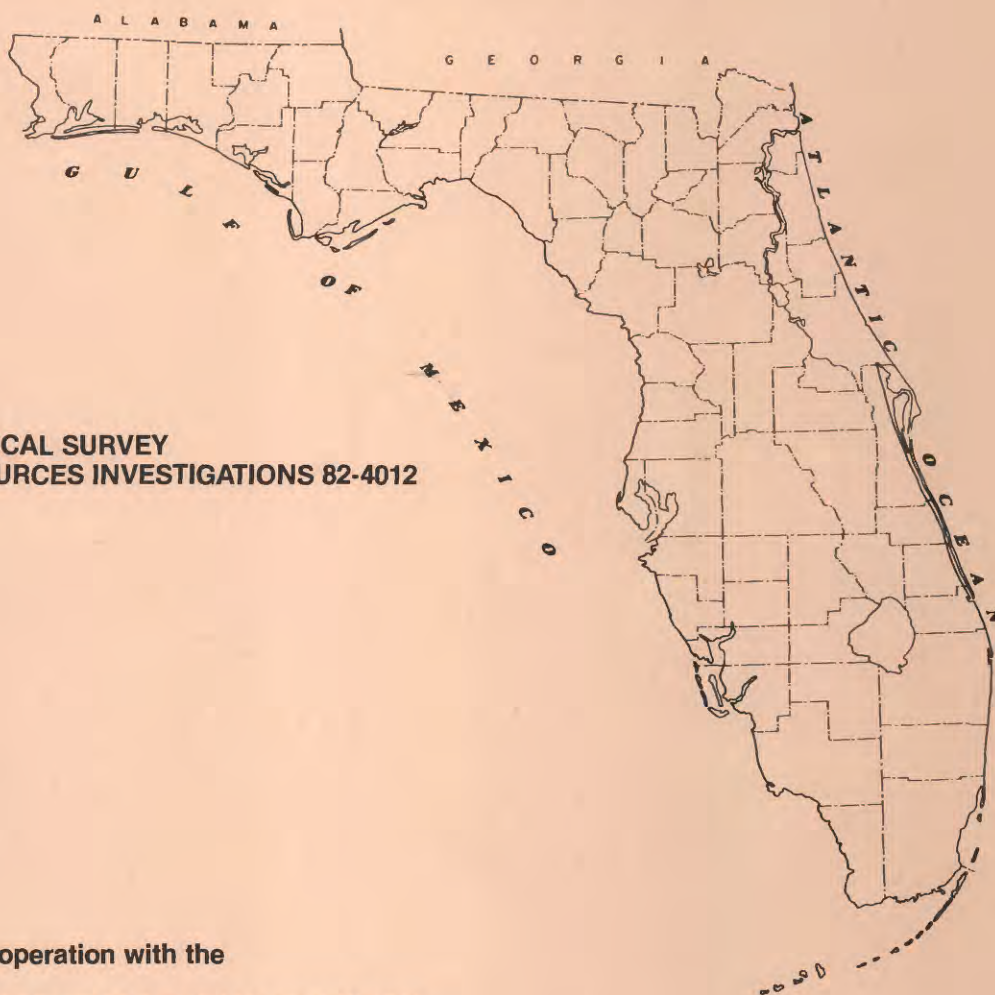


# TECHNIQUE FOR ESTIMATING MAGNITUDE AND FREQUENCY OF FLOODS ON NATURAL-FLOW STREAMS IN FLORIDA

U.S. GEOLOGICAL SURVEY  
WATER-RESOURCES INVESTIGATIONS 82-4012



Prepared in cooperation with the  
FLORIDA DEPARTMENT OF TRANSPORTATION





UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY

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ON NATURAL-FLOW STREAMS IN FLORIDA

By Wayne C. Bridges

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Tallahassee, Florida

1982

UNITED STATES DEPARTMENT OF THE INTERIOR

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GEOLOGICAL SURVEY

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## SYMBOLS

- $A_g$  = Drainage area for gaged site, in square miles;  
 $A_u$  = Drainage area for ungaged site, in square miles;  
 $B_1, B_2, B_3 \dots$  = Partial regression coefficients;  
 $C$  = Regression constant;  
 $C_2, C_{25}, C_{100}$  = Geographic coefficient for estimating 2-, 25-, and 100-year recurrence-interval flood discharge at rainfall-runoff stations;  
 $DA$  = Drainage area, in square miles;  
 $EY$  = Accuracy for a flood estimate, in equivalent years of record;  
 $K$  = Pearson Type III deviate;  
 $LE$  = Channel length, in miles;  
 $LK$  = Total area of lakes and ponds, in percent of drainage area;  
 $M$  = Mean of logarithms of the annual peaks;  
 $N$  = Number of items in a data set;  
 $n$  = Time interval, in years;  
 $P$  = Exceedance probability;  
 $p$  = Probability of at least one exceedance within the specified time interval;  
 $Q_g$  = Estimate from log-Pearson Type III distributions of T-year flood, in cubic feet per second;  
 $Q_r$  = Estimate from regression equation of T-year flood for gaged site, in cubic feet per second;  
 $Q_{ru}$  = Regional estimate of T-year flood from regression equation for ungaged site, in cubic feet per second;  
 $Q_t$  = Estimate of the T-year flood from log-Pearson Type III distribution, in cubic feet per second;  
 $Q_u$  = Adjusted estimate of T-year flood for ungaged site, in cubic feet per second;  
 $Q_{wt}$  = Weighted estimate of T-year flood at gaged site, in cubic feet per second;

R = Multiple correlation coefficient;

S = Standard deviation of the logarithms of annual peaks;

SL = Channel slope, in feet per mile;

T = Recurrence interval, in years;

$X_1, X_2, X_3 \dots$  = Independent variables in linear regression.

#### ABBREVIATION AND CONVERSION FACTORS

Factors for converting inch-pound units to International System of units (SI) and abbreviation of units.

<u>Multiply</u>	<u>By</u>	<u>To obtain</u>
inch (in)	25.40	millimeter (mm)
foot (ft)	0.3048	meter (m)
mile (mi)	1.609	kilometer (km)
square mile (mi <sup>2</sup> )	2.590	square kilometer (km <sup>2</sup> )
cubic foot per second (ft <sup>3</sup> /s)	0.02832	cubic meter per second (m <sup>3</sup> /s)





# TECHNIQUE FOR ESTIMATING MAGNITUDE AND FREQUENCY OF FLOODS

## ON NATURAL-FLOW STREAMS IN FLORIDA

By Wayne C. Bridges

### ABSTRACT

A technique is provided for estimating floods on natural-flow streams in Florida for specific recurrence intervals of 2, 5, 10, 25, 50, 100, 200, and 500 years. Flood peaks from 159 stream-gaging stations with long-term records (10-53 years) and 23 rainfall-runoff stations with short-term records (7-17 years) were used in a multiple linear regression analysis to develop the regional equations relating peak discharge to basin characteristics. The State is divided into three hydrologic regions, A, B, and C. The significant independent variables were drainage area, channel slope, and lake area in Regions A and C. In Region B, the significant independent variables were drainage area and lake area.

### INTRODUCTION

The ability to adequately define the magnitude and frequency of floods is necessary for the regulation, planning, and design of activities along rivers and streams in Florida. One of the first considerations in the safe and economical design of drainage structures is the magnitude and frequency of the design flood or the maximum peak flow that can safely pass through the structure. The most desirable basis for selection of the design discharge is a flood-frequency analysis of a long-term record of floods that have occurred at or near the site, but long-term flood records are rarely available for the site where they are needed.

In 1958, the Florida Department of Transportation and the U.S. Geological Survey began a cooperative program to establish a data base of annual peaks to be used in future statewide flood-frequency studies. This crest-stage network was expanded in 1964 to increase the geographic coverage.

With more than 50 percent of the Florida highway bridge construction funds being spent to build bridges and culverts on small basins, there was a great need for reliable flood-frequency information for small basins. As used in this report, basins that are 10 square miles or less are considered to be small. To meet this need for flood-frequency data on small basins, the Geological Survey and the Florida Department of Transportation expanded the cooperative program in July 1967 to develop a data base and to extend short-term flood peak records on small basins using the Geological Survey rainfall-runoff model (Dawdy and others, 1972).

Although the initial plan for the small-basins flood-frequency study called for a separate report dealing exclusively with small basins (Bridges, 1977), a decision was made during the study to incorporate the flood-peak data from the small basins with flood-peak data from the larger basins and have a single report covering all sizes of basins.

This report supersedes previous Geological Survey reports to estimate flood magnitudes and frequencies. Previous studies on regional flood-frequency relations are Pride (1958), Barnes and Golden (1966), and Rabon (1971). A regional flood-frequency study was done by Seijo and others (1979) for a 15-county area in west-central Florida.

The reports by Pride (1958) and Barnes and Golden (1966), based on flood-peak data through 1953 and 1961, respectively, used the index-flood method of analysis (Dalrymple, 1960). The Rabon report (1971) presented flood-frequency relations for the 2- through 50-year recurrence intervals and was based on a regression analysis of flood discharges (data to 1970) and basin characteristics. To show that the technique used in this report is comparable to that used in the regional report by Seijo and others (1979), a comparison was made of the 25-year flood for the 40 gaging stations in the study area used by Seijo. The weighted discharge for the 25-year flood from the report by Seijo averaged about 5 percent more than the weighted discharge computed in this report.

The purpose of this report is to:

1. Present flood data for the gaged sites used in the flood-frequency analysis.
2. Describe the method of analysis used to develop the flood-estimating technique.
3. Provide regression equations for estimating floods on natural-flow (unregulated) streams.
4. Provide a method for improving the flood estimate at gaged sites.
5. Provide illustrative examples of applying the flood-estimating technique.

Frequently, streamflow records are insufficient or else do not exist at the site where information is desired. Since flood characteristics at individual gaging stations have very limited transfer capability, estimates of flood characteristics should be based on a regional analysis of streamflow records. The method of multiple linear regression analysis was used to develop the regional flood-frequency relations which relate flood-peak discharge to selected basin characteristics.

The study benefited from the interest and support given by Edward G. Ringe, Jr., Engineer of Drainage, Florida Department of Transportation.

## DATA BASE

### Annual Maximum Discharge

Records of the annual maximum discharge for Florida stream-gaging stations are stored in the National Water Data Storage and Retrieval System computer file. Annual maximum discharges (through September 1978) for 182 streamflow stations were available for analysis. Long-term records (10 to 53 years) at 125 continuous and 34 crest-stage stream-gaging stations and short-term records (7 to 17 years) at 23 small-basin rainfall-runoff gaging stations were used in the flood-frequency analysis.

Dual digital recorders were used to collect concurrent rainfall and runoff data at the small basin sites. Stage-discharge ratings were defined by current meter measurements.

At the small basin sites, most of the records were short (less than 10 years) thereby increasing the probability of a time sampling error. A reliable flood-frequency curve requires many years of annual flood maximums. To overcome this deficiency on the small basins, the Survey's rainfall-runoff model, which uses long-term rainfall records as input, was utilized to synthesize long-term flood-peak data. For a detailed description of the model, computational procedures, assumptions, and reliability, see Dawdy and others (1972). The model and its application to Florida data are described by Bridges (1977).

Sites that were significantly affected by tides, regulation, diversion, or reservoirs were not used in this analysis.

### Flood-Frequency Curves

Frequency curves for individual gaging stations were developed following the guidelines described in Bulletin 17A, U.S. Water Resources Council (1977). In accordance with the recommended procedure, a log-Pearson Type III distribution function was used to fit observed data to log-probability curves. The distribution is defined by the equation:

$$\log Q_T = M + KS, \quad (1)$$

where

$Q_T$  is the peak discharge for a selected recurrence interval  $T$ , in cubic feet per second;

$M$  is the mean of the logarithms of the annual peaks;

$K$  is the Pearson Type III frequency factor expressed in number of standard deviations from the mean for selected recurrence interval;

$S$  is the standard deviation of the logarithms of the annual peaks.

To fit the log-Pearson Type III distribution to the annual maximum discharges at each gaging station, the Geological Survey computer program J-407, described by Kirby (1979), was used to perform the statistical analysis. Although program J-407 follows the guidelines of the U.S. Water Resources Council (WRC), the user is still required to use hydrologic judgment in supplying information on regional skew, historic peaks, gage-base discharge, low and high outliers, and the interpretation of the frequency distribution.

The skew coefficient determined from the station record is sensitive to extreme events; therefore, the longer the record, the more reliable the skew coefficient. It is recommended by WRC that a generalized skew be applied to station records of less than 25 years and, for station records of 25 to 100 years, a weighted-skew coefficient be used.

An effort was made to determine a better estimate of the generalized skew by plotting the station skews and drawing a skew isoline map for station records of 25 years or more. Distinct geographic and topographic patterns were not evident; therefore, the decision was made to use the WRC generalized-skew map. Values of skew can be found on the map in U.S. Water Resources Council (1977, pl. 1).

Frequency curves for 23 small-basin rainfall-runoff sites were computed using a procedure developed by Lichty and Liscum (1978) to improve the T-year (annual) flood estimates. The T-year flood estimates were computed as the weighted average of the map model estimate and the observed estimate in proportion to the accuracy of each estimate. The observed estimate is derived from the log-Pearson Type III distribution of annual peaks at the small basin site. The map model estimate is based on a long-term rainfall record that is transferred to the gaged site by means of three maps depicting the geographic variability of a coefficient,  $C_i$ , ( $i = 2-, 25-,$  and  $100\text{-year}$  recurrence intervals). Maps were extended (R. W. Lichty, written commun., 1979) to include peninsular Florida.

For each small basin site, the rainfall-runoff model is calibrated and the fitted parameters from the rainfall-runoff model are used in conjunction with the climatic factor,  $C_i$ , to define a frequency curve.

The procedure for estimating the map model yields an accuracy (in equivalent years of record) ranging from 7 years for the 2-year flood to 30 years for the 100-year flood.

### Basin Characteristics

Described below are the basin characteristics that were tested for significance as independent variables in the regression analysis. Many of the variables were not significant and do not appear in the final prediction equations. The streamflow and basin characteristics are stored in the National Water Data Storage and Retrieval System computer file.

1. Drainage area (DA), in square miles: the area that contributes to surface runoff. Basin boundaries are delineated on U.S. Geological Survey topographic maps and the contributing area is determined by planimetry.

2. Channel slope (SL), in feet per mile: the average slope of the main channel between points 10 and 85 percent of the distance upstream from the gaging site to the basin divide.

3. Channel length (LE), in miles: the length of the main channel between the gaging station and the basin divide, as measured along the channel which drains the largest area of the basin above each junction.

4. Elevation (EL), in feet: the mean basin elevation, in feet above National Geodetic Vertical Datum of 1929 (formerly referred to as "mean sea level"), measured from topographic maps by transparent grid-sampling method (20 to 80 points sampled in each basin).

5. Storage (ST), in percent: the surface area of lakes, ponds, and swamps expressed as a percentage of the contributing drainage area.

6. Lake area (LK), in percent: the surface area of lakes and ponds expressed as a percentage of the contributing drainage area.

7. Swamps (SW), in percent: the surface area of swamps (defined as marsh and wooded marsh on topographic maps) expressed as a percentage of the contributing drainage area ( $SW = ST - LK$ ).

8. Forest (FO), in percent: the area of forest expressed as a percentage of the contributing drainage area; forested area shown on topographic maps.

9. Soil (SO), in inches: the soils index represents values of potential maximum infiltration during an annual flood, under average soil moisture conditions. Values of the soils index were computed from a map provided by the Soil Conservation Service, U.S. Department of Agriculture.

10. Precipitation (PR), in inches: the mean annual precipitation determined from an isohyetal map prepared from U.S. Weather Bureau (1959, rev. 1962) precipitation records.

11. Precipitation intensity (I24,2), in inches: the maximum 24-hour precipitation expected to be exceeded on an average of once each 2 years. Values for this index were determined from a U.S. Weather Bureau (1958) publication.

## REGIONAL ANALYSIS

### Multiple Regression Analysis

A multiple regression analysis was used to develop relations between flood-peak discharge (dependent variable) and drainage-basin characteristics (independent variables). A data-analysis system called Statistical Analysis System (SAS) was used to perform the multiple regression (Nielwig and Council, eds., 1979). SAS contains five methods of stepwise regression. The stepwise procedure "maximum  $R^2$  improvement" (MAXR) was selected to determine which of the independent variables would be included in the regression model.

$R^2$  is the square of the multiple correlation coefficient and measures how much variation in the dependent variable can be accounted for by the model. The MAXR method begins by finding the one-variable model producing the highest  $R^2$  and adds another variable that will produce the greatest increase in  $R^2$ . Each variable in the two-variable model is compared to each variable not in the model. MAXR determines if removing one variable and replacing it with another would improve  $R^2$ . Comparison or replacement of variables continues until the "best" two-variable model, three-variable model, and so forth, is developed.

The regression model is in the form

$$Q_T = C X_1^{B_1} X_2^{B_2} \dots X_n^{B_n} \quad (2)$$

where

$Q_T$  is the flood peak discharge (dependent variable) for recurrence interval of T-years, cubic feet per second;

$X_1$  to  $X_n$  are the basin characteristics (independent variable);

C is the regression constant for a given recurrence interval;

$B_1$  to  $B_n$  are the regression coefficients for a given recurrence interval.

### Regression Models

Data from 182 gaging stations throughout the State were used in the initial multiple linear regression analysis. Streams with drainage areas larger than 10,000-square miles were excluded from the regression analysis. Flood magnitudes for recurrence intervals of 2, 5, 10, 25, 50, 100, 200, and 500 years (dependent variables) were regressed against the basin characteristics (independent variables). For each recurrence interval, the contributing drainage area (DA) was the most significant independent variable. Although the order of significance varied with recurrence interval, in most cases lake (LK) was the next most important variable, followed by slope (SL). For example, contributing drainage area accounted for approximately 62 percent of the variance of the 10-year recurrence interval flood.

Drainage area and lake area combined accounted for about 80 percent of the variance of the dependent variable and the addition of slope accounted for an additional 3 percent. The use of a fourth or fifth variable did not show significant improvement in the values of  $R^2$  and standard error of the regression equation.

The differences between the station value and the value from the regression, called residuals, were plotted on a State base map to determine geographic bias. A plot of the residuals indicated three hydrologic regions for the State (see figure 1). Region A, the largest of the three regions, covers about three-quarters of peninsular Florida and extends from the St. Marys River basin to the Anclote River basin. In Region A, east Florida streams flow toward the Atlantic Ocean and those on the lower-west coast flow toward the Gulf of Mexico. Region B extends from the upper-west coast to the eastern panhandle and includes river basins from the Pithlachascotee to the Aucilla. Region C extends through the western panhandle from the St. Marks River to the Perdido River. All the streams in Regions B and C flow toward the Gulf of Mexico.

A separate stepwise regression was run using only those stations contained within each of the three regions. In each region, contributing drainage area was the primary independent variable followed in importance by lake area and slope. The exception was Region B where slope was not significant.

Iterations of the stepwise regressions were made, with increments to LK and SL being added, to find the optimum slope of the regression line that best fit the data. The standard error of the regression equation was improved an average of 6 percent when a constant was added to lake area and a minimum value set for slope. In Region A a constant of 3 percent was added to lake area and the minimum value of slope set at 0.9 ft/mi. In Region B a constant of 0.6 percent was added to lake area. In Region C a constant of 3 percent was added to lake area and the minimum slope is set at 0.9 ft/mi.

The regression models for estimating the flood magnitudes for the recurrence intervals of 2, 5, 10, 25, 50, 100, 200, and 500 years are summarized by region in tables 1, 2, and 3.

The regression model for Region A (table 1) has the form:

$$Q_T = C DA^{B_1} SL^{B_2} (LK+3.0)^{B_3} \quad (3)$$

where

$Q_T$  is the discharge for a recurrence interval of T-years, in cubic feet per second;

C is the regression constant;

DA is the drainage area, in square miles;

SL is the channel slope, minimum value set at 0.9, in feet per mile (for example, if SL is less than 0.9 foot per mile, then SL = 0.9 foot per mile);

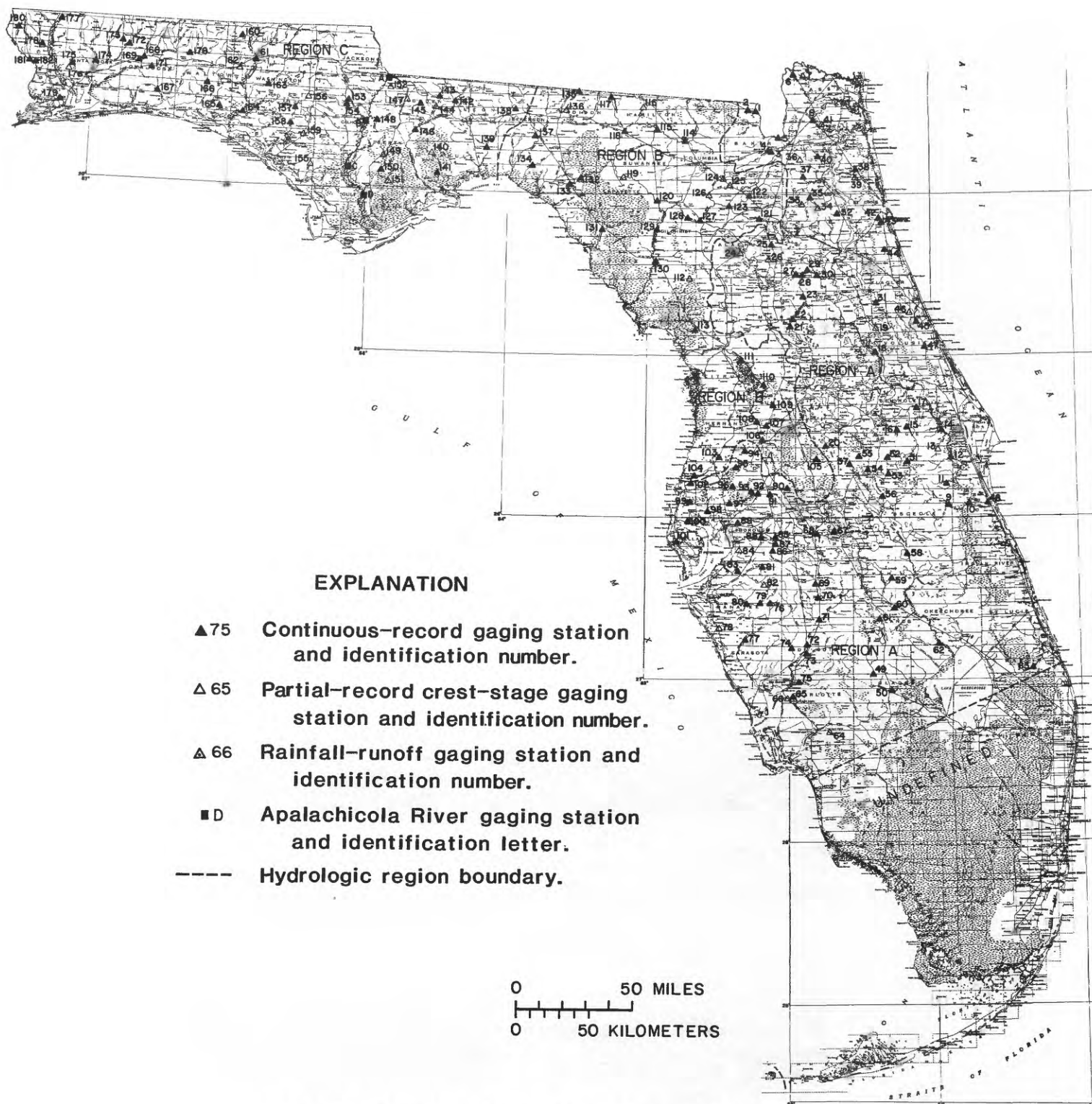


Figure 1.--Location of gaging stations and hydrologic region boundaries.



LK is lake area plus constant of 3, in percent, (for example, LK+3.0, in percent);

B<sub>1</sub>, B<sub>2</sub>, B<sub>3</sub> are exponents of the regression.

The regression model for Region B (table 2) has the form:

$$Q_T = C DA^{B_1} (LK+0.6)^{B_2} \quad (4)$$

where

Q<sub>T</sub> is the discharge for a recurrence interval of T-years, in cubic feet per second;

C is the regression constant;

DA is the contributing drainage area, in square miles;

LK is lake area plus constant of 0.6 percent, (for example, LK+0.6, in percent);

B<sub>1</sub>, B<sub>2</sub> are exponents of the regression.

The regression model for Region C (table 3) has the form:

$$Q_T = C DA^{B_1} SL^{B_2} (LK+3.0)^{B_3} \quad (5)$$

where

Q<sub>T</sub> is the discharge for a recurrence interval of T-years, in cubic feet per second;

C is the regression constant;

DA is the contributing drainage area, in square miles;

SL is the channel slope, minimum value set at 0.9, in feet per mile (for example, if SL is less than 0.9 foot per mile, then SL = 0.9 foot per mile);

LK is lake area plus constant of 3, in percent, (for example, LK+3.0, in percent);

B<sub>1</sub>, B<sub>2</sub>, B<sub>3</sub> are exponents of the regression.

#### Flood Frequency for Larger Streams

The Apalachicola River in Region C is the only basin larger than 10,000-square miles and therefore is treated separately in this section. The Apalachicola River is formed by the confluence of the Chattahoochee River, the Flint River, and Spring Creek, at Jim Woodruff Dam. There is some regulation of peak discharges by Lake Seminole (Jim Woodruff Dam) and upstream reservoirs. The Apalachicola River flows 107 miles to Apalachee Bay and to the Gulf of Mexico.

Table 1.--Regression model for Region A

Recurrence interval T, in years	Exceedance probability	Regression constant C	Regression exponents			R <sup>2</sup>	Standard error, in percent
			DA B <sub>1</sub>	SL B <sub>2</sub>	(LK+3) B <sub>3</sub>		
2	0.5	93.4	0.756	0.268	-0.803	0.868	42.6
5	.2	192	.722	.255	- .759	.858	42.4
10	.1	274	.708	.248	- .738	.843	44.2
25	.04	395	.696	.240	- .717	.821	47.3
50	.02	496	.690	.234	- .705	.803	50.0
100	.01	609	.685	.227	- .695	.784	52.9
200	.005	779	.674	.205	- .694	.763	55.8
500	.002	985	.668	.196	- .687	.738	59.7

Table 2.--Regression model for Region B

Recurrence interval T, in years	Exceedance probability	Regression constant C	Regression exponents		R <sup>2</sup>	Standard error, in percent
			DA B <sub>1</sub>	(LK+0.6) B <sub>2</sub>		
2	0.5	44.2	0.658	-0.561	0.876	60.9
5	.2	113	.614	- .573	.869	59.7
10	.1	182	.592	- .580	.863	59.9
25	.04	298	.570	- .585	.853	60.9
50	.02	410	.556	- .589	.845	61.9
100	.01	584	.543	- .591	.836	63.1
200	.005	694	.533	- .593	.827	64.4
500	.002	936	.521	- .594	.815	66.3

Table 3.--Regression model for Region C

Recurrence interval T, in years	Exceedance probability	Regression constant C	Regression exponents			R <sup>2</sup>	Standard error, in percent
			DA B <sub>1</sub>	SL B <sub>2</sub>	(LK+3) B <sub>3</sub>		
2	0.5	58.9	0.824	0.387	-0.785	0.919	43.7
5	.2	117	.844	.482	-1.06	.905	45.9
10	.1	164	.860	.534	-1.21	.891	49.3
25	.04	234	.882	.586	-1.37	.870	54.8
50	.02	291	.900	.626	-1.48	.853	59.4
100	.01	351	.918	.658	-1.58	.835	64.6
200	.005	417	.936	.685	-1.67	.819	69.7
500	.002	507	.960	.725	-1.79	.797	76.5

The locations of the Apalachicola River sites are shown in figure 1. The relation between flood discharge and drainage area for selected frequencies along the Apalachicola River is shown in figure 2. It is based on a log-Pearson Type III distribution of annual peaks at Chattahoochee (site A) and near Blountstown (site B). Records were insufficient at Wewahitchka (site C) and near Sumatra (site D) to develop reliable frequency curves. Therefore, the flood discharges, shown in figure 2, for Wewahitchka are based on a relation between drainage area and flood discharge at Blountstown. Flood discharges for Sumatra are based on a relation between the combined flood discharges of Blountstown and the Chipola River (map No. 154) and drainage area. Figure 2 shows a decrease in discharge between Chattahoochee and the downstream stations at Blountstown and Wewahitchka with a slight increase in discharge at Sumatra. This is attributed to (1) the increasing width of the flood plain in the downstream direction allowing increased flood storage, and (2) no major tributaries entering the Apalachicola River below Chattahoochee except the Chipola River, whose confluence is about 8 miles above Sumatra.

#### ACCURACY OF THE REGRESSION MODELS

The reliability of the regression model can be expressed in two ways: (1) the standard error of estimate (in percent); and (2) equivalent years of record (in years).

The standard error of estimate is the standard deviation of the distribution of residuals about the regression line. This means that 68 percent of the values estimated are within one standard error and 95 percent are within two standard errors of the observed values. Tables 1 to 3 give the standard error by region for the selected recurrence intervals.

The second method used to indicate reliability is called equivalent years of record and is defined as an estimate of the number of years of actual streamflow record required at a site to obtain an accuracy equivalent to the standard error of estimate (Hardison, 1971). Table 4 gives the accuracy in equivalent years of record and, for example, in Region A, the 100-year flood, estimated from the regression equation, would have the equivalent accuracy obtained from 8 years of actual record.

#### RISK OF FLOOD OCCURRENCE

Although a structure such as a bridge or culvert is designed for a specified flood magnitude, it does not preclude a rare event occurring during the lifetime of the structure. Risk, as defined by the U.S. Water Resources Council (1977), is "the probability that one or more events will exceed a given flood magnitude within a specified period of years." An estimate of the risk of the probability of exceedance during time periods greater than 1 year is given in table 5 and is computed by the following equation:

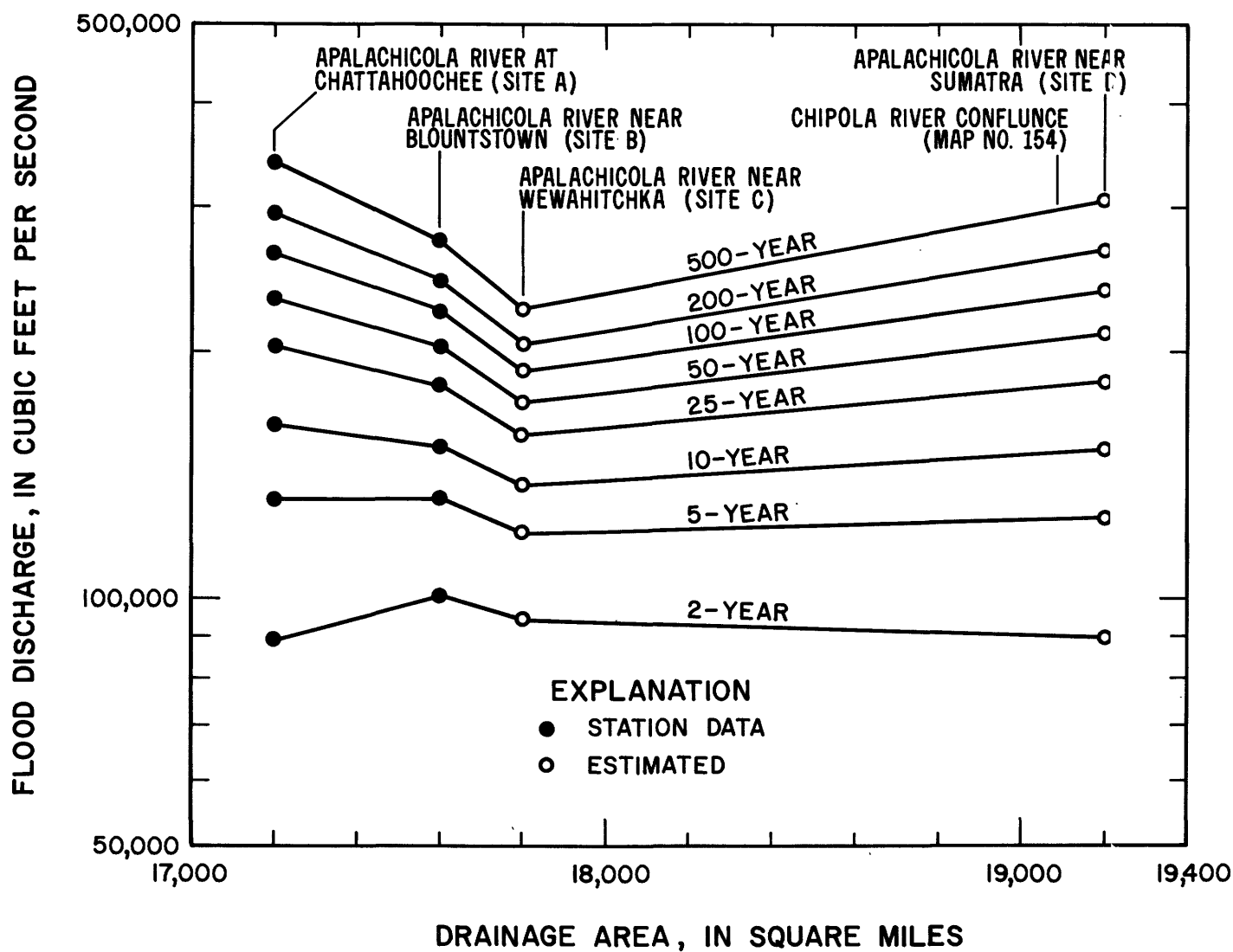


Figure 2.--Relation of flood discharge to drainage area for selected frequencies on the Apalachicola River.

Table 4.--Accuracy of regional flood relations in equivalent years of record

Recurrence interval T, in years	Exceedance probability	Accuracy in equivalent years		
		Region A	Region B	Region C
2	0.5	4	2	3
5	.2	5	3	4
10	.1	6	3	5
25	.04	7	5	6
50	.02	7	5	6
100	.01	8	6	6
200	.005	8	7	6
500	.002	9	8	6

Table 5.--Probability that a flood of given recurrence interval will be exceeded during indicated time period

Recurrence interval (years)	Period of time, in years					
	1	5	10	25	50	100
5	.20	<sup>1</sup> 0.67	0.89	( <sup>2</sup> )	( <sup>2</sup> )	( <sup>2</sup> )
10	.10	.41	.65	.93	( <sup>2</sup> )	( <sup>2</sup> )
25	.04	.18	.34	.64	.87	.98
50	.02	.10	.18	.40	.64	.87
100	.01	.05	.10	.22	.40	.63

<sup>1</sup>Multiply probability values by 100 to obtain percent chance of exceedance.

<sup>2</sup>Probability greater than 0.99, but less than 1.00.



$$P_n = 1 - (1 - 1/T)^n \quad (6)$$

where

P is the probability of at least one exceedance within the specified time interval;

n is the time period, in years;

T is the recurrence interval, in years.

An example would be: the 50-year flood has a 2 percent chance of exceedance in any 1-year period; an 18 percent chance of exceedance in any 10-year period; and a 64 percent chance of exceedance during any 50-year period.

## APPLICATIONS OF TECHNIQUE

### Improved Estimates at Gaged Sites

To compute flood estimates at gaged sites, the recommended procedure is to weight the station value with the regression value (U.S. Water Resources Council, 1977). Flood estimates from station frequency distributions tend to be independent of flood estimates from regional equations. Therefore, weighting the estimate is justified when the area of regionalization is large--radius of area more than 100 miles--(U.S. Water Resources Council, 1977) or the period of record is long when compared to the station record. To reduce the time sampling error, the gaged sites with short records need to reflect the long-term flood characteristics of hydrologically similar basins. Equation 7 can be used to compute the weighted average flood estimate.

$$\text{Log } Q_{wt} = \frac{N \log Q_g + EY \log Q_r}{N + EY} \quad (7)$$

where

$Q_{wt}$  = Weighted estimate of the T-year flood at gaged site, in cubic feet per second;

$Q_g$  = T-year flood estimate from log-Pearson Type III frequency distribution of annual peaks at gaged site, in cubic feet per second;

$Q_r$  = Regional flood estimate for the gaged site, computed from equation 3, 4, or 5, or from table 6, in cubic feet per second;

N = The number of annual peaks used to compute  $Q_g$ , in years;

EY = Accuracy of the regional flood estimate, in equivalent years from table 4.

For each of the 182 gaged sites used in the regression analysis, table 6 lists the T-year flood computed by the log-Pearson Type III distribution, the regional regression equations, and by the weighted station and regression values. At gaged sites, the weighted estimate is considered to be the best estimate for design purposes. Systematic records are annual peak flow records collected either by continuous recorder or periodic observations of a crest-stage gage for the number of years shown in table 6. The years of historic record shown in table 6 include the systematic record period as well as the intervening years to major flood events which have occurred either before or after the systematic record.

### Ungaged Sites

Flood estimates at ungaged sites are determined by direct application of the regression equations. The procedure is illustrated as follows:

1. For example--determine the 50-year flood for Hurricane Creek at the mouth at U.S. Highway 90 near Quincy. The drainage basin is in Region C (fig. 1).

2. The contributing drainage area, planimetered from U.S. Geological Survey quadrangle maps, is 12.8 square miles. The slope is 15.4 feet per mile. The lake area is 0.05 percent of the drainage area.

3. The equation for the 50-year flood in Region C (table 3) is

$$Q_{ru} = 291 \times DA^{0.900} \times SL^{0.626} \times (LK + 3.0)^{-1.48}$$

$$Q_{50} = 291 (12.8)^{0.900} (15.4)^{0.626} (0.05 + 3.0)^{-1.48}$$

$$Q_{50} = 3,070 \text{ cubic feet per second}$$

### Ungaged Site on Gaged Stream

If an ungaged site is near a gaged site on the same stream, the flood estimate can be improved by using a weighted value of the ratio of the weighted and regional estimate at the gaged site to adjust the regional estimate at the ungaged site. This estimate transfers the flood characteristics determined at the gaged site to the ungaged site on the same stream. The following procedure is suggested (Hannum, 1976) when the drainage area ratio at the ungaged site is more than half, but less than twice the drainage area of the gaged site.

$$\text{Ratio} = A_g/A_u = \text{Area gaged site} / \text{Area ungaged site} \quad (>0.5-<2.0).$$

Table 6.--A comparison of station, regional, and weighted T-year flood estimates

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years								
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500	
Region A														
1	2228500 North Prong St. Marys River at Moniac, Ga.	36	--	160	0.16	0.17	1,530	2,980	4,210	6,060	7,660	9,440	11,400	14,400
							1,670	3,040	4,140	5,760	7,120	8,630	10,500	13,000
							1,540	2,990	4,200	6,010	7,570	9,290	11,200	14,100
2	2229000 Middle Prong St. Marys River at Taylor	13	--	125	2.53	2.40	1,080	1,820	2,370	3,140	3,750	4,390	5,070	6,030
							1,190	2,210	3,030	4,240	5,250	6,360	7,570	9,330
							1,110	1,920	2,830	3,490	4,220	5,060	5,910	7,210
3	2230000 Turkey Creek at Macclenny	23	--	19.9	5.26	.10	790	1,260	1,610	2,070	2,430	2,810	3,200	3,740
							564	1,080	1,490	2,100	2,590	3,140	3,750	4,620
							752	1,230	1,580	2,080	2,470	2,890	3,330	3,970
4	2230500 South Prong St. Marys River at Glen St. Mary	22	25	156	2.69	.94	2,040	4,030	5,700	8,210	10,400	12,800	15,400	19,300
							1,840	3,340	4,550	6,300	7,750	9,350	11,100	13,600
							2,010	3,890	5,430	7,700	9,690	11,800	14,100	17,400
5	2231000 St. Marys River near Macclenny	52	--	700	2.56	.26	5,980	12,300	17,800	26,400	33,900	42,500	52,300	67,000
							6,590	11,300	14,900	20,300	24,700	29,500	34,400	41,800
							6,020	12,200	17,500	25,600	32,700	40,500	49,500	62,500
6	<sup>1</sup> 2231230 Pigeon Creek at Boulogne	10	--	9.36	13.4	0	478	882	1,170	1,510	1,750	1,960	2,140	2,390
							420	812	1,130	1,590	1,960	2,370	2,790	3,430
							461	858	1,150	1,540	1,830	2,130	2,410	2,840
7	<sup>2</sup> 2231250 Little St. Marys River near Hilliard	18	--	19.8	9.88	0	754	1,290	1,710	2,280	2,750	3,240	3,760	4,500
							682	1,290	1,780	2,490	3,070	3,690	4,350	5,330
							740	1,290	1,730	2,340	2,840	3,370	3,930	4,760
8	2231280 Thomas Creek near Crawford	13	--	29.9	7.54	0	868	1,800	2,600	3,850	4,930	6,150	7,520	9,570
							867	1,620	2,230	3,100	3,820	4,600	5,430	6,660
							868	1,750	2,480	3,570	4,510	5,510	6,640	8,250

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500				
Region A																	
9	2231600 Jane Green Creek near Deer Park	25	--	2.59	0.27	2,650 3,010 2,700	6,010 5,330 5,890	9,120 7,170 8,710	14,100 9,850 13,000	18,700 12,100 17,000	24,000 14,500 21,200	30,100 17,100 26,200	39,400 20,900 33,300				
10	2232000 St. Johns River near Melbourne	38	--	.15	3.90	3,210 3,480 3,230	6,710 6,180 6,650	9,790 8,340 9,580	14,500 11,500 14,000	18,700 14,200 17,900	23,400 17,200 22,200	28,600 20,500 27,000	36,500 25,300 34,100				
11	2232200 Wolf Creek near Dear Park	22	--	6.83	.23	995 710 945	2,220 1,340 2,020	3,350 1,850 2,950	5,160 2,590 4,370	6,800 3,200 5,670	8,690 3,850 6,990	10,800 4,570 8,590	14,200 5,610 10,800				
12	2232400 St. Johns River near Cocoa	25	--	.18	4.85	3,410 3,990 3,480	5,650 7,050 5,860	7,310 9,500 7,690	9,580 13,100 10,300	11,400 16,200 12,300	13,300 19,600 14,600	15,300 23,300 16,900	18,100 28,600 20,400				
13	2232450 Jim Creek near Christmas	19	--	6.14	.44	615 597 612	1,340 1,140 1,300	1,990 1,580 1,880	3,030 2,210 2,780	3,950 2,740 3,580	5,010 3,310 4,430	6,210 3,930 5,420	8,040 4,840 6,830				
14	2232500 St. Johns River near Christmas	44	--	.18	4.93	4,080 4,420 4,110	7,170 7,770 7,230	9,510 10,500 9,620	12,700 14,400 12,900	15,300 17,800 15,600	18,000 21,500 18,500	20,800 25,500 21,500	24,700 31,300 25,700				
15	2233102 Econlockatchee River tributary near Bithlo	10	--	3.90	.54	88 77 85	189 161 179	269 232 254	379 337 361	464 424 447	552 521 538	630 644 636	747 808 775				
16	2233200 Little Econlockatchee River near Union Park	19	--	3.73	3.84	385 344 378	837 676 801	1,240 950 1,160	1,890 1,360 1,730	2,460 1,700 2,230	3,120 2,070 2,760	3,870 2,480 3,390	5,010 3,080 4,280				

1 Rainfall-runoff gaging station.

2 Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years										
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500			
Region A																
17	2233500 Econlockhatchee River near Chuluota	43	--	2.00	1.46	2,490	4,600	6,330	8,890	11,100	13,500	16,100	20,000			
						2,140	3,860	5,240	7,260	8,950	10,800	12,800	15,800			
						2,460	4,520	6,190	8,640	10,800	13,000	15,500	19,200			
18	2236000 St. Johns River near DeLand	45	--	.18	6.07	7,200	10,600	12,900	15,900	18,200	20,500	22,800	25,900			
						6,690	11,600	15,400	21,200	26,000	31,400	36,900	45,300			
						7,160	10,700	13,200	16,500	19,100	21,900	24,500	28,400			
19	2236120 Deep Creek near Barberville	15	--	3.00	4.35	236	522	783	1,200	1,570	2,000	2,500	3,250			
						375	734	1,030	1,470	1,840	2,250	2,700	3,360			
						260	568	846	1,280	1,650	2,080	2,570	3,290			
20	2236500 Big Creek near Clermont	20	--	.75	4.64	91	208	318	498	664	857	1,080	1,430			
						431	840	1,180	1,690	2,120	2,600	3,190	4,000			
						118	275	430	684	897	1,180	1,470	1,970			
21	2239000 Oklawaha River near Ocala	38	--	.91	19.04	908	1,430	1,790	2,250	2,600	2,940	3,290	3,750			
						1,430	2,660	3,680	5,210	6,520	7,980	9,510	11,800			
						948	1,540	1,970	2,560	3,000	3,500	3,960	4,670			
22	2240000 Oklawaha River near Conner	15	--	.91	17.85	1,930	2,540	2,920	3,380	3,710	4,030	4,340	4,760			
						1,690	3,120	4,300	6,070	7,580	9,260	11,000	13,700			
						1,890	2,670	3,260	4,070	4,660	5,380	6,000	7,080			
23	2240500 Oklawaha River at Eureka	12	--	.87	14.49	3,020	4,320	5,190	6,290	7,110	7,940	8,760	9,870			
						2,140	3,910	5,360	7,530	9,380	11,400	13,600	16,800			
						2,770	4,200	5,250	6,720	7,870	9,180	10,400	12,400			
24	2240950 Hogtown Creek near Gainesville	20	--	23.53	.55	583	955	1,230	1,610	1,910	2,220	2,550	3,010			
						715	1,350	1,860	2,590	3,180	3,820	4,420	5,380			
						603	1,020	1,350	1,820	2,180	2,590	2,980	3,600			
25	12241800 Lochloosa Creek near Melrose	7	--	14.8	.36	253	502	671	880	1,040	1,200	1,330	1,510			
						158	319	452	646	805	977	1,170	1,440			
						213	416	559	754	915	1,080	1,240	1,470			

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.---A comparison of station, regional, and weighted T-year flood estimates---Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500				
Region A																	
26	22241900 Lochloosa Creek at Grove Park	21	--	37.4	6.33	6.57	416	846	1,220	1,790	2,280	2,830	3,450	4,370			
							386	756	1,060	1,510	1,890	2,300	2,720	3,370			
							411	828	1,180	1,720	2,180	2,670	3,230	4,040			
27	2243000 Orange Creek at Orange Springs	18	--	470	2.00	13.08	538	1,130	1,640	2,450	3,150	3,950	4,840	6,190			
							1,270	2,360	3,270	4,610	5,740	7,000	8,260	10,200			
							629	1,330	1,950	2,920	3,730	4,710	5,700	7,310			
28	2243500 Oklawaha River near Orange Springs	22	--	2,010	.85	14.24	3,790	5,530	6,710	8,220	9,360	10,500	11,700	13,200			
							2,900	5,220	7,120	9,960	12,400	15,000	17,800	22,000			
							3,640	5,470	6,800	8,610	10,000	11,600	13,100	15,300			
29	12243530 Bruntbridge Brook at Kenwood	7	--	4.63	11.60	2.80	166	367	526	738	889	1,040	1,170	1,360			
							140	286	407	586	734	894	1,070	1,320			
							156	331	467	658	808	959	1,120	1,340			
30	2244000 Oklawaha River at Riverside Landing near Orange Springs	25	--	2,100	.83	26.35	4,140	6,460	8,110	10,300	12,000	13,700	15,500	18,000			
							1,960	3,600	4,960	7,010	8,760	10,700	12,700	15,700			
							3,730	5,860	7,370	9,470	11,200	12,900	14,800	17,400			
31	2244420 Little Haw Creek near near Seville	27	--	93	1.55	5.04	504	918	1,250	1,720	2,110	2,530	2,980	3,630			
							606	1,160	1,620	2,310	2,880	3,520	4,260	5,290			
							516	952	1,310	1,830	2,250	2,730	3,230	3,990			
32	12245300 Clarks Creek near Green Cove Springs	11	--	8.81	23.30	0	400	800	1,090	1,440	1,680	1,930	2,130	2,400			
							466	895	1,240	1,740	2,140	2,570	3,000	3,670			
							417	829	1,140	1,550	1,850	2,180	2,460	2,910			
33	22245400 South Fork Black Creek near Camp Blanding	20	--	34.8	17.13	3.73	482	1,090	1,650	2,550	3,370	4,310	5,400	7,070			
							662	1,260	1,740	2,450	3,030	3,650	4,220	5,160			
							508	1,120	1,670	2,520	3,280	4,110	5,030	6,410			

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years									
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500		
Region A															
34	22245470 Greens Creek near Penney Farms	21	--	14.9	9.31	0.01	598	1,280	1,880	2,830	3,660	4,620	5,690	7,320	
							540	1,030	1,430	2,010	2,480	2,990	3,540	4,350	
							588	1,230	1,770	2,600	3,320	4,100	4,990	6,260	
35	2245500 South Fork Back Creek near Penney Farms	39	--	134	7.98	16.40	2,970	6,140	8,930	13,200	17,000	21,300	26,200	33,500	
							2,280	4,100	5,530	7,610	9,310	11,100	12,900	15,700	
							2,890	5,860	8,380	12,100	15,500	19,100	23,200	29,100	
36	22245900 Yellow Water Creek near Maxville	21	--	21.9	7.55	.04	796	1,390	1,860	2,510	3,030	3,600	4,200	5,060	
							678	1,280	1,770	2,480	3,060	3,690	4,360	5,360	
							776	1,370	1,840	2,500	3,040	3,620	4,240	5,150	
37	2246000 North Fork Black Creek near Middleburg	47	60	177	5.22	1.47	3,780	7,180	9,890	13,700	16,900	20,300	23,800	28,900	
							2,190	3,940	5,340	7,360	9,040	10,900	12,700	15,500	
							3,620	6,780	9,220	12,600	15,600	18,500	21,700	26,100	
38	12246150 Big Davis Creek at Bayard	15	--	13.6	8.70	.14	345	749	1,060	1,450	1,720	1,990	2,260	2,890	
							479	921	1,280	1,800	2,220	2,690	3,190	3,920	
							370	789	1,120	1,550	1,870	2,210	2,550	3,240	
39	22246200 Durbin Creek near Durbin	18	--	36.7	2.02	.31	617	1,500	2,370	3,830	5,190	6,810	8,710	11,700	
							657	1,250	1,730	2,430	3,020	3,670	4,450	5,510	
							624	1,440	2,190	3,370	4,460	5,630	7,080	9,100	
40	2246300 Ortega River near Jacksonville	13	--	30.9	2.41	.26	816	1,340	1,740	2,270	2,700	3,140	3,600	4,250	
							612	1,170	1,620	2,280	2,830	3,430	4,150	5,140	
							763	1,290	1,700	2,270	2,740	3,250	3,800	4,590	
41	22246600 Trout River at Dinsmore	18	--	20.9	10.11	.06	425	791	1,090	1,520	1,880	2,270	2,690	3,310	
							704	1,330	1,830	2,560	3,160	3,800	4,470	5,480	
							466	886	1,240	1,760	2,170	2,660	3,140	3,920	

1 Rainfall-runoff gaging station.

2 Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics				Discharge, in cubic feet per second, for recurrence interval, in years									
			System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500	
Region A																
42	2246900 Moultrie Creek at SR 207 near St. Augustine	17	--	--	19.8	2.18	0.70	343	768	1,160	1,790	2,350	3,010	3,760	4,910	
								385	749	1,050	1,490	1,860	2,260	2,760	3,430	
								351	764	1,130	1,700	2,200	2,750	3,410	4,340	
43	2247000 Moultrie Creek near St. Augustine	25	--	--	20.8	2.43	.60	504	1,010	1,450	2,110	2,690	3,330	4,040	5,090	
								420	815	1,140	1,610	2,010	2,450	2,970	3,690	
								491	975	1,380	1,990	2,520	3,090	3,750	4,670	
44	12247200 Fish Swamp Outlet near Summer Haven	17	--	--	4.62	1.80	.22	123	272	391	552	684	830	1,500	2,020	
								136	277	395	571	717	881	1,090	1,380	
								125	273	392	557	693	846	1,350	1,770	
45	2247510 Tomoka River near Holly Hill	14	--	--	76.8	2.20	.42	680	1,370	1,970	2,870	3,650	4,520	5,490	6,930	
								1,140	2,120	2,910	4,060	5,010	6,060	7,280	8,980	
								763	1,540	2,210	3,220	4,060	5,030	6,080	7,670	
46	2247600 Little Tomoka River near Ormond Beach	17	--	--	10.0	2.00	.11	145	263	356	491	602	722	852	1,040	
								258	511	719	1,030	1,280	1,570	1,930	2,410	
								162	306	428	609	750	926	1,110	1,390	
47	2248000 Spruce Creek near Samsula	27	--	--	33.4	.60	.82	506	732	884	1,080	1,220	1,370	1,520	1,710	
								439	851	1,190	1,690	2,120	2,590	3,200	4,000	
								497	749	933	1,180	1,370	1,580	1,800	2,110	
48	2249500 Crane Creek at Melbourne	17	--	--	12.6	.60	4.67	247	447	604	831	1,020	1,220	1,440	1,750	
								120	248	357	521	661	819	1,020	1,290	
								215	391	527	725	899	1,070	1,290	1,570	
49	2256000 Fisheating Creek near Venus	11	--	--	188	1.32	.11	2,060	3,570	4,730	6,350	7,680	9,090	10,600	12,800	
								2,120	3,820	5,180	7,160	8,820	10,600	12,800	15,800	
								2,080	3,650	4,880	6,650	8,100	9,700	11,500	14,100	

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.



Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis;  
Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	record		Drainage area in mi <sup>2</sup>	Slope ft/mi	Lake area in percent	Discharge, in cubic feet per second, for recurrence interval, in years							
		System-atic	His-toric				2	5	10	25	50	100	200	500
		Region A												
50	2256500 Fisheating Creek at Palmdale	47	--	311	1.33	0.15	3,290 3,080 3,270	6,740 5,450 6,600	9,730 7,340 9,420	14,300 10,100 13,700	18,300 12,400 17,400	22,800 14,900 21,400	27,800 17,800 26,100	35,400 21,900 32,800
51	2261500 Myrtle-Mary Jane Canal near Narcoossee	17	--	111	.29	28.16	267 202 253	534 412 503	760 592 712	1,100 868 1,030	1,400 1,100 1,300	1,730 1,370 1,600	2,090 1,680 1,950	2,640 2,110 2,440
52	2262900 Boggy Creek near Taft	19	--	83.6	2.04	8.79	453 443 451	969 865 946	1,430 1,220 1,380	2,150 1,740 2,030	2,800 2,180 2,620	3,530 2,670 3,250	4,360 3,210 3,980	5,630 4,000 5,040
53	2263500 St. Cloud Canal at S-59 near St. Cloud	18	--	308	.31	22.78	456 508 465	1,070 994 1,050	1,660 1,400 1,590	2,640 2,020 2,450	3,540 2,550 3,230	4,600 3,150 4,090	5,830 3,800 5,110	7,760 4,760 6,590
54	2263800 Shingle Creek at Airport, near Kissimmee	20	--	89.2	1.78	6.72	511 523 513	980 1,010 986	1,370 1,420 1,380	1,940 2,020 1,960	2,430 2,530 2,460	2,970 3,100 3,010	3,570 3,730 3,620	4,430 4,640 4,490
55	2264000 Cypress Creek at Vineland	33	--	30.3	.41	27.55	30 77 33	87 164 95	149 240 160	261 356 276	372 457 386	509 571 521	675 708 681	946 899 936
56	2265000 South Port Canal at S-61 near St. Cloud	16	--	620	.29	19.42	789 965 821	2,260 1,830 2,150	3,870 2,550 3,450	6,830 3,640 5,640	9,810 4,560 7,770	13,500 5,600 10,100	18,200 6,710 13,100	25,800 8,350 17,200
57	2266300 Reedy Creek near Vineland	17	19	75	3.60	9.92	355 441 370	662 862 703	913 1,210 983	1,280 1,730 1,400	1,590 2,170 1,740	1,920 2,650 2,130	2,290 3,150 2,540	2,830 3,900 3,160

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500				
Region A																	
58	2269000 Kissimmee River below Lake Kissimmee	36	--	1,607	0.21	17.18	2,310	4,660	6,640	9,620	12,200	15,000	18,100	22,600			
							2,160	3,940	5,410	7,610	9,480	11,600	13,700	17,000			
							2,290	4,570	6,450	9,260	11,700	14,300	17,200	21,300			
59	12269720 Morgan Hole Creek near Avon Park	8	--	13.9	6.40	1.07	872	1,590	2,090	2,740	3,240	3,790	4,240	4,930			
							364	710	993	1,410	1,750	2,120	2,540	3,130			
							652	1,170	1,520	2,010	2,430	2,830	3,280	3,880			
60	2270500 Arbuckle Creek near DeSoto City	39	--	379	1.40	8.99	1,750	3,430	4,850	6,970	8,780	10,800	13,000	16,300			
							1,240	2,310	3,190	4,500	5,600	6,830	8,140	10,100			
							1,690	3,280	4,590	6,520	8,200	9,990	12,000	14,900			
61	2271500 Josephine Creek near DeSoto City	29	--	109	3.81	19.32	379	734	1,030	1,470	1,840	2,250	2,710	3,370			
							383	756	1,070	1,540	1,930	2,370	2,800	3,480			
							379	737	1,040	1,480	1,860	2,280	2,730	3,400			
62	2273000 Kissimmee River at S65E near Okeechobee	34	--	2,899	.26	13.49	4,930	10,100	14,400	21,000	26,600	32,800	39,600	49,700			
							3,960	7,040	9,540	13,300	16,400	19,900	23,500	28,900			
							4,820	9,640	13,500	19,400	24,500	29,800	35,900	44,400			
63	2276984 Monreve Ranch Drainage Canal near Stuart	14	--	6.20	1.68	.01	199	377	524	739	920	1,120	1,340	1,650			
							176	355	503	723	907	1,110	1,380	1,730			
							194	371	518	734	916	1,120	1,350	1,680			
64	2293050 Orange River at Buckingham near Fort Myers	18	--	70	4.00	3.37	599	1,120	1,550	2,190	2,730	3,330	3,980	4,940			
							760	1,440	1,995	2,810	3,490	4,230	5,020	6,190			
							625	1,180	1,650	2,350	2,920	3,580	4,270	5,330			
65	12293390 North Prong Alligator Creek near Punta Gorda	8	--	8.46	3.55	9.69	220	422	602	875	1,100	1,340	1,590	2,000			
							86	180	261	383	486	600	730	918			
							161	304	421	595	751	897	1,080	1,320			

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years									
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent										
						2	5	10	25	50	100	200	500		
Region A															
66	2293400 Alligator Creek near Punta Gorda	13	--	31.1	2.46	5.31	645	1,290	1,850	2,710	3,460	4,300	5,250	6,680	
							292	579	818	1,180	1,470	1,810	2,200	2,730	
							535	1,030	1,430	2,030	2,560	3,090	3,770	4,630	
67	2293986 Peace Creek Drainage Canal near Alturus	24	44	160	1.26	12.79	549	989	1,350	1,880	2,340	2,850	3,410	4,240	
							503	979	1,380	1,970	2,480	3,050	3,680	4,590	
							542	987	1,360	1,900	2,370	2,900	3,480	4,330	
68	2294650 Peace River at Bartow	39	--	390	1.25	13.28	978	1,740	2,350	3,240	3,990	4,810	5,700	7,010	
							960	1,820	2,520	3,580	4,490	5,490	6,560	8,140	
							976	1,750	2,370	3,290	4,060	4,920	5,840	7,210	
69	12295435 Hog Branch near Wauchula	8	--	5.31	12.20	0	313	607	854	1,230	1,540	1,890	2,240	2,820	
							267	527	738	1,050	1,300	1,570	1,870	2,310	
							297	575	802	1,140	1,420	1,720	2,050	2,540	
70	2295637 Peace River at Zolfo Springs	46	--	826	1.38	7.15	4,830	8,370	11,300	15,600	19,400	23,600	28,400	35,600	
							2,540	4,580	6,240	8,690	10,800	13,000	15,400	19,000	
							4,590	7,890	10,600	14,400	18,000	21,600	25,900	32,100	
71	2296500 Charlie Creek near Gardner	28	--	330	1.68	.10	2,310	3,840	4,990	6,590	7,890	9,260	10,700	12,800	
							3,470	6,110	8,200	11,300	13,800	16,600	19,700	24,100	
							2,430	4,120	5,450	7,340	8,820	10,500	12,300	14,900	
72	2296750 Peace River at Arcadia	47	57	1,367	1.30	4.35	7,320	12,500	17,000	23,800	29,900	36,900	45,100	57,700	
							4,740	8,300	11,100	15,300	18,800	22,700	26,700	32,800	
							7,070	12,000	16,200	22,500	28,200	34,400	41,800	52,700	
73	2297100 Joshua Creek near Nocatee	28	--	132	4.06	.14	1,920	3,570	4,930	6,950	8,660	10,500	12,600	15,700	
							2,180	3,910	5,290	7,280	8,930	10,700	12,600	15,400	
							1,950	3,620	4,990	7,010	8,710	10,500	12,600	15,600	

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500		
Region A																	
74	2297310 Horse Creek near Arcadia	28	--		218	2.79	0.12	2,230	3,580	4,580	5,930	7,000	11,300	13,500	16,600		
								2,890	5,130	6,910	9,480	11,600	13,900	16,400	20,100		
								2,300	3,780	4,920	6,510	7,740	11,800	14,100	17,400		
75	2298202 Shell Creek near Punta Gorda	13	--		373	2.44	1.00	2,230	3,580	4,580	5,930	7,000	8,130	9,310	11,000		
								3,430	6,050	8,130	11,200	13,700	16,400	19,300	23,600		
								2,470	4,140	5,490	7,430	8,850	10,600	12,300	15,000		
76	<sup>1</sup> 2298482 Johnson Creek near Myakka Head	8	--		3.18	8.04	0	114	242	358	531	661	792	944	1,160		
								162	327	463	663	827	1,010	1,220	1,510		
								128	272	400	589	735	894	1,070	1,330		
77	2298830 Myakka River near Sarasota	42	--		229	2.14	1.81	2,080	3,490	4,590	6,160	7,470	8,890	10,400	12,700		
								1,970	3,580	4,860	6,750	8,320	10,000	11,900	14,700		
								2,070	3,500	4,620	6,240	7,590	9,060	10,600	13,000		
78	<sup>2</sup> 2299800 Phillippi Creek at Sarasota	19	--		45.1	3.24	5.79	849	2,080	3,310	5,420	7,440	9,900	12,800	17,600		
								398	779	1,090	1,560	1,950	2,390	2,860	3,550		
								744	1,700	2,540	3,880	5,190	6,500	8,210	10,500		
79	2299950 Manatee River near Mayakka Head	12	--		65.3	5.83	.17	1,860	2,310	2,580	2,900	3,130	3,350	3,560	3,830		
								1,400	2,560	3,490	4,830	5,940	7,140	8,390	10,300		
								1,730	2,380	2,850	3,500	3,960	4,530	5,020	5,850		
80	2300000 Manatee River near Bradenton	27	--		87.1	4.93	.22	2,410	4,520	6,260	8,840	11,000	13,400	16,100	20,100		
								1,640	2,990	4,060	5,610	6,890	8,280	9,740	11,900		
								2,290	4,240	5,790	8,050	9,990	12,000	14,400	17,600		
81	2300100 Little Manatee River near Fort Lonesome	15	--		32.9	5.77	.34	713	1,070	1,320	1,660	1,910	2,170	2,440	2,810		
								795	1,500	2,100	2,880	3,560	4,290	5,090	6,260		
								730	1,160	1,510	1,980	2,330	2,750	3,150	3,790		

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System-His- toric	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years									
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent										
						2	5	10	25	50	100	200	500		
Region A															
82	2300200 South Fork Little Manatee River near Duette	16	--	9.40	5.76	0.12	215	453	667	1,000	1,300	1,650	2,040	2,640	
							326	638	893	1,260	1,570	1,910	2,290	2,840	
							234	491	722	1,070	1,380	1,730	2,120	2,710	
83	2300500 Little Manatee River near Wimauma	39	--	150	5.03	.40	2,740	5,160	7,190	10,200	12,900	15,900	19,200	24,200	
							2,380	4,270	5,760	7,920	9,690	11,600	13,600	16,600	
							2,700	5,050	6,980	9,810	12,400	15,100	18,100	22,500	
84	2300700 Bullfrog Creek near Wimauma	18	--	29.1	7.01	.61	1,160	2,600	3,950	6,170	8,220	10,600	13,400	17,800	
							720	1,360	1,870	2,620	3,240	3,910	4,620	5,680	
							1,060	2,260	3,280	4,850	6,330	7,800	9,660	12,200	
85	2301000 North Prong Alafia River near Keyville	28	--	135	4.96	3.09	1,450	2,830	3,990	5,760	7,290	9,000	10,900	13,800	
							1,370	2,530	3,460	4,830	5,960	7,190	8,420	10,300	
							1,440	2,780	3,890	5,560	7,000	8,560	10,300	12,900	
86	2301300 South Prong Alafia River near Lithia	15	--	107	4.17	3.00	825	1,510	2,070	2,890	3,580	4,330	5,150	6,350	
							1,110	2,070	2,840	3,980	4,920	5,950	7,020	8,630	
							878	1,630	2,270	3,200	3,960	4,840	5,740	7,120	
87	12301314 Mizelle Creek near Keyville	9	--	3.69	24.20	0	163	245	320	440	526	604	707	869	
							244	482	676	958	1,190	1,430	1,680	2,070	
							185	312	432	618	752	906	1,060	1,340	
88	2301500 Alafia River at Lithia	46	--	335	3.45	1.16	3,060	6,580	10,000	15,900	21,700	28,800	37,500	52,000	
							3,360	5,940	7,980	10,900	13,400	16,100	18,800	22,900	
							3,080	6,510	9,740	15,100	20,400	26,400	33,900	45,500	
89	2301800 Sixmile Creek at Tampa	18	--	28.0	2.07	.99	567	932	1,210	1,580	1,890	2,210	2,550	3,040	
							464	897	1,250	1,770	2,210	2,690	3,270	4,070	
							547	924	1,220	1,630	1,970	2,350	2,750	3,350	

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis;  
Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent										
								2	5	10	25	50	100	200	500		
Region A																	
90	2301900 Fox Branch near Socrum	14	--		9.50	6.10	0.55	219	382	509	689	837	995	1,170	1,410		
								301	591	829	1,180	1,470	1,780	2,140	2,650		
								235	428	589	824	1,010	1,230	1,460	1,800		
91	2302500 Blackwater Creek near Knights	27	--		110	3.52	2.58	1,130	1,720	2,150	2,720	3,160	3,610	4,090	4,740		
								1,150	2,140	2,930	4,100	5,080	6,140	7,270	8,940		
								1,130	1,780	2,270	2,960	3,480	4,080	4,660	5,550		
92	2303000 Hillsborough River near Zephyrhills	39	--		220	3.87	1.81	2,150	3,750	5,020	6,880	8,430	10,100	12,000	14,700		
								2,240	4,040	5,480	7,570	9,300	11,200	13,100	16,000		
								2,160	3,780	5,080	6,980	8,560	10,300	12,200	14,900		
93	2303100 New River near Zephyrhills	11	--		15.0	9.80	4.42	156	232	284	351	403	456	510	584		
								267	530	748	1,070	1,330	1,620	1,920	2,370		
								180	300	400	541	641	778	891	1,100		
94	12303358 Cypress Creek near Darby	10	--		7.11	6.80	1.96	457	912	1,280	1,780	2,180	2,630	3,020	3,640		
								190	383	542	777	972	1,185	1,420	1,770		
								356	683	927	1,270	1,560	1,850	2,160	2,590		
95	2303400 Cypress Creek near San Antonio	15	--		56.0	4.60	6.00	146	307	450	676	877	1,110	1,370	1,770		
								505	978	1,370	1,940	2,420	2,950	3,490	4,320		
								190	410	619	945	1,210	1,560	1,900	2,470		
96	2303420 Cypress Creek at Worthington Gardens	13	--		117	2.65	6.00	482	829	1,100	1,480	1,790	2,120	2,480	2,990		
								760	1,450	2,010	2,840	3,540	4,310	5,130	6,340		
								537	968	1,330	1,860	2,270	2,780	3,270	4,070		
97	2303800 Cypress Creek near Sulphur Springs	14	19		160	2.10	7.00	588	1,100	1,510	2,130	2,660	3,240	3,870	4,810		
								832	1,580	2,190	3,100	3,860	4,710	5,610	6,950		
								635	1,210	1,690	2,410	3,010	3,710	4,430	5,560		

<sup>1</sup> Rainfall-runoff gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis;  
Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics				Discharge, in cubic feet per second, for recurrence interval, in years										
			System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent										
								2	5	10	25	50	100	200	500		
Region A																	
98	2307000 Rocky Creek near Sulphur Springs	25	--		35.0	4.12	3.74	423	893	1,320	1,990	2,600	3,290	4,090	5,330		
								434	843	1,180	1,680	2,090	2,550	3,040	3,770		
								425	884	1,290	1,920	2,480	3,090	3,810	4,860		
99	2307359 Brooker Creek near Tarpon Springs	28	--		30.0	2.81	6.02	219	483	729	1,130	1,500	1,930	2,440	3,230		
								276	549	776	1,120	1,400	1,720	2,070	2,580		
								225	492	737	1,130	1,480	1,880	2,350	3,060		
100	2307697 Alligator Creek at Safety Harbor	23	--		9.00	9.64	2.67	171	352	512	764	990	1,250	1,540	1,990		
								224	448	633	905	1,130	1,370	1,630	2,020		
								178	367	535	795	1,020	1,280	1,560	2,000		
101	2308889 Seminole Lake Outlet near Largo	22	--		14.0	1.71	4.33	191	328	434	585	710	844	989	1,200		
								160	329	466	676	853	1,050	1,290	1,620		
								186	328	441	606	742	895	1,060	1,310		
102	2310000 Anclote River near Elfers	34	--		72.5	3.54	3.20	908	1,810	2,600	3,810	4,880	6,090	7,460	9,520		
								772	1,460	2,020	2,850	3,540	4,290	5,110	6,300		
								893	1,760	2,500	3,630	4,620	5,700	6,940	8,730		
Region B																	
103	2310240 Jumping Gully at Loyce	15	--		43.0	3.60	10.20	66	172	282	478	670	907	1,190	1,670		
								138	291	424	632	817	1,100	1,260	1,620		
								72	188	302	513	783	958	1,210	1,650		
104	2310300 Pithlachascotee River near New Port Richey	15	--		182	2.70	3.54	319	635	908	1,330	1,690	2,110	2,570	3,280		
								612	1,220	1,740	2,520	3,210	4,260	4,790	6,060		
								344	708	1,010	1,560	1,980	2,580	3,130	4,060		

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record		Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years									
		System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500		
Region B																
105	2310800 Withlacoochee River near Eva	20	--	130	1.09	4.36	315	730	1,120	1,770	2,370	3,070	3,890	5,170		
							443	896	1,280	1,870	2,390	3,190	3,590	4,570		
							325	750	1,140	1,790	2,370	3,100	3,810	4,990		
106	2312000 Withlacoochee River at Trilby	48	--	570	1.35	1.71	1,380	2,710	3,850	5,570	7,060	8,720	10,600	13,400		
							1,800	3,440	4,790	6,800	8,530	11,200	12,400	15,500		
							1,390	2,750	3,900	5,680	7,190	8,970	10,800	13,700		
107	2312200 Little Withlacoochee River near Rerdell	20	--	145	1.75	4.40	381	841	1,260	1,940	2,550	3,260	4,080	5,330		
							474	954	1,360	1,980	2,530	3,360	3,790	4,810		
							389	855	1,270	1,950	2,550	3,280	4,000	5,180		
108	2312500 Withlacoochee River at Groom	39	--	810	1.24	2.40	1,590	3,050	4,250	6,050	7,570	9,250	11,100	13,800		
							1,960	3,680	5,070	7,130	8,890	11,600	12,400	16,000		
							1,610	3,090	4,300	6,160	7,710	9,530	11,300	14,200		
109	2312640 Jumper Creek Canal near Bushnell	15	--	40	2.10	6.27	94	148	187	239	280	323	367	428		
							170	361	528	790	1,020	1,390	1,580	2,040		
							101	172	222	322	387	490	584	737		
110	2312720 Withlacoochee River at Wysong Dam at Carlson	13	--	1,520	1.80	3.31	1,480	2,110	2,540	3,080	3,490	3,900	4,310	4,860		
							2,550	4,650	6,310	8,740	10,800	13,900	15,400	18,900		
							1,590	2,450	3,010	4,120	4,780	5,830	6,730	8,150		
111	2313000 Withlacoochee River near Holder	47	--	1,825	.86	4.95	2,340	3,920	5,100	6,740	8,060	9,450	10,900	13,000		
							2,360	4,260	5,740	7,900	9,720	12,500	13,700	16,900		
							2,340	3,940	5,140	6,840	8,210	9,750	11,200	13,500		
112	22313400 Waccasassa River near Bronson	14	--	220	1.30	3.50	221	472	700	1,060	1,380	1,750	2,170	2,810		
							697	1,380	1,960	2,820	3,580	4,740	5,330	6,725		
							255	570	839	1,370	1,770	2,360	2,930	3,860		

2 Crest-stage partial record gaging station.



Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics				Discharge, in cubic feet per second, for recurrence interval, in years								
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500		
Region B															
113	2314200 Tennile Creek at Lebanon Station	15	--	26.0	6.00	1.00	755	1,490	2,120	3,060	3,880	4,800	5,820	7,340	
							290	640	954	1,450	1,900	2,590	2,980	3,870	
							675	1,290	1,860	2,540	3,250	4,020	4,700	5,870	
114	2315500 Suwannee River at White Springs	51	--	2,430	.57	.31	7,670	14,100	19,000	25,600	30,900	36,200	41,700	49,300	
							7,870	14,300	19,400	26,800	33,100	42,600	46,800	57,500	
							7,680	14,100	19,000	25,700	31,100	36,800	42,300	50,300	
115	2315550 Suwannee River at Suwannee Springs	18	--	2,630	.60	.37	8,110	13,800	18,200	24,300	29,300	34,500	40,100	48,000	
							8,000	14,500	19,600	27,000	33,300	42,800	47,000	57,700	
							8,100	13,900	18,400	24,900	30,100	36,400	41,900	50,800	
116	22317630 Alapaha River near Jasper	13	31	1,720	1.80	0	6,360	11,000	14,600	19,600	23,700	28,100	32,800	39,400	
							7,920	14,700	20,100	28,000	34,800	45,100	49,800	61,400	
							6,550	11,600	15,500	21,600	26,400	32,600	38,000	46,700	
117	2319000 Withlacoochee River near Pinetta	47	51	2,120	1.51	.23	9,510	19,000	27,4300	40,100	51,400	64,200	78,700	101,000	
							7,580	13,900	18,900	26,200	32,400	41,700	45,900	56,500	
							9,420	18,600	26,700	38,500	49,200	61,100	73,400	92,800	
118	2319500 Suwannee River at Ellaville	51	--	6,970	.66	.27	18,500	32,800	44,000	60,000	73,100	87,200	102,000	124,000	
							16,200	28,000	37,200	50,100	61,000	77,500	84,300	102,000	
							18,400	32,500	43,600	59,000	71,900	86,100	99,700	121,000	
119	22320000 Suwannee River at Luraville	10	--	7,330	.61	.27	19,900	34,900	46,500	63,100	76,700	90,300	107,000	130,000	
							16,700	28,900	38,300	51,600	62,700	79,600	86,600	105,000	
							19,300	33,400	44,500	59,000	71,700	86,700	98,100	118,000	
120	2320500 Suwannee River at Branford	47	51	7,880	.57	.30	16,400	27,400	35,700	47,200	56,600	66,500	77,000	92,000	
							17,200	29,600	39,200	52,700	64,000	80,100	88,200	107,000	
							16,400	27,500	35,900	47,700	57,300	68,000	78,400	94,000	

2 Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record		Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years									
		System- atic	His- toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500		
Region B																
121	2320700 Santa Fe River near Graham	21	--	94.9	1.54	13.26	511 202 471	1,070 410 949	1,560 587 1,380	2,320 858 1,920	2,990 1,100 2,470	3,750 1,460 3,040	4,600 1,650 3,560	5,880 2,100 4,430		
122	2321000 New River near Lake Butler	22	--	191	2.95	.03	2,380 1,820 2,330	5,670 3,700 5,390	8,850 5,330 8,330	14,100 7,800 12,600	19,100 9,980 19,900	24,900 13,300 21,800	31,700 15,000 26,500	42,300 19,000 34,200		
123	2321500 Santa Fe River at Worthington Springs	46	--	575	3.12	2.64	4,700 1,500 4,480	9,640 2,900 8,960	13,900 3,960 12,900	20,200 5,600 17,800	25,600 7,020 22,600	31,700 9,190 27,400	38,300 10,200 32,200	48,000 12,800 39,500		
124	2321600 Olustee Creek near Lulu	15	--	49.1	3.50	.04	857 736 842	1,780 1,590 1,750	2,600 2,360 2,560	3,860 3,560 3,780	4,960 4,650 4,880	6,220 6,300 6,240	7,630 7,210 7,490	9,750 9,280 9,580		
125	2321700 Swift Creek near Lake Butler	21	--	46.0	1.85	8.67	497 157 450	857 331 761	1,130 482 1,020	1,520 718 1,320	1,830 928 1,610	2,170 1,250 1,920	2,520 1,430 2,190	3,030 1,830 2,640		
126	2321800 Olustee Creek near Providence	11	--	163	5.00	.88	2,620 1,010 2,260	4,530 2,060 3,830	6,000 2,960 5,160	8,080 4,320 6,640	9,760 5,530 8,170	11,600 7,360 9,880	13,500 8,310 11,200	16,200 10,500 13,500		
127	2322000 Santa Fee River near High Springs	41	--	868	2.33	1.90	3,460 2,270 3,390	7,260 4,260 7,000	10,500 5,870 10,100	15,500 8,250 14,500	19,800 10,300 18,400	24,600 13,400 22,800	29,900 14,800 27,000	37,800 18,400 33,600		
128	2322500 Santa Fe River near Fort White	48	--	1,017	1.48	1.73	4,120 2,620 4,050	6,870 4,890 6,730	8,940 6,720 8,790	11,800 9,410 11,600	14,100 11,700 13,900	16,500 15,200 16,400	19,100 16,800 18,800	22,800 20,900 22,500		

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis;  
Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years										
			System- atic	His- toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent									
								2	5	10	25	50	100	200	500	
Region B																
129	2323000 Suwannee River near Bell	25	29		9,390	0.55	0.49	17,100	28,000	36,100	47,300	56,300	65,800	76,000	90,300	
								17,300	29,600	38,900	52,100	63,000	79,700	86,400	104,000	
								17,100	28,200	36,400	48,100	57,400	68,300	78,200	93,400	
130	2323500 Suwannee River near Wilcox	35	48		9,640	.51	.54	17,300	27,700	35,500	46,400	55,200	64,500	74,500	88,700	
								17,200	29,300	38,500	51,500	62,300	78,700	85,300	103,000	
								17,300	27,800	35,700	47,000	56,000	66,400	76,200	91,200	
131	2324000 Steinhatchee River near Cross City	28	--		350	2.42	.53	2,000	3,970	5,650	8,230	10,500	13,000	15,900	20,200	
								1,950	3,840	5,440	7,820	9,910	13,100	14,700	18,400	
								2,000	3,960	5,630	8,170	10,400	13,000	15,700	19,800	
132	2324400 Fenholloway River near Foley	23	--		60.0	2.39	.04	422	922	1,380	2,120	2,800	3,580	4,490	5,890	
								840	1,800	2,660	3,990	5,200	7,020	8,020	10,300	
								446	996	1,490	2,370	3,130	4,120	5,140	6,800	
133	2324500 Fenholloway River at Foley	32	--		120	3.10	.37	637	1,390	2,080	3,220	4,260	5,490	6,920	9,160	
								1,050	2,170	3,150	4,650	5,980	8,000	9,070	11,500	
								656	1,440	2,160	3,380	4,460	5,830	7,260	9,590	
134	2326000 Econfina River near Perry	28	--		198	2.33	.85	571	1,180	1,720	2,550	3,300	4,150	5,110	6,570	
								1,160	2,350	3,360	4,890	6,230	8,280	9,330	11,800	
								599	1,260	1,840	2,810	3,630	4,690	5,840	7,480	
135	12326261 Little Aucilla River near Cherry Lake	8	--		13.9	8.70	1.07	248	529	751	1,060	1,310	1,560	1,790	2,130	
								187	424	642	990	1,310	1,800	2,080	2,720	
								234	498	720	1,030	1,310	1,660	1,920	2,410	
136	22326300 Little Aucilla River near Greenville	16	--		90.7	3.20	3.12	286	667	1,030	1,640	2,220	2,890	3,690	4,950	
								411	847	1,220	1,800	2,320	3,100	3,520	4,490	
								298	693	1,060	1,680	2,240	2,950	3,640	4,790	

1 Rainfall-runoff gaging station.

2 Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years								
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent									
						2	5	10	25	50	100	200	500	
Region B														
137	2326500 Aucilla River at Lamont	28	--	2.31	3.00	1,890	4,190	6,310	9,730	12,800	16,400	20,600	27,000	
						1,670	3,150	4,350	6,120	7,630	9,950	11,000	13,700	
						1,870	4,080	6,090	8,190	11,800	15,000	18,200	23,200	
Region C														
138	12326598 Caney Creek near Monticello	9	--	2.54	42.60	0.80	319	652	910	1,250	1,520	1,790	2,025	2,380
							190	381	539	771	978	1,180	1,400	1,730
							280	553	755	1,030	1,270	1,520	1,750	2,090
139	2326900 St. Marks River near Newport	21	--	535	2.04	2.20	1,810	3,040	4,000	5,360	6,470	7,670	8,970	10,800
							3,770	5,770	7,250	9,460	11,300	13,000	15,500	18,500
							1,980	3,370	4,480	6,080	7,320	8,620	10,100	20,300
140	2327050 Sopchoppy River near Arran	14	--	51.1	5.20	.37	1,190	2,480	3,650	5,530	7,260	9,280	11,600	15,300
							1,100	1,980	2,680	3,740	4,660	5,640	6,740	8,310
							1,170	2,360	3,360	4,920	6,360	7,990	9,860	12,700
141	2327100 Sopchoppy River near Sopchoppy	18	--	102	4.88	.18	2,030	3,680	5,030	7,060	8,800	10,700	12,900	16,100
							1,980	3,650	5,030	7,180	9,100	11,200	13,600	17,100
							2,020	3,670	5,030	7,090	8,870	10,800	13,100	16,300
142	2329000 Ochlocknee River near Havana	53	--	1,140	2.41	.98	6,860	13,100	18,400	26,400	33,200	40,800	49,300	61,900
							9,250	16,700	21,000	29,300	36,800	45,200	55,100	69,600
							6,970	13,300	18,600	26,700	33,500	41,200	49,900	66,600
143	2329500 Little River near Quincy	28	--	237	6.20	.21	4,260	10,100	15,800	25,800	35,400	47,100	61,300	84,400
							4,320	8,270	11,700	17,100	22,300	28,000	34,700	44,900
							4,270	9,850	15,100	24,000	32,600	43,000	55,400	75,500
144	2329600 Little River near Midway	14	--	305	5.90	.36	5,470	14,600	24,400	42,600	61,100	84,700	114,000	165,000
							5,040	9,520	13,400	19,500	25,300	31,700	39,300	50,900
							5,390	13,300	20,800	33,700	46,900	63,100	82,800	116,000

1 Rainfall-runoff gaging station.

2 Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis;  
Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record System- atic	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500				
Region C																	
145	12329700 Rocky Comfort Creek near Quincy	13	--	9.46	26.80	0.20	826	1,530	2,130	2,950	3,630	4,400	5,120	6,270			
							538	1,110	1,610	2,370	3,080	3,830	4,660	5,930			
							762	1,420	1,970	2,750	3,450	4,210	4,970	6,160			
146	2330000 Ochlockonee River near Bloxham	50	--	1,700	1.95	1.85	9,230 10,100 9,280	18,100 16,100 17,900	26,200 20,800 25,700	39,200 28,100 37,800	51,300 34,500 49,200	65,500 41,500 62,400	82,300 49,800 78,000	109,000 61,500 103,000			
147	22330050 Telogia Creek near Greensboro	14	--	28.1	11.90	1.17	1,240 782 1,140	3,210 1,420 2,680	5,310 1,930 4,070	9,140 2,680 6,330	13,000 3,340 8,650	17,900 4,010 11,400	24,100 4,760 14,800	34,500 5,830 20,200			
148	2330100 Telogia Creek near Bristol	25	--	126	5.07	.21	2,930 2,380 2,870	5,530 4,400 5,360	7,770 6,090 7,460	11,200 8,730 10,700	14,300 11,100 13,600	17,700 13,700 16,800	21,700 16,700 20,600	27,700 21,200 26,300			
149	22330200 New River at Vilas	18	--	23.2	4.47	.01	443 591 462	871 1,060 903	1,250 1,440 1,290	1,850 1,990 1,880	2,380 2,460 2,400	3,010 2,960 3,000	3,730 3,500 3,670	4,840 4,270 4,690			
150	2330300 New River near Wilma	14	--	81.7	4.51	.04	1,700 1,660 1,690	3,100 3,060 3,090	4,280 4,210 4,260	6,070 5,990 6,050	7,630 7,580 7,610	9,390 9,300 9,360	11,400 11,300 11,400	14,400 14,100 14,300			
151	22330400 New River near Sumatra	14	--	157	3.90	.01	2,470 2,710 2,510	3,830 5,000 4,060	4,840 6,920 5,320	6,240 9,920 7,170	7,370 12,600 8,660	8,570 15,600 10,300	9,860 19,100 12,000	11,700 24,300 14,600			
152	22358600 Flat Creek near Chattahoochee	18	--	24.9	19.27	.29	975 1,030 983	2,320 2,080 2,270	3,670 2,990 3,510	6,040 4,420 5,590	8,340 5,750 7,600	11,200 7,170 10,000	14,700 8,780 12,900	20,400 11,200 17,600			

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record		Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years									
		System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500		
Region C																
153	12358998 Holliman Branch near Altha	9	--	2.04	48.90	0	312	638	859	1,200	1,470	1,770	2,040	2,470		
							202	434	639	951	1,240	1,540	1,860	2,360		
							280	567	773	1,090	1,370	1,670	1,970	2,430		
154	2359000 Chipola River near Altha	43	66	781	1.61	.60	4,490	7,200	9,430	12,800	15,800	19,100	23,000	28,900		
							6,270	10,500	13,800	19,000	23,600	28,700	34,700	43,300		
							4,590	7,430	9,810	13,400	16,600	20,100	24,200	30,400		
155	22359300 Sandy Creek near Panama City	18	--	25.0	11.82	.01	1,250	1,830	2,250	2,820	3,270	3,750	4,250	4,960		
							915	1,810	2,580	3,760	4,840	6,000	7,310	9,290		
							1,200	1,830	2,320	3,030	3,610	4,220	4,870	5,800		
156	22359350 Econfina Creek near Compass Lake	17	--	40.5	13.02	3.44	751	1,060	1,280	1,570	1,800	2,030	2,280	2,620		
							778	1,270	1,640	2,150	2,580	3,000	3,450	4,060		
							755	1,100	1,350	1,700	1,980	2,250	2,540	2,940		
157	2359450 Econfina Creek near Fountain	17	--	70.2	10.40	2.00	985	1,290	1,490	1,750	1,940	2,140	2,330	2,600		
							1,370	2,380	3,160	4,330	5,340	6,380	7,550	9,200		
							1,030	1,450	1,770	2,220	2,530	2,850	3,170	3,620		
158	2359500 Econfina Creek near Bennett	43	--	122	5.61	2.50	1,310	1,830	2,200	2,710	3,120	3,550	4,010	4,660		
							1,580	2,540	3,260	4,300	5,180	6,080	7,070	8,430		
							1,330	1,880	2,290	2,870	3,320	3,790	4,300	5,010		
159	22359550 Bear Creek near Youngtown	16	--	67.2	9.10	0	1,710	2,640	3,350	4,340	5,140	6,000	6,930	8,270		
							1,870	3,690	5,260	7,750	10,100	12,600	15,500	20,000		
							1,730	2,820	3,730	5,080	6,180	7,350	8,630	10,500		
160	12365237 Fowler Branch near Leonia	8	--	5.09	15.20	.40	396	689	921	1,220	1,430	1,630	1,820	2,090		
							247	469	647	906	1,130	1,360	1,600	1,940		
							348	606	804	1,070	1,290	1,510	1,720	2,020		

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis;  
Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics			Discharge, in cubic feet per second, for recurrence interval, in years											
			Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	System-atic	His-toric	2	5	10	25	50	100	200	500		
Region C																	
161	2365500 Choctawhatchee River at Caryville	51	--	3,499	2.00	0.50		31,500	50,600	66,200	89,700	110,000	133,000	160,000	200,000		
								24,000	42,400	58,200	84,300	109,000	137,000	171,000	225,000		
								31,000	50,000	65,400	89,100	110,000	133,000	161,000	202,000		
162	2365700 Sandy Creek at Ponce DeLeon	18	--	80.7	9.47	2.97		2,730	4,870	6,680	9,430	11,800	14,600	17,700	22,500		
								1,290	2,120	2,740	3,630	4,390	5,160	6,000	7,150		
								2,450	4,190	5,500	7,430	9,220	11,300	13,500	16,900		
163	2366000 Holmes Creek at Vernon	28	--	386	3.80	.80		3,480	5,850	7,750	10,500	12,900	15,500	18,400	22,700		
								4,680	8,240	11,200	15,700	19,800	24,300	29,500	37,200		
								3,580	6,110	8,190	11,300	13,900	16,800	20,000	24,800		
164	2366500 Choctawhatchee River near Bruce	48	50	4,384	1.72	1.00		31,900	50,800	65,900	88,200	107,000	129,000	153,000	189,000		
								24,500	41,400	55,500	78,400	99,500	124,000	153,000	197,000		
								31,400	50,000	64,800	87,100	106,000	128,000	153,000	190,000		
165	2366859 Pate Branch near Freeport	8	--	1.87	30.00	0		146	251	349	487	581	661	752	893		
								155	319	457	662	845	1,030	1,230	1,520		
								148	272	387	555	682	799	929	1,120		
166	2367000 Alaqua Creek near DeFuniak Springs	26	--	65.6	11.10	0		2,390	4,290	5,910	8,380	10,600	13,100	15,900	20,300		
								1,980	3,980	5,730	8,520	11,200	14,000	17,400	22,500		
								2,340	4,250	5,880	8,410	10,700	13,300	16,200	20,700		
167	2367310 Juniper Creek at SH85 near Niceville	12	--	27.6	15.22	.01		387	659	881	1,210	1,500	1,810	2,170	2,710		
								1,090	2,220	3,210	4,760	6,200	7,760	9,540	12,300		
								476	893	1,290	1,910	2,410	2,940	3,550	4,490		
168	2368000 Yellow River at Milligan	40	--	624	3.31	.03		8,340	14,900	20,500	29,100	36,700	45,400	55,300	70,600		
								7,880	14,700	20,600	30,200	39,100	49,300	61,400	80,100		
								8,310	14,900	20,500	29,200	37,000	45,900	56,100	71,800		

<sup>1</sup> Rainfall-runoff gaging station.

<sup>2</sup> Crest-stage partial record gaging station.

Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record	Basin characteristics				Discharge, in cubic feet per second, for recurrence interval, in years									
			System- atic	His- toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent	2	5	10	25	50	100	200	500	
Region C																
169	12368300 Baggett Creek near Milligan	13	--		7.77	48.30	0.50	307	528	752	1,100	1,360	1,590	1,880	2,350	
								535	1,130	1,670	2,490	3,270	4,080	5,000	6,410	
								341	632	939	1,420	1,790	2,140	2,560	3,230	
170	2368500 Shoal River near Mossy Head	27	--		123	8.55	.20	3,040	5,750	8,140	11,900	15,300	19,300	23,900	31,100	
								2,860	5,570	7,920	11,700	15,200	19,000	23,500	30,400	
								3,020	5,730	8,110	11,900	15,300	19,200	23,800	31,000	
171	2369000 Shoal River near Crestview	40	--		474	4.04	.20	7,560	12,500	16,500	22,300	27,200	32,700	38,700	47,600	
								6,500	12,100	16,900	24,700	31,900	40,000	49,700	64,400	
								7,480	12,500	16,500	22,600	27,800	33,600	40,000	49,500	
172	2370000 Blackwater River near Baker	28	--		205	3.59		4,310	8,820	13,000	20,000	26,600	34,500	44,000	59,200	
								3,280	6,040	8,360	12,000	15,300	19,000	23,300	29,700	
								4,200	8,410	12,200	18,300	24,100	31,100	39,300	52,400	
173	12370015 Muddy Branch near Beaver Creek	8	--		1.45	75.60	0	150	336	486	686	836	992	1,120	1,320	
								180	402	602	909	1,200	1,500	1,820	2,330	
								158	357	528	774	976	1,180	1,380	1,680	
174	2370500 Big Coldwater Creek near Milton	39	--		237	6.03	0	5,150	10,200	14,900	22,600	29,900	38,600	49,100	66,100	
								4,510	8,770	12,500	18,500	24,200	30,500	38,100	49,700	
								5,100	10,100	14,600	22,000	29,100	37,400	47,500	63,600	
175	2370700 Pond Creek near Milton	21	--		58.7	11.50	.20	625	1,510	2,450	4,170	5,920	8,160	11,000	15,900	
								1,740	3,440	4,910	9,220	9,380	11,700	14,400	18,500	
								710	1,720	2,800	4,970	6,560	8,840	11,700	16,400	
176	2370750 Hurricane Branch near Milton	18	--		2.95	50.20	0	100	365	741	1,610	2,690	4,310	6,680	11,500	
								276	601	891	1,340	1,760	2,200	2,680	3,430	
								116	400	771	1,540	2,420	3,640	5,320	8,500	

<sup>1</sup> Rainfall-runoff gaging station.<sup>2</sup> Crest-stage partial record gaging station.



Table 6.--A comparison of station, regional, and weighted T-year flood estimates--Continued

[Discharge-frequency relationships for each gaging station are presented as follows: Top line--log-Pearson Type III analysis; Middle line--regression equations; Bottom line--weighted or best estimate of T-year flood]

Map No.	Station number and name	Years of record		Basin characteristics				Discharge, in cubic feet per second, for recurrence interval, in years									
		System-atic	His-toric	Drainage area mi <sup>2</sup>	Slope ft/mi	Lake area in percent											
							2	5	10	25	50	100	200	500			
Region C																	
177	2375500 Escambia River near Century	44	50	3,817	2.17	0.20	39,000 28,500 38,200	64,700 52,200 63,600	86,100 73,000 84,700	118,000 108,000 117,000	147,000 141,000 146,000	179,000 181,000 179,000	216,000 229,000 218,000	272,000 304,000 276,000			
178	2376000 Pine Barren Creek near Barth	26	--	75.3	11.90	0	2,650 2,280 2,610	6,640 4,620 6,330	11,000 6,700 10,200	19,000 10,000 16,800	27,400 13,200 23,900	38,200 16,700 32,700	52,100 20,700 43,800	76,300 27,100 62,800			
179	<sup>1</sup> 2376079 Carpenter Creek at Pensacola	8	--	8.81	23.51	.22	967 480 799	2,240 974 1,700	3,390 1,400 2,410	5,090 2,040 3,440	6,460 2,640 4,400	7,890 3,260 5,400	9,250 3,940 6,420	11,400 4,980 7,990			
180	2376300 Brushy Creek near Walnut Hill	21	--	49.0	11.00	0	1,940 1,550 1,890	3,770 3,100 3,650	5,420 4,440 5,220	8,080 6,550 7,710	10,500 8,530 10,000	13,400 10,700 12,700	16,800 13,100 15,900	22,100 16,900 20,800			
181	2376500 Perdido River near Barrineau Park	37	--	394	5.51	0	6,880 6,620 6,860	11,700 12,900 11,800	15,700 18,400 16,000	21,600 27,500 22,300	26,800 36,100 27,900	32,600 45,900 34,200	39,100 57,600 41,300	49,000 75,900 52,100			
182	<sup>1</sup> 2376551 Churchhouse Branch near Barrineau Park	8	--	.92	78.30	0	125 125 125	259 278 264	358 415 379	492 621 544	615 814 694	719 1,010 832	818 1,220 971	971 1,550 1,190			

<sup>1</sup> Rainfall-runoff gaging station.

Equation 8 or 9 can be used to adjust the regional estimate at the ungaged site with the weighted estimate from the gaged site.

$$Q_u = Q_{ru} \left[ \left( \frac{Q_{wt}}{Q_r} - 1 \right) \cdot \left( \frac{2A_g - A_u}{A_g} \right) + 1 \right] \quad \text{For site downstream from gage.} \quad (8)$$

$$Q_u = Q_{ru} \left[ \left( \frac{Q_{wt}}{Q_r} - 1 \right) \cdot \left( \frac{2A_u - A_g}{A_g} \right) + 1 \right] \quad \text{For site upstream from gage.} \quad (9)$$

where

$Q_u$  = Adjusted estimate for ungaged site, in cubic feet per second;

$Q_{ru}$  = Regional estimate for ungaged site, in cubic feet per second;

$Q_{wt}$  = Weighted estimate of the T-year flood at the gaged site, in cubic feet per second;

$Q_r$  = Regional estimate at gaged site, in cubic feet per second;

$A_u$  = Drainage area for ungaged site, in square miles;

$A_g$  = Drainage area for gaged site, in square miles.

1. For example--determine the 50-year flood for Ortega River at I-295, 7 miles downstream from 02246300 Ortega River near Jacksonville (map No. 40). The contributing drainage is in Region A (fig. 1). At the gaged site, station map No. 40, the contributing drainage area is 30.90 square miles, the slope is 2.41 feet per mile, and the lake area is 0.26 percent of the drainage area.

2. The contributing drainage area at the ungaged site, planimetered from U.S. Geological Survey quadrangle maps, is 50.7-square miles. The slope is 4.3 feet per mile. The lake area is 0.20 percent of the drainage area.

3. The regional estimate of the 50-year flood in Region A is computed using the appropriate equation from table 1, as follows:

$$Q_{ru} = 496 DA^{0.690} SL^{0.234} (LK + 3.0)^{-0.705}$$

$$Q_{50} = 496 (50.7)^{0.690} (4.3)^{0.234} (0.20 + 3.0)^{-0.705}$$

$$Q_{50} = 4,610 \text{ ft}^3/\text{s}$$

4. Compute the drainage area ratio to determine if the ungaged site is more than half but less than twice the drainage area of the gaged site.

$$r = A_g/A_u$$

$$r = 30.9/50.7$$

$$r = 0.61$$

Ratio is within acceptability and can be used to adjust the estimate at the ungaged site to the gaged site.

5. Use equation 8 to adjust the regional estimate at the ungaged site. Values for  $Q_{wt}$  and  $Q_r$  are from table 6.

$$Q_u = Q_{ru} \left[ \left( \frac{Q_{wt}}{Q_r} - 1 \right) \cdot \left( \frac{2A_g - A_u}{A_g} \right) + 1 \right]$$

$$Q_{50} = 4,610 \left[ \left( \frac{2740}{2830} - 1 \right) \cdot \left( \frac{2(30.9) - 50.7}{30.9} \right) + 1 \right]$$

$$Q_{50} = 4,560 \text{ cubic feet per second}$$

#### LIMITATIONS OF TECHNIQUE

Consideration should be given to the following limitations when applying the regional regression equations:

1. Regression equations, shown in tables 1, 2, and 3, were developed using basin characteristics within the ranges shown below. The relationship of the regression equations outside these ranges is not known.

Basin characteristics	Range		
	Region A	Region B	Region C
Contributing drainage area	1.83 to 3,066 mi <sup>2</sup>	13.9 to 9,640 mi <sup>2</sup>	0.92 to 4,384 mi <sup>2</sup>
Slope	0.15 to 24.20 ft/mi	--	1.61 to 78.30 ft/mi
Lake area	0 to 28.16 percent	0 to 13.26 percent	0 to 3.44 percent

2. In areas of karst topography, some basins may contain closed depressions and sinkholes which do not contribute to direct surface runoff. Karst areas are more likely to be found in Region B. When the drainage area is determined from 7½ minute topographic maps, any area containing sinkholes or depressions (noncontributing area) should be subtracted from the total drainage area. All basins used in the regression analysis were adjusted, as necessary, to contributing drainage area.

3. Regional equations are not applicable where manmade changes have a significant effect on flood runoff. Flood runoff can be affected by regulation from dams and reservoirs, levees, diversion canals, strip mines, and basins that have significant urban development.

#### SUMMARY

Regional flood estimating equations were developed using flood-peak data and basin characteristics for 182 gaging stations in Florida in a multiple linear regression analysis. Floods can be estimated for recurrence intervals ranging from 2 to 500 years for natural-flow streams. The regional relationships can also be used to improve flood estimates at gaged sites by weighting the log-Pearson Type III estimate with the regression estimate.

The basin characteristics used in the regression equations are not the only factors that influence the magnitude of floods in Florida. However, they represent the best combination of parameters for explaining peak flows with the least number of variables and smallest standard error.

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