1/4 NW 1/4 sec. 28	B-2	4-69	260	256	220-260	203.26	9- 9-71	-	4,015.4	3,812.14	-
NE 1/4 SE 1/4 sec. 28	B-3	4-69	280	280	220-280	-	-	-	4,019.7	-	-
SW 1/4 NW 1/4 sec. 28	B-4	3-71	260	252	220-260	200.73	3- 9-72	-	4,016.6	3,815.87	-
NE 1/4 NW 1/4 sec. 29	T-11	11-66	1,808	780	306-760	275.58	6- 7-72	336	4,081.2	3,805.62	-
SW 1/4 NW 1/4 sec. 30	B-11	4-71	300	284	275-285	dry	-	-	4,220.1	-	-
SE 1/4 SE 1/4 sec. 30	B-56	12-71	350	350	320-350	227.80	3- 9-72	440	4,162	3,934.20	-
SE 1/4 SE 1/4 sec. 31	SW-9	6-46	348	348	259-328	234	9-10-47	248	4,128.0	3,894.0	-
SE 1/4 NW 1/4 sec. 32	SW-1	-	-	257	237-257	dry	1-31-53	-	4,130	-	-
SW 1/4 NW 1/4 sec. 32	B-5	3-71	-	249	210-249	189.63	3- 9-72	-	3,996.2	3,806.57	-
NE 1/4 NW 1/4 sec. 32	SW-2	-	-	296	254-296	dry	1-31-53	-	4,130	-	-

Table 1.--Record of wells and test holes in Post Headquarters and adjacent areas - Concluded

Location	Well no.	Date drilled (month-year)	Depth drilled (feet)	Total depth (feet)	Per- forations (Depth in- terval, in feet)	Water level		Specific conductance (micromhos at 25°C)	Altitude		Remarks
						Depth below surface (feet)	Date of measure- ment		Land surface (feet)	Water level (feet)	
<u>T. 22 S., R. 5 E. - Concluded</u>											
SE 1/4 SW 1/4 sec. 32	SW-4	-	452	270	234-270	222.31	5- 4-53	297	4,110	3,887.69	-
SW 1/4 SW 1/4 sec. 32	SW-4a	-	-	326	-	240	-	-	4,115	3,875	-
NE 1/4 SW 1/4 sec. 32	SW-3	-	-	381	-	dry	1-31-53	-	4,115	-	-
NE 1/4 SW 1/4 sec. 32	SW-6	6-46	338	318	248-268	235.58	1-31-53	281	4,104.0	3,868.42	-
SW 1/4 SW 1/4 sec. 32	SW-7	5-46	-	304	254-284	237.06	1-31-53	268	4,083.5	3,846.44	-
NE 1/4 SW 1/4 sec. 32	SW-5	4-46	-	267	183-267	225	4- 9-47	293	4,112.0	3,887.0	-
SE 1/4 SW 1/4 sec. 32	SW-8	-	-	256	216-256	210.05	1-31-53	-	4,084	3,873.95	-
SE 1/4 SE 1/4 sec. 33	T-15	12-68	2,034	670	446-650	179.08	6- 6-72	567	3,990	3,820.92	-
<u>T. 22 S., R. 6 E.</u>											
SE 1/4 SW 1/4 sec. 8	Gregg	8-61	1,010	478	263-465	214.30	6- 6-72	7,840	4,045	3,830.70	-
SW 1/4 NE 1/4 sec. 23	B-41	6-71	244	241	189-199 229-244	dry	-	-	4,061.1	-	-
NE 1/4 SE 1/4 sec. 31	B-48	12-71	300	288	270-300	203.94	3- 9-72	1,250	4,007	3,803.06	-
<u>T. 23 S., R. 5 E.</u>											
SW 1/4 NE 1/4 sec. 1	B-6	3-71	200	180	150-175	131.38	3- 7-72	660	3,928.7	3,797.32	-
NE 1/4 SE 1/4 sec. 5	T-18	5-69	894	704	506-684	244.92	6- 6-72	641	4,065	3,820.08	-
SW 1/4 SW 1/4 sec. 10	T-16	2-69	2,007	710	310-700	186.58	6- 6-72	-	3,980	3,793.42	-
SW 1/4 SW 1/4 sec. 24	B-45a	6-71	240	-	187-209 211-225	dry	-	-	3,962	-	Plugged & abandoned
SW 1/4 SW 1/4 sec. 24	B-45b	12-71	270	255	240-270	181.40	1-27-72	540	3,962	3,780.60	-
NE 1/4 SE 1/4 sec. 27	T-17	5-69	2,500	564	440-544	242.15	6- 6-72	301	4,020	3,777.85	-
SW 1/4 SW 1/4 sec. 35	F-1	1953	-	1,200	-	165.1	4- 4-53	308	3,937.4	3,772.3	-
<u>T. 23 S., R. 6 E.</u>											
SW 1/4 SW 1/4 sec. 20	B-44	6-71	260	251	220-260	196.46	2- 3-72	1,300	3,972	3,775.54	-
NE 1/4 NE 1/4 sec. 35	C-1	1953	-	650	-	287.5	3-29-53	19,000	4,080.7	3,793.2	-
<u>T. 23 S., R. 7 E.</u>											
NE 1/4 NE 1/4 sec. 30	B-43	6-71	240	240	180-200	dry	-	-	4,080	-	-
<u>T. 24 S., R. 5 E.</u>											
SE 1/4 SW 1/4 sec. 20	F-3	1953	-	1,205	-	381.0	6-27-53	761	4,135.7	3,754.7	-
SE 1/4 SE 1/4 sec. 28	F-5	1953	-	580	-	256.7	4- 4-53	1,630	4,015.2	3,758.5	-
<u>T. 25 S., R. 4 E.</u>											
NE 1/4 SE 1/4 sec. 11	K-15	1923	798	794	474-494	330.5	5-13-53	639	4,077.4	3,746.9	-
<u>T. 25 S., R. 6 E.</u>											
NE 1/4 NE 1/4 sec. 4	L-1	1953	-	1,208	-	300.3	3-31-53	11,000	4,051.6	3,751.3	-

Table 2.--Hydrologic characteristics of the aquifer in the vicinity of supply and test wells

Location	Well no.	Completion depth (feet)	Saturated thickness penetrated (feet)	Apparent transmissibility (gpd/ft)	Apparent transmissivity (ft ² /day)	Specific capacity (gpm/ft)	Sand fraction 500-1,000 feet or total depth
<u>T.20 S., R.5 E.</u> SW $\frac{1}{4}$ SW $\frac{1}{4}$ NW $\frac{1}{4}$ sec. 34	SMR-3	1,000	703	350,000	46,900	96	52
<u>T.21 S., R.4 E.</u> NW $\frac{1}{4}$ NW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 23	HTA-1	392	314	1,700	228	1.4	-
<u>T.21 S., R.5 E.</u> SE $\frac{1}{4}$ SW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 14	SMR-5	Plugged	666	no test	-	-	70
NW $\frac{1}{4}$ SW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 16	SMR-1	473	192	7,900	1,158	5.9	-
SE $\frac{1}{4}$ NE $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 17	SMR-2	765	460	20,000	2,680	12.3	-
SE $\frac{1}{4}$ SW $\frac{1}{4}$ SW $\frac{1}{4}$ sec. 20	SMR-4	580	306	100,000	13,400	29	32
NE $\frac{1}{4}$ NE $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 32	T-13	710	501	6,000	804	3.1	38
<u>T.22 S., R.4 E.</u> NW $\frac{1}{4}$ SW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 1	T-9	598	208	32.7	4.4	.1	.80
SE $\frac{1}{4}$ SE $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 1	T-1	450	50	no test	-	-	.56
SE $\frac{1}{4}$ SE $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 11	T-8	895	342	1,200	160	2.0	.52
SE $\frac{1}{4}$ NW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 12	SW-20	842	380	828,000	111,900	132	.61

Table 2.--Hydrologic characteristics of the aquifer in the vicinity of supply and test wells - Continued

Location	Well no.	Completion depth (feet)	Saturated thickness penetrated (feet)	Apparent transmissibility (gpd/ft)	Apparent transmissivity (ft ² /day)	Specific capacity (gpm/ft)	Sand fraction 500-1,000 feet or total depth
T.22 S., R.4 E.- Continued							
SE $\frac{1}{4}$ NW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 12	SW-19	800	391	79,600	10,666	44	45
SE $\frac{1}{4}$ SW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 12	SW-18	800	405	4,780	632	18.1	44
			385	5,440	743	21.2	
NW $\frac{1}{4}$ SW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 13	SW-17	800	504	30,000	4,020	26.1	44
NW $\frac{1}{4}$ NW $\frac{1}{4}$ SW $\frac{1}{4}$ sec. 13	SW-13	534	234	5,000	670	3.5	64
SW $\frac{1}{4}$ NE $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 13	T-2	400	62	no test	-	-	35
NW $\frac{1}{4}$ NW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 13	SW-14	810	453	8,000	1,070	7.8	40
SE $\frac{1}{4}$ NE $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 13	SW-15	820	482	28,300	3,790	18.6	42
NE $\frac{1}{4}$ SW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 13	SW-16	890	540	33,000	4,420	45.0	40
SW $\frac{1}{4}$ SW $\frac{1}{4}$ NW $\frac{1}{4}$ sec. 14	T-6	515	311	no test	-	2.7	-
NW $\frac{1}{4}$ NW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 14	T-3	450	69	no test	-	-	32*
SE $\frac{1}{4}$ NW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 23	SW-12	570	285	5,000	670	3.2	59
SE $\frac{1}{4}$ SE $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 23	T-12	1,820	1,589	1,360	182	1.5	49
NE $\frac{1}{4}$ NW $\frac{1}{4}$ NW $\frac{1}{4}$ sec. 24	SW-11	500	195	2,500	335	12.0	-

Table 2.--Hydrologic characteristics of the aquifer in the vicinity of supply and test wells - Concluded

Location	Well no.	Completion depth (feet)	Saturated thickness penetrated (feet)	Apparent trans- missi- bility (gpd/ft)	Apparent trans- missi- vity (ft ² /day)	Specific capacity (gpm/ft)	Sand fraction 500-1,000 feet or total depth
<u>T.22 S., R.4 E. - Concluded</u>							
NE $\frac{1}{4}$ NW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 24	SW-10	505	139	61,600	8,170	23.6	-
NE $\frac{1}{4}$ NW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 24	SW-10A	805	404	114,000	15,300	37.5	48
NE $\frac{1}{4}$ NE $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 24	Main Gate	430	73	17,600	2,360	11.5	-
<u>T.22 S., R.5 E.</u>							
SW $\frac{1}{4}$ NW $\frac{1}{4}$ SW $\frac{1}{4}$ sec. 5	T-10	555	305	13,900	1,862	7	14
NE $\frac{1}{4}$ SE $\frac{1}{4}$ SW $\frac{1}{4}$ sec. 7	T-7	1,000	660	12,000	1,620	12	22
NW $\frac{1}{4}$ NE $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 15	T-14	370	239	no test	-	-	45
NW $\frac{1}{4}$ NW $\frac{1}{4}$ NW $\frac{1}{4}$ sec. 16	T-4	400	177	no test	-	-	39
NW $\frac{1}{4}$ NW $\frac{1}{4}$ NW $\frac{1}{4}$ sec. 20	T-5	400	130	no test	-	-	40
NE $\frac{1}{4}$ SW $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 29	T-11	800	521	12,750	1,698	6	35
SE $\frac{1}{4}$ SE $\frac{1}{4}$ NE $\frac{1}{4}$ sec. 33	T-15	670	483	no test	-	-	40
<u>T.22 S., R. 6 E.</u>							
SE $\frac{1}{4}$ NW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 8	Gregg	500	270	19,600	2,626	12.4	54
<u>T.23 S., R.5 E.</u>							
NW $\frac{1}{4}$ NE $\frac{1}{4}$ SW $\frac{1}{4}$ sec. 5	T-18	704	447	1,150	254	1.0	32*
SW $\frac{1}{4}$ NW $\frac{1}{4}$ SE $\frac{1}{4}$ sec. 10	T-16	710	523	37,600	5,040	10.8	61
NE $\frac{1}{4}$ SE $\frac{1}{4}$ NW $\frac{1}{4}$ sec. 27	T-17	564	322	16,400	2,197	5.7	54

*Lower portion of hole in bedrock.

Table 3.--Specific capacity of supply wells

Well number	Year																					
	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972
10	-	-	-	-	17.7	18.7	10.1	9.6	10.9	13.1	11.9	11.7	12.8	-	-	-	-	-	-	-	-	-
10A	-	-	-	-	-	-	-	-	-	-	-	-	-	39.6	44.4	57.5	90.0	53.3	51.6	45.8	47.9	46.8
11	-	-	-	-	-	16.6	20.7	23.5	23.4	23.3	24.8	24.2	47.3	-	31.0	25.0	29.8	32.6	16.3	25.3	26.4	-
12	-	-	9.7	12.3	4.8	8.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
13	13.9	-	-	-	16.5	30.9	8.3	10.4	16.8	6.9	8.9	12.9	9.0	8.5	8.0	9.2	-	14.4	6.6	9.1	15.8	9.5
14	-	-	-	-	13.5	15.9	13.6	9.6	31.2	11.7	11.0	6.6	7.5	5.9	-	-	-	-	-	-	-	-
15	-	-	-	-	32.0	26.9	29.0	25.0	22.6	23.0	22.1	29.0	20.0	14.6	21.5	15.6	16.5	16.6	15.2	15.4	12.5	15.0
16	-	-	-	-	25.7	30.6	40.8	43.1	31.0	26.4	28.4	35.9	55.5	41.0	41.6	46.8	44.0	46.6	36.8	38.2	38.5	47.0
17	-	-	-	-	-	-	-	-	-	-	-	35.0	33.1	31.1	26.0	37.4	-	40.4	30.8	30.2	39.8	29.3
18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.8	9.2	14.0	11.1	8.4	8.9	-	7.6
19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	62.0	60.6	51.3	66.7	50.2	53.3	62.8	55.3
20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	156.4	117.3	-	156.4	111.2	194.4	125.0	117.1
SMR-1	-	-	-	-	-	-	-	-	-	-	-	7.7	7.7	6.3	6.3	-	-	-	-	-	-	-

The sand percentage was calculated from geophysical logs for the depth interval 500 to 1,000 feet (table 2 and fig. 2). This interval was selected because in most cases it is below the water table and because various sources of information indicate that permeability significantly decreases below 1,000 feet. Therefore this interval is believed to be the major water-producing zone. Although several exceptions were noted, in general the areas having the highest sand percentages are those where transmissivity and specific capacity are greatest. The sand percentage generally decreases basinward, but nearly all supply wells are located in areas where the sand percentage exceeds 40 percent. Sixty-one percent sand was present in supply well 20; this well also has the highest transmissivity recorded in the well field (table 2). Other wells show very poor correlation between sand percentage and transmissivity.

Precipitation and runoff data are being monitored throughout the Post Headquarters area. The location of the stations are shown on figure 3. These data have been published annually (Cruz, 1972, table 5); no new data were collected as part of this investigation.

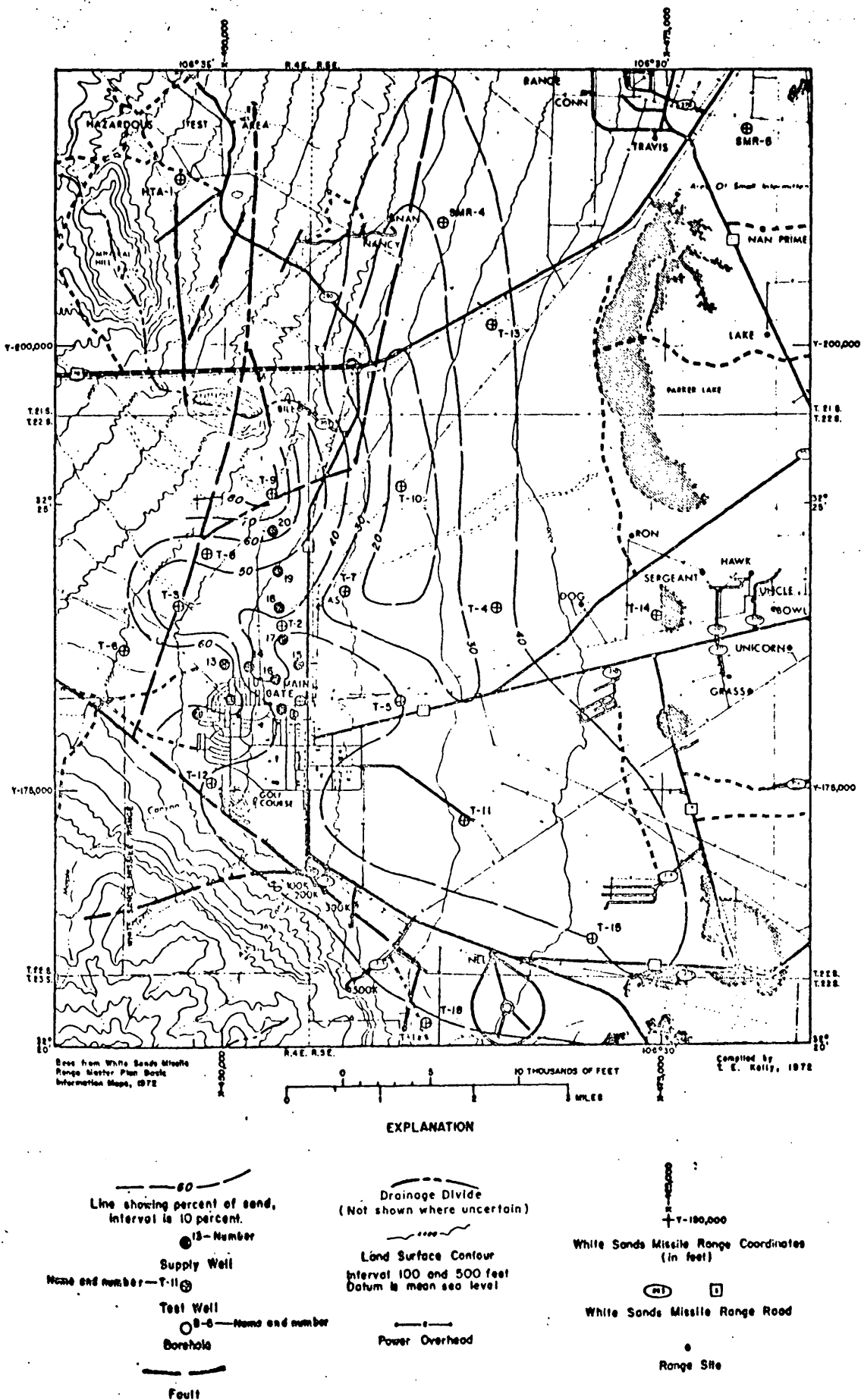


Figure 2.--Percentage of sand between 500 and 1,000 feet.

Accurate records of pumpage from wells in the Post Headquarters area have been kept by the Utilities Division, Facilities Engineering Directorate, since 1953 (fig. 4). In general, there was a gradual increase in water use during the first 10 years of record. Subsequently the annual total production has ranged from 775.2 million gallons in 1966 to 939.0 million gallons in 1971; the average is 864.3 million gallons during the period 1964 to 1971. The decline in water level recorded in Main Gate well (fig. 4) reflects the downward trend of the water table which has been caused by this withdrawal.

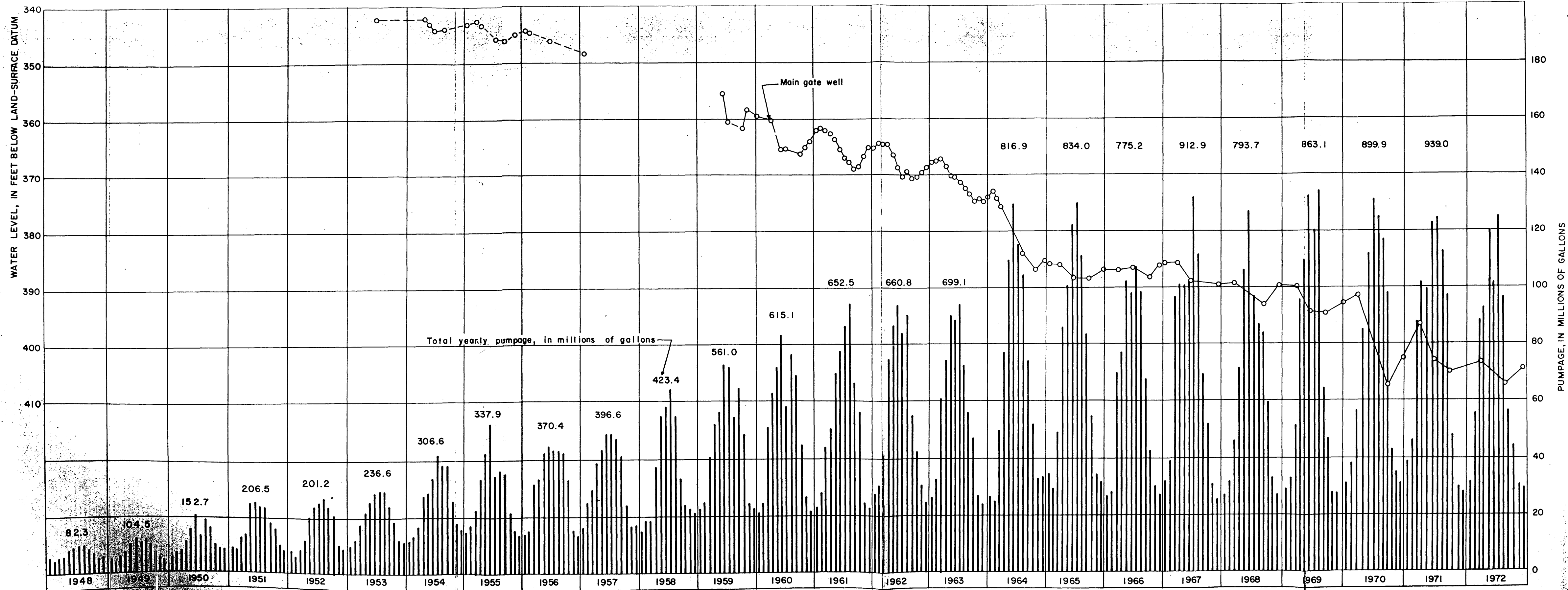


FIGURE 4.-- HYDROGRAPH OF MAIN GATE WELL AND MONTHLY PUMPAGE FIGURES FOR WELL FIELD.

Figures 5 through 11 show the water-level changes that have occurred during the period of record in each test well. Most of these observation wells show a decline of water level; the amount of decline usually is dependent upon the location and proximity of the observation well to the well field.

The annual pumpage and corresponding water-level changes for each of the currently operative supply wells are illustrated in figures 12 through 20. Most of these wells have declining water levels. However since about 1965, wells 15 through 20 have been the major source of supply, thus the water levels have risen in supply wells 11 and 13 (figs. 13 and 14).

Water levels have been measured intermittently in supply wells HTA-1 and SMR-1 (fig. 21). These wells produce small quantities of water for local use. Two wells, 12 and 14, have been utilized as observation wells after having been abandoned as supply wells (fig. 22). Supply well 12 reflects the rise in water table near the south end of the well field.

W. C. Ballance and S. M. Longwill (written commun., 1968) analyzed much of the data that was collected prior to 1964. This early work provided a background for construction of various maps illustrating the early well development in the Post Headquarters area.

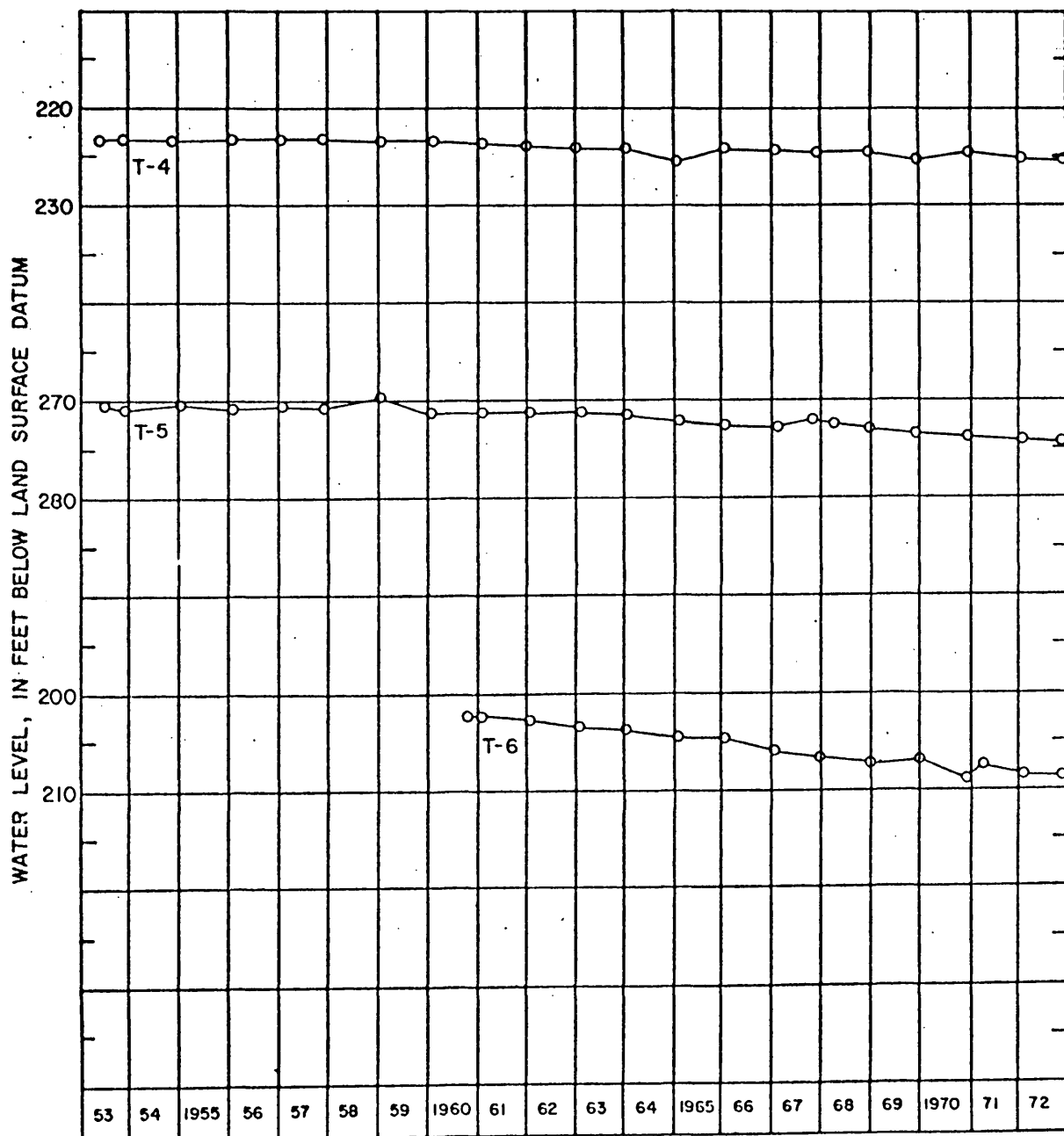


Figure 5.--Hydrograph of Test wells T-4, T-5, and T-6.

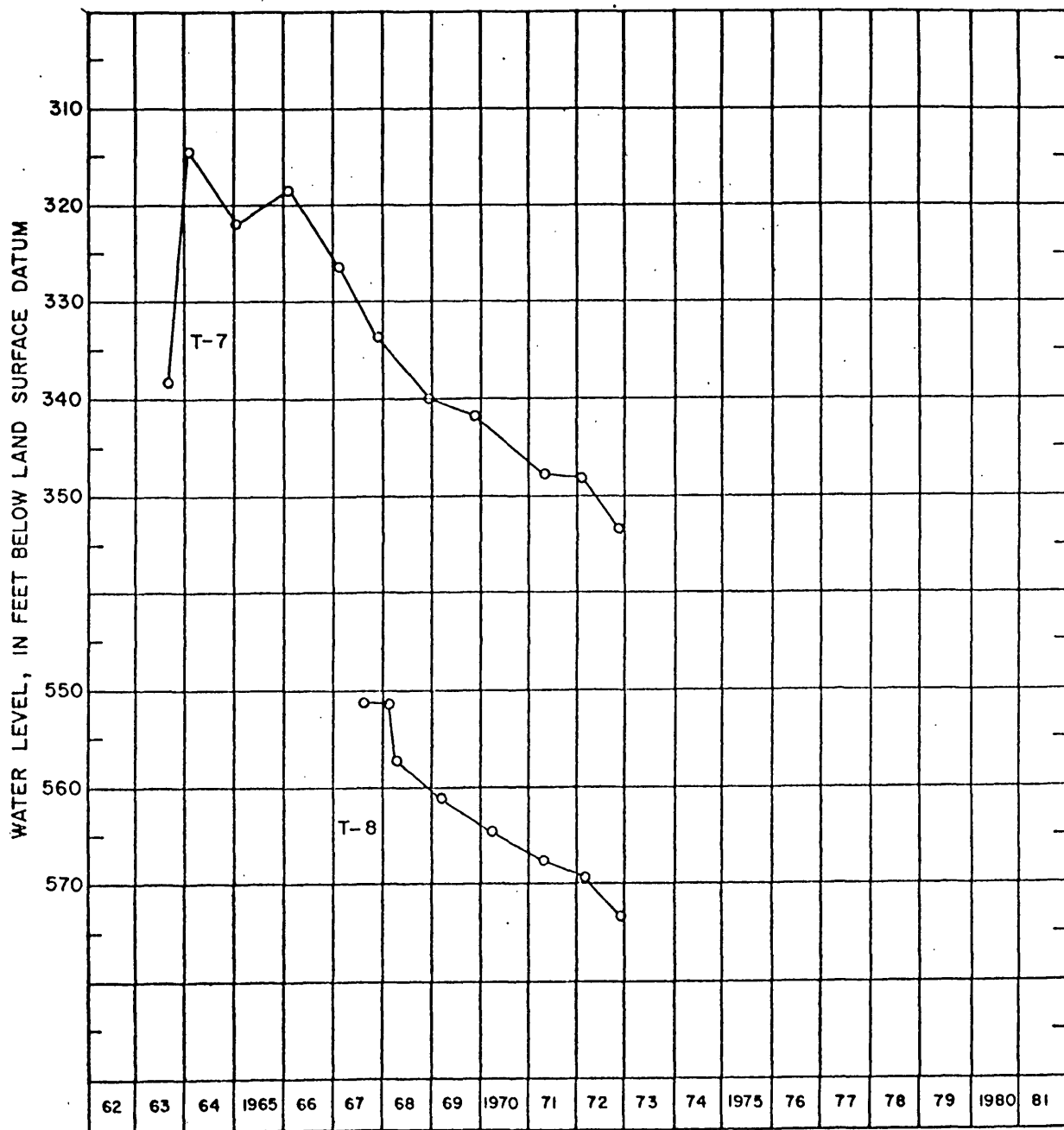


Figure 6.--Hydrograph of Test wells T-7 and T-8.

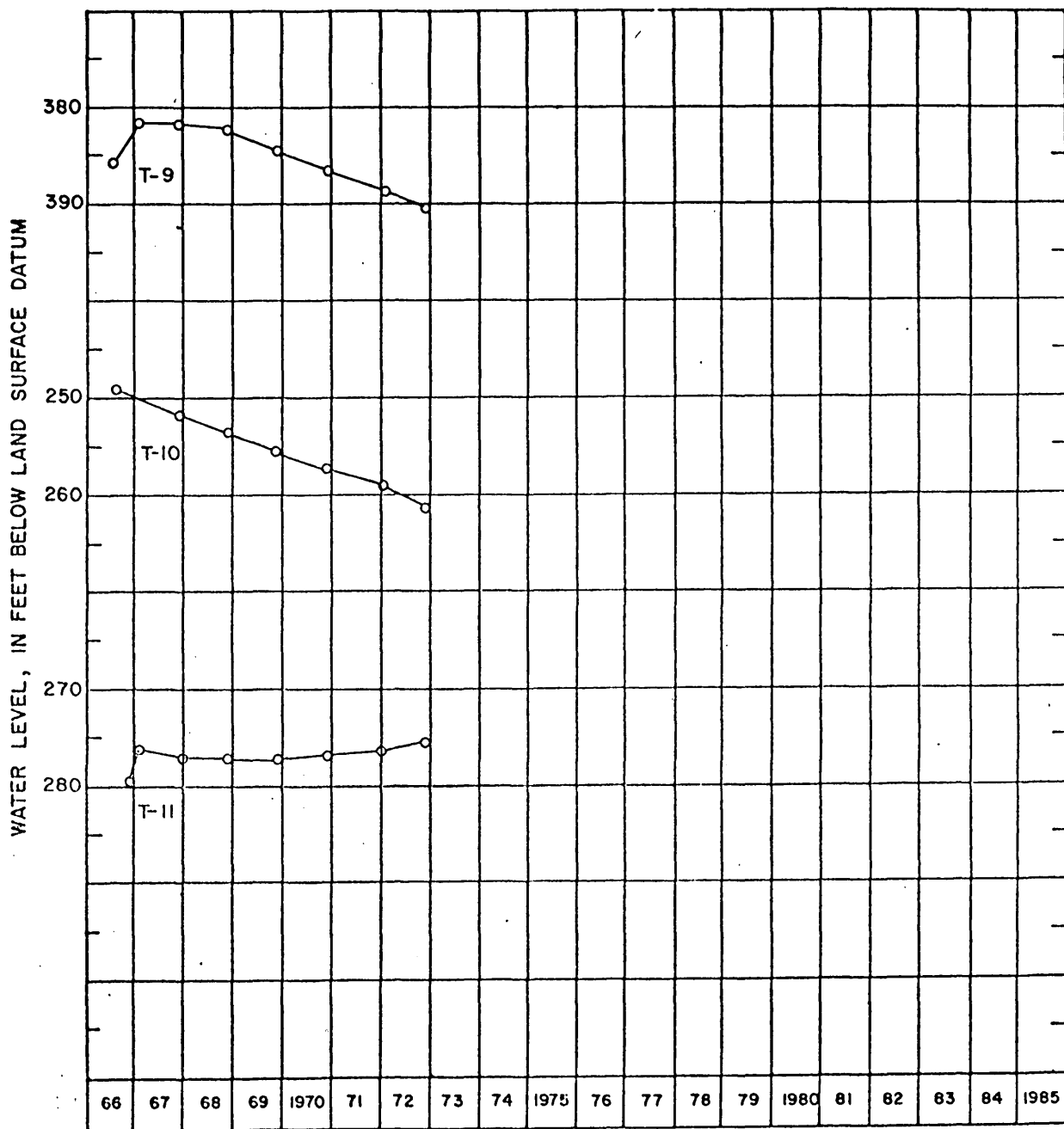


Figure 7.--Hydrograph of Test wells T-9, T-10, and T-11.

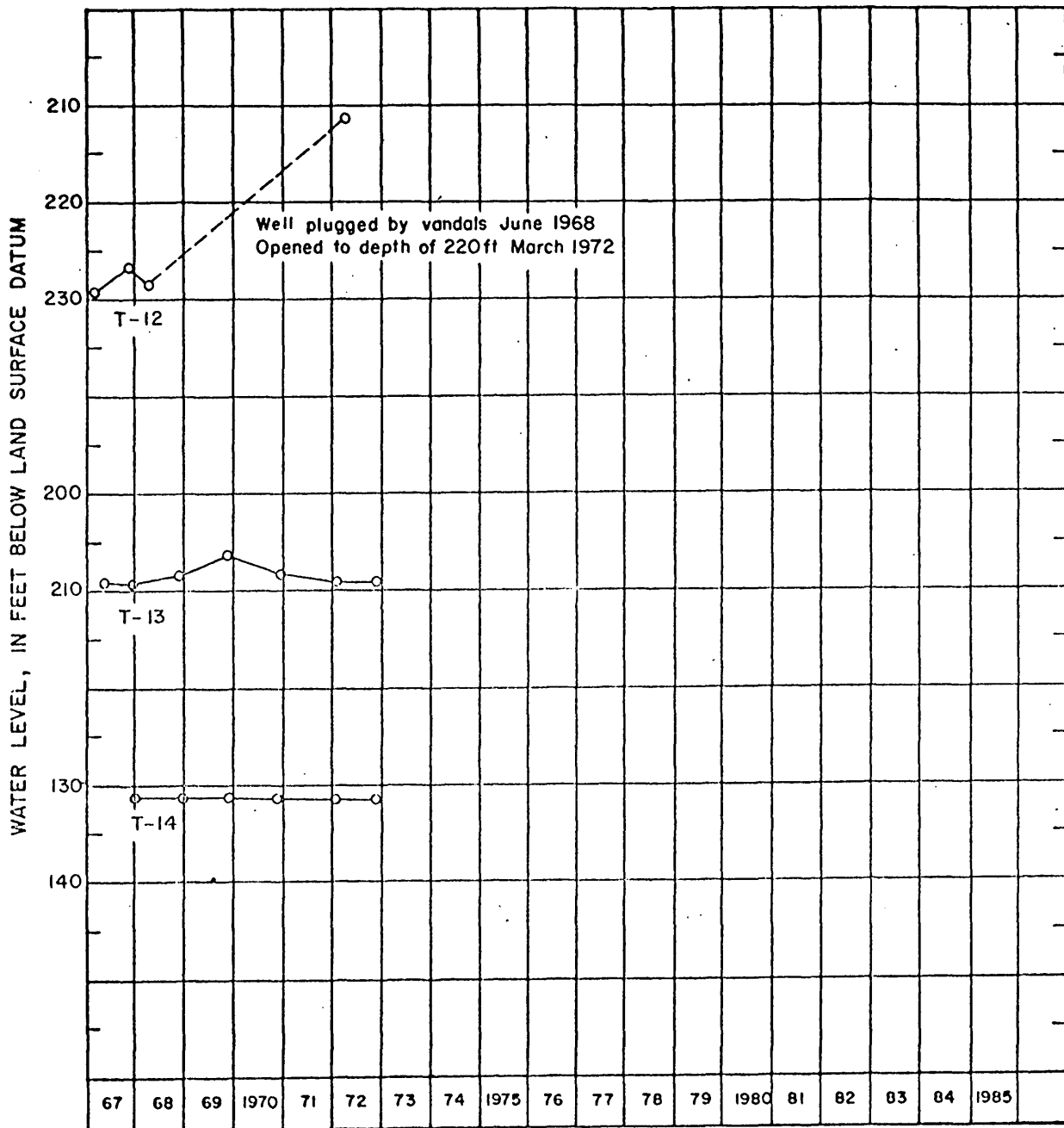


Figure 8.--Hydrograph of Test wells T-12, T-13, and T-14.

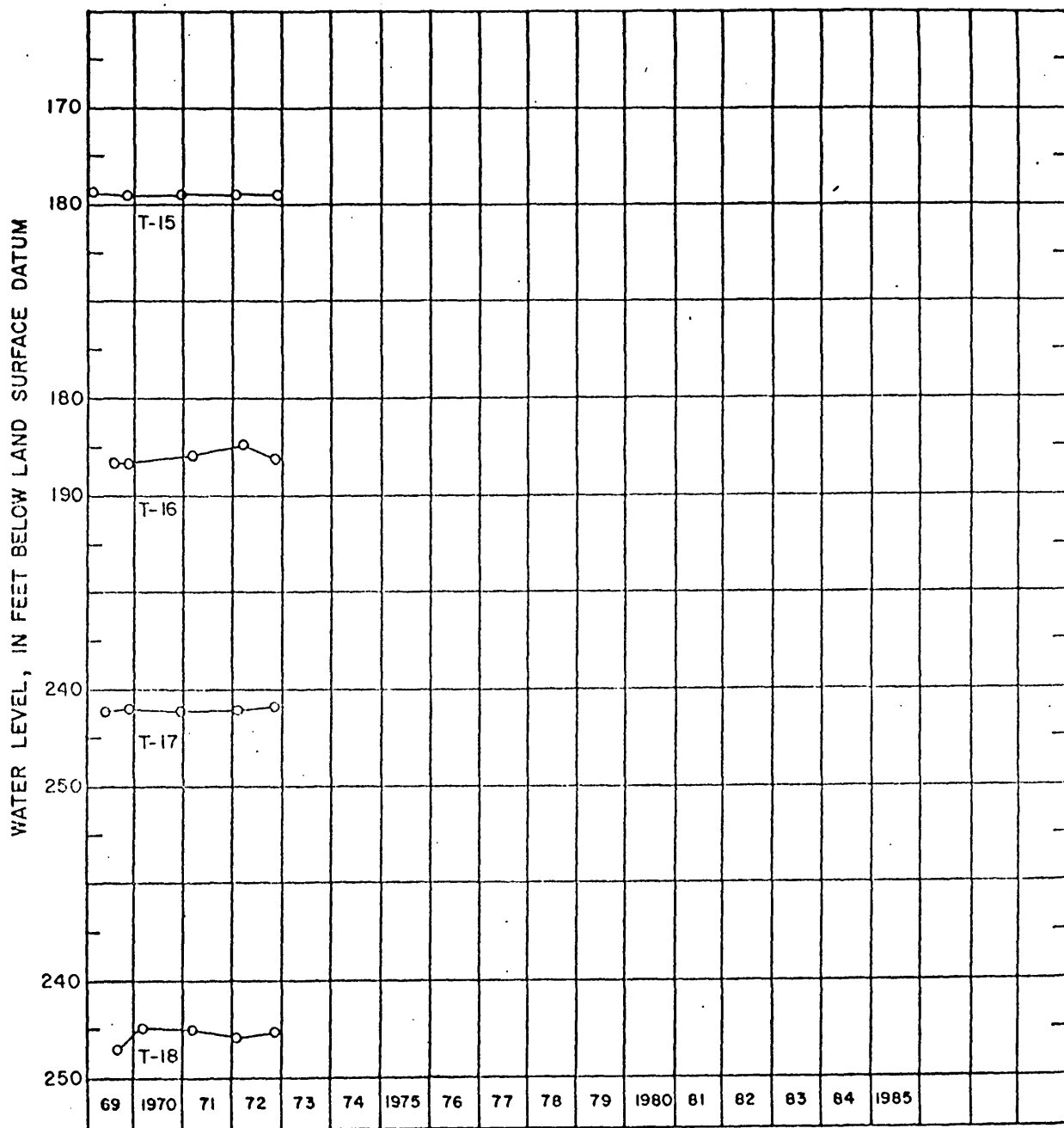


Figure 9.--Hydrograph of Test wells T-15, T-16, T-17, and T-18.

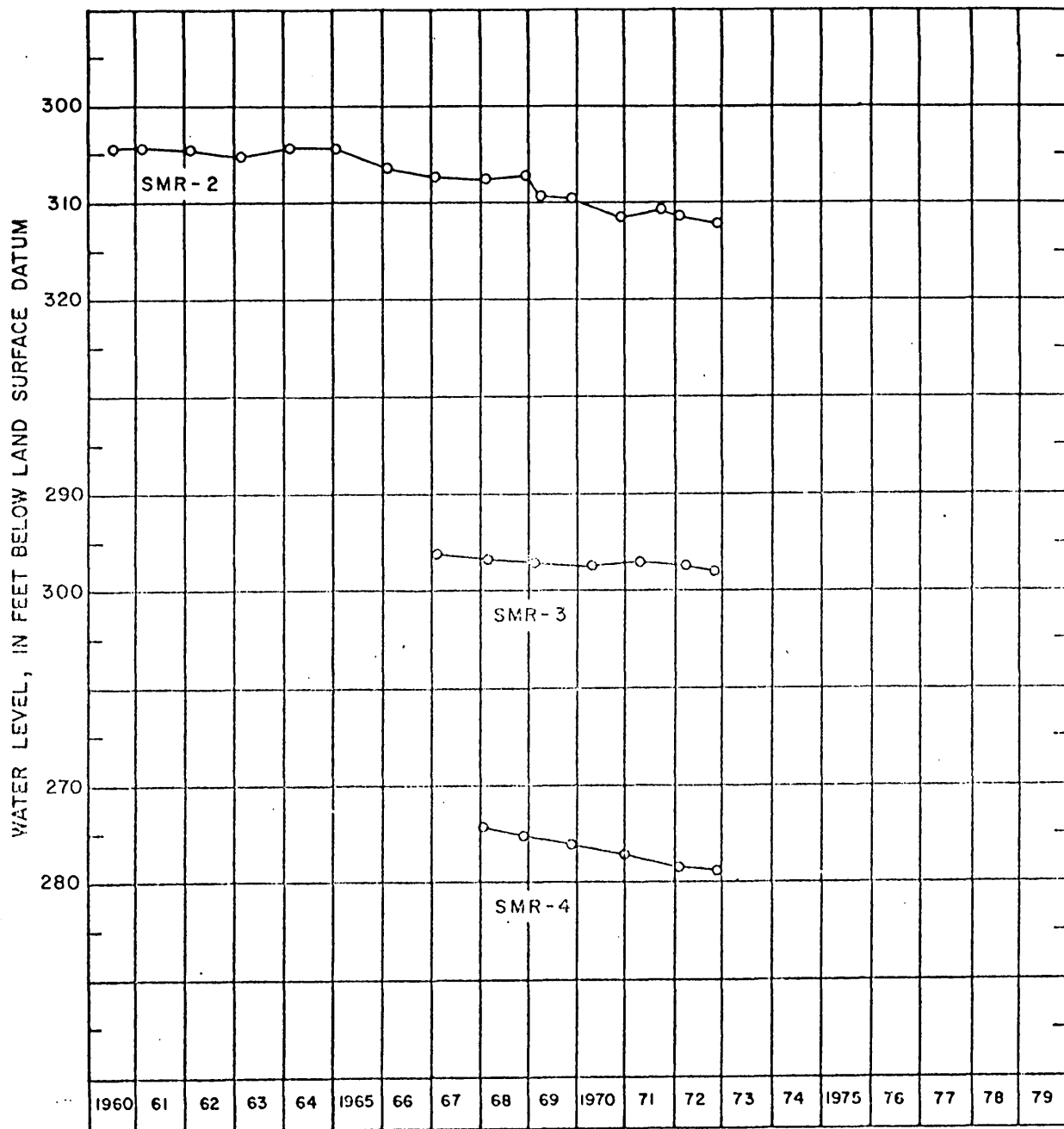


Figure 10.--Hydrograph of Test wells SMR-2, SMR-3, and SMR-4.

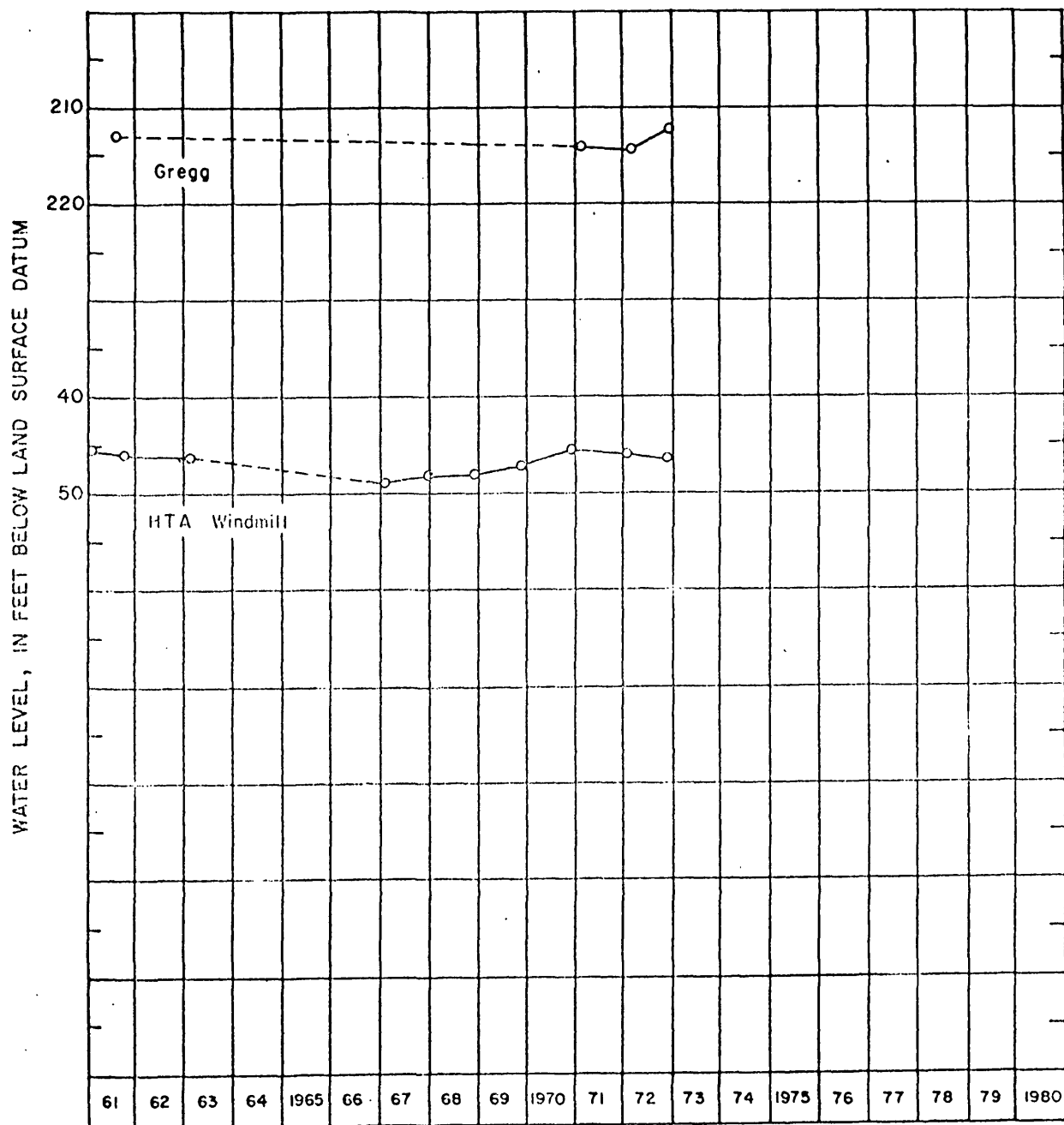


Figure 11.--Hydrograph of Gregg well and HTA windmill.

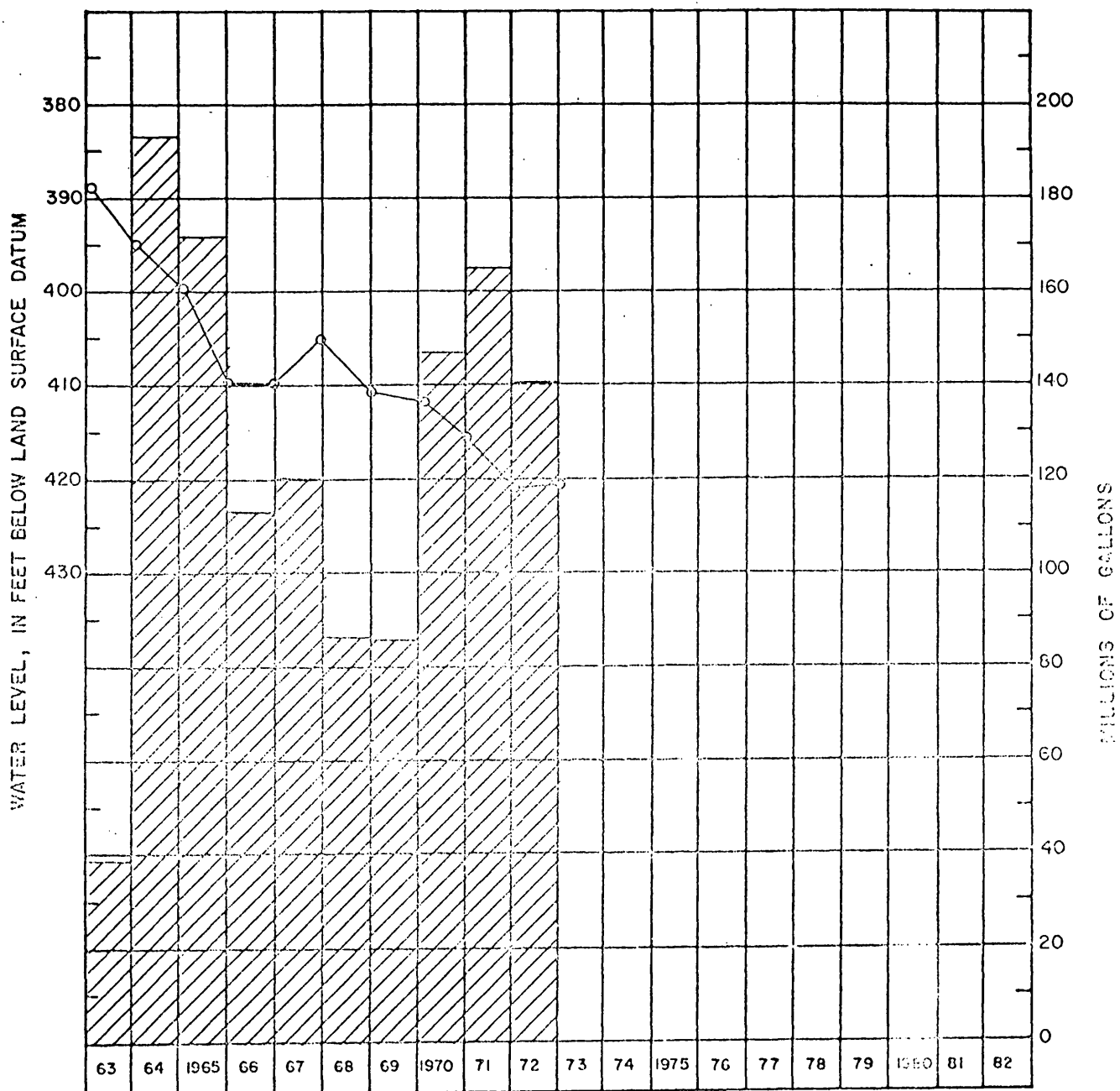


Figure 12.--Annual pumpage and hydrograph of supply well 10A.

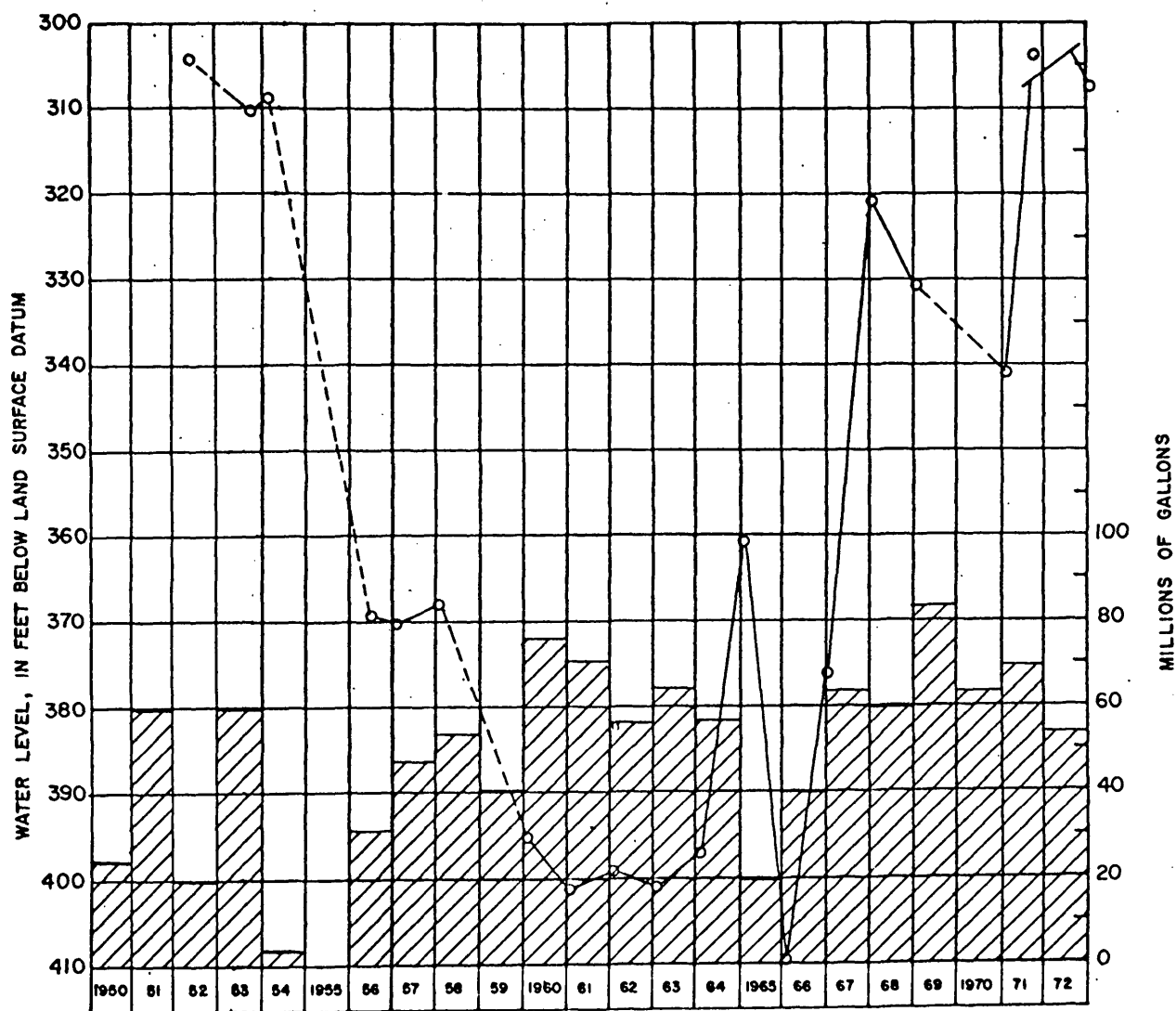
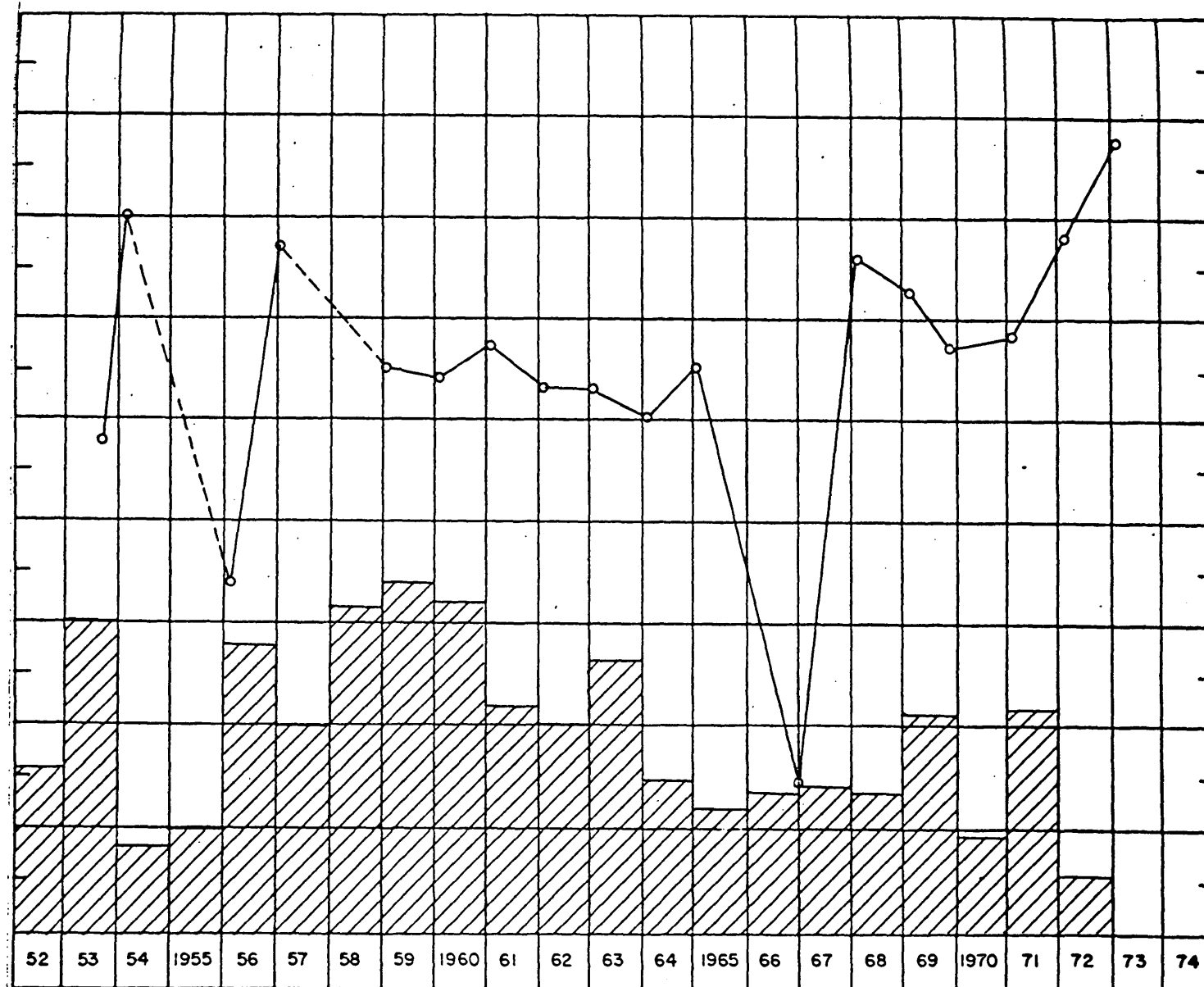


Figure 13.--Annual pumpage and hydrograph of supply well 11.

WATER LEVEL, IN FEET BELOW LAND SURFACE DATUM



MILLIONS OF GALLONS

Figure 14.--Annual pumpage and hydrograph of supply well 13.

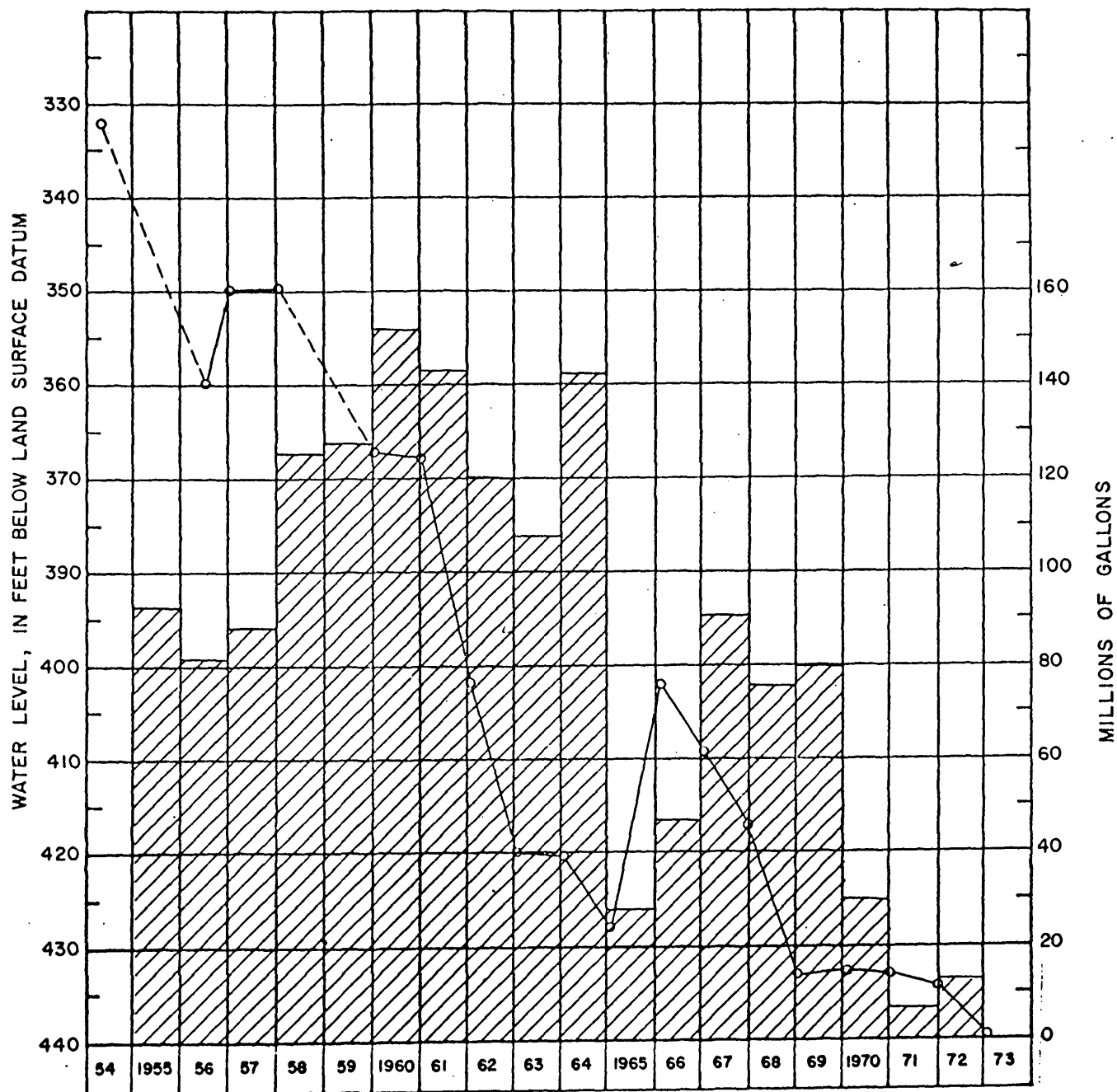


Figure 15.--Annual pumpage and hydrograph of supply well 15.

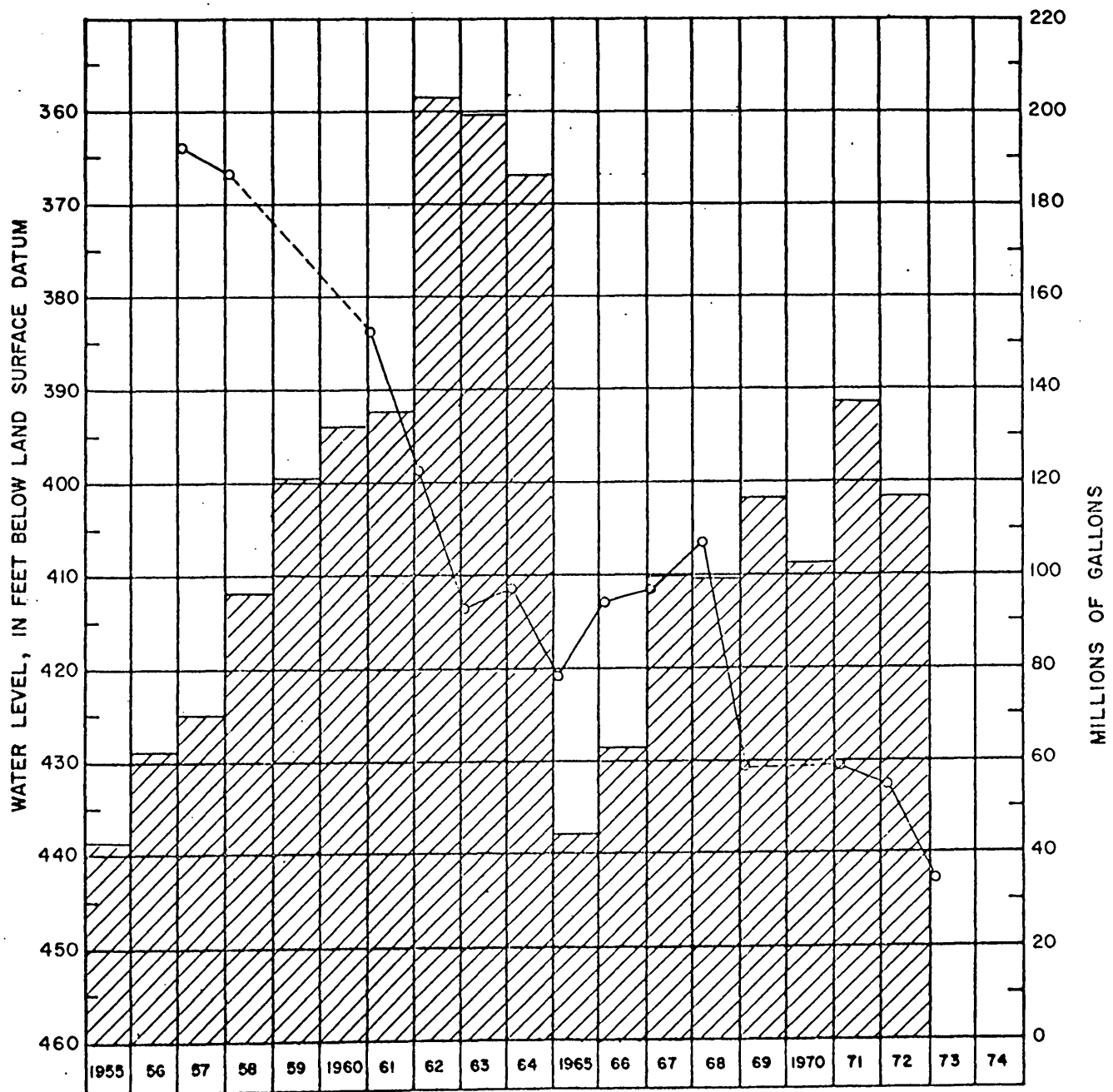


Figure 16.--Annual pumpage and hydrograph of supply well 16.

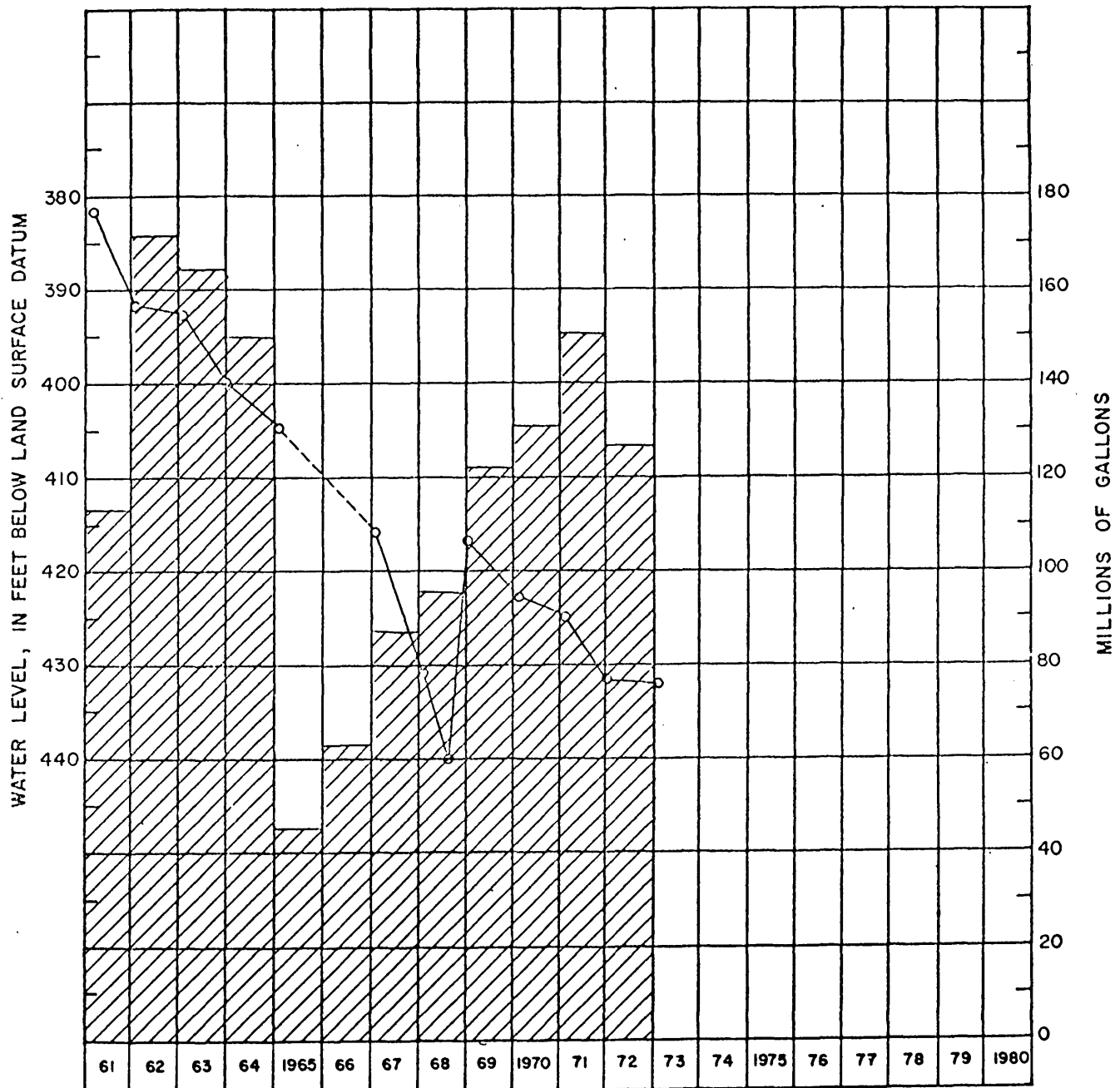


Figure 17.--Annual pumpage and hydrograph of supply well 17.

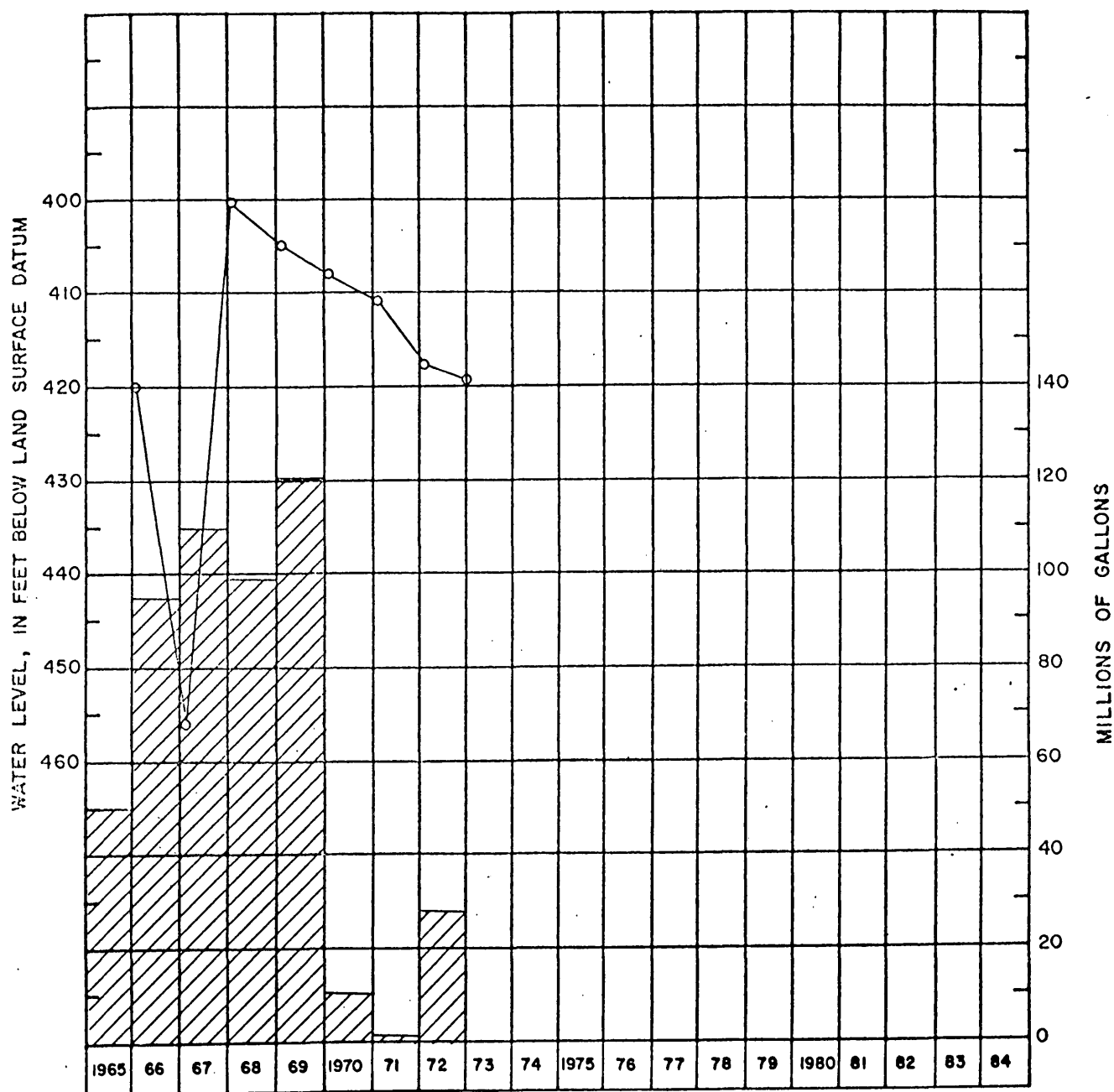


Figure 18.--Annual pumpage and hydrograph of supply well 18.

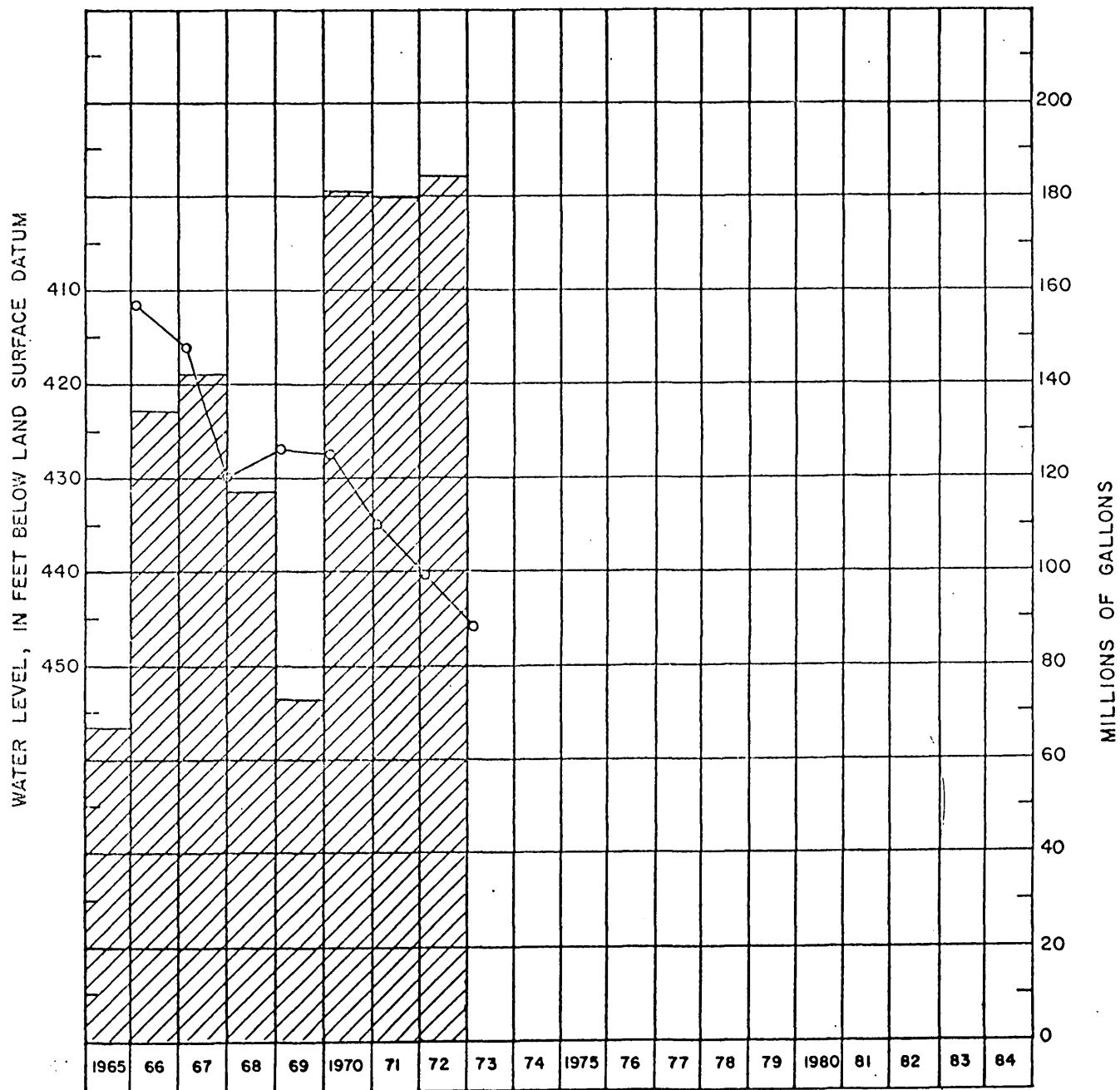


Figure 19.--Annual pumpage and hydrograph of supply well 19.

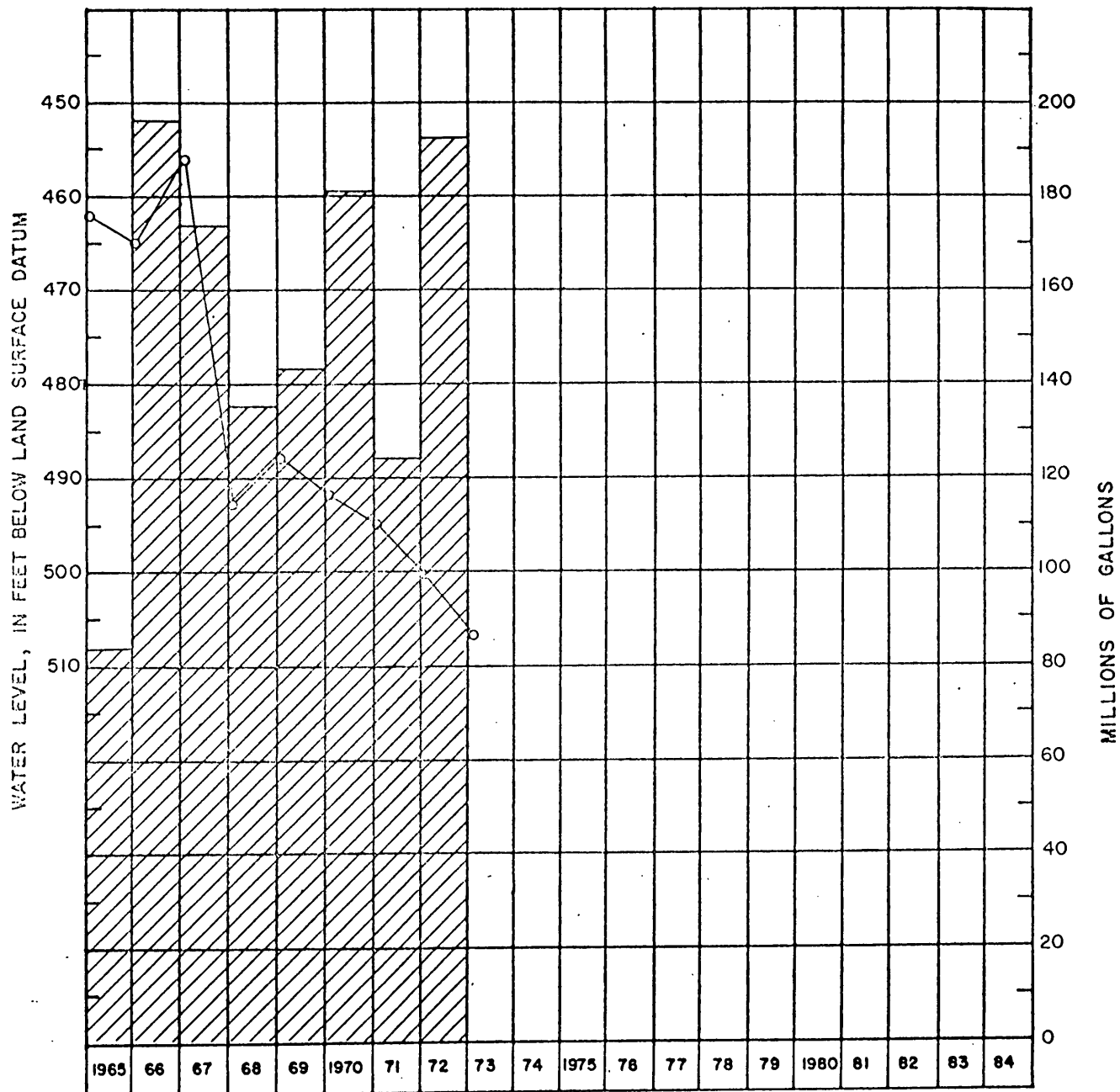


Figure 20.--Annual pumpage and hydrograph of supply well 20.

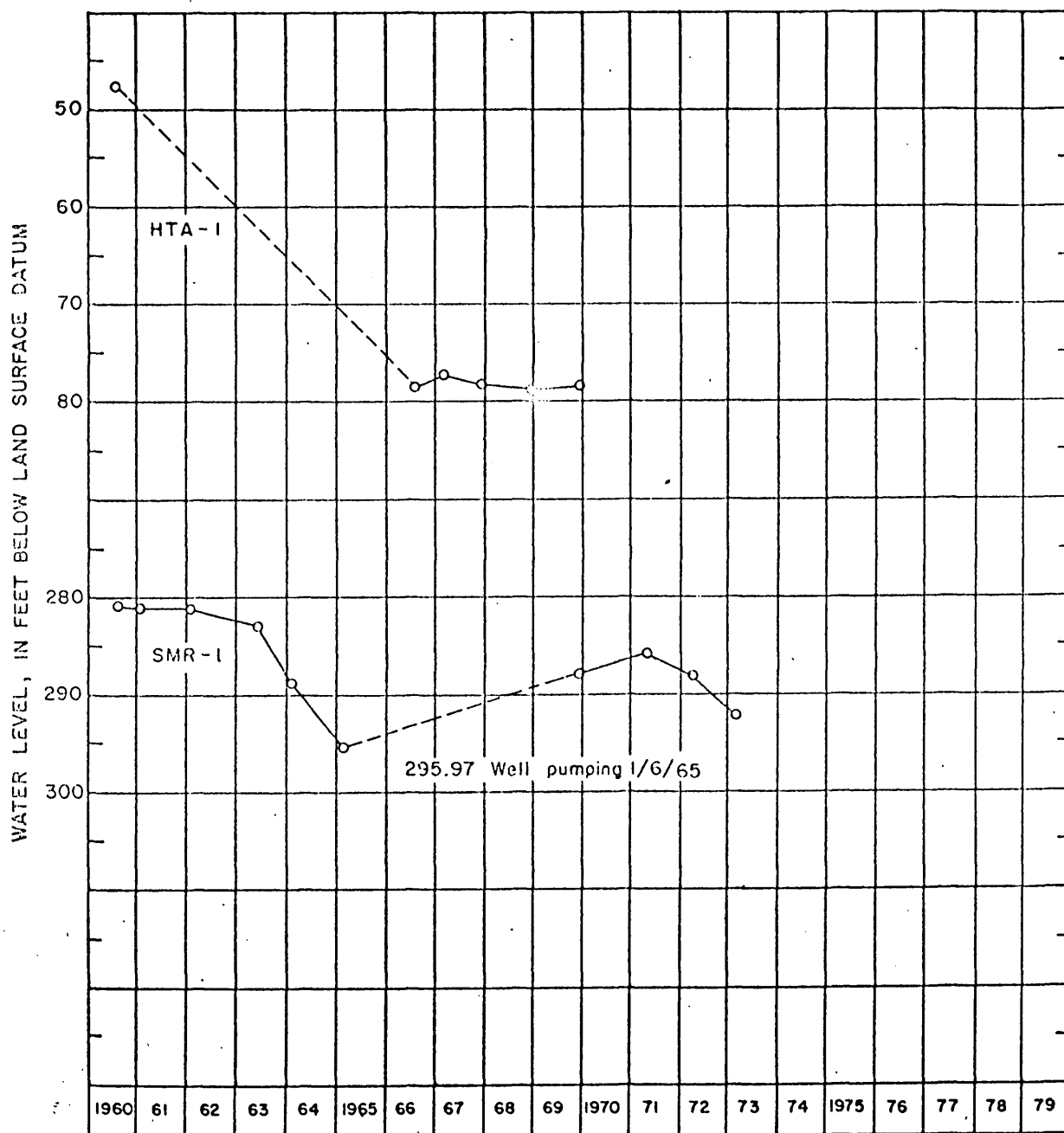


Figure 21.--Hydrograph of supply wells HTA-1 and SMR-1.

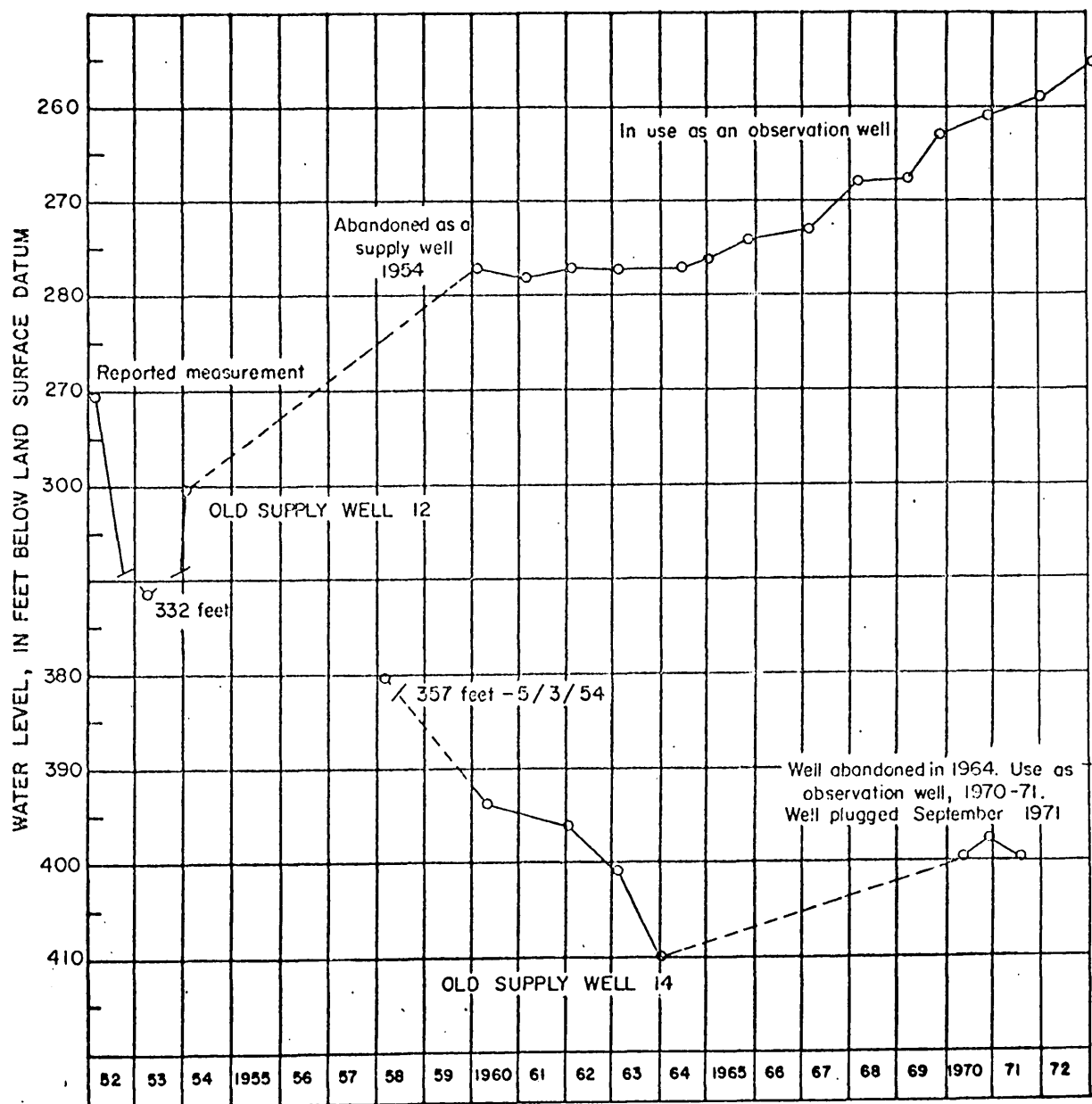


Figure 22.--Hydrograph of old supply wells 12 and 14.

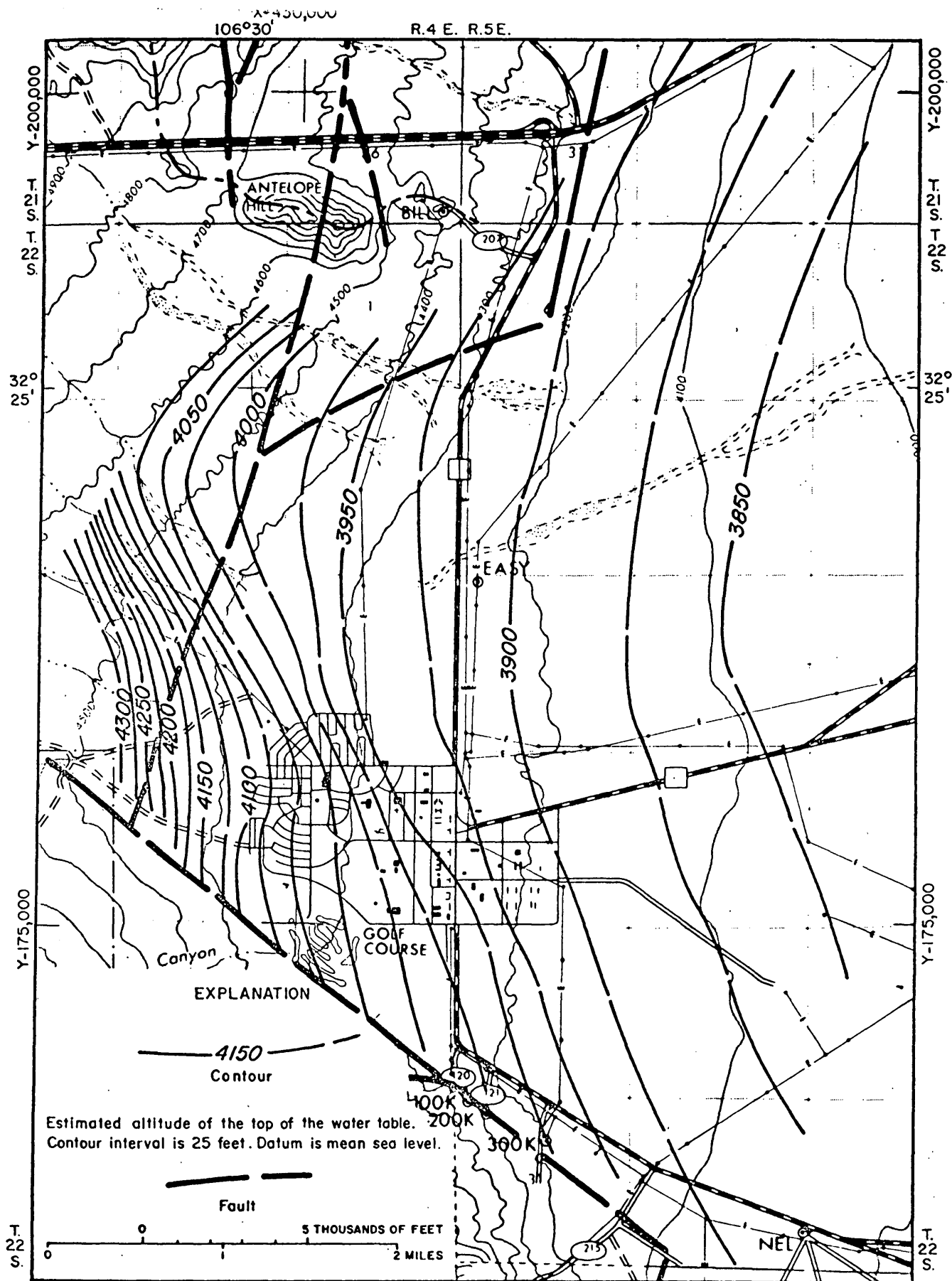
The estimated configuration of the water table in 1949 is shown on figure 23. Although only a few stock wells provided the control, this map shows a regional slope of the water table from the nearby mountains to the Tularosa Basin across the White Sands re-entrant. Undoubtedly this reflects the ground-water conditions prior to development.

After 15 years of production from the Post Headquarters well field, a clearly defined cone of depression existed (fig. 24). Although there had been little change in the water-table contours west of the well field, the contours east of the field showed a pronounced influence due to pumping.

During the period 1949 through 1964, an estimated 20,000 acre-feet of water was withdrawn from the aquifer beneath the Post Headquarters well field. The maximum drawdown was slightly more than 75 feet in the area of maximum production (fig. 25). At that time (1964) the cone of depression had not extended beyond the reentrant.

In July 1972, the axis of the cone of depression roughly paralleled the line of supply wells (fig. 26). The area influenced by pumping had extended to the limits of the reentrant, and eastward into the Tularosa Basin.

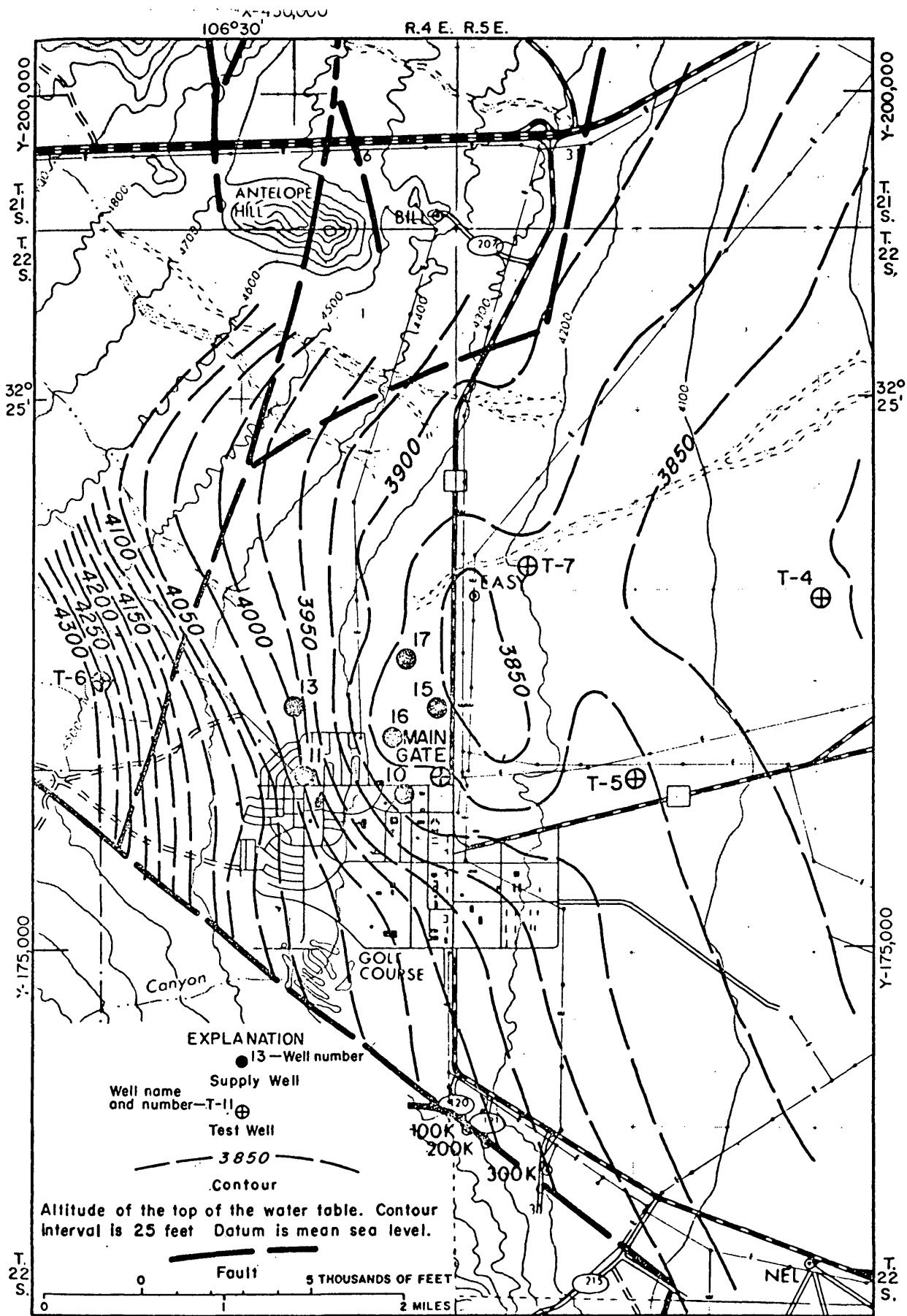
From 1964 until July 1972, approximately 20,000 acre-feet of water was withdrawn from the aquifer. This caused an additional drawdown of more than 25 feet in the four major producing wells (fig. 27). Unlike the drawdown shown in figure 25 for the 1949-1964 interval, the area of influence was spread more evenly throughout the well field. Also, wells 12 and 14 were not in production during this time, so there was a general recovery in the southwest part of the well field.



Base from White Sands Missile Range
Master Plan Basic Information Maps, 1972

Compiled by T.E. Kelly, 1972. Adapted from
W.C. Ballance and S.M. Longwill (written commun. 1968)

Figure 23.-- Contour map of water table, 1949 (estimated).



Base from White Sands Missile Range
Master Plan Basic Information Maps, 1972

Compiled by T.E. Kelly, 1972. Adapted from
W.C. Ballance and S.M. Longwill (written commun. 1968)

Figure 24--Contour map of water table, 1964.

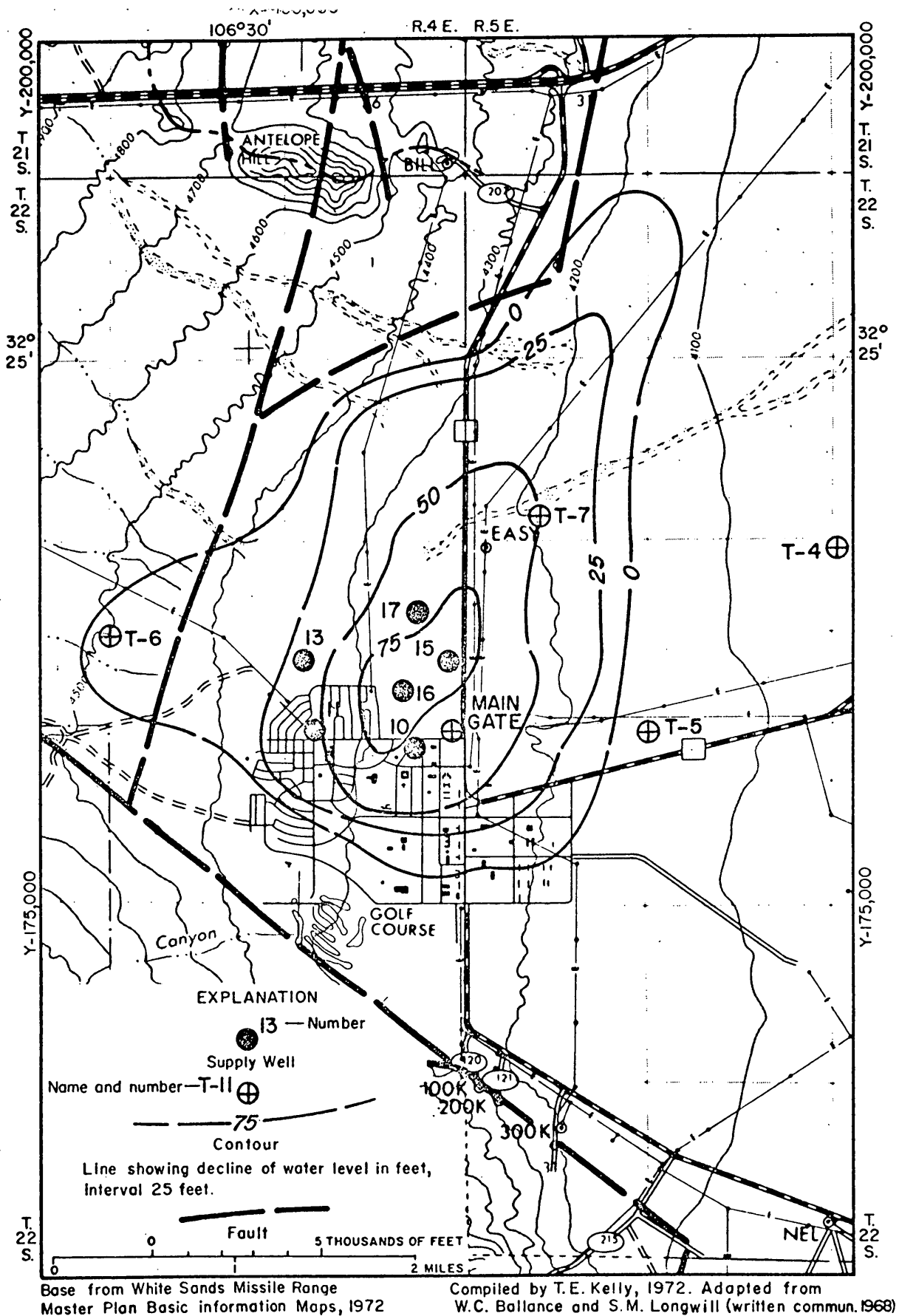


Figure 25.--Water-level change between 1949 and 1964.

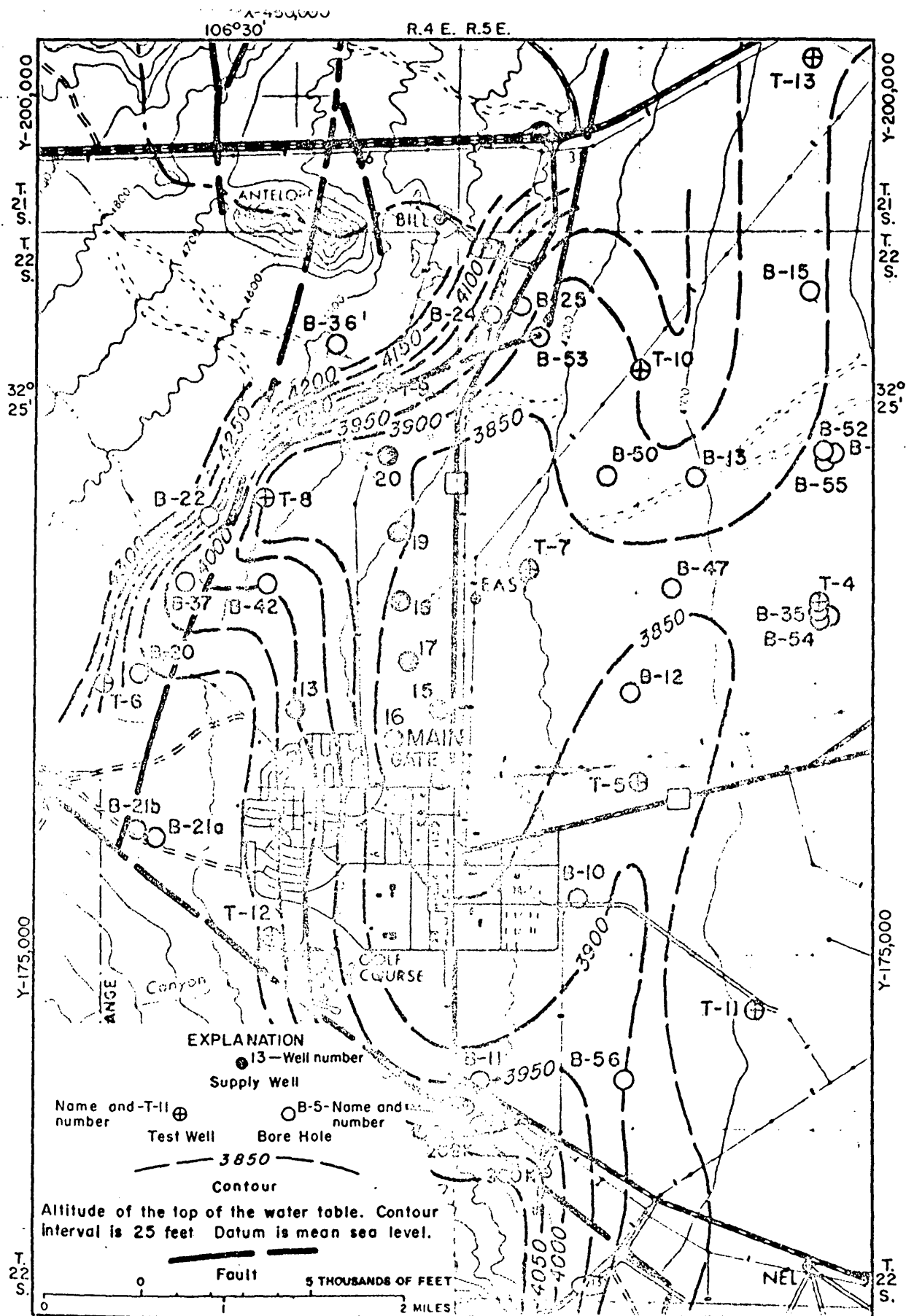
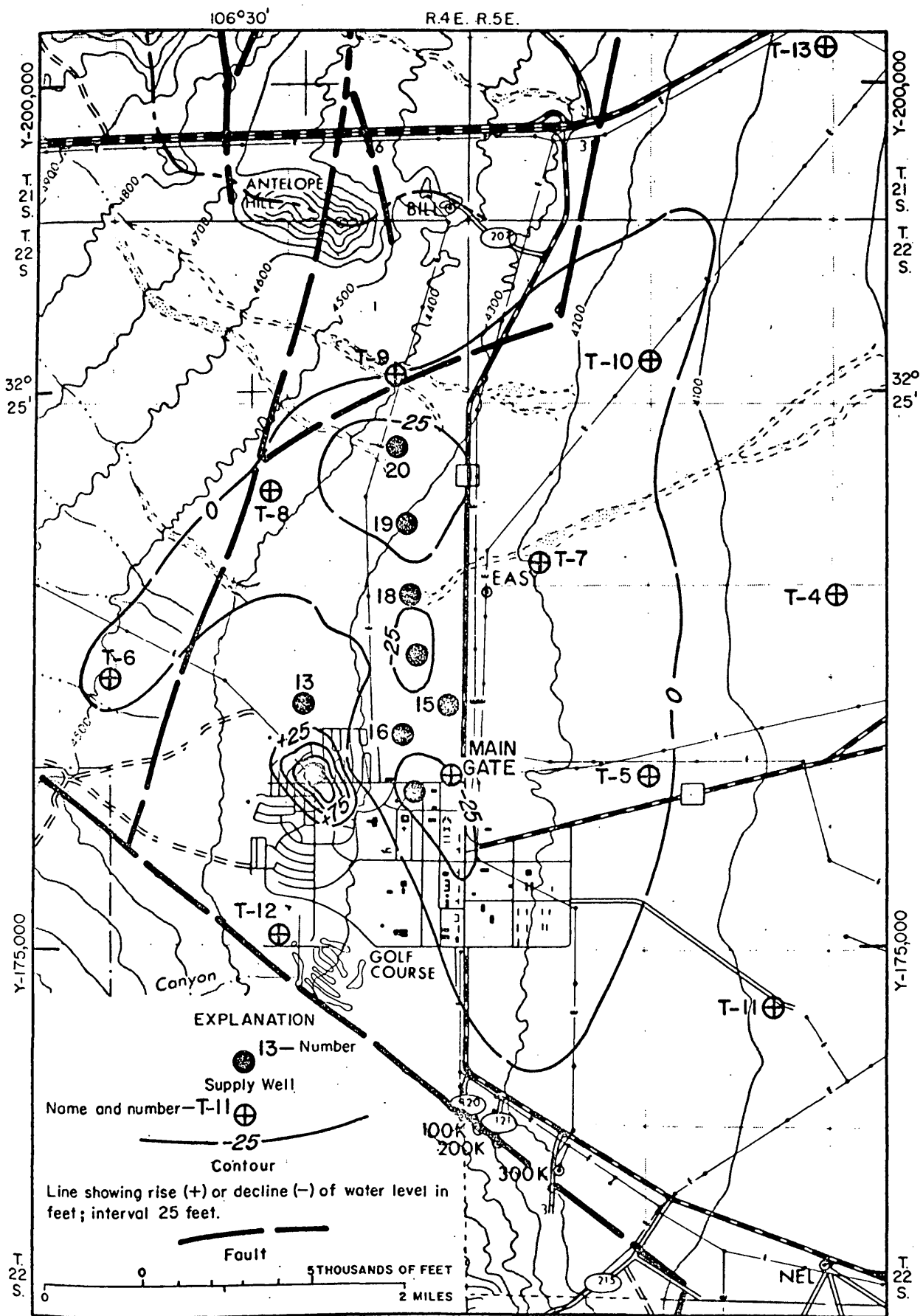


Figure 26.--Contour map of water table in Post Headquarters area, July 1972



Base from White Sands Missile Range
Master Plan Basic information Maps, 1972

Compiled by T.E. Kelly, 1972. Adapted from
W.C. Ballance and S.M. Longwill (written commun. 1968)

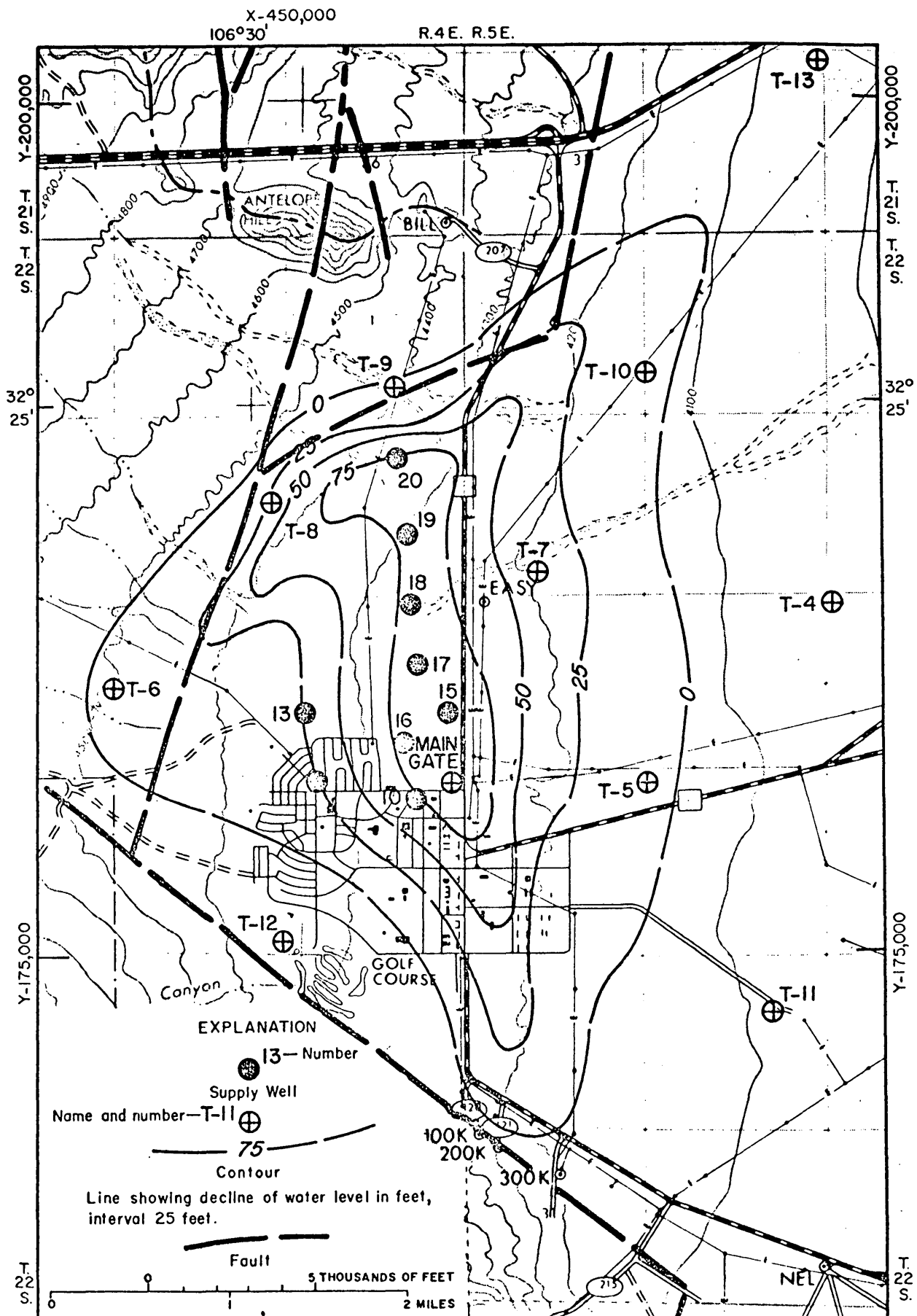
Figure 27.--Water-level change between 1964 and 1972.

The total drawdown of the water table between 1949 and 1972 is shown in figure 28. This is the combined drawdown illustrated in figures 25 and 27. The axis of the cone of depression underlies the major producing wells and the area of influence has extended approximately 2 miles east of the well field.

West of the fault zone shown in figure 29, monzonite is the major geologic unit underlying the permeable clastics containing the fresh-water zone. On the east side of this fault zone, a consolidated conglomerate has been identified beneath the permeable clastics of the fresh-water zone. This conglomerate probably is considerably older than the bolson fill inasmuch as cores from this unit reveal that it is well lithified. Monzonite pebbles derived from nearby mountains comprise a large percentage of the conglomerate, therefore this unit has been difficult to recognize in well cuttings. However, it does have rather prominent characteristics on some geophysical logs. The more mineralized water forms a sloping boundary of the fresh-water zone on the east. These relationships are shown on figure 29.

Figure 30 shows the configuration of the base of the fresh-water zone (less than 1,000 milligrams per liter dissolved solids), and total thickness of the fresh water in the Post Headquarters and adjacent areas is shown in figure 31. This map, based on all data available in July 1972, shows that the maximum thickness is at least 1,500 feet. There is no doubt that the size and configuration of this area is controlled by the Organ Mountain fault zone.

The configuration of the water table in July 1972 is shown in figure 32.



Base from White Sands Missile Range
Master Plan Basic Information Maps, 1972

Compiled by T.E. Kelly, 1972. Adapted from
W.C. Ballance and S.M. Longwill (written commun. 1968)

Figure 28.--Water-level change between 1949 and 1972.

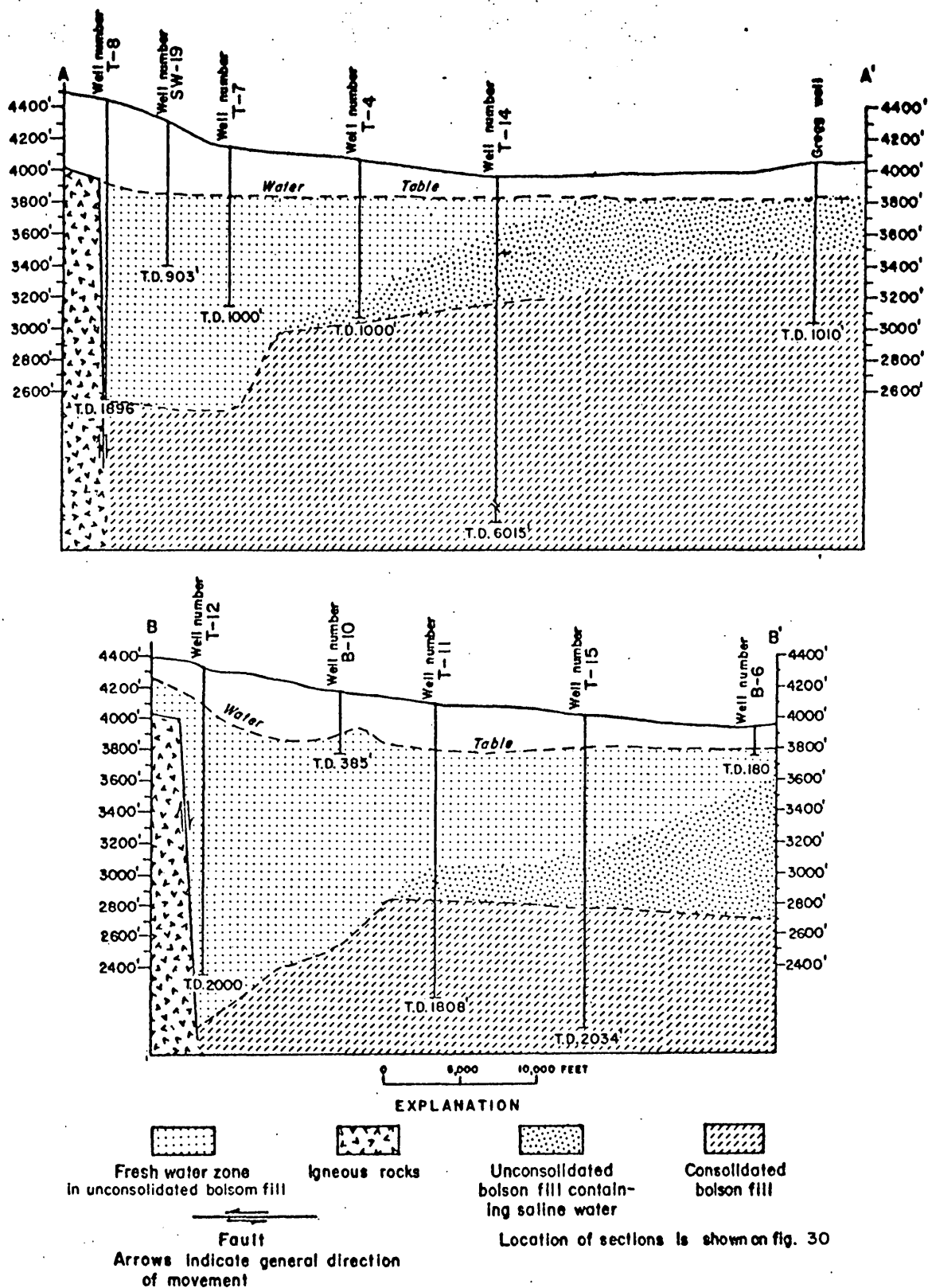


Figure 29.--Cross sections of the Post Headquarters area.

A trough of fresh water, having a maximum thickness of about 700 feet, parallels the mountain front north of the Post Headquarters. A similar trough extends southward from the Post Headquarters to the limits of the study area. Throughout the area, fresh water interfaces with saline water along a line which roughly parallels the mountain front.

Water-quality data has been collected during the various ground-water investigations; this is on file in the offices of the U.S. Geological Survey in Albuquerque. Although minor changes in water quality have been noted which deserve continued monitoring, in general there is no evidence to indicate significant intrusion of saline water into the White Sands aquifer. Bar graphs showing the principal chemical constituents in the water from various wells in the project area are illustrated on figure 33.

SUMMARY

Hydrologic data show great variation in transmissivity at different test sites; much of this may be due to well construction and development. Specific capacities based on production figures probably are the most reliable data.

As the well field was expanded northward where greater yields were obtained, water-level declines were distributed more uniformly throughout the aquifer. As much as 100 feet of recovery was recorded in supply well 11.

The Organ Mountain fault zone is the major controlling factor of the size and configuration of the aquifer; maximum aquifer thickness is 1,500 feet.

In addition to that in the Post Headquarters area, potable water is present in significant quantities along the mountain front; however, hydrologic data are lacking in these areas.

There is considerable variation in the principal chemical constituents found in ground water of the project area.

There is no evidence to indicate that saline-water encroachment has begun in the present well field.

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