

A MODIFICATION OF THE FINITE-DIFFERENCE MODEL FOR SIMULATION  
OF TWO DIMENSIONAL GROUND-WATER FLOW TO INCLUDE SURFACE-GROUND  
WATER RELATIONSHIPS

By Melih M. Ozbilgin and David C. Dickerman

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## CONVERSION FACTORS

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For use of those readers who may prefer to use metric (SI) units rather than inch-pound units, the conversion factors for terms used in this report are listed below.

Multiply inch-pound unit -----	By --	To obtain metric (SI) unit -----
LENGTH		
foot (ft)	0.3048	meter (m)
inch (in)	25.40	millimeter (mm)
FLOW		
cubic foot per second (ft <sup>3</sup> /s)	2.832x10 <sup>-2</sup>	cubic meter per second (m <sup>3</sup> /s)
TRANSMISSIVITY		
foot squared per day (ft <sup>2</sup> /d)	0.0929	meter squared per day (m <sup>2</sup> /d)
HYDRAULIC CONDUCTIVITY		
foot per day (ft/d)	0.3048	meter per day (m/d)

A MODIFICATION OF THE FINITE-DIFFERENCE MODEL FOR SIMULATION  
OF TWO-DIMENSIONAL GROUND-WATER FLOW TO INCLUDE  
SURFACE-GROUND WATER RELATIONSHIPS

By Melih M. Ozbilgin\* and David C. Dickerman\*\*

ABSTRACT

The two-dimensional finite-difference model for simulation of ground-water flow described by Trescott and others (1976) was modified to enable simulation of the interaction between surface water and ground water during periods of low streamflow. Modifications were designed to allow calculation of surface-water heads for, and flow either to or from, contiguous surface-water bodies in simulation of aquifer response to imposed stresses; and to allow more convenient data input.

The method of data input and output in the 1976 program was modified and two entries (RSORT and HRIVER) were added to the COEF and CHECKI subroutines to calculate surface-water heads. A new subroutine CALC was added to the program which initiates the modified program for surface water calculations. If CALC is not specified as a simulation option, the program runs the original version. The subroutines which solve the ground-water flow equations were not changed.

Arrays were added or moved around in the modified program so that recharge, evapotranspiration, inflow to surface-water bodies, number of wells, pumping rate, and duration of pumping could be varied for any time period. The Manning formula was used to relate stream depth and discharge in surface water streams. The interaction between surface water and ground water is represented through the leakage term which is included in both the ground-water flow and surface-water mass balance equations.

The documentation includes a flow chart, data deck instructions, input data, output summary, and a complete program listing. The modified program has been tested under a variety of conditions simulated for idealized aquifers. It has been used to develop a field model of a stream-pond-aquifer system in the Beaver-Pasquiset ground-water reservoir in southern Rhode Island. Numerical results from the modified program are in good agreement with published analytical results; however, users of the modified program should be aware that undiscovered errors in logic may exist.

This report is intended as a manual for use by the Rhode Island Water Resources Board, as well as other users.

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## INTRODUCTION

Digital models that simulate ground-water flow are widely used in the management of ground-water resources in order to assess the impact of withdrawals on streamflow and ground-water levels. In Rhode Island, the Water Resources Board is primarily responsible for the management of the State's water resources. In order for the Water Resources Board to manage the State's ground-water resources more effectively, a model was needed that could simulate the interaction between surface and ground water during periods of low streamflow. The purpose of this study was to modify the ground-water flow model of Trescott and others (1976) in order to meet the management needs of the Rhode Island Water Resources Board.

The two-dimensional finite-difference model described by Trescott and others (1976) was designed to simulate the response of an aquifer to imposed stresses. The aquifer may be artesian, water table, or a combination of artesian and water table. Also, it may be heterogeneous and anisotropic, and may have irregularly shaped boundaries. The model permits leakage from confining beds, constant recharge, well discharge, and evapotranspiration as a linear function of depth to water. The user may choose either the Alternating Direction Implicit (ADI), Line Successive Overrelaxation (LSOR), or Strongly Implicit Procedure (SIP) equation solving schemes.

The model of Trescott and others (1976) was modified to allow (1) calculation of surface-water heads for, and flow either to or from, contiguous surface-water bodies, and (2) recharge, evapotranspiration, inflow to surface-water bodies, number of wells, pumping rate, and duration of pumping to be input conveniently and varied for any time period.

## THEORETICAL DEVELOPMENT

The following four equations are necessary for the development of the mathematical model of flow in a surface-water/ground-water system. They are, (1) a ground-water flow equation, (2) an equation describing the relationship between stream depth and discharge, (3) a mass balance equation, and (4) an equation describing the interaction between surface water and ground water.

The ground-water flow equation used in the modified program is the same one developed and solved in the two-dimensional program by Trescott and others (1976). The reader is referred to Trescott and others (1976) for theoretical development of the ground-water flow equation and its finite-difference approximation.

Flow in natural streams is assumed to be gradually varied, which is a special class of steady nonuniform flow. The depth, area, roughness, bottom slope, and hydraulic radius are assumed to change very slowly, if at all, along the channel. It is also assumed that the rate of head loss, at a given section, is defined by the Manning formula for the same depth and discharge, regardless of trends in depth.

The Manning formula is widely used to relate stream depth and discharge in prismatic open channels. For incompressible, steady flow at constant depth, the Manning formula is written as:

$$Q = \frac{C}{n} \times A \times (R)^{2/3} \times (S)^{1/2}, \quad (1)$$

in which

$Q$  = discharge ( $L^3/T$ ),

$n$  = Manning's roughness coefficient,

$A$  = cross-sectional area ( $L^2$ ),

$R$  = hydraulic radius =  $A/P$  ( $L$ ),

$P$  = wetted perimeter ( $L$ ),

$S$  = losses per unit weight per unit length of channel, or  
slope of the bottom of the channel, and

$C$  = constant = 1.486 for inch-pound units or  
1.0 for metric units.

For a rectangular channel, the area and the hydraulic radius may be expressed as:

$$A = w \times d, \text{ and} \quad (2)$$

$$R = A/P = (w \times d)/[w + (2 \times d)], \quad (3)$$

in which

$d$  = depth of water in stream ( $L$ ), and

$w$  = width of the channel ( $L$ ).

By substituting equations 2 and 3 in equation 1, stream depth may be determined from a known discharge by numerical integration or by trial and error assuming a value for stream depth to satisfy the equation. To simplify equation 1, it was assumed that small, natural streams usually have depths much less than widths. Therefore, the term  $[w + (2 \times d)]$  in equation 3 may be approximated by the stream width (w). Using equation 3 this results in an approximation of the hydraulic radius (R) equal to stream depth (d). Equation 1 may now be rewritten as:

$$Q = \frac{C}{n} \times w \times (d)^{5/3} \times (S)^{1/2},$$

or

$$d = [(Q \times n) / (C \times w \times S^{1/2})]^{3/5}. \quad (4)$$

Equation 4 is used in the modified program to determine stage from a known discharge.

The Manning's roughness coefficient is dependent upon surface roughness and upon the size and shape of the channel cross section (Streeter, 1971). The roughness coefficient (n) varies from 0.01 for a smooth, glass channel to 0.15 for a tree-lined floodplain (White, 1979). Experimental values of Manning's roughness coefficient are given in table 1. White (1979) indicates that Manning's approximation is accurate in an intermediate range of roughness coefficient, but predicts unrealistically low friction and high discharge for deep, smooth channels and shallow, rough channels. The roughness coefficient can be determined from stream depth and discharge measurements. If field data are not available, values can be chosen from table 1 and varied within the indicated range.

Table 1. Experimental values of Manning's roughness coefficient (White, 1979, p. 605)

	<u>n</u>
Excavated earth channels:	
Clean	0.022 ± 0.004
Gravelly	0.025 ± 0.005
Weedy	0.030 ± 0.005
Stony, cobbles	0.035 ± 0.010
Natural channels:	
Clean and straight	0.030 ± 0.005
Sluggish, deep pools	0.040 ± 0.010
Major rivers	0.035 ± 0.010
Floodplains:	
Pasture, farmland	0.035 ± 0.010
Light brush	0.050 ± 0.020
Heavy brush	0.075 ± 0.025
Trees	0.150 ± 0.050



Discharge at a surface-water segment can be determined from the mass balance of that segment. The mass balance equation, in its simplest form, may be expressed as:

$$Q_{out} = Q_{in} \pm \frac{\Delta V}{\Delta t}, \quad (5)$$

in which

$Q_{in}$  = inflow to a segment ( $L^3/T$ ),

$Q_{out}$  = discharge from a segment ( $L^3/T$ ),

$\frac{\Delta V}{\Delta t}$  = change in storage =  $(\Delta d \times A_s) / \Delta t$  ( $L^3/T$ ),

$d$  = change in depth ( $L$ ),

$A_s$  = area of the segment ( $L^2$ ), and

$t$  = elapsed time ( $T$ ).

The inflow to a given stream segment may be written as:

$$Q_{in} = Q_p + Q_r - Q_e \pm Q_1,$$

in which

$Q_r$  = rainfall ( $L^3/T$ ),

$Q_e$  = evaporation from the stream surface ( $L^3/T$ ),

$Q_p$  = inflow from previous stream segment ( $L^3/T$ ), and

$Q_1$  = leakage from (-) or into (+) the aquifer ( $L^3/T$ ).

For streams where surface areas are small, changes in stream storage, rainfall to the stream, and evaporation from the stream surface may be neglected. The mass balance equation for a stream segment then becomes:

$$Q_{out} = Q_p \pm Q_1. \quad (6)$$

Inflow from a previous stream segment ( $Q_p$ ) is input to the first stream segment in the model or calculated by the computer program. Leakage either into or out of the aquifer ( $Q_1$ ) is calculated from equation 10. The stream depth can be determined by substituting  $Q_{out}$  from equation 6, into equation 4.

For ponds where surface areas are large, changes in pond storage, rainfall to the pond, and evaporation from the pond surface cannot be neglected. The sum of the mass balances for all pond segments is used in order to calculate a flat water surface for ponds. The total mass balance for the pond may be expressed as:

$$Q_d = Q_p + \left[ \sum_{i=1}^m (Q_r^i - Q_e^i \pm Q_l^i) \right] \pm \frac{\Delta d_p \times \sum_{i=1}^m A_s^i}{\Delta t}, \quad (7)$$

in which

$Q_d$  = discharge from the pond into a stream, if any ( $L^3/T$ ),

$Q_p$  = inflow to the pond from a stream, if any ( $L^3/T$ ),

$\Delta d_p$  = change in pond depth ( $L$ ), and

$m$  = number of segments in the pond.

When no discharge occurs from the pond segment to a stream segment ( $Q_d = 0$ ), changes in pond level are calculated from equation 7. However, when a stream segment discharges from the pond, pond levels depend upon the critical depth in the stream.

Assuming constant atmospheric pressure, the Bernoulli equation for steady, frictionless, incompressible flow along a streamline between points 1 and 2 (fig. 1) can be written as (Streeter and Wylie, 1979):

$$d_1 + \frac{V_1^2}{2g} = d_2 + \frac{V_2^2}{2g}, \quad (8-a)$$

in which

$g$  = acceleration of gravity ( $L/T^2$ ), and

$V$  = velocity ( $L/T$ ).

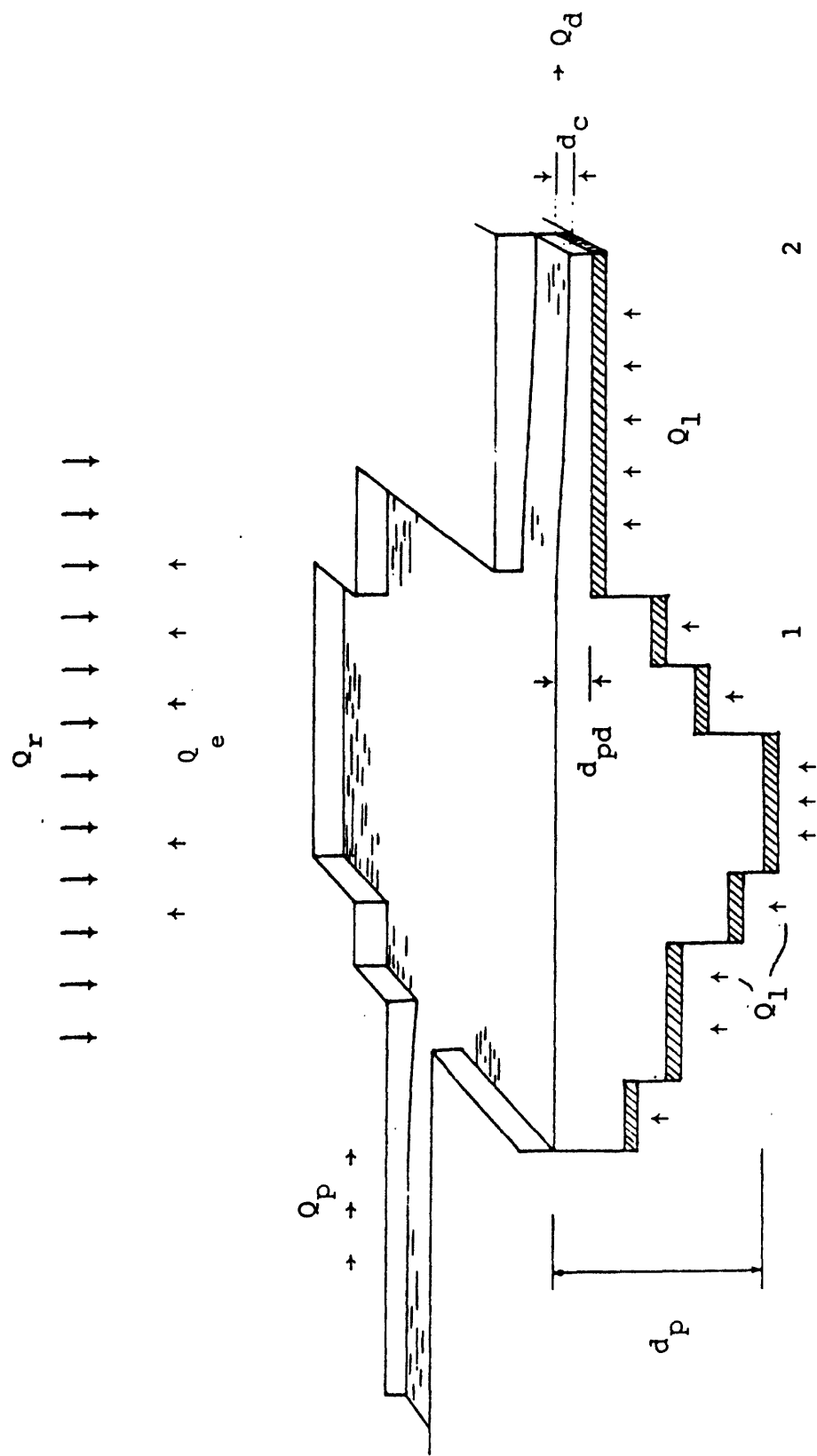


Figure 1.--Stream-pond-aquifer system representation.

For the pond,  $V_1 = 0.0$  and  $d_1 = d_{pd}$  (fig. 1); then

$$d_{pd} = d_2 + \frac{V_2^2}{2g}, \quad (8-b)$$

in which

$$d_{pd} = d_p \pm \Delta d_p (L), \text{ and}$$

$$d_p = \text{pond depth at the beginning of time step}(L).$$

The right side of equation 8-b is the specific energy (E) at point 2 in figure 1. It has a minimum at a certain value of  $d_2$  called the critical depth. The critical depth ( $d_c$ ) corresponds to a critical channel velocity ( $V_c$ ) equal to the shallow-water wave-propagation speed, which is given as (White, 1979):

$$V_c = (g \times d_c)^{1/2}. \quad (8-c)$$

Substituting equation 8-c into equation 8-b will give:

$$d_{pd} = d_c + \frac{g \times d_c}{2g} = \frac{3}{2} d_c,$$

or

$$d_c = \frac{2}{3} (d_p \pm \Delta d_p). \quad (8-d)$$

For derivation of equation 8-d, specific energy (E) at the mouth of the stream is assumed equal to minimum energy ( $E_{min}$ ). No flow occurs for  $E < E_{min}$ . For  $E > E_{min}$  two types of flow occur; (1) subcritical flow, for large depth with  $V < V_c$ , and (2) supercritical flow, for shallow depth with  $V > V_c$  (White, 1979). For small streams with shallow depths, subcritical flow does not occur. The major assumption is that channel velocity (V) will not exceed critical velocity ( $V_c$ ), and supercritical flow will not occur.

Uniform critical flow can occur if the bottom slope of the channel is the critical slope ( $S_c$ ) value for which the velocity is critical (White, 1979). For a wide rectangular channel where  $R = d_c$  in equation 1, the uniform critical-flow rate would be:

$$Q_d = \frac{C}{n} \times w \times \left[ \frac{2}{3} (d_p \pm \Delta d_p) \right]^{5/3} \times S_c^{1/2}. \quad (9)$$

Equation 9 can be substituted into equation 7 and solved for the change in pond level,  $\Delta d_p$ .

The interaction between a surface-water body and an aquifer is represented in the model by the leakage term in equations 6 and 7. Leakage from a surface-water body either into or out of an aquifer is assumed to occur through a confining bed. When storage in the confining bed is neglected, the leakage term is expressed as (Trescott and others, 1976):

$$Q_1 = \frac{K'}{m'} \times (H_s - H_a) \times A_a, \quad (10)$$

in which

$Q_1$  = leakage from (-) or into (+) the aquifer ( $L^3/T$ ),

$K'$  = hydraulic conductivity of the confining bed ( $L/T$ ),

$m'$  = thickness of the confining bed ( $L$ ),

$H_s$  = surface-water head ( $L$ ),

$H_a$  = aquifer head ( $L$ ), and

$A_a$  = area corresponding to aquifer node ( $L^2$ ).

The model is capable of calculating transient effects of the leakage (equation 9; Trescott and others, 1976). However, for natural situations considered in this study, storage in the confining bed and time steps are small, and transient effects are negligible.

#### MODEL DEVELOPMENT

Streams and ponds within the model are treated as areas of either known aquifer inflow or outflow. A grid is superimposed on the stream and pond areas and the length of each stream segment is set equal to the length of the corresponding grid block. The width of each stream segment is set equal to the actual channel width. Figure 2 shows a generalized stream-aquifer grid representation. The area term in equation 10, which describes the interaction between the stream and aquifer, is the area contributing to the aquifer node. Therefore, streambed hydraulic conductivity is adjusted so calculations will be done for leakage through the actual stream area. This is done by applying the following relationship:

$$K_{adj} = K' \frac{A_s}{A}, \quad (11)$$

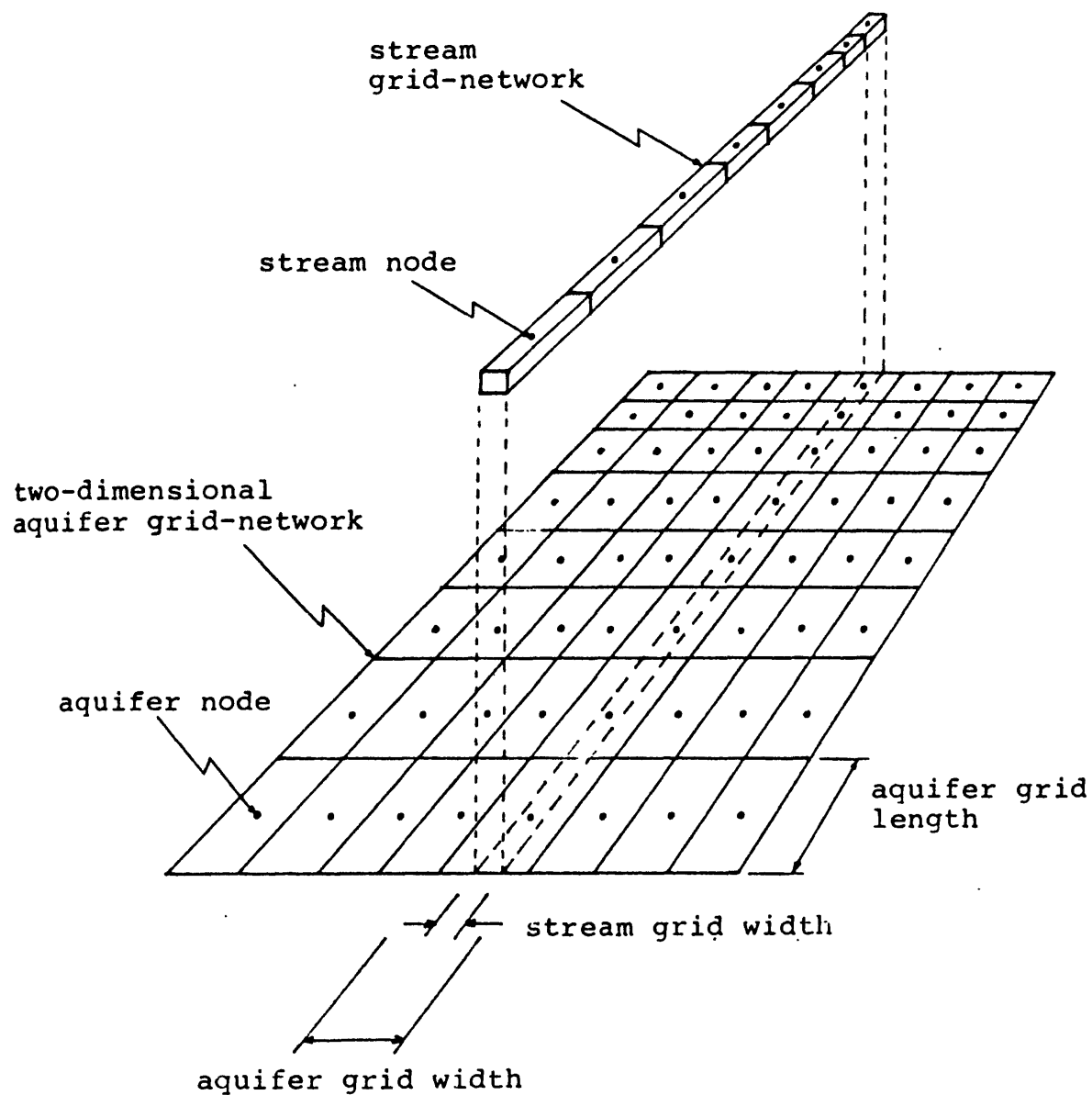


Figure 2.--Stream-aquifer grid representation.

in which

$K_{adj}$  = streambed hydraulic conductivity adjusted for area (L/T),

$K'$  = streambed hydraulic conductivity (L/T),

$A_s$  = area of the streambed in the grid block ( $L^2$ ), and

$A$  = area of the grid block ( $L^2$ ).

When the surface water area represents a pond, no adjustment is necessary as long as the pond and grid block areas are equal.

At the beginning of each time step, an initial surface-water head is determined at a node using known inflow and the leakage either to or from the aquifer that was computed in the previous time step. Net inflow or outflow to each aquifer node under the stream or pond is computed using the surface-water head, and input as a known recharge or discharge to the ground-water flow equation at that node. The finite-difference form of the ground-water flow equation is then solved for the entire aquifer. Next, new values for leakage at the surface-water nodes are calculated and these new values are then used to adjust surface-water heads. The ground-water flow equations are solved using the new surface-water heads. This procedure is continued until the largest difference in leakage between two successive trials is less than a given error. The procedure just described can be followed graphically on page 27 with the simplified flow chart for the modified program.

The error criterion needed to satisfy this difference in leakage may be set equal to any number by the user. However, this number should depend upon the expected leakage and the number of trials for each time period. The minimum value for the error criterion can be calculated from the following equation:

$$E_1 = 4 \times E_h \times \frac{K'_{max}}{m'_{min}} \times A_{max}, \quad (12)$$

in which

$E_1$  = error criterion satisfying the interaction between surface water and ground water ( $L^3/T$ ),

$E_h$  = error criterion satisfying the change in aquifer head between two successive iterations (L),

$K'_{max}$  = maximum confining bed hydraulic conductivity in the model (L/T),

$m'_{min}$  = minimum confining bed thickness (L), and

$A_{max}$  = maximum area contributing to an aquifer node ( $L^2$ ).

It should be noted that the calculation of net leakage to surface-water bodies is determined in the model to four significant digits. Therefore, an E value less than 0.001 should not be used unless modifications to the model are made.

For treatment of pond areas, first the depth at the deepest point in the pond is determined by solving equation 7. Second, the altitude at remaining pond nodes is set equal to the altitude at the deepest pond node. This gives the pond a flat water surface. Third, if the water-surface altitude of the pond becomes less than the altitude of the pond bottom, the pond node is assumed to be dry. The pond altitude is then set equal to the altitude of the pond bottom at that node, and leakage from that node is set equal to zero.

For treatment of stream nodes, calculations are performed at each stream node and at appropriate stream reaches. At stream nodes one of the following three conditions will apply:

1. Flow occurs in the stream from the upstream node ( $Q_{in}$ ), with leakage from the aquifer ( $Q_1$ ) (fig. 3-a). In this case, outflow from the stream node ( $Q_{out}$ ) is equal to the sum of the inflows ( $Q_{in} + Q_1$ ), and stream depth is determined from the Manning formula.
2. Flow occurs in the stream from the upstream node ( $Q_{in}$ ) with leakage to the aquifer ( $Q_1$ ); for example, during ground-water pumpage near the stream. In this case, if the inflow rate ( $Q_{in}$ ) is larger than leakage to the aquifer ( $Q_1$ ), then outflow from the stream node ( $Q_{out}$ ) is equal to inflow ( $Q_{in}$ ) minus leakage ( $Q_1$ ), and stream depth is determined from the Manning formula (fig. 3-b and 3-c). Figure 3-c shows a threshold condition that exists when the water table becomes detached from a flowing stream. Maximum leakage to the aquifer ( $Q_1$ ) occurs when the aquifer head is equal to the altitude of the stream bottom. If, on the other hand, leakage from the stream node to the aquifer ( $Q_1$ ) is larger than inflow ( $Q_{in}$ ), then there will be no outflow ( $Q_{out}$ ) from the stream node. The stream head, in this case, is equal to the altitude of the ground surface at the node, and leakage ( $Q_1$ ) from the node is set equal to the inflow rate ( $Q_{in}$ ) (fig. 3-d).



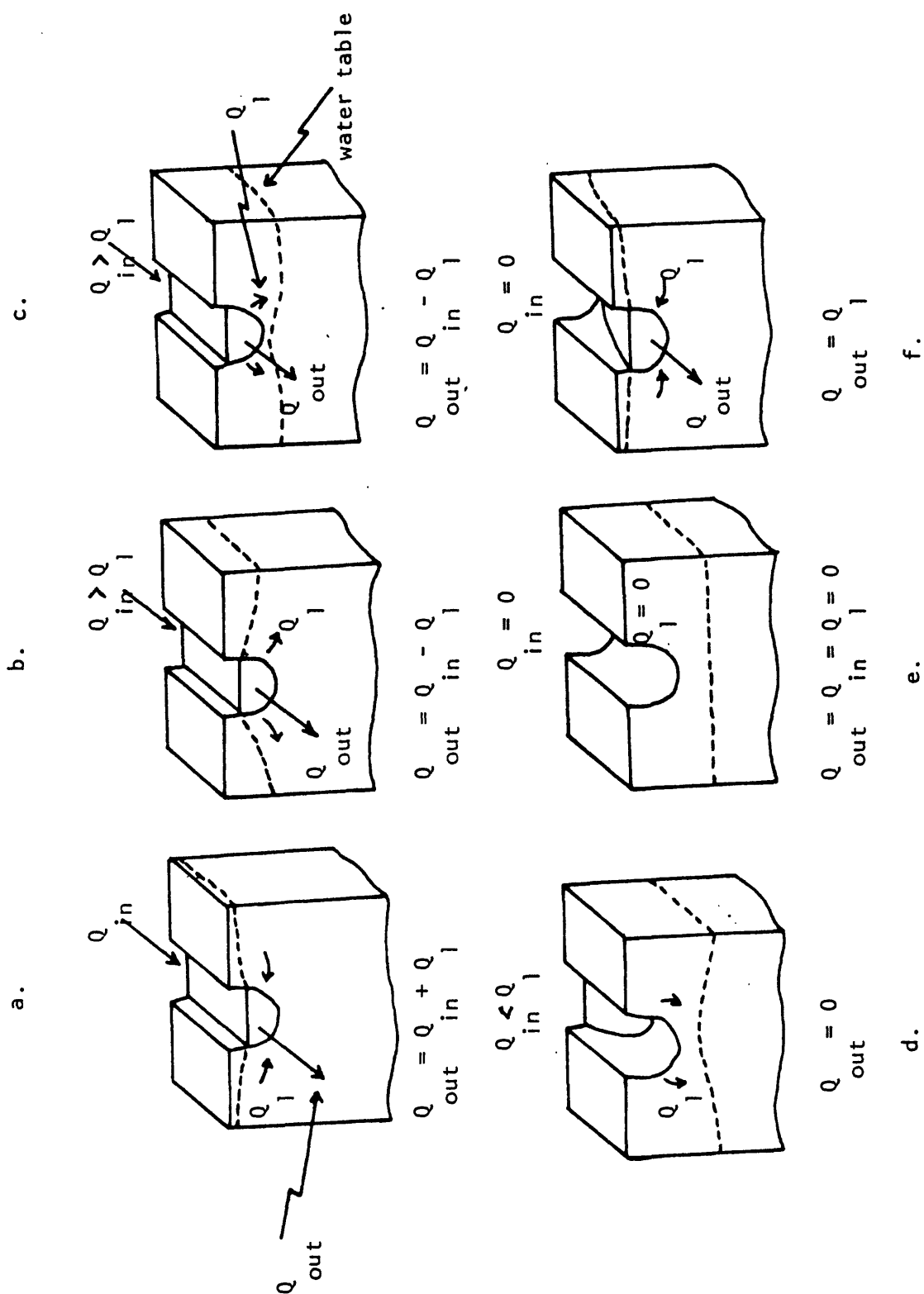


Figure 3.--Representation of stream-aquifer interaction.

3. No flow occurs in the stream from the upstream node ( $Q_{in} = 0$ ), and stream head depends upon aquifer head. If the calculated aquifer head at the node is below the altitude of the stream bottom, outflow from the stream node ( $Q_{out}$ ) is zero (fig. 3-e). If the aquifer head is above the altitude of the stream bottom, leakage from the aquifer ( $Q_1$ ) to the stream node is calculated. In this case, outflow from the stream node ( $Q_{out}$ ) is equal to leakage ( $Q_1$ ), and stream depth is determined from the Manning formula (fig. 3-f).

Most main streams have tributaries feeding them. Treatment of each tributary stream node is the same as described above. Tributaries and ponds are numbered by segment ( $s_n$ ) in downstream order. Numbering starts upstream, and increases sequentially as each tributary enters the main stream channel. Calculations of flow are done from lowest to highest order. In figure 4, for example, calculations of flow are done first in segments  $S_1$  and  $S_2$ . The sum of the cumulative flows at the last downstream node of segments  $S_1$  and  $S_2$  are set equal to the inflow in the first upstream node of segment  $S_3$ . This procedure is continued until the  $n$ th segment is calculated. The pond segment is treated the same as stream segments in the numbering order sequence.

The average width, average bottom slope, and Manning's roughness coefficient are read into the modified program, as are inflow to the first upstream node and the stream segment number to which that stream segment discharges. In figure 4, for example, segments  $S_1$  and  $S_2$  discharge to  $S_3$ , and segments  $S_3$  and  $S_4$  discharge to  $S_5$ , etc. If no inflow is specified to the first upstream node, then the node is treated as described previously under condition number three.

#### MODEL TESTING

The modified program was tested first to insure that computational schemes in the original program had not changed. For this purpose, two steady-state problems were selected, one for idealized conditions and the other for an actual field situation. Both steady-state problems were run using the original and modified programs with SIP, ADI, and LSOR solver routines. The results from these programs were identical for both steady-state problems.

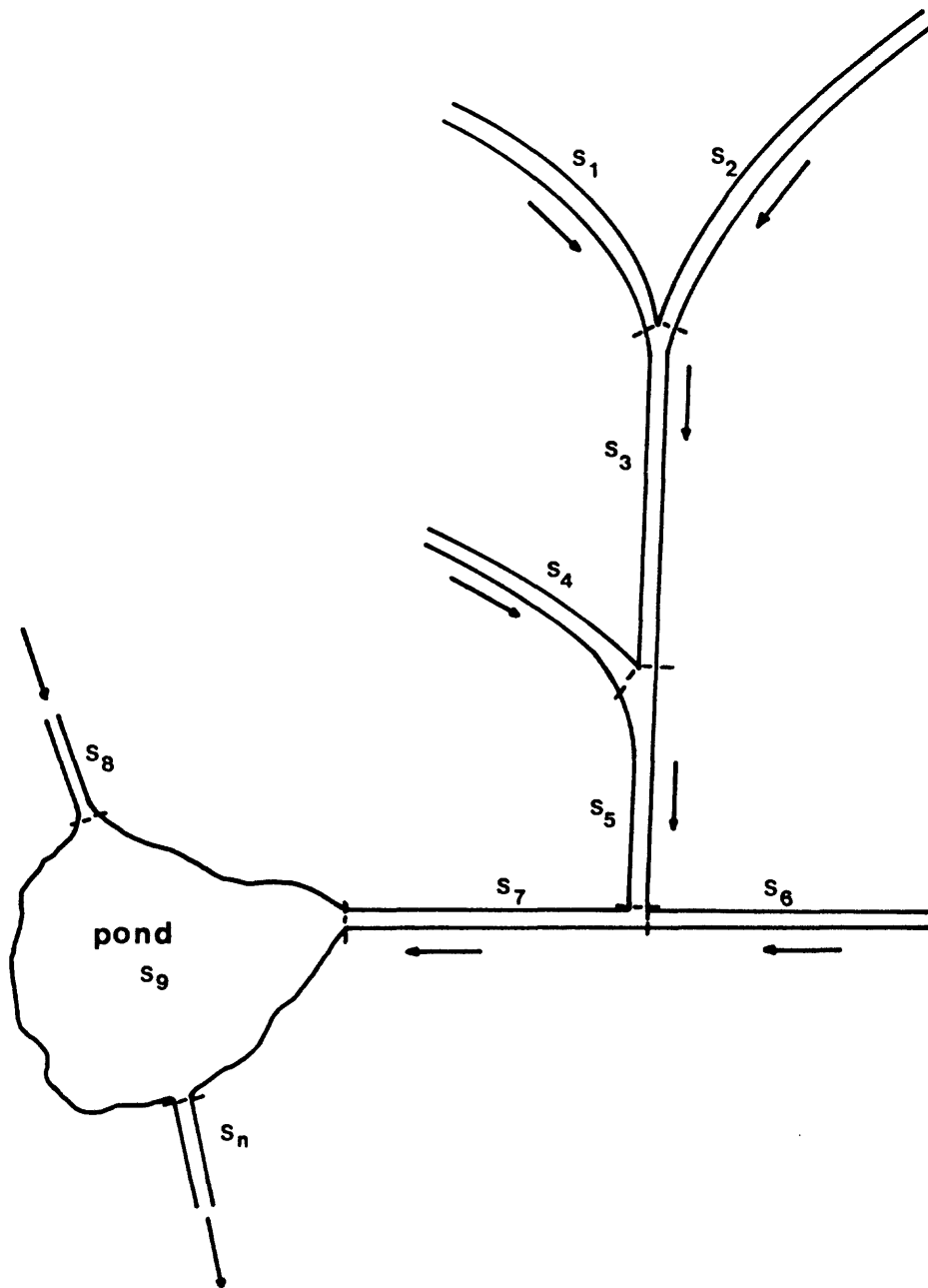


Figure 4.--Numbering sequence for surface-water segments.

The interaction between surface-water and ground-water systems was tested by modeling a hypothetical stream-aquifer system bounded on all sides by no-flow boundaries. A uniform recharge rate was applied to the aquifer and the model was simulated for steady-state. Using the steady-state heads as the starting condition, the model was simulated for one year. The results show that ground-water runoff from the total stream length at the end of the year equaled the recharge applied to the aquifer. This provided a useful check showing that inflow equaled outflow, and that the stream stage routine kept the mass balance of the total system intact.

To test the transient simulation capabilities of the modified program on a stream-aquifer system, the idealized aquifer shown in figure 5 was simulated. The results of numerical solutions were compared against analytical solutions given by Oakes and Wilkinson (1972). For this test the following values were assumed: storage coefficient, 0.2; streambed hydraulic conductivity, 1 ft/d; streambed thickness, 1 ft; and transmissivity, 3200 ft<sup>2</sup>/d. Ground-water head in an observation well (fig. 5) and base flow from the entire aquifer area were simulated using the recharge distribution shown in figure 6. The model was simulated for six years to reach equilibrium, after which cyclic variations remained constant. The numerical results from the modified program for ground-water head (fig. 7) and base flow (fig. 8) are in good agreement with the analytical results presented by Oakes and Wilkinson (1972).

The comparisons indicate that the modified program: (1) is capable of simulating effects of transient stresses on stream-aquifer systems, and (2) can accurately simulate water-level and base-flow data for a given recharge distribution under constant stream depth and flow conditions. The capability of the modified program to simulate base flow for varying stream-head conditions was tested against a solution developed by Cooper and Rorabaugh (1963). The idealized aquifer shown in figure 5 was used to simulate flood wave passage through a stream. Comparison of base flows (fig. 9), for a unit length of stream (1 ft), indicates good agreement between numerical model simulations and analytical solutions developed by Cooper and Rorabaugh (1963). Small differences occur between numerical and analytical solutions because calculated stream heads in the model are not exactly the same as assumed in the analytical solution. This is because in the modified program, head changes as the stream loses or gains flow from the aquifer. Although small, the change in stream head results in a variation in base flow since leakage into (-) or from (+) the stream is a function of the stream head (equation 10).

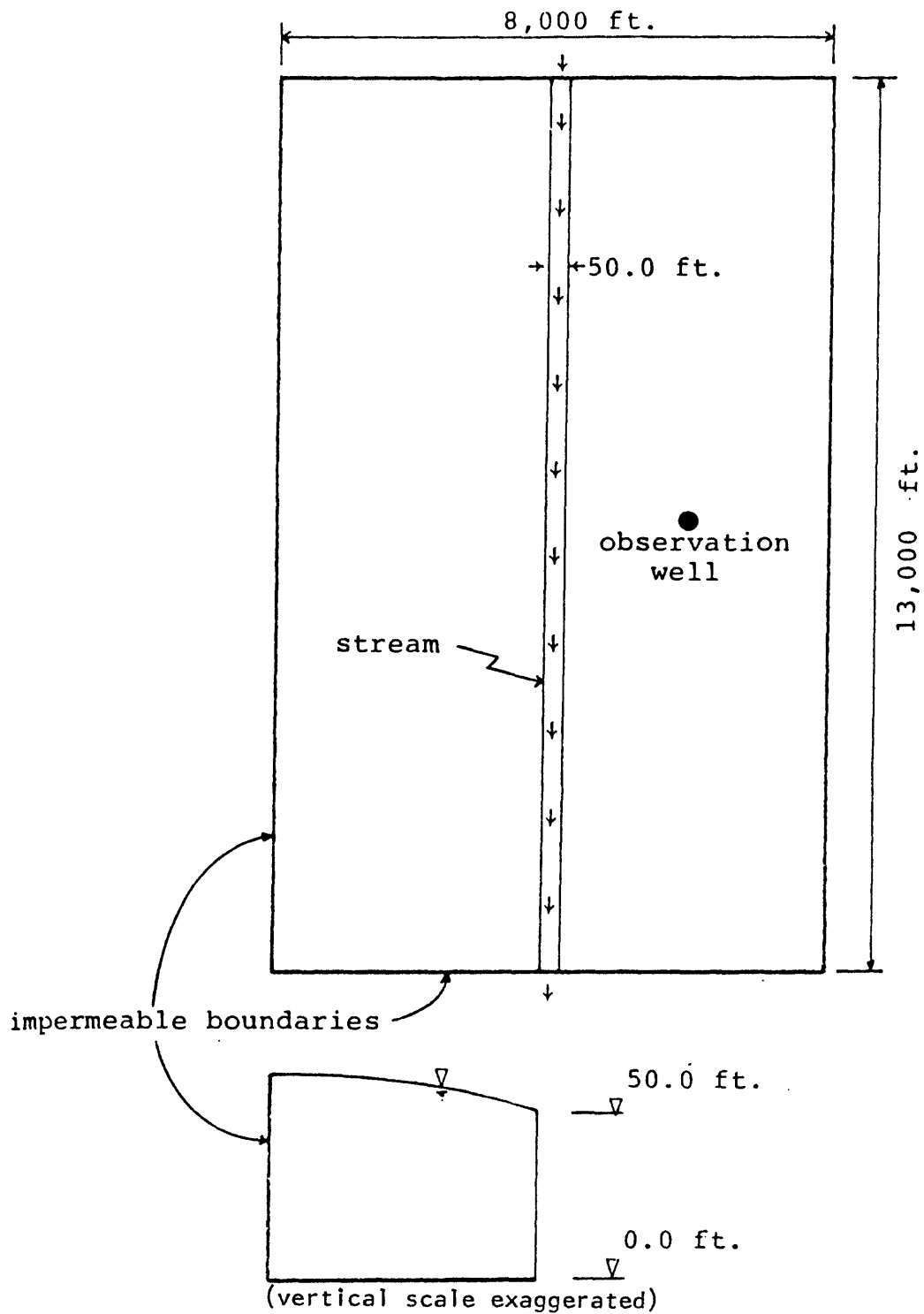


Figure 5.--Idealized aquifer for stream-aquifer system.

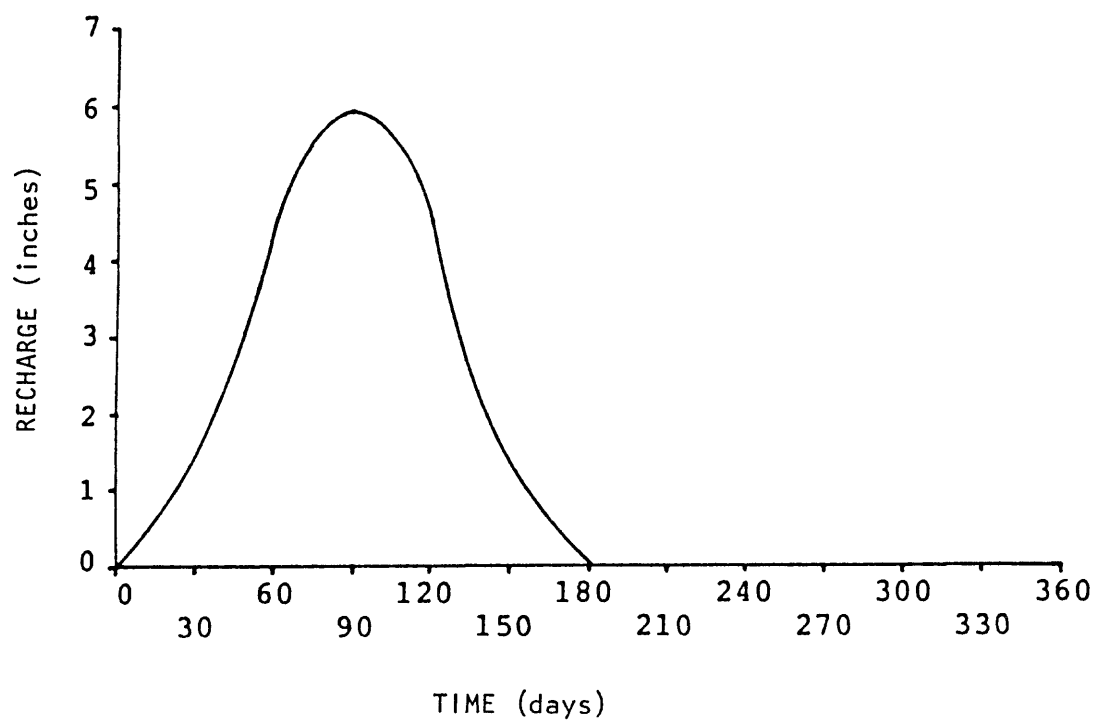


Figure 6.--Recharge distribution applied to the idealized aquifer for stream-aquifer system.

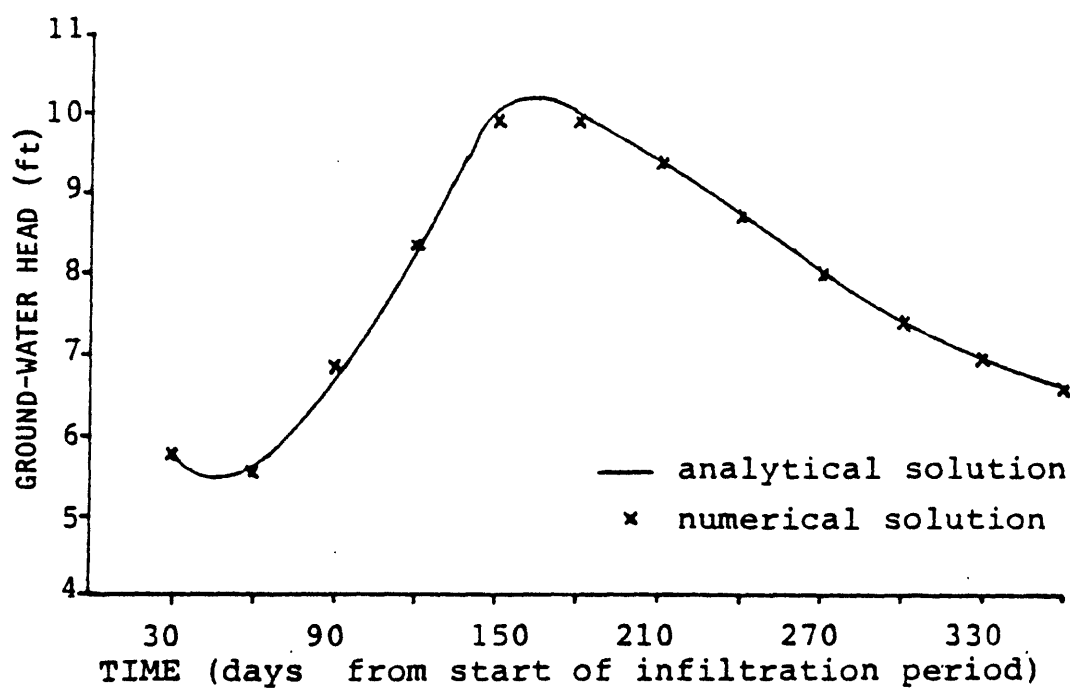


Figure 7.--Comparison of ground-water heads for numerical (model simulation) and analytical (Oakes and Wilkinson, 1972) solutions.

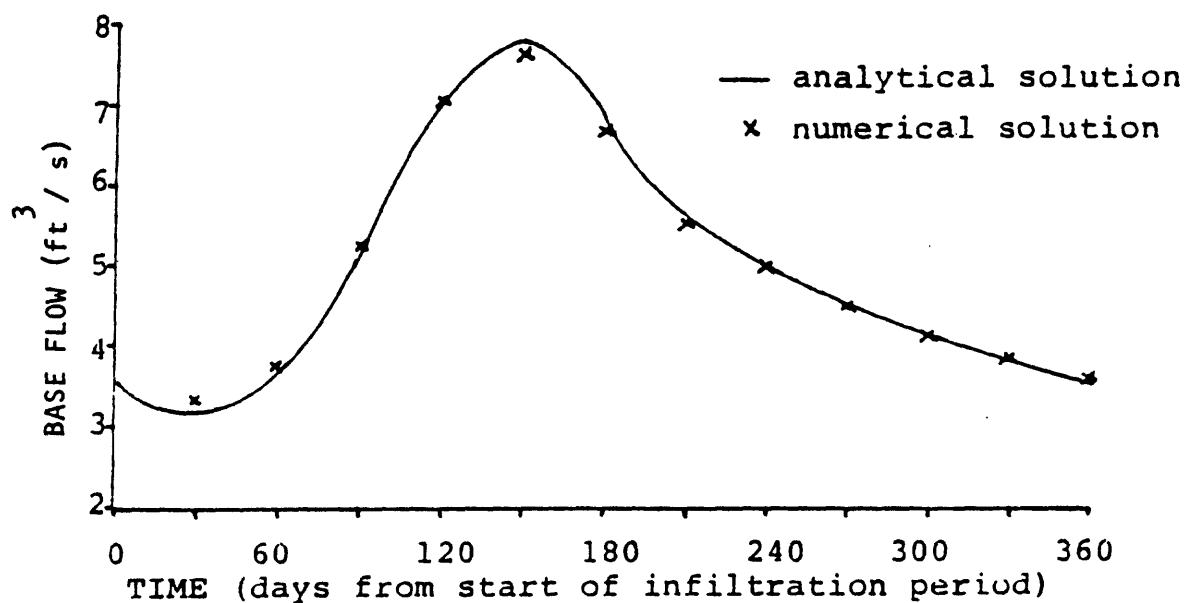


Figure 8.--Comparison of base flows for numerical (model simulation) and analytical (Oakes and Wilkinson, 1972) solutions.

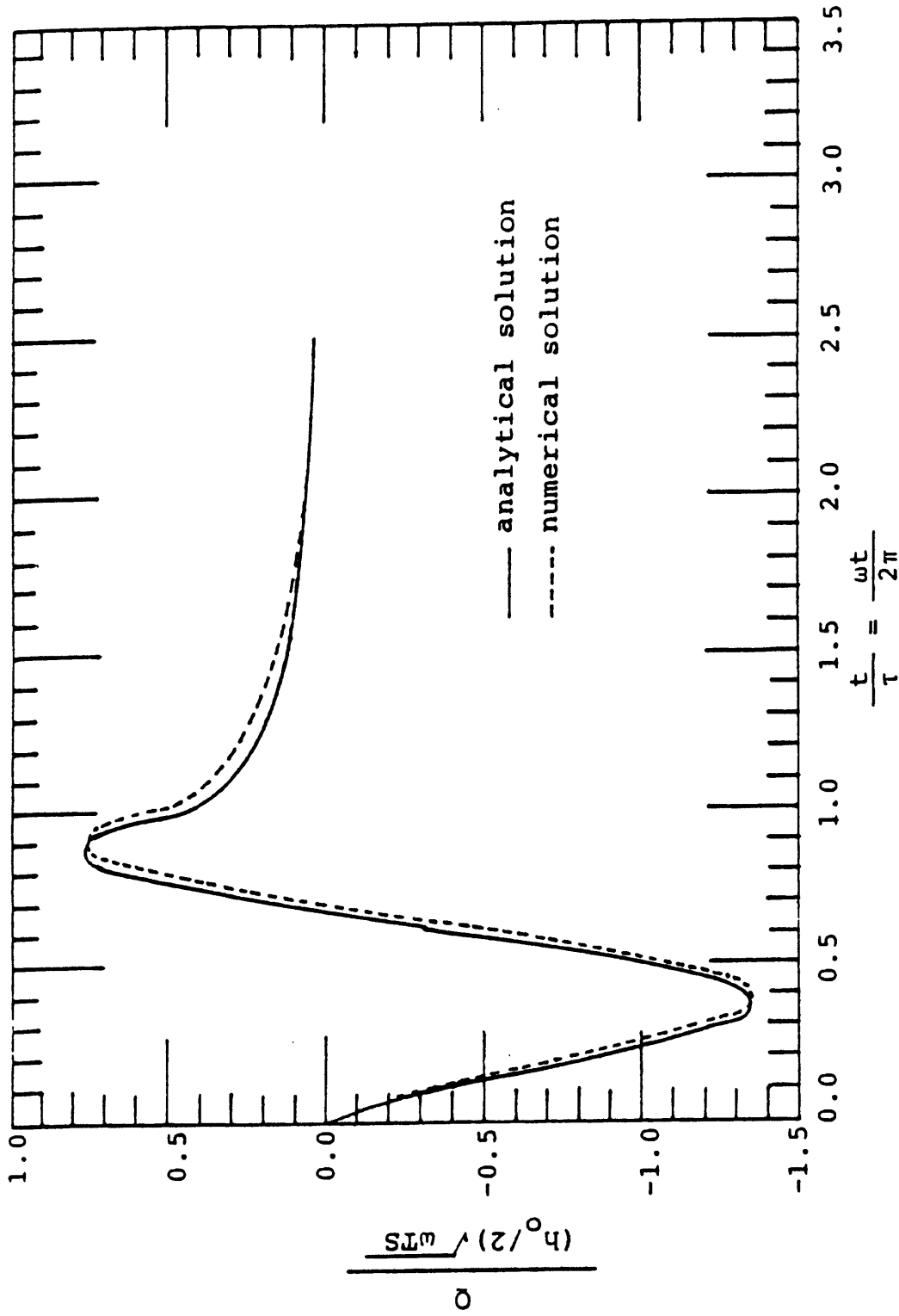


Figure 9.--Comparison of base flows due to sinusoidal flood wave for numerical (model simulation) and analytical (Cooper and Rorabaugh, 1963) solutions.  
 (S=storage coefficient; T=transmissivity;  $h_0$ =peak flood wave height;  
 $\omega$ =frequency of stage oscillation; and  $\tau$ =period of stage oscillation).



The modified program was also tested against a one-dimensional transient model. The idealized aquifer's response to sinusoidal fluctuations in stream head were examined 1000 feet from the stream. The comparison shown in figure 10 indicates good agreement between one- and two-dimensional solutions.

Model output results, in table 2, show the modified program's capability to simulate a stream-pond-aquifer system. For this test, the idealized aquifer shown in figure 11 was simulated. Hydraulic conductivity of the confining layer beneath the stream and pond was assumed to be 1.0 ft/d and streambed thickness was assumed to be 1 ft. The streambed hydraulic conductivity was adjusted for a 20-foot wide stream using equation 11. The hydraulic conductivity of the homogeneous, isotropic, water-table aquifer was assumed to be 200 ft/d. The aquifer specific yield was assumed to be 0.2. If the pond were known to be in good hydraulic connection with the aquifer, then an appropriately higher specific yield should be assigned to aquifer grid blocks below the pond.

The model simulation was run for a six-year period, with ground-water recharge and evapotranspiration, to reach equilibrium conditions. A pumping well, located near the southern end of the pond, was pumped at 1.55 ft<sup>3</sup>/s for one year. The objective of this test was to demonstrate that: (1) the modified program could handle stream reaches going dry for periods of time and then recover, (2) the interactions of the pond-aquifer, stream-aquifer, and pond-stream systems could be simulated, and (3) the mass balance of the system remained intact.

Table 2 shows that the mass balance of the system remained intact, since the sum of discharges from the aquifer (columns 2+4+7+9) closely matched the recharge applied to the aquifer. The small difference (0.50 ft<sup>3</sup>/s) between recharge to (+70.40 ft<sup>3</sup>/s), and discharge from (-70.90 ft<sup>3</sup>/s) the aquifer was probably due to the four digit calculation performed on mass balances within the program.

The results shown in table 2 also indicate that the modified program can handle a stream-pond-aquifer system when stream reaches go dry during low-flow periods. Column 5 shows that discharge from the pond to the stream ceases when the pond altitude (column 3) is equal to or less than the altitude of the stream bottom (51.0 ft). However, column 6 shows that stream nodes during the 5th, 10th, and 11th months did not go dry, even though no discharge occurs to the stream from the pond. This happens because ground-water runoff to the stream (column 7) during those months is high enough to sustain some flow in the stream.

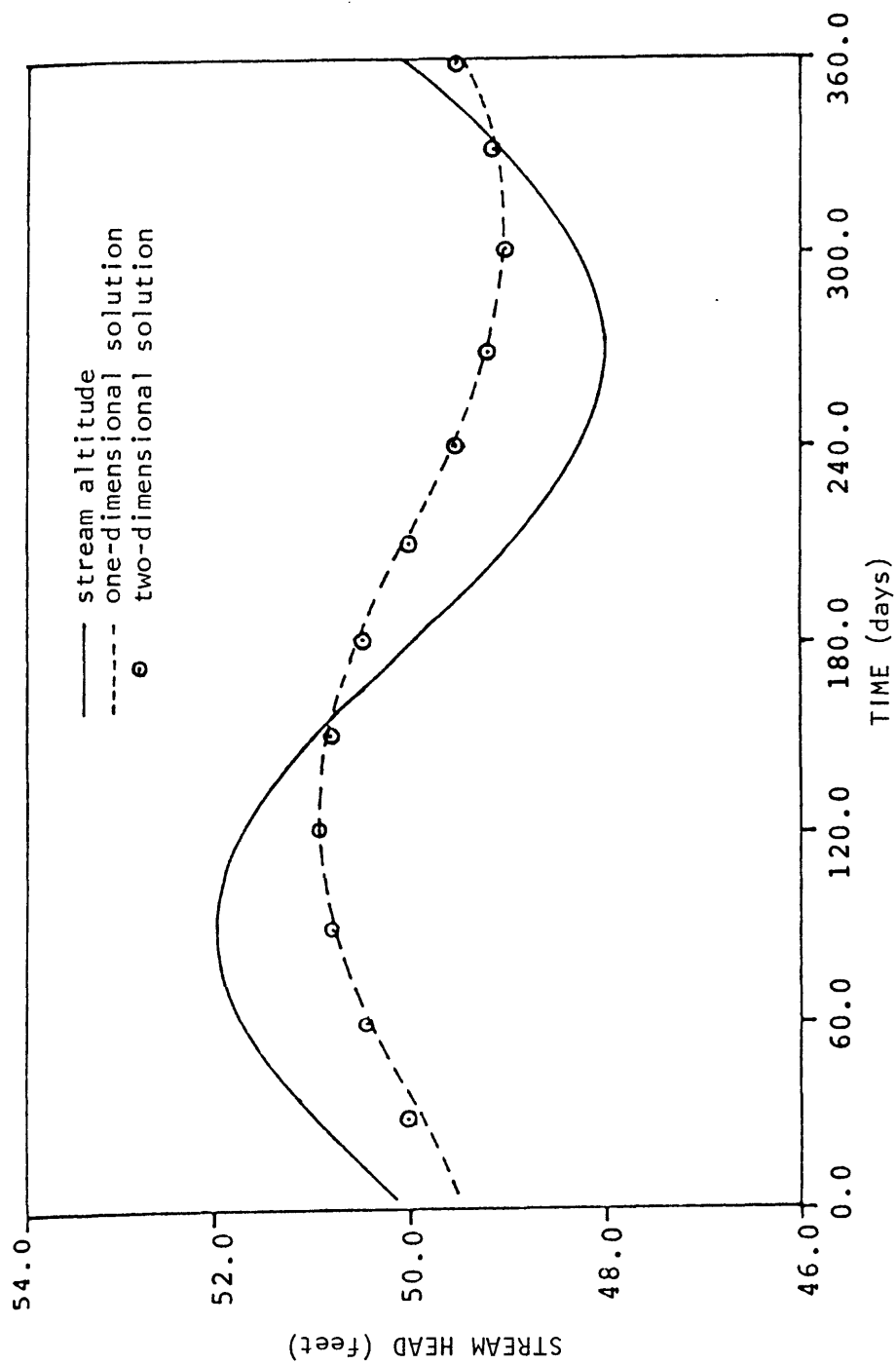


Figure 10.--Comparison of one- and two-dimensional solutions for a sinusoidal fluctuation of stream heads.

Table 2. Model results for stream-pond-aquifer interaction pumping 1.55 ft<sup>3</sup>/s  
(- discharge from, + recharge into the aquifer).

(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)
Month	Well pumpage	Pond alti- tude <sup>1</sup>	Ground- water runoff to pond <sup>2</sup>	Pond discharge to stream <sup>2</sup>	Stream alti- tude <sup>1,3</sup>	Ground- water runoff to stream <sup>2</sup>	Stream dis- charge <sup>2</sup>	Evapotran- piration <sup>2</sup>	Ground-water Recharge <sup>2,4</sup>
1	-1.55	51.4	-3.38	-3.25	51.3	-1.76	-5.01	-0.26	9.90
2	-1.55	51.6	-5.89	-5.76	51.4	-2.36	-8.12	-0.45	15.47
3	-1.55	51.3	-2.05	-1.92	51.2	-1.82	-3.74	-2.29	3.48
4	-1.55	51.1	+1.29	-0.56	51.1	-1.12	-1.68	-3.43	0.07
5	-1.55	50.5	+0.38	0.00	51.0	-0.75	-0.75	-4.52	2.54
6	-1.55	49.5	+0.41	0.00	DRY (2)	-0.30	-0.30	-5.00	0.16
7	-1.55	48.9	+0.50	0.00	DRY (3)	-0.12	-0.12	-4.78	0.84
8	-1.55	48.6	+0.41	0.00	DRY (3)	-0.12	-0.12	-3.45	2.31
9	-1.55	49.4	-0.39	0.00	DRY (1)	-0.64	-0.64	-1.93	10.40
10	-1.55	50.4	-0.42	0.00	51.0	-1.42	-1.42	-1.05	10.40
11	-1.55	51.0	-0.34	0.00	51.0	-1.26	-1.26	-0.25	5.73
12	-1.55	51.3	-2.00	-2.14	51.2	-1.52	-3.66	-0.22	9.10
Total	-18.60		-11.48	-13.63		-13.19	-26.82	-27.63	70.40

1 In feet. The altitude of the stream bottom is 51.0 feet.

2 In cubic feet per second (ft<sup>3</sup>/s).

3 Altitude of the water surface at the first stream node discharging from the pond; numeral in parenthesis indicates the number of stream nodes downstream from the pond that went dry.

4 Total simulated discharge from the aquifer equals (columns 2+4+7+9) - 70.90.

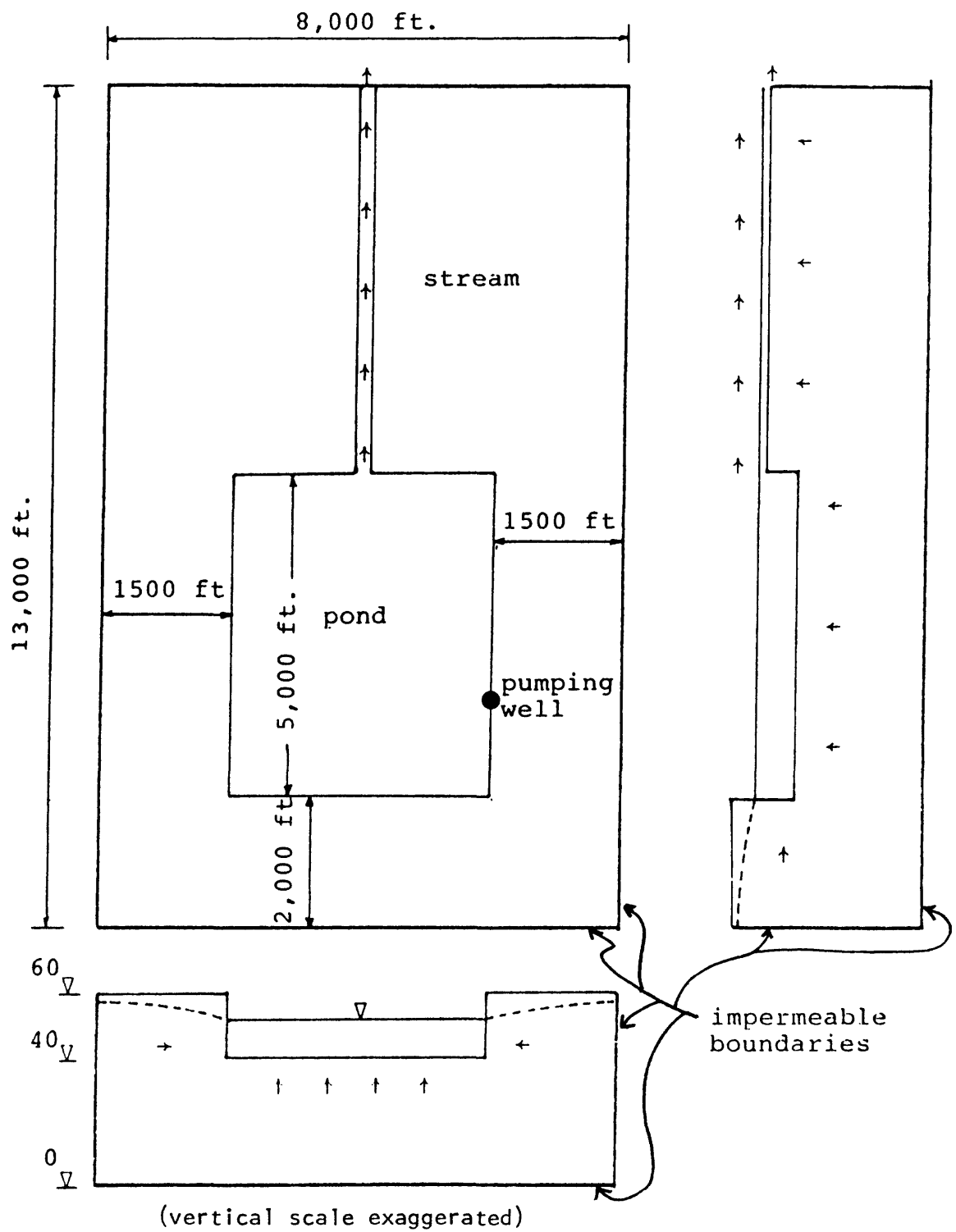


Figure 11.--Idealized aquifer for stream-pond-aquifer system.

The modified program described in this report was used to develop a field model of a stream-pond-aquifer system in the Beaver-Pasquisset ground-water reservoir in southern Rhode Island (Dickerman and Ozbilgin, written commun., 1983). The Beaver-Pasquisset model simulated breaks in the hydraulic connection between the stream-aquifer, and the pond-aquifer over stream and pond reaches influenced by drawdown from nearby pumping wells.

Complete documentation for the modified program includes: (1) explanation of modifications, (2) a flow chart, (3) data deck instructions, (4) input data, (5) output summary, and (6) a complete program listing. The modified program presented in this report can be used by the reader as a stand-alone manual. Users of the modified program should be aware that undiscovered errors in logic may exist.

#### REFERENCES

- Cooper, H.H., Jr., and Rorabaugh, M.I., 1963, Ground-water movements and bank storage due to flood stages in surface streams: U.S. Geol. Survey Water-Supply Paper 1536-J, p. 343-366.
- Oakes, D.B., and Wilkinson, W.B., 1972, Modeling of groundwater and surface water systems, I-Theoretical relationships between groundwater abstraction and base flow: Water Resources Board, Great Britain, Reading Bridge House, p. 37.
- Streeter, V.L., 1971, Fluid mechanics: New York, McGraw-Hill Book Co., p. 278-280.
- Streeter, V.L., and Wylie, E.B., 1979, Fluid mechanics: New York, McGraw-Hill Book Co., p. 227-232.
- Trescott, P.C., Pinder, G.F., and Larson, S.P., 1976, Finite-difference model for aquifer simulation in two dimensions with results of numerical experiments: U.S. Geol. Survey Techniques of Water-Resources Inv., book 7, ch. C1, 116 p.
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## SUPPLEMENTAL DATA

### Program Modifications

To allow for more convenient data handling, the method of data input and output for transient simulations was modified from the finite-difference model for aquifer simulation in two-dimensions (Trescott and others, 1976). A new entry was added to calculate transient surface-water heads from known flows. The generalized flow chart for the modified program is shown in figure 12.

The major modifications in the program were made in the MAIN program and in subroutines DATAI, COEF, and CHECKI. The rest of the program was modified only to the extent necessary to handle modifications in the MAIN program and in subroutines listed above. Format statements and specifications (for example, dimensions, common blocks ...etc.) were changed throughout the program. Except for the specifications part, computational schemes remain unchanged. The lines changed in the modified program were designated by dropping the first two letters in columns 73 and 74, and adding the "-" symbol to column 79 at the end of the line. For example, in the original program the line identified by code MAN 240 was changed to read N 2400-.

A new subroutine CALC was added to initiate the modified program for surface-water calculations. If CALC is not specified by the modeler as a simulation option, the program runs the original version. The CALC option is designed to work only with the LEAK or combined WATER/LEAK options.

Twelve new arrays were added to the program to accommodate calculations of surface-water heads. Five of the arrays have the size DIML x DIMW, while seven have the size NSEG. The dimensions of these arrays are calculated and passed to subroutines within the MAIN program. Statements calling the entry ARRAY in the MAIN program were moved to change the sequence of matrix data input. A new statement calling the entry ARRAY was added to read the new array RSEG (surface-water segment identification). Statements were added or moved between lines MAN2200 and MAN2500 to control the flow of computations in the modified program.

The method of data input and output for pumping periods in the entry NEWPER of subroutine DATAI was changed. Additional read statements were added to read new parameters and problem options. The rest of the changes in subroutine DATAI were made to handle those changes in entry NEWPER (for example, addition of new format statements, initialization of added variables, etc.).

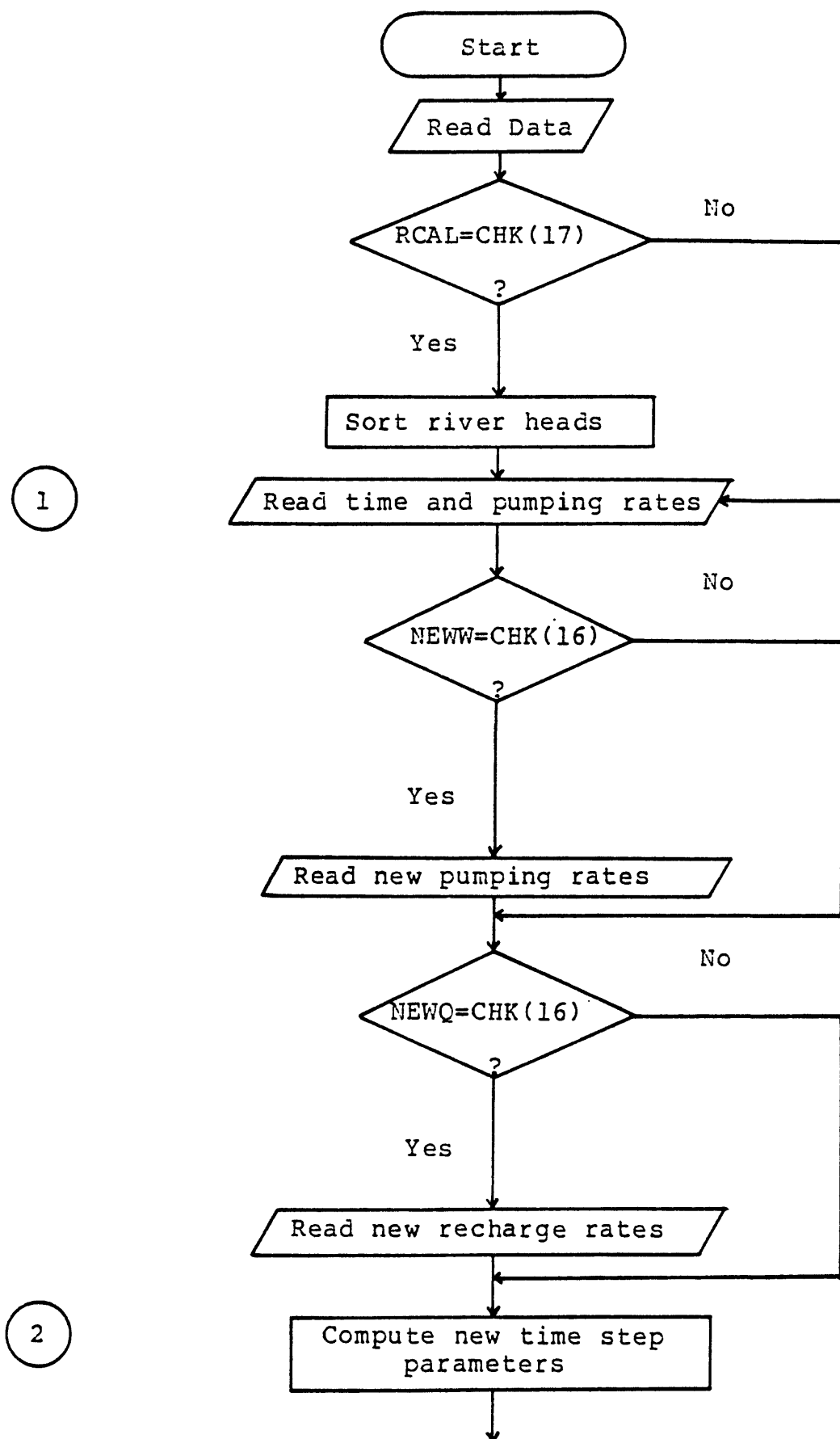
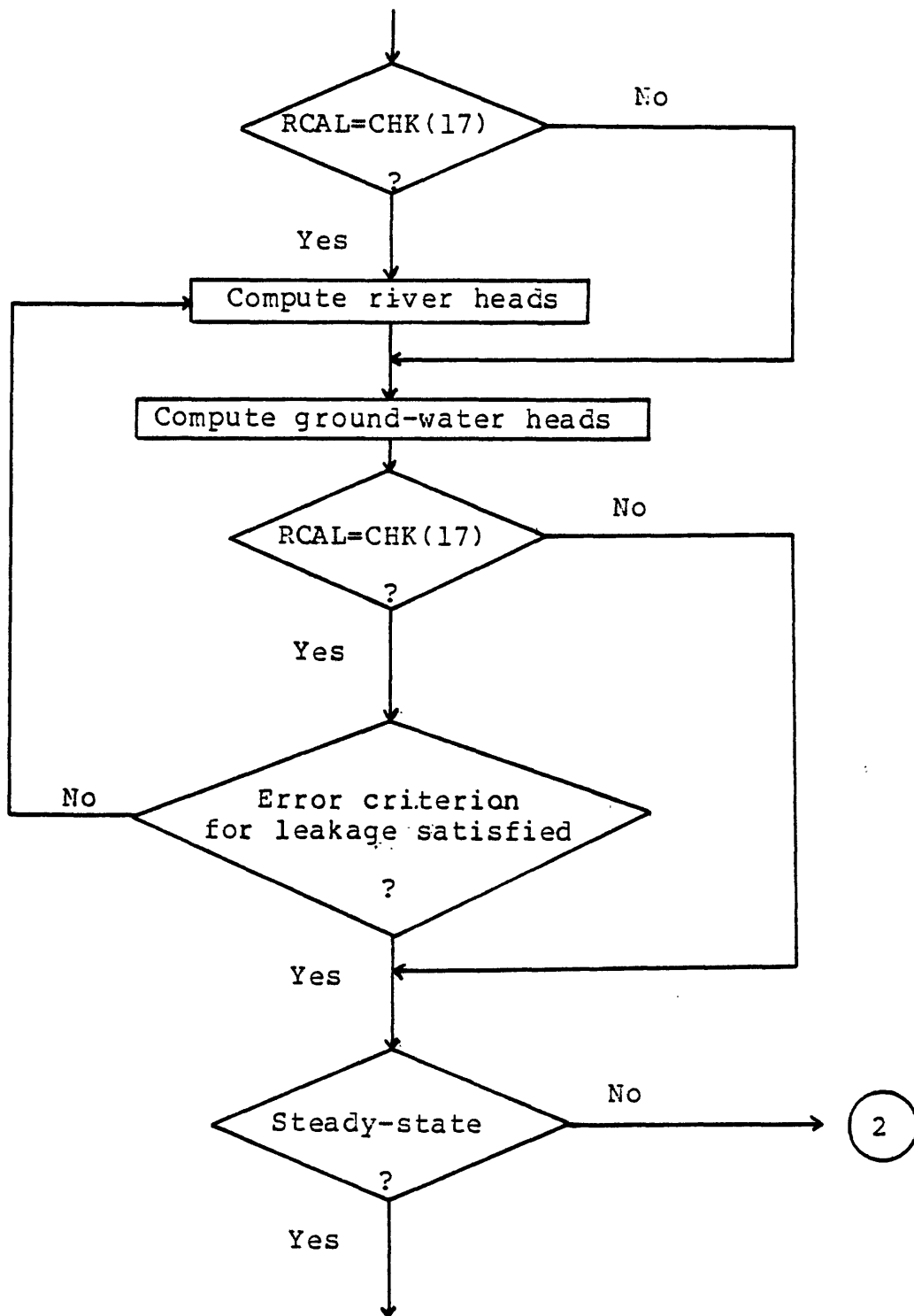


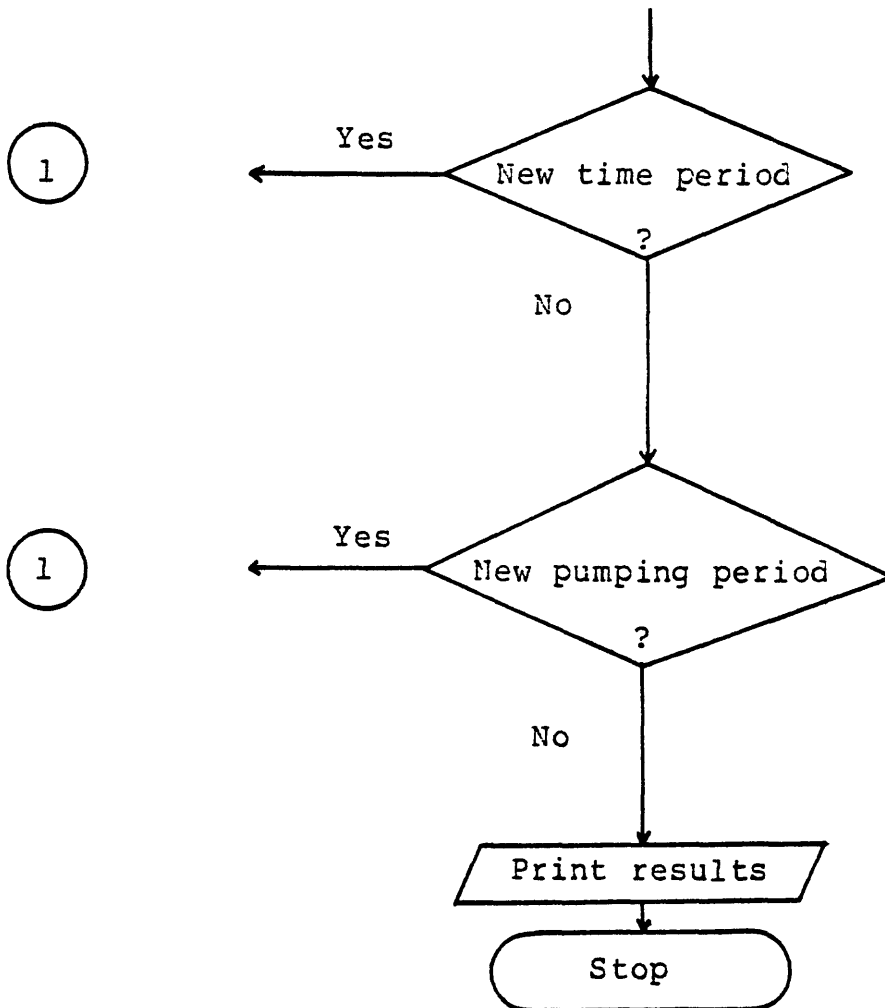
Figure 12.-- Simplified flow chart for the modified program.

flow chart - Continued





flow-chart - Continued



A new entry RSORT was added to subroutine COEF to order stream nodes by highest to lowest initial stream head, and store this order on array IRIV for later retrieval. This was necessary for both stream head calculations and an orderly printout of leakages from surface-water nodes.

The major changes in the modified program were made in subroutine CHECKI. A new entry HRIVER was added to calculate surface-water heads. The entry CWRITE was modified to handle transient output of leakages and to print calculated surface-water heads. Statements were added to the entry CHECK, as needed, to calculate leakages into surface-water bodies and to initialize some variables used in the new entry HRIVER.

Table 3.--Data deck instructions  
 (\*Indicates new variable used in the modified program)

GROUP I: TITLE, SIMULATION OPTIONS, AND PROBLEM DIMENSIONS

This group of cards, which are read by the main program, contains data required to dimension the model. To specify an option on card 3, punch the characters underlined in the definition, starting in the first column of the field. For any option not used, leave the appropriate columns blank.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
1	1-80	20A4		
			HEADING	Any title the user wishes to print on one line at the start of the output.
2	1-48	12A4		
3	1-5	A4,1X	WATER	<u>WATE</u> for water table or combined water-table - artesian aquifer.
	6-10	A4,1X	LEAK	<u>LEAK</u> for an aquifer system including leakage from a surface water or confining bed. Required if CALC is specified on column 61.
	11-15	A4,1X	CONVRT	<u>CONV</u> for combined water-table - artesian aquifer.
	16-20	A4,1X	EVAP	<u>EVAP</u> to permit discharge by evapotranspiration.
	21-25	A4,1X	RECH	<u>RECH</u> to include a constant recharge rate.
	26-30	A4,1X	NUMS	<u>SIP</u> or <u>LSOR</u> or <u>ADI</u> to designate the equation-solving scheme.
	31-35	A4,1X	CHCK	<u>CHEC</u> to compute a mass balance.
	36-40	A4,1X	PNCH	<u>PUNC</u> for punched output at the end of the simulation.
	41-45	A4,1X	IDK1	<u>DK1</u> to read initial head and mass balance parameters from disk (unit 4).

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
	46-50	A4,1X	IDK2	<u>DK2</u> to save (write) computed head, elapsed time, and mass balance parameters on disk (unit 4).
	51-55	A4,1X	NUM	<u>NUME</u> to print drawdown in numeric form.
	56-60	A4,1X	HEAD	<u>HEAD</u> to print the head matrix.
	61-54	A4,1X	*RCAL	<u>CALC</u> to calculate surface-water heads.

(All variables on card 4 are integers)

4	1-10	I10	DIML	Number of rows.
	11-20	I10	DIMW	Number of columns.
	21-30	I10	NW	Number of pumping wells for which drawdown is to be computed at a "real" well radius.
	31-40	I10	ITMAX	Maximum number of iterations per time step.
	41-50	I10	*NSEG	Number of surface-water segments to be specified.

NOTE - Steady-state simulations often require more than 50 iterations. Transient time steps usually require less than 30 iterations.

## GROUP II: SCALAR PARAMETERS

The parameters required in every problem are underlined. The other parameters are required as noted; when not required, their location on the card can be left blank. The G format is used to read E, F, and I data. Minimize mistakes by always right-justifying data in the field. If F format data do not contain significant figures to the right of the decimal point, the decimal point can be omitted. Default typing of variables applies.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
1	1-4	A4	CONTR	<u>CONT</u> to generate a map of drawdown and (or) hydraulic head; for no maps insert a blank card.
	11-20	G10.0	XSCALE	Factor to convert model length unit to unit used in X direction on maps (that is, to convert from feet to miles, XSCALE=5280).
	21-30	G10.0	YSCALE	Factor to convert model length unit to unit used in Y direction on maps.
	31-40	G10.0	DINCH	Number of map units per inch.
	41-50	G10.0	FACT1	Factor to adjust value of drawdown printed.
	51-60	G10.0	FACT2	Factor to adjust value of head printed.
	61-68	A8	MESUR	Name of map length unit.

NOTE - For value of drawdown or head 52.57, for example:

FACT1 or FACT2	Printed value
.01	0
.1	5
1	52
10	525
100	***

2	1-10	G10.0	<u>NPER</u>	Number of pumping periods for this simulation.
	11-20	G10.0	<u>KTH</u>	Number of time steps between printouts.

NOTE - To print only the results for the final time step in a pumping period, make KTH greater than the expected number of time steps. The program always prints the results for the final time step.

	21-30	G10.0	<u>ERR</u>	Error criterion for closure (L).
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NOTE - When the head change at all nodes on subsequent iterations is less than this value (for example 0.01 foot), the program has reached a solution for the time step.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
	31-40	G10.0	EROR	Steady-state error criterion (L).
NOTE - If the head change between time steps in transient simulations is less than this amount, the pumping period is terminated.				
	41-50	G10.0	*ERLEAK	Error criterion for surface water - ground water interaction ( $L^3/T$ ).
NOTE - If the largest change in leakage from surface waters is less than this amount (for example $0.01 \text{ feet}^3/\text{sec.}$ ), the program has reached a solution for the time step when CALC option is specified in card 3 of Group I parameters. When CALC option is used, the program will try to satisfy ERR and ERLEAK simultaneously within the time step.				
	51-60	G10.0	SS	Specific storage of confining bed (1/L)
NOTE - SS has a finite value only in transient simulations where leakage is a function of storage in the confining bed.				
	61-70	G10.0	<u>LENGTH</u>	Definition depends on the numerical solution used: LSOR: number of LSOR iterations between 2-D corrections. ADI and SIP: number of iteration parameters; unless the program is modified, code 10 for SIP
	71-80	G10.0	<u>HMAX</u>	Definition depends on the numerical solution used: LSOR: acceleration parameter. ADI: maximum iteration parameter. SIP: value of $B'$ .
NOTE - See the discussion of the numerical methods in Trescott and others (1976) for information on iteration parameters.				
3	1-10	G10.0	<u>FACTX</u>	Multiplication factor for transmissivity in X direction.
	11-20	G10.0	<u>FACTY</u>	Multiplication factor for transmissivity in Y direction.
NOTE - FACTX=FACTY=1 for isotropic aquifers.				

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
4	1-20	G20.10	SUM	Parameters in which elapsed time and cumulative volumes for mass balance are stored. For the start of a simulation insert three blank cards. For continuation of a previous run from punched output, remove the three blank cards and insert the first three cards of the punched output from the previous run. If continuation is from interim storage on disk, the three blank cards should remain.
	21-40	G20.10	SUMP	
	41-60	G20.10	PUMPT	
	61-80	G20.10	CFLUXT	
5	1-20	G20.10	QRET	
	21-40	G20.10	CHST	
	41-60	G20.10	CHDT	
	61-80	G20.10	FLUXT	
6	1-20	G20.10	STORT	
	21-40	G20.10	ETFLXT	
	41-60	G20.10	FLXNT	

### GROUP III: ARRAY DATA

Each of the following data sets, except for the first one (PHI), consists of a parameter card and, if the data set contains variable data, may include a set of data cards. Default typing applies except for M(I,J) which is a real array. Each parameter card contains five variables defined as follows:

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
	1-10	G10.0	FACT	If IVAR=0, FACT is the value assigned to every element of the matrix; if IVAR=1, FACT is the multiplication factor for the following set of data cards.
	11-20	G10.0	IVAR	=0 if no data cards are to be read for this matrix; =1 if data cards for this matrix follow.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
	21-30	G10.0	IPRN	=0 if input data for this matrix are to be printed; =1 if input data for this matrix are <u>not</u> to be printed.
	31-40	G10.0	IRECS	=0 if the matrix is being read from cards or if each element is being set equal to FACT; =1 if the matrix is to be read from disk (unit 2).
	41-50	G10.0	IRECD	=0 if the matrix is <u>not</u> to be stored on disk; =1 if the matrix being read from cards or set equal to FACT <u>is</u> to be stored on disk (unit 2) for later retrieval.

For the uniform starting head=100, FACT=100, IVAR=IPRN=IRECS=IRECD=0 and no data cards are required. The save matrix, which is being read from cards, on disk, for example (provided unit 2 has been defined on a DD statement; see technical information on pages 43-45 of original 1976 program), set FACT=1, IVAR=1, IPRN=IRECS=0, IRECD=1, and include the set of data cards (note that the input matrix will not be printed for IPRN=0). After this has been processed successfully, subsequent runs need only include a parameter card with the following: FACT=IVAR=IPRN=0, IRECS=1, IRECD=0. The set of data cards are not included and the matrix is input via unit 2 from disk storage.



When data cards are included, start each row on a new card.

To prepare a set of data cards for an array that is a function of space, the general procedure is to overlay the finite-difference grid on a contoured map of a parameter and record the average value of the parameter for each finite-difference block on coding forms according to the appropriate format. In general, record only significant digits and no decimal points (except for data set 2); use the multiplication factor to convert the data to their appropriate values. For example, if vertical hydraulic conductivity of the confining bed (RATE) ranges from  $2 \times 10^{-9}$  to  $9 \times 10^{-8}$  ft/sec., coded values should range from 2 to 90; the multiplication factor (FACT) would be 1.0E-09.

Arrays needed in every simulation are underlined. Omit parameter cards and data cards not used in the simulation (however, see the note for the S matrix).

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
1	1-80	8F10.4	PHI(I,J)	Head values for continuation of a previous run (L).

NOTE - For a new simulation this data set is omitted. Do not include a parameter card with this data set.

2	1-80	8F10.4	<u>STRT(I,J)</u>	Starting head matrix (L).
3	1-80	20F4.0	S(I,J)	Storage coefficient (dimensionless).

NOTE - Always required. In addition to specifying storage coefficient values for artesian aquifers, this matrix is used to locate constant-head boundaries by coding a negative number at constant head nodes. At these nodes T or PERM must be greater than zero. For a problem with no constant-head nodes and that does not require S values, insert a blank parameter card.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
4	1-80	20F4.0	T(I,J)	Transmissivity ( $L^2/T$ )

NOTE - (1) Required for artesian aquifer simulation only.

(2) Zero values must be placed around the perimeter of the T or PERM matrix for reasons inherent in the computational scheme. If IVAR=0, zero values are automatically inserted around the border of the model.

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5	1-80	20F4.0	PERM(I,J)	Hydraulic conductivity(L/T) (see note 2 for data set 4).
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6	1-80	20F4.0	BOTTOM (I,J)	Elevation of bottom of aquifer (L).
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7	1-80	20F4.0	SY (I,J)	Specific yield (dimensionless).
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NOTE - Data sets 5, 6, and 7 are required for water table or combined artesian - water table simulations.

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8	1-80	20F4.0	TOP(I,J)	Elevation of top of aquifer (L).
---	------	--------	----------	-------------------------------------

NOTE - Required only in combined artesian - water table simulations.

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9	1-80	20F4.0	RATE(I,J)	Hydraulic conductivity of confining bed (L/T).
---	------	--------	-----------	---

10	1-80	20F4.0	RIVER(I,J)	Head on the other side of confining bed (also the surface-water head) (L).
----	------	--------	------------	--

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
11	1-80	20F4.0	M(I,J)	Thickness of confining bed (L).

NOTE - Data sets 9, 10, and 11 are required in simulations with leakage. They are required for calculation of surface-water heads. If the confining bed or streambed does not extend over the entire aquifer use the M matrix to locate the confining bed. If RATE and RIVER do not vary over the extent of the confining bed they can be initialized to a uniform value. For calculation of stream heads, a RIVER matrix is required. The RIVER matrix is used in the program to locate stream nodes in the order they appear from upstream to downstream. Therefore, stream head values must descend downstream to the end of a stream reach. This is not required for the pond areas.

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12	1-80	20F4.0	*RSEG(I,J)	Surface-water segment identification (dimensionless).
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NOTE - Required in simulations with surface water option (when CALC is coded on column 61 of card 3 in Group I data, otherwise omit). The value left to the decimal point (whole part of a real number) designates the segment number. Mantissa (fraction part of a real number) is for classifying the segment as stream or pond, and to specify the type of calculation to be done. For example, for surface water segment number one;

mantissa = 0 if no calculation is to be done. Nodes are part of either a stream or pond segment. (RSEG=1.0).

mantissa=1 if no calculation is to be done, but leakage from each node of the segment is to be printed. Nodes are part of either a stream or a pond segment. (RSEG=1.1).

mantissa=2 if stream heads are to be calculated and leakage from each node of the segment is to be printed. Nodes are part of a stream segment (RSEG=1.2).

mantissa=3 if pond elevations are to be calculated and leakage from each node of the segment is to be printed. Nodes are part of a pond segment (RSEG=1.3).

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CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
13	1-80	20F4.0	GRND(I,J)	Land elevation (L).

NOTE - Required for simulations with surface water option and (or) evapotranspiration. For simulations with evapotranspiration option only, if GRND does not vary over the extent of the aquifer it can be initialized to a uniform value. For surface water simulations, value of GRND refers to the elevation of bottom of the pond or stream channel; and it may not be initialized to a uniform value.

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14	1-80	8G10.0	DELX(J)	Grid spacing in X direction (L).
15	1-80	8G10.0	DELY(I)	Grid spacing in Y direction (L).

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#### GROUP IV: PARAMETERS THAT CHANGE WITH THE PUMPING PERIOD

The program has three options for the simulation period.

1. To simulate a given number of time steps within a time period, set TMAX to a value larger than the expected simulation period. The program will use NUMT, CDLT, and DELT as coded.
2. To simulate a given time period within a pumping period, set NUMT larger than the number required for the simulation period (for example 100). The program will compute the exact DELT (which will be less than or equal to DELT coded) and NUMT to arrive exactly at TMAX at the last time step.
3. To simulate a given pumping period, set KNUM=KPER and TMAX, NUMT, CDLT, and DELT to appropriate values as described above.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
1	1-10	G10.0	<u>KP</u>	Number of the pumping period.
	11-20	G10.0	<u>KPML</u>	Number of the previous pumping period.

NOTE - In general KPML=0 if KP=1  
                   KPML=1 if KP=2, etc.

This causes the time parameter used in ENTRY CLAY to be set to zero and STRT to be initialized to PHI. However, for continuation of a previous pumping period KPML=KP, and STRT and the time parameter are not affected.

	21-30	G10.0	* <u>KPER</u>	Number of time periods in this pumping period (for example, number of months in a pumping period).
	31-40	G10.0	* <u>KNUM</u>	Number of the present time period.
	41-50	G10.0	<u>TMAX</u>	Number of days in this time period.
	51-60	G10.0	<u>NUMT</u>	Number of time steps in this time period.
	61-70	G10.0	<u>CDLT</u>	Multiplying factor for DELT.

NOTE - 1.5 is commonly used.

	71-80	G10.0	<u>DELT</u>	Initial time step in hours.
2	1-10	G10.0	* <u>TPUMP</u>	Number of days in this pumping period.
	11-20	G10.0	NWEL	Number of wells for this time period.
	21-30	G10.0	QET	Maximum evapotranspiration rate for this time period (L/T).
	31-40	G10.0	ETDIST	Depth at which evapotranspiration ceases below land surface (L).
	41-50	T10.0	*FACTQ	Multiplication factor for recharge matrix.

NOTE - The recharge rate from the previous time period is multiplied by FACTQ. If the present recharge rate is some factor of the previous recharge rate, assign the appropriate factor for FACTQ; otherwise FACTQ=1).

DATA SET 2. (NSEG cards)

	COLUMNS	FORMAT	VARIABLE	DEFINITION
	1-10	G10.0	*K	Surface water segment number.
	11-20	G10.0	*WIDE(K)	Width of the stream channel (L), (WIDE(K)=0 for a pond segment).
	21-30	G10.0	*SLOPE(K)	Slope of the stream channel bottom (dimensionless) (SLOPE(K)=0 for a pond segment).
	31-40	G10.0	*ROUGH(K)	Manning's roughness coefficient for the stream segment (dimensionless) (ROUGH (K)=0 for a pond segment).
	41-50	G10.0	*FLOWIN(K)	Inflow to a segment (for a stream segment, inflow to the first upstream node) ( $L^3/T$ ).
	51-60	G10.0	*IFLOUT(K)	The segment number to which segment K empties (IFLOUT(K)=0 if the surface water segment does not discharge into another surface water segment)
CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
1	1-10	G10.0	*RAIN	Rainfall to a surface water segment, if pond ( $L/T$ ).
	11-20	G10.0	*PANEVA	Evaporation rate from a pond surface ( $L/T$ ).

---

If NEWQ=NO the following set of cards is to be omitted. When used, a parameter card is required for the data set (see definition of variables for the parameter card in Group III data).

---

DATA SET 3.

	COLUMNS	FORMAT	VARIABLE	DEFINITION
	1-80	20F4.0	QRE(I,J)	Recharge rate ( $L/T$ ).

---

NOTE: (1) For each additional time period, another set of Group IV cards is required (that is, KPER sets of Group IV cards are required).

(2) For each additional pumping period, another KPER set of Group IV cards are required (that is, NPER x KPER sets of Group IV cards are required for the total simulation period).

(3) If another simulation is included in the same job, insert a blank card before the next Group I cards.

CARD	COLUMNS	FORMAT	VARIABLE	DEFINITION
3	1-5	A4,1X	*NEWW	<u>YES</u> to read new pumping rates for this time period; <u>NO</u> to use previous pumping rates.

NOTE - For the start of a simulation, code YES for NEWW to read the pumping rates; code NO for a problem with no pumping. For continuation, code NO for NEWW to use the pumping rates from previous time period; when YES is coded, the matrix WELL(I,J) is initialized to zero and new pumping rates are read for the time period.

6-10	A4,1X	*NEWQ	<u>YES</u> to read new recharge rate for the time period; <u>NO</u> to use the recharge rate from previous time period.
------	-------	-------	---

NOTE - For the start of a simulation, code YES for NEWQ to read a constant recharge rate; code NO for a problem with no constant recharge. For continuation, code NO for NEWQ to use the recharge rate from previous time period; recharge rate from previous time period will be multiplied by FACTQ. When YES is coded for continuation of a problem, the matrix QRE(I,J) is initialized to zero and new recharge rate is read for the present time period.

If NEWW=NO, or for the start of a simulation NWEL=0, the following set of cards is omitted.

---

DATA SET 1. (NWEL cards)

COLUMNS	FORMAT	VARIABLE	DEFINITION
1-10	G10.0	I	Row location of well.
11-20	G10.0	J	Column location of well.
21-30	G10.0	WELL(I,J)	Pumping rate ( $L^3/T$ ); negative for a pumping, positive for a recharge well.
31-40	G10.0	RADIUS	Real well radius (L).

NOTE - Radius is required only for those wells, if any, where computation of drawdown at a real well radius is to be made.

---

For problems without surface water option, the following set of cards is omitted.

---



**\*\*\*\*\***

**GROUP I**

WATE LEAK NCON EVAP RECH SIP    CHEC PUNC NDK1 NDK2 NNUM HEAD CALC

11	15	0	100	2
----	----	---	-----	---

**GROUP 11**

1	100	0.001	0.001	0.02	0.5	10
1.0	1.0					

-----  
 STRT  
 S  
 PERM  
 BOTTOM  
 Sy  
 RATE

```

52.0
0.0
0.002900
0.0
0.2
2.3140E-07
1
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 050.050.050.050.050.0 0 0 0 0 0 0 0 0
0 0 050.050.050.050.050.0 0 0 0 0 0 0 0 0
0 0 050.050.050.050.050.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
0 0 050.050.050.050.050.0 0 0 0 0 0 0 0 0
0 0 050.050.050.050.050.0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

```

RIVER  
I  
V  
E  
R

[illegible]

**GROUP III**

**M  
A  
T  
R  
I  
X  
M**

[illegible]

RSEG  
S  
E  
G  
  
M  
A  
T

		1.0			1										
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	1.3	1.3	1.3	1.3	1.3	0	0	0	0	0	0	0	0
0	0	0	1.3	1.3	1.3	1.3	1.3	0	0	0	0	0	0	0	0
0	0	0	1.3	1.3	1.3	1.3	1.3	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
0	0	0	1.3	1.3	1.3	1.3	1.3	0	0	0	0	0	0	0	0

OUP III	R	0	0	0	1.3	1.3	1.3	1.3	1.3	0	0	0	0	0	0	0
	I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	X	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	GRND	1.0				1										
	R	58	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	N	58	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	D	58	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	M	58	58	58	40	40	40	40	40	58	58	58	58	58	58	58
	A	58	58	58	40	40	40	40	40	58	58	58	58	58	58	58
	T	58	58	58	40	40	40	40	40	51	51	51	51	51	51	51
OUP IV	R	58	58	58	40	40	40	40	40	58	58	58	58	58	58	58
	I	58	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	X	58	58	58	58	58	58	58	58	58	58	58	58	58	58	58
		58	58	58	58	58	58	58	58	58	58	58	58	58	58	58
	DELX	1000.0				1										
	DELY	1.0				1										
		500.				500.										
		1000.				500.										
		1				0										
		1095.0				16.2226E-09										
	YES	YES														
		5				8										
		1				1.0										
		2				20.0										
		0.				0.										
		8.7428E-08														
		1				1										
		1095.0				16.8893E-09										
	NO	YES														
		1				20.0										
		2				20.0										
		0.				0.										
		9.5162E-08														
		1				1										
		1095.0				19.3339E-09										
	NO	YES														
		1				20.0										
		2				20.0										
		0.				0.										
		1.4872E-07														
		1				1										
		1095.0				15.4655E-08										
	NO	YES														
		1				20.0										
		2				20.0										
		0.				0.										
		3.3436E-08														
		1				1										
		1095.0				19.8006E-08										
	NO	YES														
		1				20.0										
		2				20.0										
		0.				0.										
		6.4300E-10														
		1				1										
		1095.0				11.3825E-07										
	NO	YES														
		1				20.0										

	2	20.0	0.001	0.035	0.0	0		
	0.	0						
2. 4434E-08								
	1	1	36	7	31.	1	1.0	744.0
1095.0		11.6179E-07		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
1. 5557E-09								
	1	1	36	8	31.	1	1.0	744.0
1095.0		11.5557E-07		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
8. 0894E-09								
	1	1	36	9	30.	1	1.0	720.0
1095.0		11.1253E-07		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
2. 2184E-08								
	1	1	36	10	31.	1	1.0	744.0
1095.0		16.2226E-08		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
1. 0000E-07								
	1	1	36	11	30.	1	1.0	720.0
1095.0		13.2150E-08		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
1. 0000E-07								
	1	1	36	12	31.	1	1.0	744.0
1095.0		17.7783E-09		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
5. 5070E-08								
	1	1	36	13	31.	1	1.0	744.0
1095.0		16.2226E-09		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
8. 7428E-08								
	1	1	36	14	28.	1	1.0	672.0
1095.0		16.8893E-09		5.0	1.0			
NO YES								
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
9. 5162E-08								
	1	1	36	15	31.	1	1.0	744.0

	1095.0		19.3339E-09	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	1.4872E-07						
	1	1	36	16	30.	1	1.0 .720.0
	1095.0		15.4655E-08	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	3.3436E-08						
	1	1	36	17	31.	1	1.0 744.0
	1095.0		19.8006E-08	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	6.4300E-10						
	1	1	36	18	30.	1	1.0 720.0
	1095.0		11.3825E-07	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	2.4434E-08						
	1	1	36	19	31.	1	1.0 744.0
	1095.0		11.6179E-07	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	1.5557E-09						
	1	1	36	20	31.	1	1.0 744.0
	1095.0		11.5557E-07	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	8.0894E-09						
	1	1	36	21	30.	1	1.0 720.0
	1095.0		11.1253E-07	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	2.2184E-08						
	1	1	36	22	31.	1	1.0 744.0
	1095.0		16.2226E-08	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	
	0.	0.					
	1.0000E-07						
	1	1	36	23	30.	1	1.0 720.0
	1095.0		13.2150E-08	5.0	1.0		
NO	YES						
	1	20.0	0.001	0.035	0.0	2	
	2	20.0	0.001	0.035	0.0	0	

0.	0.						
1. 0000E-07							
1	1	36	24	31.	1	1.0	744.0
1095.0	17. 7783E-09		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
5. 5070E-08							
1	1	36	25	31.	1	1.0	744.0
1095.0	16. 2224E-09		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
8. 7428E-08							
1	1	36	26	28.	1	1.0	672.0
1095.0	16. 8893E-09		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
9. 5162E-08							
1	1	36	27	31.	1	1.0	744.0
1095.0	19. 3339E-09		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
1. 4872E-07							
1	1	36	28	30.	1	1.0	720.0
1095.0	15. 4655E-08		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
3. 3436E-08							
1	1	36	29	31.	1	1.0	744.0
1095.0	19. 8006E-08		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
6. 4300E-10							
1	1	36	30	30.	1	1.0	720.0
1095.0	11. 3825E-07		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
2. 4434E-08							
1	1	36	31	31.	1	1.0	744.0
1095.0	11. 6179E-07		5.0	1.0			
NO YES							
1	20.0	0.001	0.035	0.0	2		
2	20.0	0.001	0.035	0.0	0		
0.	0.						
1. 5557E-09							
1	1	36	32	31.	1	1.0	744.0
1095.0	11. 5557E-07		5.0	1.0			

NO	YES							
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
8.0894E-09								
	1	1	36	33	30.	1	1.0	720.0
	1095.0	11.1253E-07		5.0	1.0			
NO	YES							
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
2.2184E-08								
	1	1	36	34	31.	1	1.0	744.0
	1095.0	16.2226E-08		5.0	1.0			
NO	YES							
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
1.0000E-07								
	1	1	36	35	30.	1	1.0	720.0
	1095.0	13.2150E-08		5.0	1.0			
NO	YES							
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
1.0000E-07								
	1	1	36	36	31.	1	1.0	744.0
	1095.0	17.7783E-09		5.0	1.0			
NO	YES							
	1	20.0	0.001	0.035	0.0	2		
	2	20.0	0.001	0.035	0.0	0		
	0.	0.						
5.5070E-08								
//								

Table 5.--Program listing of computer source code.

```

C *****MAN 10
C FINITE-DIFFERENCE MODEL MAN 20
C FOR MAN 30
C SIMULATION OF GROUND-WATER FLOW MAN 40
C IN TWO DIMENSIONS MAN 50
C BY P. C. TRESCOTT, G. F. PINDER AND S. P. LARSON MAN 60
C U. S. GEOLOGICAL SURVEY MAN 70
C SEPTEMBER, 1975 MAN 80
C MODIFIED BY MELIH M. OZBILGIN MAN 90
C SEPTEMBER, 1982 N 901-
C N 902-
C N 903-
C *****MAN 100
C MAIN PROGRAM TO DIMENSION DIGITAL MODEL AND CONTROL SEQUENCE MAN 110
C OF COMPUTATIONS MAN 120
C -----MAN 130
C SPECIFICATIONS: MAN 140
C REAL *4KEEP, M, HEADNG(32) MAN 150
C REAL *8PHI, G, BE, TEMP, Z, YY MAN 160
C INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, MAN 170
C 1CONTR, LEAK, RECH, SIP, ADI, NEWW, NEWG, RCAL N 1800-
C MAN 190
C DIMENSION Y(70000), L(49), IFMT1(9), IFMT2(9), IFMT3(9), NAME(108) N 2000-
C 1, YY(1) N 2100-
C EQUIVALENCE (YY(1),Y(1)) MAN 220
C MAN 230
C COMMON /SARRAY/ VF4(11), CHK(17) N 2400-
C COMMON /MPARAM/ FACTG, NEWW, NEWG, ERLEAK, DAYS N 2401-
C COMMON /ARSIZE/ IZ, JZ, IP, JP, IR, JR, IC, JC, IL, JL, IS, JS, IH, IMAX, IMX1, IN 2500-
C 1K, IA, JA N 2501-
C COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, ERDR, LEMAN 260
C 1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, MAN 270
C 2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETGB, ETGD, FACTX, FACTY, MAN 280
C 3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DIMAN 290
C 4MW, JND1, INO1, R, P, PU, I, J, IDK1, IDK2, NSEQ, RCAL N 3000-
C COMMON /CK/ ETFLXT, STORT, QRET, CHST, CHDT, FLUXT, PUMPT, CFLUXT, FLXNT, IN 3001-
C 1RCHK, RAIN, PANEVA, IRCHK1 N 3002-
C MAN 310
C DATA IFMT1/4H(1H0, 4H, I5, , 4H10E1, 4H1. 3/, 4H(1H , 4H, 5X, , 4H10E1, 4H1. 3)MAN 320
C 1, 4H) / MAN 330
C DATA IFMT2/4H('O', 4H, I2, , 4H2X, 2, 4HOF6. , 4H1/(5, 4HX, 20, 4HF6. 1, 4H)) MAN 340
C 1, 4H / MAN 350
C DATA IFMT3/4H(1H0, 4H, I5, , 4H14F9, 4H, 5/(, 4H1H , , 4H5X, 1, 4H4F9. , 4H5)) MAN 360
C 1, 4H / MAN 370
C DATA NAME/2*4H , 4H STD, 4HRAQE, 4H COE, 4HFFIC, 4HIENT, 4*4H , 4H MAN 380
C 1 T, 4HRANS, 4HMISS, 4HIVIT, 4HY , 2*4H , 4H A, 4HGUIF, 4HER H, 4HYDMAN 390
C 2RA, 4HULIC, 4H CON, 4HDUCT, 4HIVIT, 4HY , 4H , 4H A, 4HGUIF, 4HER B, MAN 400
C 34HASE , 4HELEV, 4HATIO, 4HN , 3*4H , 4H S, 4HPECI, 4HFIC , 4HYIEL, 4MAN 410
C 4HD , 4*4H , 4HAGUI, 4HFER , 4HTOP , 4HELEV, 4HATIO, 4HN , 4H , 4HMAN 420
C 5CONF, 4HININ, 4HG BE, 4HD HY, 4HDRAU, 4HLIC , 4HCOND, 4HUCTI, 4HVITY, 3*4H MAN 430
C 6 , 4H RIV, 4HER H, 4HEAD , 4*4H , 4H C, 4HONFI, 4HNING, 4H BED, 4H TMAN 440
C 7HI, 4HCKNE, 4HSS , 2*4H , 4H L, 4HAND , 4HSURF, 4HACE , 4HELEV, 4HATIMAN 450
C 8D, 4HN , 3*4H , 4H ARE, 4HAL R, 4HECHA, 4HRGE , 4HRATE, 3*4H , 4H N 4600-
C 9RI, 4HVER , 4HNODE, 4H IDE, 4HNTIF, 4HICAT, 4HION , 4H / N 4601-
C MAN 470
C DEFINE FILE 2(15, 2624, U, KKK) N 4800-
C ..... MAN 490
C ..... MAN 500
C ---READ TITLE, PROGRAM OPTIONS AND PROGRAM SIZE--- MAN 510

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10	READ (R, 370) HEADNG	MAN 520
	WRITE (P, 360) HEADNG	MAN 530
	READ (R, 380) WATER, LEAK, CONVRT, EVAP, RECH, NUMS, CHCK, PNCH, IDK1, IDK2,	MAN 540
	1NUM, HEAD, RCAL	N 5500-
	WRITE (P, 390) WATER, LEAK, CONVRT, EVAP, RECH, NUMS, CHCK, PNCH, IDK1, IDK2	MAN 560
	1, NUM, HEAD, RCAL	N 5700-
	IF (NUMS. EQ. CHK(11). OR. NUMS. EQ. CHK(12). OR. NUMS. EQ. CHK(13)) GO TO 2	MAN 580
	10	MAN 590
	WRITE (P, 350)	MAN 600
	STOP	MAN 610
20	READ (R, 320) DIML, DIMW, NW, ITMAX, NSEG	N 6200-
	WRITE (P, 340) DIML, DIMW, NW, ITMAX, NSEG	N 6300-
C		MAN 640
C	---COMPUTE DIMENSIONS FOR ARRAYS---	MAN 650
	IZ=DIML	MAN 660
	JZ=DIMW	MAN 670
	INSEG=NSEG	N 6701-
	IF (NSEG. EQ. 0) INSEG=1	N 6702-
	IH=MAX0(1, NW)	MAN 680
	IMAX=MAX0(DIML, DIMW)	MAN 690
	ISIZ=DIML*DIMW	MAN 700
	ISUM=2*ISIZ+1	MAN 710
	IMX1=ITMAX+1	MAN 720
	L(1)=1	MAN 730
	DO 30 I=2, 4	MAN 740
	L(I)=ISUM	MAN 750
30	ISUM=ISUM+2*IMAX	MAN 760
	DO 40 I=5, 16	MAN 770
	L(I)=ISUM	MAN 780
40	ISUM=ISUM+ISIZ	MAN 790
	IF (WATER. NE. CHK(2)) GO TO 60	MAN 800
	DO 50 I=17, 19	MAN 810
	L(I)=ISUM	MAN 820
50	ISUM=ISUM+ISIZ	MAN 830
	IP=DIML	MAN 840
	JP=DIMW	MAN 850
	GO TO 80	MAN 860
60	DO 70 I=17, 19	MAN 870
	L(I)=ISUM	MAN 880
70	ISUM=ISUM+1	MAN 890
	IP=1	MAN 900
	JP=1	MAN 910
80	IF (LEAK. NE. CHK(9)) GO TO 100	MAN 920
	DO 90 I=20, 22	MAN 930
	L(I)=ISUM	MAN 940
90	ISUM=ISUM+ISIZ	MAN 950
	IR=DIML	MAN 960
	JR=DIMW	MAN 970
	GO TO 120	MAN 980
100	DO 110 I=20, 22	MAN 990
	L(I)=ISUM	MAN1000
110	ISUM=ISUM+1	MAN1010
	IR=1	MAN1020
	JR=1	MAN1030
120	IF (CONVRT. NE. CHK(7)) GO TO 130	MAN1040
	L(23)=ISUM	MAN1050
	ISUM=ISUM+ISIZ	MAN1060
	IC=DIML	MAN1070
	JC=DIMW	MAN1080
	GO TO 140	MAN1090



130	L(23)=ISUM	MAN1100
	ISUM=ISUM+1	MAN1110
	IC=1	MAN1120
	JC=1	MAN1130
140	IF (EVAP. NE. CHK(6). AND. RCAL. NE. CHK(17)) GO TO 150	N11400-
	L(24)=ISUM	MAN1150
	ISUM=ISUM+ISIZ	MAN1160
	IL=DIML	MAN1170
	JL=DIMW	MAN1180
	GO TO 160	MAN1190
150	L(24)=ISUM	MAN1200
	ISUM=ISUM+1	MAN1210
	IL=1	MAN1220
	JL=1	MAN1230
160	IF (NUMS. NE. CHK(11)) GO TO 180	MAN1240
	DO 170 I=25, 28	MAN1250
	L(I)=ISUM	MAN1260
170	ISUM=ISUM+ISIZ	MAN1270
	IS=DIML	MAN1280
	JS=DIMW	MAN1290
	GO TO 200	MAN1300
180	DO 190 I=25, 28	MAN1310
	L(I)=ISUM	MAN1320
190	ISUM=ISUM+1	MAN1330
	IS=1	MAN1340
	JS=1	MAN1350
200	DO 210 I=29, 31	MAN1360
	L(I)=ISUM	MAN1370
210	ISUM=ISUM+DIMW	MAN1380
	DO 220 I=32, 33	MAN1390
	L(I)=ISUM	MAN1400
220	ISUM=ISUM+DIML	MAN1410
	L(34)=ISUM	MAN1420
	ISUM=ISUM+IH	MAN1430
	L(35)=ISUM	MAN1440
	ISUM=ISUM+2*IH	MAN1450
	IF (MOD(ISUM, 2). EQ. 0) ISUM=ISUM+1	MAN1460
	CONTINUE	MAN1470
230	L(36)=ISUM	MAN1480
	ISUM=ISUM+2*IMAX	MAN1490
	L(37)=ISUM	MAN1500
	ISUM=ISUM+IMX1	MAN1510
	IF (LEAK. NE. CHK(9)) GO TO 235	N15101-
	DO 231 I=38, 40	N15102-
	L(I)=ISUM	N15103-
231	ISUM=ISUM+ISIZ	N15104-
	IF (RCAL. NE. CHK(17)) GO TO 233	N15105-
	L(41)=ISUM	N15106-
	ISUM=ISUM+ISIZ	N15107-
	L(42)=ISUM	N15108-
	ISUM=ISUM+ISIZ	N15109-
	IA=DIML	N15110-
	JA=DIMW	N15111-
	DO 232 I=43, 49	N15112-
	L(I)=ISUM	N15113-
232	ISUM=ISUM+INSEG	N15114-
	IK=INSEG	N15115-
	GO TO 237	N15116-
233	DO 234 I=41, 49	N15117-
	L(I)=ISUM	N15118-

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234 ISUM=ISUM+1                                N15119-
      IK=1                                      N15120-
      IA=1                                      N15121-
      JA=1                                      N15122-
      GO TO 237                                N15123-
235 DO 236 I=38,49                            N15124-
      L(I)=ISUM                                N15125-
236 ISUM=ISUM+1                                N15126-
      IK=1                                      N15127-
      IA=1                                      N15128-
      JA=1                                      N15129-
237 ISUM=ISUM+1                                N15130-
      WRITE (P,330) ISUM                      MAN1520
C                                              MAN1530
C      ---PASS INTIIAL ADDRESSES OF ARRAYS TO SUBROUTINES---    MAN1540
      CALL DATAI(Y(L(1)),Y(L(7)),Y(L(8)),Y(L(9)),Y(L(10)),Y(L(11)),Y(L(12)),Y(L(13)),Y(L(14)),Y(L(15)),Y(L(16)),Y(L(17)),Y(L(18)),Y(L(19)),Y(L(20)),Y(L(21)),Y(L(22)),Y(L(23)),Y(L(24)),Y(L(29)),Y(L(32)),Y(L(34)),Y(L(35)),Y(L(38)),Y(L(39)),Y(L(40)),Y(L(44)),Y(L(45)),Y(L(46)),Y(L(47)),Y(L(48))) MAN1550
      CALL STEP(Y(L(1)),Y(L(5)),Y(L(7)),Y(L(8)),Y(L(9)),Y(L(14)),Y(L(17)),Y(L(18)),Y(L(23)),Y(L(29)),Y(L(30)),Y(L(32)),Y(L(34)),Y(L(35)),Y(L(37)),Y(L(13)),Y(L(38)),Y(L(42))) MAN1560
      IF (NUMS.EQ.CHK(11)) CALL SOLVE1(Y(L(1)),Y(L(2)),Y(L(3)),Y(L(4)),Y(L(5)),Y(L(6)),Y(L(7)),Y(L(9)),Y(L(12)),Y(L(13)),Y(L(14)),Y(L(15)),Y(L(16)),Y(L(25)),Y(L(26)),Y(L(27)),Y(L(28)),Y(L(29)),Y(L(31)),Y(L(32)),Y(L(33)),Y(L(37)),Y(L(10)),Y(L(11)),Y(L(24)),Y(L(19)),Y(L(20)),Y(L(22)),Y(L(21))) MAN1570
      IF (NUMS.EQ.CHK(12)) CALL SOLVE2(Y(L(1)),Y(L(2)),Y(L(3)),Y(L(4)),Y(L(5)),Y(L(6)),Y(L(7)),Y(L(9)),Y(L(12)),Y(L(13)),Y(L(14)),Y(L(15)),Y(L(16)),Y(L(25)),Y(L(26)),Y(L(27)),Y(L(28)),Y(L(29)),Y(L(31)),Y(L(32)),Y(L(33)),Y(L(37)),Y(L(10)),Y(L(11)),Y(L(24)),Y(L(19)),Y(L(20)),Y(L(22)),Y(L(21))) MAN1600
      IF (NUMS.EQ.CHK(13)) CALL SOLVE3(Y(L(1)),Y(L(2)),Y(L(3)),Y(L(4)),Y(L(5)),Y(L(6)),Y(L(7)),Y(L(9)),Y(L(12)),Y(L(13)),Y(L(14)),Y(L(15)),Y(L(16)),Y(L(25)),Y(L(26)),Y(L(27)),Y(L(28)),Y(L(29)),Y(L(31)),Y(L(32)),Y(L(33)),Y(L(36)),Y(L(37)),Y(L(10)),Y(L(11)),Y(L(24)),Y(L(19)),Y(L(20)),Y(L(22)),Y(L(21))) MAN1620
      CALL COEF(Y(L(1)),Y(L(5)),Y(L(6)),Y(L(7)),Y(L(8)),Y(L(9)),Y(L(10)),Y(L(11)),Y(L(12)),Y(L(14)),Y(L(15)),Y(L(16)),Y(L(17)),Y(L(18)),Y(L(19)),Y(L(20)),Y(L(21)),Y(L(22)),Y(L(23)),Y(L(24)),Y(L(29)),Y(L(32)),Y(L(40)),Y(L(41)),Y(L(43))) MAN1630
      CALL CHECKI(Y(L(1)),Y(L(5)),Y(L(6)),Y(L(7)),Y(L(9)),Y(L(10)),Y(L(11)),Y(L(12)),Y(L(13)),Y(L(14)),Y(L(15)),Y(L(17)),Y(L(18)),Y(L(19)),Y(L(20)),Y(L(21)),Y(L(22)),Y(L(23)),Y(L(24)),Y(L(29)),Y(L(32)),Y(L(38)),Y(L(39)),Y(L(40)),Y(L(41)),Y(L(43)),Y(L(44)),Y(L(45)),Y(L(46)),Y(L(47)),Y(L(48)),Y(L(42)),Y(L(16)),Y(L(49))) MAN1640
      CALL PRNTAI(Y(L(1)),Y(L(8)),Y(L(9)),Y(L(12)),Y(L(14)),Y(L(29)),Y(L(32))) MAN1650
C                                              MAN1660
C      ..... MAN1670
C      ---START COMPUTATIONS--- MAN1680
C      ***** MAN1690
C      ---READ AND WRITE DATA FOR GROUPS II AND III--- MAN1700
      CALL DATAIN MAN1710
      CALL ARRAY(Y(L(12)),IFMT3,NAME(1),2) MAN1720
      IF (WATER.EQ.CHK(2)) GO TO 240 MAN1730
      CALL ARRAY(Y(L(9)),IFMT3,NAME(10),3) MAN1740
      GO TO 250 MAN1750
240 CALL ARRAY(Y(L(17)),IFMT1,NAME(19),4) MAN1760

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	CALL ARRAY(Y(L(18)), IFMT2, NAME(28), 5)	MAN1970
	CALL ARRAY(Y(L(19)), IFMT3, NAME(37), 6)	MAN1980
250	IF (CONVRT. EQ. CHK(7)) CALL ARRAY(Y(L(23)), IFMT2, NAME(46), 7)	MAN1990
	IF (LEAK. NE. CHK(9)) GO TO 260	MAN2000
	CALL ARRAY(Y(L(20)), IFMT1, NAME(55), 8)	MAN2010
	CALL ARRAY(Y(L(21)), IFMT2, NAME(64), 9)	MAN2020
	CALL ARRAY(Y(L(22)), IFMT2, NAME(73), 10)	MAN2030
	CALL ARRAY(Y(L(40)), IFMT2, NAME(100), 15)	N20301-
260	IF (EVAP. EQ. CHK(6). OR. RCAL. EQ. CHK(17)) CALL ARRAY(Y(L(24)), IFMT2, NAME(82), 11)	NN20400-
	NAME(82), 11)	N20401-
C	IF (RECH. EQ. CHK(10)) CALL ARRAY(Y(L(13)), IFMT1, NAME(91), 12)	MAN2050
	CALL MDAT	MAN2060
C		MAN2070
C	---INITIALIZE TRANSMISSIVITY VALUES IN WATER TABLE PROBLEM---	MAN2080
	KT=0	MAN2090
	IF (WATER. EQ. CHK(2)) CALL TRANS	MAN2100
C		MAN2110
C	---COMPUTE ITERATION PARAMETERS---	MAN2120
	IF (NUMS. EQ. CHK(11)) CALL ITER1	MAN2130
	IF (NUMS. EQ. CHK(12)) CALL ITER2	MAN2140
	IF (NUMS. EQ. CHK(13)) CALL ITER3	MAN2150
C		MAN2160
C	---INITIALIZE PARAMETERS FOR ALPHAMERIC MAP---	MAN2170
	IF (CONTR. EQ. CHK(3)) CALL MAP	MAN2180
C		MAN2190
C	---COMPUTE T COEFFICIENTS FOR ARTESIAN PROBLEM---	MAN2200
	IF (WATER. NE. CHK(2)) CALL TCOF	MAN2210
C		MAN2220
C	---READ TIME PARAMETERS AND PUMPING DATA FOR A NEW PUMPING PERIOD---	MAN2230
	IF (RCAL. EQ. CHK(17)) CALL RSORT	N22301-
270	CALL NEWPER	MAN2240
C		MAN2250
	KT=0	MAN2260
	IFINAL=0	MAN2270
	IERR=0	MAN2280
	IF (RECH. NE. CHK(10)) GO TO 280	N22801-
	IF (NEWQ. EQ. CHK(16)) CALL ARRAY(Y(L(13)), IFMT1, NAME(91), 12)	N22802-
C		MAN2290
C	---START NEW TIME STEP COMPUTATIONS---	MAN2300
280	CALL NEWSTP	MAN2310
	IRCHK1=1	N23101-
	IRCHK=1	N23102-
	IF (RCAL. EQ. CHK(17)) IRCHK=0	N23103-
	IF (RCAL. EQ. CHK(17)) IRCHK1=0	N23104-
	IF (RCAL. EQ. CHK(17)) CALL HRIVER	N23105-
C		MAN2320
C	---COMPUTE TRANSIENT PART OF LEAKAGE TERM---	MAN2330
282	IF (LEAK. EQ. CHK(9). AND. SS. NE. O. ) CALL CLAY	MAN2340
C		MAN2350
C	---ENTER APPROPRIATE SOLUTION ROUTINE AND COMPUTE SOLUTION---	MAN2360
	IF (NUMS. EQ. CHK(11)) CALL NEWITA	MAN2370
	IF (NUMS. EQ. CHK(12)) CALL NEWITB	MAN2380
	IF (NUMS. EQ. CHK(13)) CALL NEWITC	MAN2390
C		N23901-
C	---CALCULATE RIVER HEADS IF OPTION SPECIFIED---	N23902-
C		N23903-
	IF (RCAL. NE. CHK(17)) GO TO 284	N23904-
	CALL CHECK	N23905-
C	CALL CWRITE	N23906-
	IF (IRCHK. EQ. 1) GO TO 284	N23907-

CALL HRIVER	N23908-
GO TO 282	N23909-
C	MAN2400
C	MAN2410
C	MAN2420
284 CALL STEADY	MAN2430
C	MAN2440
C	MAN2450
C	MAN2460
C	MAN2470
C	MAN2480
C	N24900-
C	MAN2500
C	MAN2510
C	MAN2520
C	MAN2530
C	MAN2540
C	MAN2550
290 IF (PNCH.NE.CHK(1)) GO TO 300	MAN2560
CALL PUNCH	MAN2570
C	MAN2580
C	MAN2590
300 READ (R,320,END=310) NEXT	MAN2600
IF (NEXT.EQ.0) GO TO 10	MAN2610
310 STOP	MAN2620
C	MAN2630
C	MAN2640
C	MAN2650
C	MAN2660
C	MAN2670
C	MAN2680
320 FORMAT (5I10)	N26900-
330 FORMAT ('0',54X,'WORDS OF Y VECTOR USED =',I7)	MAN2700
340 FORMAT ('0',62X,'NUMBER OF ROWS =',I5/60X,'NUMBER OF COLUMNS =',I5/9X,'NUMBER OF WELLS FOR WHICH DRAWDOWN IS COMPUTED AT A SPECIFIED	MAN2710
2 RADIUS =',I5,/,39X,'MAXIMUM PERMITTED NUMBER OF ITERATIONS =',I5,N27300-	
3/,43X,'NUMBER OF RIVER SEGMENTS SPECIFIED =',I5)	N27301-
350 FORMAT ('-',36X,'NO EQUATION SOLVING SCHEME SPECIFIED, EXECUTION T	MAN2740
1ERMINATED'/37X,58('*'))	MAN2750
360 FORMAT ('1',60X,'U. S. G. S. '//55X,'FINITE-DIFFERENCE MODEL '//65X,'	MAN2760
1FOR '//51X,'SIMULATION OF GROUND-WATER FLOW '//60X,'JANUARY, 1975 '//4N27700-	
28X,'MODIFIED BY MELIH M. OZBILGIN, PH. D. ',//59X,'DECEMBER, 1982',	N27800-
3//133('*'))/'0',32A4//133('*'))	N27801-
370 FORMAT (20A4)	MAN2790
380 FORMAT (16(A4,1X))	MAN2800
390 FORMAT ('-SIMULATION OPTIONS: ',13(A4,4X))	MAN2810
END	MAN2820-

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SUBROUTINE DATAI(PHI, STRT, SUR1, T, TR, TC, S, GRE, WELL, TL, SL, PERM, BOTTDAT 10
1M, SY, RATE, RIVER, M, TOP, GRND, DELX, DELY, WR, NWR, PICK, PICKUP, RSEG, FLOWIT 200-
2N, WIDE, SLOPE, IFLOUT, ROUGH) T 201-
C -----DAT 30
C READ AND WRITE INPUT DATA DAT 40
C -----DAT 50
C SPECIFICATIONS: DAT 60
C REAL *8PHI, DBLE, XLABEL, YLABEL, TITLE, XN1, MESUR DAT 70
C REAL *4M DAT 80
C INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, DAT 100
1CONTR, LEAK, RECH, SIP, ADI, NEWW, NEWQ, RCAL T 1100-
C -----DAT 120
C DIMENSION PHI(IZ, JZ), STRT(IZ, JZ), SUR1(IZ, JZ), T(IZ, JZ), TR(IZ, JZ) DAT 130
1), TC(IZ, JZ), S(IZ, JZ), GRE(IZ, JZ), WELL(IZ, JZ), TL(IZ, JZ), SL(IZ, JZ) DAT 140
2JZ), PERM(IP, JP), BOTTOM(IP, JP), SY(IP, JP), RATE(IR, JR), RIVER(IR, JR) DAT 150
3JR), M(IR, JR), TOP(IC, JC), GRND(IL, JL), DELX(JZ), DELY(JZ), WR(IH) DAT 160
4, NWR(IH, 2), PICK(IR, JR), PICKUP(IR, JR), RSEG(IR, JR), FLOWIN(IK), T 1700-
5WIDE(IK), SLOPE(IK), IFLOUT(IK), ROUGH(IK), A(IZ, JZ), IN(9), IFMT(T 1701-
69) T 1702-
C -----DAT 180
C COMMON /SARRAY/ VF4(11), CHK(17) T 1900-
C COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LEDAT 200
1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, DAT 210
2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETQB, ETQD, FACTX, FACTY, DAT 220
3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DIDAT 230
4MW, JND1, IND1, R, P, PU, I, J, IDK1, IDK2, NSEG, RCAL T 2400-
C COMMON /CK/ ETFLXT, STORT, GRET, CHST, CHDT, FLUXT, PUMPT, CFLUXT, FLXNT, IT 2500-
1RCHK, RAIN, PANEVA, IRCHK1 T 2501-
C COMMON /PR/ XLABEL(3), YLABEL(6), TITLE(5), XN1, MESUR, PRNT(122), BLANKDAT 260
1(60), DIGIT(122), VF1(6), VF2(6), VF3(7), XSCALE, DINCH, SYM(17), XN(100), DAT 270
2YN(13), NA(4), N1, N2, N3, YSCALE, FACT1, FACT2 DAT 280
C COMMON /ARSize/ IZ, JZ, IP, JP, IR, JR, IC, JC, IL, JL, IS, JS, IH, IMAX, IMX1, IT 2900-
1K, IA, JA T 2901-
C COMMON /MPARAM/ FACTQ, NEWW, NEWQ, ERLEAK, DAYS T 2902-
C RETURN DAT 300
C ..... DAT 310
C ***** DAT 320
C ENTRY DATAIN DAT 330
C ***** DAT 340
C ..... DAT 350
C ---READ AND WRITE SCALAR PARAMETERS--- DAT 360
C READ (R, 500) CONTR, XSCALE, YSCALE, DINCH, FACT1, FACT2, MESUR DAT 370
C IF (CONTR.EQ.CHK(3)) WRITE (P, 610) XSCALE, YSCALE, MESUR, MESUR, DINCH DAT 380
1, FACT1, FACT2 DAT 390
C READ (R, 490) NPER, KTH, ERR, EROR, ERLEAK, SS, LENGTH, HMAX, FACTX, FACTY T 4000-
C WRITE (P, 520) NPER, KTH, ERR, EROR, ERLEAK, SS, FACTX, FACTY T 4300-
C ..... DAT 440
C ---READ CUMULATIVE MASS BALANCE PARAMETERS--- DAT 450
C READ (R, 600) SUM, SUMP, PUMPT, CFLUXT, GRET, CHST, CHDT, FLUXT, STORT, ETFL DAT 460
1XT, FLXNT DAT 470
C IF (IDK1.EQ.CHK(14)) GO TO 20 DAT 480
C IF (SUM.EQ.0.0) GO TO 40 DAT 490
C WRITE (P, 480) SUM DAT 500
C ..... DAT 510
C ..... DAT 520
C ---HEAD DATA TO CONTINUE PREVIOUS COMPUTATIONS READ HERE--- DAT 530
C -----FROM CARDS: DAT 540
C DO 10 I=1, DIML DAT 550

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	READ (R,540) (PHI(I,J),J=1,DIMW)	DAT 560
10	WRITE (P,530) I, (PHI(I,J),J=1,DIMW)	DAT 570
	GO TO 40	DAT 580
C	-----READ AND WRITE DATA FROM UNIT 4 ON DISK RATHER THAN CARDS:	DAT 590
20	READ (4) PHI, SUM, SUMP, PUMPT, CFLUXT, GRET, CHST, CHDT, FLUXT, STORT, ETFL	DAT 600
	1XT, FLXNT	DAT 610
	WRITE (P,480) SUM	DAT 620
	DO 30 I=1,DIML	DAT 630
30	WRITE (P,530) I, (PHI(I,J),J=1,DIMW)	DAT 640
	REWIND 4	DAT 650
C	..... STRT (STARTING HEAD) .....	DAT 660
40	READ (R,490) FACT, IVAR, IPRN, IRECS, IRECD	DAT 670
	IF (IRECS.EQ.1) READ (2'1) STRT	DAT 680
	IF ((IVAR.EQ.1.OR. IRECS.EQ.1).AND. IPRN.NE.1) WRITE (P,470)	DAT 690
	DO 80 I=1,DIML	DAT 700
	IF (IVAR.EQ.1) READ (R,540) (STRT(I,J),J=1,DIMW)	DAT 710
	DO 70 J=1,DIMW	DAT 720
	IF (IRECS.EQ.1) GO TO 60	DAT 730
	IF (IVAR.NE.1) GO TO 50	DAT 740
	STRT(I,J)=STRT(I,J)*FACT	DAT 750
	GO TO 60	DAT 760
50	STRT(I,J)=FACT	DAT 770
60	SURI(I,J)=STRT(I,J)	DAT 780
	T(I,J)=0.	DAT 785
	TL(I,J)=0.	DAT 790
	SL(I,J)=0.	DAT 800
	TR(I,J)=0.	DAT 810
	TC(I,J)=0.	DAT 820
	WELL(I,J)=0.0	DAT 830
	PICK(I,J)=0.0	T 8400-
	PICKUP(I,J)=0.0	T 8401-
	GRE(I,J)=0.0	T 8402-
70	IF (SUM.EQ.0.0.AND. IDK1.NE. CHK(14)) PHI(I,J)=STRT(I,J)	DAT 850
	IF (IVAR.EQ.0.AND. IRECS.EQ.0.OR. IPRN.EQ.1) GO TO 80	DAT 860
	WRITE (P,530) I, (STRT(I,J),J=1,DIMW)	DAT 870
80	CONTINUE	DAT 880
	IF (IVAR.NE.1.AND. IRECS.NE.1) WRITE (P,420) FACT	DAT 890
	IF (IRECD.EQ.1) WRITE (2'1) STRT	DAT 900
	RETURN	DAT 910
C		DAT 920
C	---READ REMAINING ARRAYS FROM CARDS OR DISK (AS SPECIFIED IN THE	DAT 930
C	OPTIONS) AND WRITE THEM ON DISK IF SPECIFIED IN THE OPTIONS---	DAT 940
C	*****	DAT 950
	ENTRY ARRAY(A, IFMT, IN, IRN)	DAT 960
C	*****	DAT 970
	READ (R,490) FACT, IVAR, IPRN, IRECS, IRECD	DAT 980
	IB=4*IRECS+2*IVAR+IPRN+1	DAT 990
	GO TO (90,90,110,110,140,140), IB	DAT1000
90	DO 100 I=1,DIML	DAT1010
	DO 100 J=1,DIMW	DAT1020
100	A(I,J)=FACT	DAT1030
	WRITE (P,430) IN, FACT	DAT1040
	GO TO 160	DAT1050
110	IF (IB.EQ.3) WRITE (P,440) IN	DAT1060
	DO 130 I=1,DIML	DAT1070
	READ (R,510) (A(I,J),J=1,DIMW)	DAT1080
	DO 120 J=1,DIMW	DAT1090
120	A(I,J)=A(I,J)*FACT	DAT1100
130	IF (IB.EQ.3) WRITE (P, IFMT) I, (A(I,J),J=1,DIMW)	DAT1110
	GO TO 160	DAT1120

140	READ (2'IRN) A	DAT1130
	IF (IB.EQ.6) GO TO 160	DAT1140
	WRITE (P,440) IN	DAT1150
	DO 150 I=1,DIML	DAT1160
150	WRITE (P,IFMT) I, (A(I,J),J=1,DIMW)	DAT1170
160	IF (IRECD.EQ.1) WRITE (2'IRN) A	DAT1180
	RETURN	DAT1190
C		DAT1200
C	---INSERT ZERO VALUES IN THE T OR PERM MATRIX AROUND THE	DAT1210
C	BORDER OF THE MODEL---	DAT1220
C	*****	DAT1230
	ENTRY MDAT .	DAT1240
C	*****	DAT1250
	DO 180 I=1,DIML	DAT1260
	DO 180 J=1,DIMW	DAT1270
	IF (WATER.EQ.CHK(2)) GO TO 170	DAT1280
	IF (I.EQ.1.OR.I.EQ.DIML.OR.J.EQ.1.OR.J.EQ.DIMW) T(I,J)=0.	DAT1290
	GO TO 180	DAT1300
170	IF (I.EQ.1.OR.I.EQ.DIML.OR.J.EQ.1.OR.J.EQ.DIMW) PERM(I,J)=0.	DAT1310
180	CONTINUE	DAT1320
C	..... DELX,DELY .....	DAT1330
	READ (R,490) FACT,IVAR,IPRN,IRECS,IRECD	DAT1340
	IF (IRECS.EQ.1) GO TO 210	DAT1350
	IF (IVAR.EQ.1) READ (R,490) DELX	DAT1360
	DO 200 J=1,DIMW	DAT1370
	IF (IVAR.NE.1) GO TO 190	DAT1380
	DELX(J)=DELX(J)*FACT	DAT1390
	GO TO 200	DAT1400
190	DELX(J)=FACT	DAT1410
200	CONTINUE	DAT1420
	GO TO 220	DAT1430
210	READ (2'13) DELX	DAT1440
220	IF (IRECD.EQ.1) WRITE (2'13) DELX	DAT1450
	IF (IVAR.EQ.1.OR.IRECS.EQ.1.AND.IPRN.NE.1) WRITE (P,550) DELX	DAT1460
	IF (IVAR.NE.1.AND.IRECS.NE.1) WRITE (P,450) FACT	DAT1470
	READ (R,490) FACT,IVAR,IPRN,IRECS,IRECD	DAT1480
	IF (IRECS.EQ.1) GO TO 250	DAT1490
	IF (IVAR.EQ.1) READ (R,490) DELY	DAT1500
	DO 240 I=1,DIML	DAT1510
	IF (IVAR.NE.1) GO TO 230	DAT1520
	DELY(I)=DELY(I)*FACT	DAT1530
	GO TO 240	DAT1540
230	DELY(I)=FACT	DAT1550
240	CONTINUE	DAT1560
	GO TO 260	DAT1570
250	READ (2'14) DELY	DAT1580
260	IF (IRECD.EQ.1) WRITE (2'14) DELY	DAT1590
	IF (IVAR.EQ.1.OR.IRECS.EQ.1.AND.IPRN.NE.1) WRITE (P,560) DELY	DAT1600
	IF (IVAR.NE.1.AND.IRECS.NE.1) WRITE (P,460) FACT	DAT1610
C		DAT1620
C	---INITIALIZE VARIABLES---	DAT1630
	JND1=DIMW-1	DAT1640
	IND1=DIML-1	DAT1650
	IF (LEAK.NE.CHK(9).OR.SS.NE.0.) GO TO 280	DAT1660
	DO 270 I=2,IND1	DAT1670
	DO 270 J=2,JND1	DAT1680
	IF (M(I,J).EQ.0.) GO TO 270	DAT1690
	TL(I,J)=RATE(I,J)/M(I,J)	DAT1700
270	CONTINUE	DAT1710
280	ETQB=0.0	DAT1720

ETGD=0.0	DAT1730
SUBS=0.0	DAT1740
U=1.0	DAT1750
TT=0.0	DAT1760
IM=MINO(6*DIMW+4,124)	DAT1770
IM=(132-IM)/2	DAT1780
VF4(3)=DIGIT(IM)	DAT1790
VF4(8)=DIGIT(IM+5)	DAT1800
WIDTH=0.	DAT1810
DO 290 J=2,JND1	DAT1820
290 WIDTH=WIDTH+DELX(J)	DAT1830
YDIM=0.	DAT1840
DO 300 I=2,IND1	DAT1850
300 YDIM=YDIM+DELY(I)	DAT1860
RETURN	DAT1870
.....	DAT1880
---	DAT1890
---READ TIME PARAMETERS AND PUMPING DATA FOR A NEW PUMPING PERIOD---	DAT1900
*****	DAT1910
ENTRY NEWPER	DAT1920
*****	DAT1930
READ (R,490) KP,KPM1,KPER,KNUM,TMAX,NUMT,CDLT,DELT	DAT1940
READ (R,490) TPUMP,NWEL,GET,ETDIST,FACTQ	T19500-
IF (ETDIST.LE.0.) ETDIST=1.	T19501-
READ (R,630) NEWW,NEWQ	T19502-
	T19503-
	DAT1960
---	DAT1970
---COMPUTE ACTUAL DELT AND NUMT---	DAT1980
DT=DELT/24.	DAT1990
TM=0.0	DAT2000
DO 310 I=1,NUMT	DAT2010
DT=CDLT*DT	DAT2020
TM=TM+DT	DAT2030
IF (TM.GE.TMAX) GO TO 320	DAT2040
310 CONTINUE	DAT2050
GO TO 330	DAT2060
320 DELT=TM/TMAX*DELT	DAT2070
NUMT=I	T20701-
330 WRITE (P,620) KP,TPUMP,KPER	T20800-
WRITE (P,570) KNUM,TMAX,NUMT,DELT,CDLT,GET,ETDIST,FACTQ	DAT2090
DELT=DELT*3600.	DAT2100
TMAX=TMAX*86400.	T21001-
WRITE (P,640) NEWW,NEWQ	DAT2110
	DAT2120
---	DAT2130
---INITIALIZE SUMP, STRT, SL, WELL AND WR---	DAT2140
WRITE (P,580) NWEL	DAT2150
IF (KP.GT.KPM1) SUMP=0.	DAT2160
DO 350 I=1,DIML	DAT2170
DO 350 J=1,DIMW	DAT2180
IF (KP.EQ.KPM1) GO TO 340	DAT2190
STRT(I,J)=PHI(I,J)	DAT2200
340 IF (LEAK.NE.CHK(9)) GO TO 350	DAT2210
IF (M(I,J).EQ.0.) GO TO 350	T22200-
SL(I,J)=RATE(I,J)/M(I,J)*(RIVER(I,J)-STRT(I,J))	DAT2230
350 IF (NEWW.EQ.CHK(16)) WELL(I,J)=0.	DAT2240
IF (NW.EQ.0) GO TO 370	DAT2250
DO 360 I=1,NW	DAT2260
360 WR(I)=0.	T22601-
370 IF (NWEL.EQ.0) GO TO 410	
IF (NEWW.EQ.CHK(16)) GO TO 374	



DO 372 I=1, DIML	T22602-
DO 372 J=1, DIMW	T22603-
RWELL=WELL(I, J)*DELX(J)*DELY(I)	T22604-
372 IF (WELL(I, J).NE.0.) WRITE (P, 590) I, J, RWELL	T22605-
GO TO 410	T22606-
C	DAT2270
C ---READ AND WRITE WELL PUMPING RATES AND WELL RADII---	DAT2280
374 KW=0	DAT2290
DO 400 II=1, NWEL	DAT2300
READ (R, 490) I, J, WELL(I, J), RADIUS	DAT2310
IF (RADIUS.EQ.0.) GO TO 380	DAT2320
KW=KW+1	DAT2330
IF (KW.GT.NW) GO TO 380	DAT2340
NWR(KW, 1)=I	DAT2350
NWR(KW, 2)=J	DAT2360
WR(KW)=RADIUS	DAT2370
WRITE (P, 590) I, J, WELL(I, J), WR(KW)	DAT2380
GO TO 390	DAT2390
380 WRITE (P, 590) I, J, WELL(I, J)	DAT2400
390 WELL(I, J)=WELL(I, J)/(DELX(J)*DELY(I))	DAT2410
400 CONTINUE	DAT2420
410 CONTINUE	T24201-
C ---READ AND WRITE DATA IF RIVER HEADS TO BE COMPUTED---	T24202-
IF (RCAL.NE.CHK(17)) GO TO 414	T24203-
WRITE (P, 650)	T24204-
DO 412 K=1, NSEQ	T24205-
READ (R, 490) KK, WIDE(KK), SLOPE(KK), ROUGH(KK), FLOWIN(KK), IFLOUT(KK)	T24206-
412 WRITE (P, 660) KK, WIDE(KK), SLOPE(KK), ROUGH(KK), FLOWIN(KK), IFLOUT(KK)	T24207-
1)	T24208-
READ (R, 490) RAIN, PANEVA	T24209-
414 IF (KNUM.EQ.KPER) KP=KP+1	T24210-
RETURN	T24300-
C	DAT2440
C	DAT2450
C FORMATS:	DAT2460
C	DAT2470
C -----	DAT2480
C	DAT2490
C	DAT2500
420 FORMAT ('0', 63X, 'STARTING HEAD =', G15.7)	DAT2510
430 FORMAT ('0', 41X, 9A4, '=', G15.7)	DAT2520
440 FORMAT ('1', 49X, 9A4, '/', 65X, 'MATRIX', '/', 50X, 36('-', ''))	DAT2530
450 FORMAT ('0', 72X, 'DELX =', G15.7)	DAT2540
460 FORMAT ('0', 72X, 'DELY =', G15.7)	DAT2550
470 FORMAT ('1', 60X, 'STARTING HEAD MATRIX'//61X, 20('-', ''))	DAT2560
480 FORMAT ('1', 40X, ' CONTINUATION - HEAD AFTER ', G20.7, ' SEC PUMPING	DAT2570
1'/42X, 58('-', ''))	DAT2580
490 FORMAT (BG10.0)	DAT2590
500 FORMAT (A4, 6X, 5G10.0, AB)	DAT2600
510 FORMAT (20F4.0)	DAT2610
520 FORMAT ('0', 51X, 'NUMBER OF PUMPING PERIODS =', I5/49X, 'TIME STEPS B	DAT2620
ETWEEN PRINTOUTS =', I5//51X, 'ERROR CRITERION FOR CLOSURE =', G15.7/T26300-	
241X, ' STEADY STATE ERROR CRITERION =', G15.7//26X, 'ERROR CRT26400-	
3ITERION TO SATISFY RIVER-AQUIFER INTERACTION =', G15.7//44X, 'SPECIFT26500-	
4IC STORAGE OF CONFINING BED =', G15.7//22X, 'MULTIPLICATION FACTOR T26600-	
5FOR TRANSMISSIVITY IN X DIRECTION =', G15.7/63X, 'IN Y DIRECTION =', T26700-	
6G15.7)	T26800-
530 FORMAT ('0', I2, 2X, 20F6.1/(5X, 20F6.1))	DAT2690
540 FORMAT (8F10.4)	DAT2700
550 FORMAT (1H1, 46X, 40HGRID SPACING IN PROTOTYPE IN X DIRECTION/47X, 40D	DAT2710

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1(' ')/( '0',12F10.0)) DAT2720
560 FORMAT (1H-,46X,40HGRID SPACING IN PROTOTYPE IN Y DIRECTION/47X,40DAT2730
1(' ')/( '0',12F10.0)) DAT2740
570 FORMAT ('-',50X, ' TIME PERIOD NO. ',I4, ': ',F10.2, ' DAYS'/51X,38('T27500-
1-')/53X, 'NUMBER OF TIME STEPS=',I6//59X, 'DELT IN HOURS =',F10.3//DAT2760
253X, 'MULTIPLIER FOR DELT =',F10.3,/,49X, 'EVAPOTRANSPIRATION RATE T27700-
3=',G15.7,/,51X, 'EFFECTIVE DEPTH OF ET =',G15.7,/,31X, 'MULTIPLICATIT27701-
4ON FACTOR FOR RECHARGE MATRIX =',G15.7) - T27702-
580 FORMAT ('-',63X,I4, ' WELLS'/65X,9(' ')/50X, 'I',9X, 'J PUMPING RDATE2780
1ATE WELL RADIUS'/) DAT2790
590 FORMAT (41X,2I10,2F13.3) DAT2800
600 FORMAT (4G20.10) DAT2810
610 FORMAT ('0';30X, 'ON ALPHAMERIC MAP: '/40X, 'MULTIPLICATION FACTOR FODAT2820
1R X DIMENSION =',G15.7/40X, 'MULTIPLICATION FACTOR FOR Y DIMENSION DAT2830
2=',G15.7/55X, 'MAP SCALE IN UNITS OF ',A11/50X, 'NUMBER OF ',A8, ' PDAT2840
3ER INCH =',G15.7/43X, 'MULTIPLICATION FACTOR FOR DRAWDOWN =',G15.7/DAT2850
447X, 'MULTIPLICATION FACTOR FOR HEAD =',G15.7) DAT2860
620 FORMAT (1H1,/,/,24(' ->'), 'PUMPING PERIOD NO. ',I4, ': ',F10.2, ' DAYST28601-
1',/,72X,38(' ')/,81X, 'NUMBER OF TIME PERIODS =',I5,////////) T28602-
630 FORMAT (2(A4,1X)) T28603-
640 FORMAT ('-',/,48X, 'FOR THIS TIME PERIOD -> NEW PUMPING RATES USED T28604-
1?.....',A4,/,69X, '-> NEW AREAL RECHARGE RATE USED ?.....',T28605-
2A4,/) T28606-
650 FORMAT ('-',/,/,10X, 'RIVER SEGMENT',5X, 'AVERAGE WIDTH',5X, 'AVERAGE T28607-
1 SLOPE',5X, 'MANNING COEF. ',5X, 'FLOWIN (L**3/T)',5X, 'DISCHARGE TO ST28608-
2EGMENT',/,10X,4(13(' '),5X),15(' '),5X,20(' ')) T28609-
660 FORMAT ('-',14X,I3,13X,F7.4,3(11X,F7.4),21X,I3) T28610-
END DAT2870-

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SUBROUTINE STEP(PHI, KEEP, STRT, SURI, T, WELL, PERM, BOTTOM, TOP, DELX, DDNSTP 10
1, DELY, WR, NWR, TEST3, GRE, PICK, PREPIC) P 200-
C -----STP 30
C INITIALIZE DATA FOR TIME STEP, CHECK FOR STEADY STATE, STP 40
C PRINT AND PUNCH RESULTS STP 50
C -----STP 60
C STP 70
C SPECIFICATIONS: STP 80
C REAL *8PHI, DBLE, DABS, TEST2, DMAX1, XLABEL, YLABEL, XN1, MESUR, TITLE STP 90
C REAL *4MINS, M, KEEP STP 100
C INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, STP 110
1CONTR, LEAK, RECH, SIP, ADI, NEWW, NEWG, RCAL P 1200-
C STP 130
C DIMENSION PHI(IZ, JZ), KEEP(IZ, JZ), STRT(IZ, JZ), SURI(IZ, JZ), T(IZ, STP 140
1JZ), BOTTOM(IP, JP), WELL(IZ, JZ), PERM(IP, JP), TOP(IC, JC), DELX(JZ) STP 150
2, DDN(JZ), DELY(IZ), WR(IH), NWR(IH, 2), ITTO(200), TEST3(IMX1), GRP 1600-
3E(IZ, JZ), PICK(IR, JR), PREPIC(IA, JA) P 1601-
C STP 170
C COMMON /SARRAY/ VF4(11), CHK(17) P 1800-
C COMMON /MPARAM/ FACTG, NEWW, NEWG, ERLEAK, DAYS P 1801-
C COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LESTP 190
1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, STP 200
2NUMS, LSQR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETQB, ETGD, FACTX, FACTY, STP 210
3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DIST 220
4MW, JNO1, INO1, R, P, PU, I, J, IDK1, IDK2, NSEG, RCAL P 2300-
C COMMON /CK/ ETFLXT, STORT, GRET, CHST, CHDT, FLUXT, PUMPT, CFLUXT, FLXNT, IP 2400-
1RCHK, RAIN, PANEVA, IRCHK1 P 2401-
C COMMON /ARSIZE/ IZ, JZ, IP, JP, IR, JR, IC, JC, IL, JL, IS, JS, IH, IMAX, IMX1, IP 2500-
1K, IA, JA P 2501-
C COMMON /PR/ XLABEL(3), YLABEL(6), TITLE(5), XN1, MESUR, PRNT(122), BLANKSTP 260
1(60), DIGIT(122), VF1(6), VF2(6), VF3(7), XSCALE, DINCH, SYM(17), XN(100), STP 270
2YN(13), NA(4), N1, N2, N3, YSCALE, FACT1, FACT2 STP 280
C STP 290
C DATA PIE/3. 141593/, YYY/Z000000000/ STP 300
C RETURN STP 310
C ..... STP 320
C STP 330
C ---START A NEW TIME STEP--- STP 340
C ***** STP 350
C ENTRY NEWSTP STP 360
C ***** STP 370
C KT=KT+1 STP 380
C KOUNT=0 STP 390
C DO 10 I=1, DIML STP 400
C DO 10 J=1, DIMW STP 410
C GRE(I, J)=GRE(I, J)*FACTG P 4101-
10 KEEP(I, J)=PHI(I, J) STP 420
C DELT=CDLT*DELT STP 430
C SUM=SUM+DELT STP 440
C SUMP=SUMP+DELT STP 450
C DAYSP=SUMP/86400. STP 460
C YRSP=DAYSP/365. STP 470
C HRS=SUM/3600. STP 480
C MINS=HRS*60. STP 490
C DAYS=HRS/24. STP 500
C YRS=DAYS/365. STP 510
C RETURN STP 520
C ..... STP 530
C STP 540

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C	---CHECK FOR STEADY STATE---	STP 550
C	*****	STP 560
	ENTRY STEADY	STP 570
C	*****	STP 580
	TEST2=0.	STP 590
	DO 20 I=2, IND1	STP 600
	DO 20 J=2, JND1	STP 610
20	TEST2=DMAX1(TEST2, DABS(DBLE(KEEP(I, J))-PHI(I, J)))	STP 620
	IF (TEST2. GE. ERROR) GO TO 30	STP 630
	WRITE (P, 330) KT	STP 640
	IFINAL=1	STP 650
	GO TO 40	STP 660
30	IF (KT. EQ. NUMT) IFINAL=1	STP 670
C		STP 680
C	---ENTRY FOR TERMINATING COMPUTATIONS IF MAXIMUM ITERATIONS	STP 690
C	EXCEEDED---	STP 700
C	*****	STP 710
	ENTRY TERM1	STP 720
C	*****	STP 730
40	IF (KT. GT. 200) WRITE (P, 400)	STP 740
	ITTO(KT)=KOUNT	STP 750
	IF (KOUNT. LE. ITMAX) GO TO 80	STP 760
	IERR=2	STP 770
	KOUNT=KOUNT-1	STP 780
	ITTO(KT)=KOUNT	STP 790
	IF (KT. EQ. 1) GO TO 60	STP 800
C		STP 810
C	---WRITE ON DISK OR PUNCH CARDS AS SPECIFIED IN THE OPTIONS---	STP 820
	XXX=SUM-DELT	STP 830
	IF (IDK2. EQ. CHK(15)) WRITE (4) ((KEEP(I, J), YYY, I=1, DIML), J=1, DIMW)	STP 840
	1, XXX, SUMP, PUMPT, CFLTXT, GRET, CHST, CHDT, FLTXT, STORT, ETFLXT, FLXNT	STP 850
	IF (PNCH. NE. CHK(1)) GO TO 80	STP 860
	WRITE (PU, 360) XXX, SUMP, PUMPT, CFLTXT, GRET, CHST, CHDT, FLTXT, STORT, ETSTP	STP 870
	1FLXT, FLXNT	STP 880
	DO 50 I=1, DIML	STP 890
50	WRITE (PU, 350) (KEEP(I, J), J=1, DIMW)	STP 900
	GO TO 80	STP 910
60	IF (IDK2. EQ. CHK(15)) WRITE (4) PHI, SUM, SUMP, PUMPT, CFLTXT, GRET, CHST	STP 920
	1, CHDT, FLTXT, STORT, ETFLXT, FLXNT	STP 930
	IF (PNCH. NE. CHK(1)) GO TO 80	STP 940
	WRITE (PU, 360) SUM, SUMP, PUMPT, CFLTXT, GRET, CHST, CHDT, FLTXT, STORT, ETSTP	STP 950
	1FLXT, FLXNT	STP 960
	DO 70 I=1, DIML	STP 970
70	WRITE (PU, 350) (PHI(I, J), J=1, DIMW)	STP 980
C		STP 990
80	IF (CHCK. EQ. CHK(5)) CALL CHECK	STP1000
	IF (IERR. EQ. 2) GO TO 90	STP1010
C		STP1020
C	---PRINT OUTPUT AT DESIGNATED TIME STEPS---	STP1030
	IF (MOD(KT, KTH). NE. 0. AND. IFINAL. NE. 1) RETURN	STP1040
90	WRITE (P, 340) KT, DELT, SUM, MINS, HRS, DAYS, YRS, DAYSP, YRSP	STP1050
	IF (CHCK. EQ. CHK(5)) CALL CWRITE	STP1060
	IF (TT. NE. 0.) WRITE (P, 320) TMIN, TT	STP1070
	KOUNT=KOUNT+1	STP1080
	WRITE (P, 300) (TEST3(J), J=1, KOUNT)	STP1090
	WRITE (P, 290) TEST2	STP1100
	I3=1	STP1110
	I5=0	STP1120
100	I5=I5+40	STP1130
	I4=MINO(KT, I5)	STP1140

WRITE (P,390) (I,I=I3,I4)	STP1150
WRITE (P,380)	STP1160
WRITE (P,370) (ITTO(I),I=I3,I4)	STP1170
WRITE (P,380)	STP1180
IF (KT.LE.I5) GO TO 110	STP1190
I3=I3+40	STP1200
GO TO 100	STP1210
C	STP1220
C ---PRINT ALPHAMERIC MAPS---	STP1230
110 IF (CONTR.NE.CHK(3)) GO TO 120	STP1240
IF (FACT1.NE.O.) CALL PRNTA(1)	STP1250
IF (FACT2.NE.O.) CALL PRNTA(2)	STP1260
120 IF (HEAD.NE.CHK(8)) GO TO 140	STP1270
C	STP1280
C ---PRINT HEAD MATRIX---	STP1290
WRITE (P,310)	STP1300
DO 130 I=1,DIML	STP1310
130 WRITE (P,VF4) I,(PHI(I,J),J=1,DIMW)	STP1320
140 IF (NUM.NE.CHK(4)) GO TO 170	STP1330
C	STP1340
C ---PRINT DRAWDOWN---	STP1350
WRITE (P,280)	STP1360
C *****	STP1370
ENTRY DRDN	STP1380
C *****	STP1390
DO 160 I=1,DIML	STP1400
DO 150 J=1,DIMW	STP1410
150 DDN(J)=SURI(I,J)-PHI(I,J)	STP1420
160 WRITE (P,VF4) I,(DDN(J),J=1,DIMW)	STP1430
170 IF (NW.EQ.O.OR.IERR.EQ.1) GO TO 230	STP1440
C	STP1450
C	STP1460
C ---COMPUTE APPROXIMATE HEAD FOR PUMPING WELLS---	STP1470
WRITE (P,260)	STP1480
DO 220 KW=1,NW	STP1490
IF (WR(KW).EQ.O.) GO TO 220	STP1500
I=NWR(KW,1)	STP1510
J=NWR(KW,2)	STP1520
C	STP1530
C COMPUTE EFFECTIVE RADIUS OF WELL IN MODEL---	STP1540
RE=(DELX(J)+DELY(I))/9.62	STP1550
IF (WATER.NE.CHK(2)) GO TO 180	STP1560
IF (CONVRT.NE.CHK(7)) GO TO 190	STP1570
IF (PHI(I,J).LT.TOP(I,J)) GO TO 190	STP1580
C	STP1590
C ---COMPUTATION FOR WELL IN ARTESIAN AQUIFER---	STP1600
180 HW=PHI(I,J)+WELL(I,J)*ALOG(RE/WR(KW))/(2.*PIE*T(I,J))*DELX(J)*DELY	STP1610
1(I)	STP1620
GO TO 210	STP1630
C	STP1640
C ---COMPUTATION FOR WELL IN WATER TABLE AQUIFER	STP1650
190 HED=PHI(I,J)-BOTTOM(I,J)	STP1660
ARG=HED*HED+WELL(I,J)*ALOG(RE/WR(KW))/(PIE*PERM(I,J))*DELX(J)*DELY	STP1670
1(I)	STP1680
IF (ARG.GT.O.) GO TO 200	STP1690
WRITE (P,270) I,J	STP1700
GO TO 220	STP1710
200 HW=SGRT(ARG)+BOTTOM(I,J)	STP1720
C	STP1730
C ---COMPUTE DRAWDOWN AT THE WELL AND PRINT RESULTS---	STP1740

210	DRAW=SURI(I,J)-HW	STP1750
	WRITE (P,250) I,J,WR(KW),HW,DRAW	STP1760
220	CONTINUE	STP1770
230	IF (IERR.NE.2) RETURN	STP1780
	STOP	STP1790
C		STP1800
C	---DISK OUTPUT---	STP1810
C	*****	STP1820
	ENTRY DISK	STP1830
C	*****	STP1840
	WRITE (4) PHI,SUM,SUMP,PUMPT,CFLUXT,GRET,CHST,CHDT,FLUXT,STORT,ET	STP1850
	1LXT,FLXNT	STP1860
	RETURN	STP1870
C	.....	STP1880
C		STP1890
C	---PUNCHED OUTPUT---	STP1900
C	*****	STP1910
	ENTRY PUNCH	STP1920
C	*****	STP1930
	WRITE (PU,360) SUM,SUMP,PUMPT,CFLUXT,GRET,CHST,CHDT,FLUXT,STORT,ET	STP1940
	1FLXT,FLXNT	STP1950
	DO 240 I=1,DIML	STP1960
240	WRITE (PU,350) (PHI(I,J),J=1,DIMW)	STP1970
	RETURN	STP1980
C		STP1990
C	.....	STP2000
C		STP2010
C	FORMATS:	STP2020
C		STP2030
C		STP2040
C	-----	STP2050
C		STP2060
C		STP2070
	250 FORMAT (' ',43X,2I5,3F11.2)	STP2080
	260 FORMAT ('-',50X,'HEAD AND DRAWDOWN IN PUMPING WELLS'/51X,34('-')//	STP2090
	148X,'I J WELL RADIUS HEAD DRAWDOWN'//)	STP2100
	270 FORMAT (' ',43X,2I5,' WELL IS DRY')	STP2110
	280 FORMAT (1H1,60X,'DRAWDOWN'/61X,8('-'))	STP2120
	290 FORMAT ('OMAXIMUM CHANGE IN HEAD FOR THIS TIME STEP =',F10.3/' ',5STP2130	
	13('-'))	STP2140
	300 FORMAT ('OMAXIMUM HEAD CHANGE FOR EACH ITERATION: '/' ',39('-')/('OSTP2150	
	1',10F12.4))	STP2160
	310 FORMAT ('1',60X,'HEAD MATRIX'/61X,11('-'))	STP2170
	320 FORMAT ('ODIMENSIONLESS TIME FOR THIS STEP RANGES FROM',G15.7,' TSTP2180	
	10',G15.7)	STP2190
	330 FORMAT ('-*****STEADY STATE AT TIME STEP',I4,'*****')	STP2200
	340 FORMAT (1H1,44X,57('-')/45X,'!',14X,'TIME STEP NUMBER =',I9,14X,'!STP2210	
	1'/45X,57('-')//50X,29HSIZE OF TIME STEP IN SECONDS=,F14.2//55X,'TOSTP2220	
	2TAL SIMULATION TIME IN SECONDS=,F14.2/80X,8HMINUTES=,F14.2/82X,6HSTP2230	
	3HOURS=,F14.2/83X,5HDAYS=,F14.2/82X,'YEARS=,F14.2//45X,'DURATION STP2240	
	4OF CURRENT PUMPING PERIOD IN DAYS=,F14.2/82X,'YEARS=,F14.2//)	STP2250
	350 FORMAT (8F10.4)	STP2260
	360 FORMAT (4G20.10)	STP2270
	370 FORMAT ('OITERATIONS:',40I3)	STP2280
	380 FORMAT (' ',10('-'))	STP2290
	390 FORMAT ('OTIME STEP:',40I3)	STP2300
	400 FORMAT ('O',10('*'),'THE NUMBER OF TIME STEPS EXCEEDS THE DIMENSIONSTP2310	
	IN OF THE VECTOR ITTO AND MAY CAUSE UNEXPECTED RESULTS IN ADDITIONASTP2320	
	2L//OCOMPUTATION. AVOID PROBLEMS BY INCREASING THE DIMENSION OF TSTP2330	
	3HE VECTOR ITTO IN STEP',10('*'))	STP2340
	END	STP2350-

	SUBROUTINE SOLVE1(PHI, BE, G, TEMP, KEEP, PHE, STRT, T, S, GRE, WELL, TL, SL, DSIP	10
	1EL, ETA, V, XI, DELX, BET, DELY, ALF, TEST3, TR, TC, GRND, SY, TOP, RATE, M, RIVERSIP	20
	2)	SIP 30
C	-----SIP	40
C	SOLUTION BY THE STRONGLY IMPLICIT PROCEDURE	SIP 50
C	-----SIP	60
C		SIP 70
C	SPECIFICATIONS:	SIP 80
	REAL *BPHI, DBLE, RHOP(20), G, BE, TEMP, DABS, W, TEST2, DMAX1, RHO, B, D, F, H, SIP	90
	1B1, E, CH, GH, BH, DH, EH, FH, HH, ALFA, BETA, GAMA, RES	SIP 100
	REAL *4KEEP, M	SIP 110
	INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, SIP	120
	1CONTR, LEAK, RECH, SIP, IORDER(21), ADI, RCAL	P 1300-
C		SIP 140
	DIMENSION PHI(1), BE(1), G(1), TEMP(1), KEEP(1), PHE(1), STRT(1), SIP	150
	1T(1), S(1), GRE(1), WELL(1), TL(1), SL(1), DEL(1), ETA(1), V(1), XSIP	160
	2I(1), DELX(1), BET(1), DELY(1), ALF(1), TEST3(1), TR(1), TC(1), GRSIP	170
	3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DISIP	180
C		SIP 190
	COMMON /SARRAY/ VF4(11), CHK(17)	P 2000-
	COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LESIP	210
	1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, SIP	220
	2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETQB, ETQD, FACTX, FACTY, SIP	230
	3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DISIP	240
	4MW, JNO1, IND1, R, P, PU, I, J, IDK1, IDK2, NSEG, RCAL	P 2500-
	RETURN	SIP 260
C	.....	SIP 270
C		SIP 280
C	---COMPUTE AND PRINT ITERATION PARAMETERS---	SIP 290
C	*****	SIP 300
	ENTRY ITER1	SIP 310
C	*****	SIP 320
C	---INITIALIZE ORDER OF ITERATION PARAMETERS (OR REPLACE WITH A	SIP 330
C	READ STATEMENT)---	SIP 340
	DATA IORDER/1, 2, 3, 4, 5, 1, 2, 3, 4, 5, 11*1/	SIP 350
	I2=IND1-1	SIP 360
	J2=JNO1-1	SIP 370
	L2=LENGTH/2	SIP 380
	PL2=L2-1.	SIP 390
	W=0.	SIP 400
	PI=0.	SIP 410
C		SIP 420
C	---COMPUTE AVERAGE MAXIMUM PARAMETER FOR PROBLEM---	SIP 430
	DO 10 I=2, IND1	SIP 440
	DO 10 J=2, JNO1	SIP 450
	N=I+DIML*(J-1)	SIP 460
	IF (T(N).EQ.0.) GO TO 10	SIP 470
	PI=PI+1.	SIP 480
	DX=DELX(J)/WIDTH	SIP 490
	DY=DELY(I)/YDIM	SIP 500
	W=W+1. -AMIN1(2. *DX*DX/(1. +FACTY*DX*DX/(FACTX*DY*DY)), 2. *DY*DY/(1. +SIP	510
	1FACTX*DY*DY/(FACTY*DX*DX)))	SIP 520
	10 CONTINUE	SIP 530
	W=W/PI	SIP 540
C		SIP 550
C	---COMPUTE PARAMETERS IN GEOMETRIC SEQUENCE---	SIP 560
	PJ=-1.	SIP 570
	DO 20 I=1, L2	SIP 580
	PJ=PJ+1.	SIP 590

20	TEMP(I)=1.-(1.-W)**(PJ/PL2)	SIP 600
C		SIP 610
C	---ORDER SEQUENCE OF PARAMETERS---	SIP 620
	DO 30 J=1,LENGTH	SIP 630
30	RHOP(J)=TEMP(IORDER(J))	SIP 640
	WRITE (P,370) HMAX	SIP 650
	WRITE (P,380) LENGTH, (RHOP(J), J=1, LENGTH)	SIP 660
	RETURN	SIP 670
C	.....	SIP 680
C		SIP 690
C	---INITIALIZE DATA FOR A NEW ITERATION---	SIP 700
40	KOUNT=KOUNT+1	SIP 710
	IF (KOUNT.LE. ITMAX) GO TO 50	SIP 720
	WRITE (P,360)	SIP 730
	CALL TERM1	SIP 740
50	IF (MOD(KOUNT,LENGTH)) 60,60,70	SIP 750
C	*****	SIP 760
	ENTRY NEWITA	SIP 770
C	*****	SIP 780
60	NTH=0	SIP 790
70	NTH=NTH+1	SIP 800
	W=RHOP(NTH)	SIP 810
	TEST3(KOUNT+1)=0.	SIP 820
	TEST=0.	SIP 830
	N=DIML*DIMW	SIP 840
	DO 80 I=1,N	SIP 850
	PHE(I)=PHI(I)	SIP 860
	DEL(I)=0.	SIP 870
	ETA(I)=0.	SIP 880
	V(I)=0.	SIP 890
80	XI(I)=0.	SIP 900
	BIGI=0.0	SIP 910
C		SIP 920
C	---COMPUTE TRANSMISSIVITY AND T COEFFICIENTS IN WATER TABLE	SIP 930
C	OR WATER TABLE-ARTESIAN SIMUATION---	SIP 940
	IF (WATER.NE. CHK(2)) GO TO 90	SIP 950
	CALL TRANS	SIP 960
C		SIP 970
C	---CHOOSE SIP NORMAL OR REVERSE ALGORITHM---	SIP 980
90	IF (MOD(KOUNT,2)) 100,230,100	SIP 990
C	.....	SIP1000
C	---ORDER EQUATIONS WITH ROW 1 FIRST - 3X3 EXAMPLE:	SIP1010
C	1 2 3	SIP1020
C	4 5 6	SIP1030
C	7 8 9	SIP1040
C	.....	SIP1050
100	DO 210 I=2,IND1	SIP1060
	DO 210 J=2,JND1	SIP1070
	N=I+DIML*(J-1)	SIP1080
	NL=N-DIML	SIP1090
	NR=N+DIML	SIP1100
	NA=N-1	SIP1110
	NB=N+1	SIP1120
C		SIP1130
C	---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---	SIP1140
	IF (T(N).EQ.0..OR.S(N).LT.0.) GO TO 210	SIP1150
C		SIP1160
C	---COMPUTE COEFFICIENTS---	SIP1170
	D=TR(NL)/DELX(J)	SIP1180
	F=TR(N)/DELX(J)	SIP1190



	B=TC(NA)/DELY(I)	SIP1200
	H=TC(N)/DELY(I)	SIP1210
	IF (EVAP.NE.CHK(6)) GO TO 120	SIP1220
C		SIP1230
C	----COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE----	SIP1240
	ETQB=0.	SIP1250
	ETQD=0.0	SIP1260
	IF (PHE(N).LE.GRND(N)-ETDIST) GO TO 120	SIP1270
	IF (PHE(N).GT.GRND(N)) GO TO 110	SIP1280
	ETQB=QET/ETDIST	SIP1290
	ETQD=ETQB*(ETDIST-GRND(N))	SIP1300
	GO TO 120	SIP1310
110	ETQD=QET	SIP1320
C		SIP1330
C	----COMPUTE STORAGE TERM----	SIP1340
120	IF (CONVRT.EG.CHK(7)) GO TO 130	SIP1350
	RHO=S(N)/DELT	SIP1360
	IF (WATER.EG.CHK(2)) RHO=SY(N)/DELT	SIP1370
	GO TO 200	SIP1380
C		SIP1390
C	----COMPUTE STORAGE COEFFICIENT FOR CONVERSION PROBLEM----	SIP1400
130	SUBS=0.0	SIP1410
	IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 170	SIP1420
	IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 160	SIP1430
	IF (KEEP(N)-PHE(N)) 140,150,150	SIP1440
140	SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))	SIP1450
	GO TO 170	SIP1460
150	SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))	SIP1470
160	RHO=SY(N)/DELT	SIP1480
	GO TO 180	SIP1490
170	RHO=S(N)/DELT	SIP1500
180	IF (LEAK.NE.CHK(9)) GO TO 200	SIP1510
C		SIP1520
C	----COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION----	SIP1530
	IF (RATE(N).EQ.0..OR.M(N).EQ.0.) GO TO 200	SIP1540
	HED1=AMAX1(STRT(N),TOP(N))	SIP1550
	U=1.	SIP1560
	HED2=0.	SIP1570
	IF (PHE(N).GE.TOP(N)) GO TO 190	SIP1580
	HED2=TOP(N)	SIP1590
	U=0.	SIP1600
190	SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))	SIP1610
200	CONTINUE	SIP1620
C		SIP1630
C	---SIP 'NORMAL' ALGORITHM---	SIP1640
C	---FORWARD SUBSTITUTE, COMPUTING INTERMEDIATE VECTOR V---	SIP1650
	E=-B-D-F-H-RHO-TL(N)*U-ETQB	SIP1660
	CH=DEL(NA)*B/(1.+W*DEL(NA))	SIP1670
	GH=ETA(NL)*D/(1.+W*ETA(NL))	SIP1680
	BH=B-W*CH	SIP1690
	DH=D-W*GH	SIP1700
	EH=E+W*CH+W*GH	SIP1710
	FH=F-W*CH	SIP1720
	HH=H-W*GH	SIP1730
	ALFA=BH	SIP1740
	BETA=DH	SIP1750
	GAMA=EH-ALFA*ETA(NA)-BETA*DEL(NL)	SIP1760
	DEL(N)=FH/GAMA	SIP1770
	ETA(N)=HH/GAMA	SIP1780
	RES=-D*PHI(NL)-F*PHI(NR)-H*PHI(NB)-B*PHI(NA)-E*PHI(N)-RHO*KEEP(N)-	SIP1790

	1SL(N)-GRE(N)-WELL(N)+ETGD-SUBS-TL(N)*STRT(N)	SIP1800
	V(N)=(HMAX*RES-ALFA*V(NA)-BETA*V(NL))/GAMA	SIP1810
	210 CONTINUE	SIP1820
C		SIP1830
C	---BACK SUBSTITUTE FOR VECTOR XI---	SIP1840
	DO 220 I=1,I2	SIP1850
	I3=DIML-I	SIP1860
	DO 220 J=1,J2	SIP1870
	J3=DIMW-J	SIP1880
	N=I3+DIML*(J3-1)	SIP1890
	IF (T(N).EQ.0..OR.S(N).LT.0.) GO TO 220	SIP1900
	XI(N)=V(N)-DEL(N)*XI(N+DIML)-ETA(N)*XI(N+1)	SIP1910
C		SIP1920
C	---COMPARE MAGNITUDE OF CHANGE WITH CLOSURE CRITERION---	SIP1930
	TCHK=ABS(XI(N))	SIP1940
	IF (TCHK.GT.BIGI) BIGI=TCHK	SIP1950
	PHI(N)=PHI(N)+XI(N)	SIP1960
	220 CONTINUE	SIP1970
	IF (BIGI.GT.ERR) TEST=1.	SIP1980
	TEST3(KOUNT+1)=BIGI	SIP1990
	IF (TEST.EQ.1.) GO TO 40	SIP2000
	RETURN	SIP2010
C		SIP2020
C		SIP2030
C	---ORDER EQUATIONS WITH THE LAST ROW FIRST - 3X3 EXAMPLE:	SIP2040
C	7 8 9	SIP2050
C	4 5 6	SIP2060
C	1 2 3	SIP2070
C		SIP2080
	230 DO 340 II=1,I2	SIP2090
	I=DIML-II	SIP2100
	DO 340 J=2,JN01	SIP2110
	N=I+DIML*(J-1)	SIP2120
	NL=N-DIML	SIP2130
	NR=N+DIML	SIP2140
	NA=N-1	SIP2150
	NB=N+1	SIP2160
C		SIP2170
C	---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---	SIP2180
	IF (T(N).EQ.0..OR.S(N).LT.0.) GO TO 340	SIP2190
C		SIP2200
C	---COMPUTE COEFFICIENTS---	SIP2210
	D=TR(NL)/DELX(J)	SIP2220
	F=TR(N)/DELX(J)	SIP2230
	B=TC(NA)/DELY(I)	SIP2240
	H=TC(N)/DELY(I)	SIP2250
	IF (EVAP.NE.CHK(6)) GO TO 250	SIP2260
C		SIP2270
C	---COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE---	SIP2280
	ETQB=0.	SIP2290
	ETGD=0.0	SIP2300
	IF (PHE(N).LE.GRND(N)-ETDIST) GO TO 250	SIP2310
	IF (PHE(N).GT.GRND(N)) GO TO 240	SIP2320
	ETQB=GET/ETDIST	SIP2330
	ETGD=ETQB*(ETDIST-GRND(N))	SIP2340
	GO TO 250	SIP2350
	240 ETGD=GET	SIP2360
C		SIP2370
C	---COMPUTE STORAGE TERM---	SIP2380
	250 IF (CONVRT.EQ.CHK(7)) GO TO 260	SIP2390

	RHO=S(N)/DELT	SIP2400
	IF (WATER.EQ.CHK(2)) RHO=SY(N)/DELT	SIP2410
	GO TO 330	SIP2420
C		SIP2430
C	---COMPUTE STORAGE COEFFICIENT FOR CONVERSION PROBLEM---	SIP2440
260	SUBS=0.0	SIP2450
	IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 300	SIP2460
	IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 290	SIP2470
	IF (KEEP(N)-PHE(N)) 270,280,280	SIP2480
270	SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))	SIP2490
	GO TO 300	SIP2500
280	SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))	SIP2510
290	RHO=SY(N)/DELT	SIP2520
	GO TO 310	SIP2530
300	RHO=S(N)/DELT	SIP2540
310	IF (LEAK.NE.CHK(9)) GO TO 330	SIP2550
C		SIP2560
C	---COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION---	SIP2570
	IF (RATE(N).EQ.0..OR.M(N).EQ.0.) GO TO 330	SIP2580
	HED1=AMAX1(STRT(N),TOP(N))	SIP2590
	U=1.	SIP2600
	HED2=0.	SIP2610
	IF (PHE(N).GE.TOP(N)) GO TO 320	SIP2620
	HED2=TOP(N)	SIP2630
	U=0.	SIP2640
320	SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))	SIP2650
330	CONTINUE	SIP2660
C		SIP2670
C	---SIP 'REVERSE' ALGORITHM---	SIP2680
C	---FORWARD SUBSTITUTE, COMPUTING INTERMEDIATE VECTOR V---	SIP2690
	E=-B-D-F-H-RHO-TL(N)*U-ETQB	SIP2700
	CH=DEL(NB)*H/(1.+W*DEL(NB))	SIP2710
	GH=ETA(NL)*D/(1.+W*ETA(NL))	SIP2720
	BH=H-W*CH	SIP2730
	DH=D-W*GH	SIP2740
	EH=E+W*CH+W*GH	SIP2750
	FH=F-W*CH	SIP2760
	HH=B-W*GH	SIP2770
	ALFA=BH	SIP2780
	BETA=DH	SIP2790
	GAMA=EH-ALFA*ETA(NB)-BETA*DEL(NL)	SIP2800
	DEL(N)=FH/GAMA	SIP2810
	ETA(N)=HH/GAMA	SIP2820
	RES=-D*PHI(NL)-F*PHI(NR)-H*PHI(NB)-B*PHI(NA)-E*PHI(N)-RHO*KEEP(N)-	SIP2830
	1SL(N)-GRE(N)-WELL(N)+ETQB-SUBS-TL(N)*STRT(N)	SIP2840
	V(N)=(HMAX*RES-ALFA*V(NB)-BETA*V(NL))/GAMA	SIP2850
340	CONTINUE	SIP2860
C		SIP2870
C	---BACK SUBSTITUTE FOR VECTOR XI---	SIP2880
	DO 350 I3=2,IND1	SIP2890
	DO 350 J=1,J2	SIP2900
	J3=DIMW-J	SIP2910
	N=I3+DIML*(J3-1)	SIP2920
	IF (T(N).EQ.0..OR.S(N).LT.0.) GO TO 350	SIP2930
	XI(N)=V(N)-DEL(N)*XI(N+DIML)-ETA(N)*XI(N-1)	SIP2940
C		SIP2950
C	---COMPARE MAGNITUDE OF CHANGE WITH CLOSURE CRITERION---	SIP2960
	TCHK=ABS(XI(N))	SIP2970
	IF (TCHK.GT.BIGI) BIGI=TCHK	SIP2980
	PHI(N)=PHI(N)+XI(N)	SIP2990

350	CONTINUE	SIP3000
	IF (BIGI.GT.ERR) TEST=1.	SIP3010
	TEST3(KDUNT+1)=BIGI	SIP3020
	IF (TEST.EQ.1.) GO TO 40	SIP3030
	RETURN	SIP3040
C		SIP3050
C	.....	SIP3060
C		SIP3070
C	---FORMATS---	SIP3080
C		SIP3090
C	-----	SIP3100
C		SIP3110
C		SIP3120
360	FORMAT ('OEXCEEDED PERMITTED NUMBER OF ITERATIONS'// ' ',39('*'))	SIP3130
370	FORMAT ('-',44X,'SOLUTION BY THE STRONGLY IMPLICIT PROCEDURE'/45X,	SIP3140
	143('_'),///,61X,'BETA=',F5.2)	SIP3150
380	FORMAT (1H0,15,22H ITERATION PARAMETERS:,6D15.7/(/28X,6D15.7/))	SIP3160
	END	SIP3170-

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SUBROUTINE SOLVE2(PHI, BE, G, TEMP, KEEP, PHE, STRT, T, S, GRE, WELL, TL, SL, DSOR 10
1EL, ETA, V, XI, DELX, BETA, DELY, ALFA, TEST3, TR, TC, GRND, SY, TOP, RATE, M, RIVSOR 20
2ER) SOR 30
C -----SOR 40
C SOLUTION BY LINE SUCCESSIVE OVERRELAXATION SOR 50
C -----SOR 60
C SOR 70
C SPECIFICATIONS: SOR 80
C REAL *BPHI, DBLE, RHOP(20), G, BE, TEMP, IMK, DABS, W, PARAM, TEST2, DMAX1, B2SOR 90
1, A, C, B1, E, G, RHO, B, D, F, H SOR 100
C REAL *4KEEP, M SOR 110
C INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, SOR 120
1CONTR, LEAK, RECH, SIP, ADI, RCAL R 1300-
C SOR 140
C DIMENSION PHI(1), BE(1), Q(1), TEMP(1), KEEP(1), PHE(1), STRT(1), SOR 150
1T(1), S(1), GRE(1), WELL(1), TL(1), SL(1), DEL(1), ETA(1), V(1), XSOR 160
2I(1), DELX(1), BETA(1), DELY(1), ALFA(1), TEST3(1), TR(1), TC(1), SOR 170
3GRND(1), SY(1), TOP(1), RATE(1), M(1), RIVER(1) SOR 180
C SOR 190
C COMMON /SARRAY/ VF4(11), CHK(17) R 2000-
C COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LESOR 210
1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, SOR 220
2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETQB, ETGD, FACTX, FACTY, SOR 230
3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DISOR 240
4MW, JND1, IND1, R, P, PU, I, J, IDK1, IDK2, NSEQ, RCAL R 2500-
C RETURN SOR 260
C ..... SOR 270
C ..... SOR 280
C ---WRITE ACCELERATION PARAMETER--- SOR 290
C ***** SOR 300
C ENTRY ITER2 SOR 310
C ***** SOR 320
C WRITE (P, 490) SOR 330
C WRITE (P, 500) HMAX, LENGTH SOR 340
C RETURN SOR 350
C ..... SOR 360
C ..... SOR 370
C ---INITIALIZE DATA FOR A NEW ITERATION--- SOR 380
10 KOUNT=KOUNT+1 SOR 390
C IF (KOUNT.LE. ITMAX) GO TO 20 SOR 400
C WRITE (P, 510) SOR 410
C CALL TERM1 SOR 420
C ***** SOR 430
C ENTRY NEWITB SOR 440
C ***** SOR 450
20 TEST3(KOUNT+1)=0. SOR 460
C TEST=0. SOR 470
C N=DIML*DIMW SOR 480
C DO 30 I=1, N SOR 490
30 PHE(I)=PHI(I) SOR 500
C BIGI=0.0 SOR 510
C ..... SOR 520
C ---COMPUTE TRANSMISSIVITY AND T COEFFICIENTS IN WATER TABLE SOR 530
C OR WATER TABLE-ARTESIAN SIMULATION--- SOR 540
C IF (WATER.NE. CHK(2)) GO TO 40 SOR 550
C CALL TRANS SOR 560
C ..... SOR 570
C ..... SOR 580
C ---SOLUTION BY LSOR--- SOR 590

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C	-----	SOR 600
40	NO3=DIMW-2	SOR 610
	TEMP(DIMW)=0.0	SOR 620
	DO 170 I=2, INQ1	SOR 630
	DO 150 J=2, JND1	SOR 640
	N=I+DIML*(J-1)	SOR 650
	NA=N-1	SOR 660
	NB=N+1	SOR 670
	NL=N-DIML	SOR 680
	NR=N+DIML	SOR 690
	BE(J)=0.0	SOR 700
	Q(J)=0.0	SOR 710
C		SOR 720
C	---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---	SOR 730
	IF (T(N).EQ.0. .OR. S(N).LT.0.) GO TO 150	SOR 740
C		SOR 750
C	---COMPUTE COEFFICIENTS---	SOR 760
	D=TR(N-DIML)/DELX(J)	SOR 770
	F=TR(N)/DELX(J)	SOR 780
	B=TC(N-1)/DELY(1)	SOR 790
	H=TC(N)/DELY(1)	SOR 800
	IF (EVAP.NE.CHK(6)) GO TO 60	SOR 810
C		SOR 820
C	---COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE---	SOR 830
	ETQB=0.	SOR 840
	ETGD=0.0	SOR 850
	IF (PHE(N).LE.GRND(N)-ETDIST) GO TO 60	SOR 860
	IF (PHE(N).GT.GRND(N)) GO TO 50	SOR 870
	ETQB=GET/ETDIST	SOR 880
	ETGD=ETQB*(ETDIST-GRND(N))	SOR 890
	GO TO 60	SOR 900
50	ETGD=GET	SOR 910
C		SOR 920
C	---COMPUTE STORAGE TERM---	SOR 930
60	IF (CONVRT.EQ.CHK(7)) GO TO 70	SOR 940
	RHO=S(N)/DELT	SOR 950
	IF (WATER.EQ.CHK(2)) RHO=SY(N)/DELT	SOR 960
	GO TO 140	SOR 970
C		SOR 980
C	---COMPUTE STORAGE COEFFICIENT FOR CONVERSION PROBLEM---	SOR 990
70	SUBS=0.0	SOR1000
	IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 110	SOR1010
	IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 100	SOR1020
	IF (KEEP(N)-PHE(N)) 80,90,90	SOR1030
80	SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))	SOR1040
	GO TO 110	SOR1050
90	SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))	SOR1060
100	RHO=SY(N)/DELT	SOR1070
	GO TO 120	SOR1080
110	RHO=S(N)/DELT	SOR1090
120	IF (LEAK.NE.CHK(9)) GO TO 140	SOR1100
C		SOR1110
C	---COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION---	SOR1120
	IF (RATE(N).EQ.0. .OR. M(N).EQ.0.) GO TO 140	SOR1130
	HED1=AMAX1(STRT(N),TOP(N))	SOR1140
	U=1.	SOR1150
	HED2=0.	SOR1160
	IF (PHE(N).GE.TOP(N)) GO TO 130	SOR1170
	HED2=TOP(N)	SOR1180
	U=0.	SOR1190

130	SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))	SOR1200
140	CONTINUE	SOR1210
C		SOR1220
C	---FORWARD SUBSTITUTE, COMPUTING INTERMEDIATE VECTOR G---	SOR1230
	E=-D-F-B-H-RHO-TL(N)*U-ETQB	SOR1240
	W=E-D*BE(J-1)	SOR1250
	BE(J)=F/W	SOR1260
	G=-B*PHI(NA)-H*PHI(NB)-RHO*KEEP(N)-SL(N)-GRE(N)-WELL(N)+ETQB-SUBS-	SOR1270
	1TL(N)*STRT(N)-D*PHI(NL)-F*PHI(NR)-E*PHI(N)	SOR1280
	G(J)=(G-D*G(J-1))/W	SOR1290
150	CONTINUE	SOR1300
C		SOR1310
C	---BACK SUBSTITUTE FOR TEMP---	SOR1320
	DO 160 KNO4=1,NO3	SOR1330
	NO4=DIMW-KNO4	SOR1340
	TEMP(NO4)=G(NO4)-BE(NO4)*TEMP(NO4+1)	SOR1350
160	CONTINUE	SOR1360
C		SOR1370
C	---EXTRAPOLATED VALUE OF PHI---	SOR1380
	DO 170 J=2,JNO1	SOR1390
	N=I+DIML*(J-1)	SOR1400
	PHI(N)=PHI(N)+HMAX*TEMP(J)	SOR1410
C		SOR1420
C	---COMPARE MAGNITUDE OF CHANGE WITH CLOSURE CRITERION---	SOR1430
	TCHK=DABS(TEMP(J))	SOR1440
	IF (TCHK.GT.BIGI) BIGI=TCHK	SOR1450
170	CONTINUE	SOR1460
	IF (BIGI.GT.ERR) TEST=1.	SOR1470
	TEST3(KOUNT+1)=BIGI	SOR1480
	IF (KOUNT.EQ.0) GO TO 10	SOR1490
	IF (TEST.EQ.0.) RETURN	SOR1500
C		SOR1510
C	---TEST FOR TWO DIMENSIONAL CORRECTION---	SOR1520
	IF (MOD(KOUNT,LENGTH).NE.0) GO TO 10	SOR1530
	GO TO 200	SOR1540
180	DO 190 I=2,INO1	SOR1550
	DO 190 J=2,JNO1	SOR1560
	N=I+DIML*(J-1)	SOR1570
	IF (T(N).EQ.0.) GO TO 190	SOR1580
	PHI(N)=PHI(N)+ALFA(I)+BETA(J)	SOR1590
190	CONTINUE	SOR1600
	GO TO 10	SOR1610
C	.....	SOR1620
C		SOR1630
C	---TWO DIMENSIONAL CORRECTION TO LSOR---	SOR1640
C	-----	SOR1650
C		SOR1660
C	---COMPUTE ALFA CORRECTION FOR ROWS---	SOR1670
200	DO 210 I=1,DIML	SOR1680
	ALFA(I)=0.	SOR1690
	BE(I)=0.0	SOR1700
210	G(I)=0.0	SOR1710
	DO 330 I=2,INO1	SOR1720
	A=0.	SOR1730
	B2=0.	SOR1740
	C=0.	SOR1750
	G=0.	SOR1760
C		SOR1770
C	---SUMMATION OF COEFFICIENTS FOR EACH ROW---	SOR1780
	DO 320 J=2,JNO1	SOR1790

	N=I+DIML*(J-1)	SOR1800
	NA=N-1	SOR1810
	NB=N+1	SOR1820
	NL=N-DIML	SOR1830
	NR=N+DIML	SOR1840
	IF (S(N).LT.0.) GO TO 330	SOR1850
	IF (T(N).EQ.0.) GO TO 320	SOR1860
C		SOR1870
C	---COMPUTE COEFFICIENTS---	SOR1880
	D=TR(N-DIML)/DELX(J)	SOR1890
	F=TR(N)/DELX(J)	SOR1900
	B=TC(N-1)/DELY(I)	SOR1910
	H=TC(N)/DELY(I)	SOR1920
	IF (EVAP.NE.CHK(6)) GO TO 230	SOR1930
C		SOR1940
C	---COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE---	SOR1950
	ETQB=0.	SOR1960
	ETGD=0.0	SOR1970
	IF (PHE(N).LE.QRND(N)-ETDIST) GO TO 230	SOR1980
	IF (PHE(N).GT.QRND(N)) GO TO 220	SOR1990
	ETQB=GET/ETDIST	SOR2000
	ETGD=ETQB*(ETDIST-QRND(N))	SOR2010
	GO TO 230	SOR2020
	220 ETGD=GET	SOR2030
C		SOR2040
C	---COMPUTE STORAGE TERM---	SOR2050
	230 IF (CONVRT.EQ.CHK(7)) GO TO 240	SOR2060
	RHO=S(N)/DELT	SOR2070
	IF (WATER.EQ.CHK(2)) RHO=SY(N)/DELT	SOR2080
	GO TO 310	SOR2090
	240 SUBS=0.0	SOR2100
	IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 280	SOR2110
	IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 270	SOR2120
	IF (KEEP(N)-PHE(N)) 250,260,260	SOR2130
	250 SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))	SOR2140
	GO TO 280	SOR2150
	260 SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))	SOR2160
	270 RHO=SY(N)/DELT	SOR2170
	GO TO 290	SOR2180
	280 RHO=S(N)/DELT	SOR2190
	290 IF (LEAK.NE.CHK(9)) GO TO 310	SOR2200
C		SOR2210
C	---COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION---	SOR2220
	IF (RATE(N).EQ.0..OR.M(N).EQ.0.) GO TO 310	SOR2230
	HED1=AMAX1(STRT(N),TOP(N))	SOR2240
	U=1.	SOR2250
	HED2=0.	SOR2260
	IF (PHE(N).GE.TOP(N)) GO TO 300	SOR2270
	HED2=TOP(N)	SOR2280
	U=0.	SOR2290
	300 SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))	SOR2300
	310 CONTINUE	SOR2310
C		SOR2320
	A=A-B	SOR2330
	B1=B+H+RHO+TL(N)*U+ETQB	SOR2340
	B2=B2+B1	SOR2350
	C=C-H	SOR2360
	Q=Q+(D*PHI(NL)+F*PHI(NR)+B*PHI(NA)+H*PHI(NB)+RHO*KEEP(N)+SL(N)+GRES	SOR2370
	1(N)+WELL(N)-ETGD+SUBS+TL(N)*STRT(N)-(D+F+B1)*PHI(N))	SOR2380
	320 CONTINUE	SOR2390



C		SOR2400
C	---COMPUTATION OF INTERMEDIATE VECTOR Q---	SOR2410
	W=B2-A*BE(I-1)	SOR2420
	BE(I)=C/W	SOR2430
	Q(I)=(Q-A*G(I-1))/W	SOR2440
	330 CONTINUE	SOR2450
C		SOR2460
C	---BACK SUBSTITUTE FOR ALFA---	SOR2470
	NO3=DIML-2	SOR2480
	DO 340 KNO4=1, NO3	SOR2490
	NO4=DIML-KNO4	SOR2500
	340 ALFA(NO4)=Q(NO4)-BE(NO4)*ALFA(NO4+1)	SOR2510
	*****	SOR2520
C		SOR2530
C	---COMPUTE BETA CORRECTION FOR COLUMNS---	SOR2540
	DO 350 J=1, DIMW	SOR2550
	BETA(J)=0.	SOR2560
	BE(J)=0.0	SOR2570
	350 G(J)=0.0	SOR2580
	DO 470 J=2, JNO1	SOR2590
	A=0.	SOR2600
	B2=0.	SOR2610
	C=0.	SOR2620
	Q=0.	SOR2630
C		SOR2640
C	---SUMMATION OF COEFFICIENTS FOR EACH COLUMN---	SOR2650
	DO 460 I=2, INO1	SOR2660
	N=I+DIML*(J-1)	SOR2670
	NA=N-1	SOR2680
	NB=N+1	SOR2690
	NL=N-DIML	SOR2700
	NR=N+DIML	SOR2710
	IF (S(N).LT.0.) GO TO 470	SOR2720
	IF (T(N).EQ.0.) GO TO 460	SOR2730
	D=TR(N-DIML)/DELX(J)	SOR2740
	F=TR(N)/DELX(J)	SOR2750
	B=TC(N-1)/DELY(I)	SOR2760
	H=TC(N)/DELY(I)	SOR2770
	IF (EVAP.NE.CHK(6)) GO TO 370	SOR2780
C		SOR2790
C	---COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE---	SOR2800
	ETQB=0.	SOR2810
	ETGD=0.0	SOR2820
	IF (PHE(N).LE.GRND(N)-ETDIST) GO TO 370	SOR2830
	IF (PHE(N).GT.GRND(N)) GO TO 360	SOR2840
	ETQB=GET/ETDIST	SOR2850
	ETGD=ETQB*(ETDIST-GRND(N))	SOR2860
	GO TO 370	SOR2870
	360 ETGD=GET	SOR2880
C		SOR2890
C	---COMPUTE STORAGE TERM---	SOR2900
	370 IF (CONVRT.EQ.CHK(7)) GO TO 380	SOR2910
	RHO=S(N)/DELT	SOR2920
	IF (WATER.EQ.CHK(2)) RHO=SY(N)/DELT	SOR2930
	GO TO 450	SOR2940
C		SOR2950
C	---COMPUTE STORAGE COEFFICIENT FOR CONVERSION PROBLEM---	SOR2960
	380 SUBS=0.0	SOR2970
	IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 420	SOR2980
	IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 410	SOR2990

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      IF (KEEP(N)-PHE(N)) 390,400,400                                SOR3000
390 SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))                        SOR3010
      GO TO 420                                                        SOR3020
400 SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))                        SOR3030
410 RHO=SY(N)/DELT                                                  SOR3040
      GO TO 430                                                        SOR3050
420 RHO=S(N)/DELT                                                  SOR3060
430 IF (LEAK.NE.CHK(9)) GO TO 450                                    SOR3070
C                                                                    SOR3080
C      ---COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION---    SOR3090
      IF (RATE(N).EQ.0..OR.M(N).EQ.0.) GO TO 450                    SOR3100
      HED1=AMAX1(STRT(N),TOP(N))                                     SOR3110
      U=1.                                                            SOR3120
      HED2=0.                                                         SOR3130
      IF (PHE(N).GE.TOP(N)) GO TO 440                                SOR3140
      HED2=TOP(N)                                                    SOR3150
      U=0.                                                            SOR3160
440 SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))  SOR3170
450 CONTINUE                                                         SOR3180
C                                                                    SOR3190
      A=A-D                                                            SOR3200
      B1=D+F+RHO+TL(N)*U+ETQB                                         SOR3210
      B2=B2+B1                                                         SOR3220
      C=C-F                                                            SOR3230
      G=G+(D*PHI(NL)+F*PHI(NR)+B*PHI(NA)+H*PHI(NB)+RHO*KEEP(N)+SL(N)+GRESOR3240
      1(N)+WELL(N)-ETGD+SUBS+TL(N)*STRT(N)-(B+H+B1)*PHI(N))        SOR3250
460 CONTINUE                                                         SOR3260
C                                                                    SOR3270
C      ---COMPUTATION OF INTERMEDIATE VECTOR G---                  SOR3280
      W=B2-A*BE(J-1)                                                  SOR3290
      BE(J)=C/W                                                        SOR3300
      G(J)=(G-A*G(J-1))/W                                             SOR3310
470 CONTINUE                                                         SOR3320
C                                                                    SOR3330
C      ---BACK SUBSTITUTE FOR BETA---                                SOR3340
      NO3=DIMW-2                                                       SOR3350
      DO 480 KNO4=1,NO3                                               SOR3360
      NO4=DIMW-KNO4                                                    SOR3370
480 BETA(NO4)=G(NO4)-BE(NO4)*BETA(NO4+1)                            SOR3380
      GO TO 180                                                        SOR3390
C                                                                    SOR3400
C      .....                                                       SOR3410
C                                                                    SOR3420
C      ---FORMATS---                                                 SOR3430
C      -----                                                       SOR3440
C                                                                    SOR3450
C                                                                    SOR3460
490 FORMAT ('-',45X,'SOLUTION BY LINE SUCCESSIVE OVERRELAXATION'/46X,4SOR3470
      12(' '))                                                        SOR3480
500 FORMAT ('-',26X,'ACCELERATION PARAMETER =',F6.3,' TWO DIMENSIONALSOR3490
      1 CORRECTION EVERY',I5,' ITERATIONS')                          SOR3500
510 FORMAT ('OEXCEEDED PERMITTED NUMBER OF ITERATIONS'' ',39('*'))  SOR3510
      END                                                            SOR3520-

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SUBROUTINE SOLVE3(PHI, BE, Q, TEMP, KEEP, PHE, STRT, T, S, GRE, WELL, TL, SL, DADI 10
1EL, ETA, V, XI, DELX, BETA, DELY, ALFA, XII, TEST3, TR, TC, GRND, SY, TOP, RATE, MADI 20
2, RIVER)-----ADI 30
C-----ADI 40
C SOLUTION BY THE ALTERNATING DIRECTION IMPLICIT PROCEDURE-----ADI 50
C-----ADI 60
C-----ADI 70
C SPECIFICATIONS:-----ADI 80
REAL *8PHI, DBLE, RHOP(20), Q, BE, TEMP, IMK, DABS, W, PARAM, TEST2, DMAX1, DTADI 90
1ERMS, B1, E, G, B, D, F, H, RHO, XII-----ADI 100
REAL *4KEEP, M-----ADI 110
INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, ADI 120
1CONTR, LEAK, RECH, SIP, ADI, RCAL-----I 1300-
C-----ADI 140
DIMENSION PHI(1), BE(1), Q(1), TEMP(1), KEEP(1), PHE(1), STRT(1), ADI 150
1T(1), S(1), GRE(1), WELL(1), TL(1), SL(1), DEL(1), ETA(1), V(1), XADI 160
2I(1), DELX(1), BETA(1), DELY(1), ALFA(1), XII(1), TEST3(1), TR(1), ADI 170
3 TC(1), GRND(1), SY(1), TOP(1), RATE(1), M(1), RIVER(1)-----ADI 180
C-----ADI 190
COMMON /SARRAY/ VF4(11), CHK(17)-----I 2000-
COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LEADI 210
1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, ADI 220
2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETQB, ETGD, FACTX, FACTY, ADI 230
3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DIADI 240
4MW, JNO1, INO1, R, P, PU, I, J, IDK1, IDK2, NSEG, RCAL-----I 2500-
RETURN-----ADI 260
C-----ADI 270
C-----ADI 280
C ---COMPUTE AND PRINT ITERATION PARAMETERS---ADI 290
C *****ADI 300
C ENTRY ITER3ADI 310
C *****ADI 320
HMIN=2.-----ADI 330
IN4=DIMW-2-----ADI 340
IN5=DIML-2-----ADI 350
XVAL=3.1415**2/(2.*IN4*IN4)-----ADI 360
YVAL=3.1415**2/(2.*IN5*IN5)-----ADI 370
DO 10 I=2, INO1-----ADI 380
DO 10 J=2, JNO1-----ADI 390
N=I+DIML*(J-1)-----ADI 400
IF (T(N).EQ.0.) GO TO 10-----ADI 410
XPART=XVAL*(1/(1+DELX(J)**2*FACTY/DELY(I)**2*FACTX))-----ADI 420
YPART=YVAL*(1/(1+DELY(I)**2*FACTX/DELX(J)**2*FACTY))-----ADI 430
HMIN=AMIN1(HMIN, XPART, YPART)-----ADI 440
10 CONTINUE-----ADI 450
ALPHA=EXP(ALOG(HMAX/HMIN)/(LENGTH-1))-----ADI 460
RHOP(1)=HMIN-----ADI 470
DO 20 NTIME=2, LENGTH-----ADI 480
20 RHOP(NTIME)=RHOP(NTIME-1)*ALPHA-----ADI 490
WRITE (P, 400)-----ADI 500
WRITE (P, 410) LENGTH, (RHOP(J), J=1, LENGTH)-----ADI 510
RETURN-----ADI 520
C-----ADI 530
C-----ADI 540
C ---INITIALIZE DATA FOR A NEW ITERATION---ADI 550
30 KOUNT=KOUNT+1-----ADI 560
IF (KOUNT.LE.ITMAX) GO TO 40-----ADI 570
WRITE (P, 390)-----ADI 580
CALL TERM1-----ADI 590

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40	IF (MOD(KOUNT,LENGTH)) 50,50,60	ADI 600
C	*****	ADI 610
	ENTRY NEWITC	ADI 620
C	*****	ADI 630
50	NTH=0	ADI 640
60	NTH=NTH+1	ADI 650
	PARAM=RHOP(NTH)	ADI 660
	TEST3(KOUNT+1)=0.	ADI 670
	TEST=0.	ADI 680
	N=DIML*DIMW	ADI 690
	DO 70 I=1,N	ADI 700
70	PHE(I)=PHI(I)	ADI 710
	BIGI=0.0	ADI 720
C		ADI 730
C	---COMPUTE TRANSMISSIVITY AND T COEFFICIENTS IN WATER TABLE	ADI 740
C	OR WATER TABLE-ARTESIAN SIMUATION---	ADI 750
	IF (WATER.NE.CHK(2)) GO TO 80	ADI 760
	CALL TRANS	ADI 770
C	.....	ADI 780
C		ADI 790
C	---SOLUTION BY ADI---	ADI 800
C	-----	ADI 810
C	---COMPUTE IMPLICITLY ALONG ROWS---	ADI 820
80	ND3=DIMW-2	ADI 830
	DO 90 J=1,DIMW	ADI 840
	N=1+DIML*(J-1)	ADI 850
90	TEMP(J)=PHI(N)	ADI 860
	DO 230 I=2,DIML	ADI 870
	DO 200 J=2,JND1	ADI 880
	N=I+DIML*(J-1)	ADI 890
	NA=N-1	ADI 900
	NB=N+1	ADI 910
	NL=N-DIML	ADI 920
	NR=N+DIML	ADI 930
	BE(J)=0.0	ADI 940
	G(J)=0.0	ADI 950
C		ADI 960
C	---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---	ADI 970
	IF (T(N).EQ.0..OR.S(N).LT.0.) GO TO 200	ADI 980
C		ADI 990
C	---COMPUTE COEFFICIENTS---	ADI1000
	D=TR(N-DIML)/DELX(J)	ADI1010
	F=TR(N)/DELX(J)	ADI1020
	B=TC(N-1)/DELY(I)	ADI1030
	H=TC(N)/DELY(I)	ADI1040
	IF (EVAP.NE.CHK(6)) GO TO 110	ADI1050
C		ADI1060
C	---COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE---	ADI1070
	ETQB=0.	ADI1080
	ETGD=0.0	ADI1090
	IF (PHE(N).LE.GRND(N)-ETDIST) GO TO 110	ADI1100
	IF (PHE(N).GT.GRND(N)) GO TO 100	ADI1110
	ETQB=GET/ETDIST	ADI1120
	ETGD=ETQB*(ETDIST-GRND(N))	ADI1130
	GO TO 110	ADI1140
100	ETGD=GET	ADI1150
C		ADI1160
C	---COMPUTE STORAGE TERM---	ADI1170
110	IF (CONVRT.EQ.CHK(7)) GO TO 120	ADI1180
	RHO=S(N)/DELT	ADI1190

	IF (WATER.EQ.CHK(2)) RHO=SY(N)/DELT	ADI1200
	GO TO 190	ADI1210
C		ADI1220
C	---COMPUTE STORAGE COEFFICIENT FOR CONVERSION PROBLEM---	ADI1230
120	SUBS=0.0	ADI1240
	IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 160	ADI1250
	IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 150	ADI1260
	IF (KEEP(N)-PHE(N)) 130,140,140	ADI1270
130	SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))	ADI1280
	GO TO 160	ADI1290
140	SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))	ADI1300
150	RHO=SY(N)/DELT	ADI1310
	GO TO 170	ADI1320
160	RHO=S(N)/DELT	ADI1330
170	IF (LEAK.NE.CHK(9)) GO TO 190	ADI1340
C		ADI1350
C	---COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION---	ADI1360
	IF (RATE(N).EQ.0..OR.M(N).EQ.0.) GO TO 190	ADI1370
	HED1=AMAX1(STRT(N),TOP(N))	ADI1380
	U=1.	ADI1390
	HED2=0.	ADI1400
	IF (PHE(N).GE.TOP(N)) GO TO 180	ADI1410
	HED2=TOP(N)	ADI1420
	U=0.	ADI1430
180	SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))	ADI1440
190	CONTINUE	ADI1450
C		ADI1460
C	---CALCULATE VALUES FOR PARAMETERS USED IN THOMAS ALGORITHM	ADI1470
C	AND FORWARD SUBSTITUTE TO COMPUTE INTERMEDIATE VECTOR G---	ADI1480
	IMK=(B+D+F+H)*PARAM	ADI1490
	E=-D-F-RHO-IMK-TL(N)*U-ETQB	ADI1500
	W=E-D*BE(J-1)	ADI1510
	BE(J)=F/W	ADI1520
	Q=-B*PHI(NA)+(B+H-IMK-E)*PHI(N)-H*PHI(NB)-RHO*KEEP(N)-SL(N)-GRE(N)	ADI1530
	1-WELL(N)+ETQB-SUBS-TL(N)*STRT(N)-D*PHI(NL)-F*PHI(NR)	ADI1540
	G(J)=(Q-D*G(J-1))/W	ADI1550
200	CONTINUE	ADI1560
C		ADI1570
C	---BACK SUBSTITUTE FOR HEAD VALUES AND PLACE THEM IN TEMP---	ADI1580
	XII(DIMW)=0.DO	ADI1590
	DO 220 KNO4=1,NO3	ADI1600
	NO4=DIMW-KNO4	ADI1610
	N=I+DIML*(NO4-1)	ADI1620
C		ADI1630
C	---FIRST PLACE TEMP VALUES IN PHI(N-1)---	ADI1640
	PHI(N-1)=TEMP(NO4)	ADI1650
	IF (T(N).NE.0..AND.S(N).GE.0.) GO TO 210	ADI1660
	XII(NO4)=0.DO	ADI1670
	GO TO 220	ADI1680
210	XII(NO4)=G(NO4)-BE(NO4)*XII(NO4+1)	ADI1690
220	TEMP(NO4)=PHI(N)+XII(NO4)	ADI1700
230	CONTINUE	ADI1710
C		ADI1720
C	.....	ADI1730
C	---COMPUTE IMPLICITLY ALONG COLUMNS---	ADI1740
	NO3=DIML-2	ADI1750
	DO 240 I=1,DIML	ADI1760
240	TEMP(I)=PHI(I)	ADI1770
	DO 380 J=2,DIMW	ADI1780
	DO 350 I=2,INO1	ADI1790

N=I+DIML*(J-1)	ADI1800
NA=N-1	ADI1810
NB=N+1	ADI1820
NL=N-DIML	ADI1830
NR=N+DIML	ADI1840
BE(I)=0.0	ADI1850
Q(I)=0.0	ADI1860
C	ADI1870
C ---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---	ADI1880
IF (T(N).EQ.0..OR.S(N).LT.0.) GO TO 350	ADI1890
C	ADI1900
C ---COMPUTE COEFFICIENTS---	ADI1910
D=TR(N-DIML)/DELX(J)	ADI1920
F=TR(N)/DELX(J)	ADI1930
B=TC(N-1)/DELY(I)	ADI1940
H=TC(N)/DELY(I)	ADI1950
IF (EVAP.NE.CHK(6)) GO TO 260	ADI1960
C	ADI1970
C ---COMPUTE EXPLICIT AND IMPLICIT PARTS OF ET RATE---	ADI1980
ETQB=0.	ADI1990
ETGD=0.0	ADI2000
IF (PHE(N).LE.GRND(N)-ETDIST) GO TO 260	ADI2010
IF (PHE(N).GT.GRND(N)) GO TO 250	ADI2020
ETQB=GET/ETDIST	ADI2030
ETGD=ETQB*(ETDIST-GRND(N))	ADI2040
GO TO 260	ADI2050
250 ETGD=GET	ADI2060
C	ADI2070
C ---COMPUTE STORAGE TERM---	ADI2080
260 IF (CONVRT.EQ.CHK(7)) GO TO 270	ADI2090
RHO=S(N)/DELT	ADI2100
IF (WATER.EQ.CHK(2)) RHO=SY(N)/DELT	ADI2110
GO TO 340	ADI2120
C	ADI2130
C ---COMPUTE STORAGE COEFFICIENT FOR CONVERSION PROBLEM---	ADI2140
270 SUBS=0.0	ADI2150
IF (KEEP(N).GE.TOP(N).AND.PHE(N).GE.TOP(N)) GO TO 310	ADI2160
IF (KEEP(N).LT.TOP(N).AND.PHE(N).LT.TOP(N)) GO TO 300	ADI2170
IF (KEEP(N)-PHE(N)) 280,290,290	ADI2180
280 SUBS=(SY(N)-S(N))/DELT*(KEEP(N)-TOP(N))	ADI2190
GO TO 310	ADI2200
290 SUBS=(S(N)-SY(N))/DELT*(KEEP(N)-TOP(N))	ADI2210
300 RHO=SY(N)/DELT	ADI2220
GO TO 320	ADI2230
310 RHO=S(N)/DELT	ADI2240
320 IF (LEAK.NE.CHK(9)) GO TO 340	ADI2250
C	ADI2260
C ---COMPUTE NET LEAKAGE TERM FOR CONVERSION SIMULATION---	ADI2270
IF (RATE(N).EQ.0..OR.M(N).EQ.0.) GO TO 340	ADI2280
HED1=AMAX1(STRT(N),TOP(N))	ADI2290
U=1.	ADI2300
HED2=0.	ADI2310
IF (PHE(N).GE.TOP(N)) GO TO 330	ADI2320
HED2=TOP(N)	ADI2330
U=0.	ADI2340
330 SL(N)=RATE(N)/M(N)*(RIVER(N)-HED1)+TL(N)*(HED1-HED2-STRT(N))	ADI2350
340 CONTINUE	ADI2360
C	ADI2370
C ---CALCULATE VALUES FOR PARAMETERS USED IN THOMAS ALGORITHM	ADI2380
C AND FORWARD SUBSTITUTE TO COMPUTE INTERMEDIATE VECTOR G---	ADI2390

	IMK=(B+D+F+H)*PARAM	ADI2400
	E=-B-H-RHO-IMK-TL(N)*U-ETQB	ADI2410
	W=E-B*BE(I-1)	ADI2420
	BE(I)=H/W	ADI2430
	Q=-D*PHI(NL)+(D+F-IMK-E)*PHI(N)-F*PHI(NR)-RHO*KEEP(N)-SL(N)-GRE(N)	ADI2440
	1-WELL(N)+ETGD-SUBS-TL(N)*STRT(N)-B*PHI(NA)-H*PHI(NB)	ADI2450
	Q(I)=(Q-B*G(I-1))/W	ADI2460
350	CONTINUE	ADI2470
C		ADI2480
C	---BACK SUBSTITUTE FOR HEAD VALUES AND PLACE THEM IN TEMP---	ADI2490
	XII(DIML)=0. DO	ADI2500
	DO 370 KNO4=1, NO3	ADI2510
	NO4=DIML-KNO4	ADI2520
	N=NO4+DIML*(J-1)	ADI2530
C		ADI2540
C	---FIRST PLACE TEMP VALUES IN PHI(N-DIML)----	ADI2550
	PHI(N-DIML)=TEMP(NO4)	ADI2560
	IF (T(N). NE. 0. . AND. S(N). GE. 0. ) GO TO 360	ADI2570
	XII(NO4)=0. DO	ADI2580
	TEMP(NO4)=PHI(N)	ADI2590
	GO TO 370	ADI2600
360	XII(NO4)=G(NO4)-BE(NO4)*XII(NO4+1)	ADI2610
	TEMP(NO4)=PHI(N)+XII(NO4)	ADI2620
C		ADI2630
C	---COMPARE MAGNITUDE OF CHANGE WITH CLOSURE CRITERION---	ADI2640
	TCHK=ABS(SNGL(TEMP(NO4))-PHE(N))	ADI2650
	IF (TCHK. GT. BIGI) BIGI=TCHK	ADI2660
370	CONTINUE	ADI2670
380	CONTINUE	ADI2680
	IF (BIGI. GT. ERR) TEST=1.	ADI2690
	TEST3(KOUNT+1)=BIGI	ADI2700
	IF (TEST. EQ. 1. ) GO TO 30	ADI2710
	RETURN	ADI2720
C	.....	ADI2730
C		ADI2740
C	---FORMATS---	ADI2750
C		ADI2760
C	-----	ADI2770
C		ADI2780
C		ADI2790
390	FORMAT ('OEXCEEDED PERMITTED NUMBER OF ITERATIONS'' ',39('*'))	ADI2800
400	FORMAT ('-',38X, 'SOLUTION BY THE ALTERNATING DIRECTION IMPLICIT PRADI2810	
	1OCEDURE'/39X, 56('_'))	ADI2820
410	FORMAT (///1H0, I5, 22H ITERATION PARAMETERS: , 8D12. 3//28X, 10D12. 3)	ADI2830
	END	ADI2840-

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SUBROUTINE COEF(PHI,KEEP,PHE,STRT,SURI,T,TR,TC,S,WELL,TL,SL,PERM,BCOF 10
1OTTOM,SY,RATE,RIVER,M,TOP,GRND,DELX,DELY,RSEQ,IRIV,NRSEQ) F 200-
C -----COF 30
C COMPUTE COEFFICIENTS COF 40
C -----COF 50
C COF 60
C SPECIFICATIONS: COF 70
C REAL *8PHI,DBLE,RHO,B,D,F,H COF 80
C REAL *4KEEP,M COF 90
C INTEGER R,P,PU,DIML,DIMW,CHK,WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD, COF 100
1CONTR,LEAK,RECH,SIP,ADI,RCAL F 1100-
C DIMENSION ISORT(150) F 1101-
C COF 120
C DIMENSION PHI(1),KEEP(1),PHE(1),STRT(1),SURI(1),T(1),TR(1), COF 130
1TC(1),S(1),WELL(1),TL(1),SL(1),PERM(1),BOTTOM(1),SY(1),RATCOF 140
2E(1),RIVER(1),M(1),TOP(1),GRND(1),DELX(1),DELY(1),RSEQ(1), F 1500-
3IRIV(1),NRSEQ(1) F 1501-
C COF 160
C COMMON /SARRAY/ VF4(11),CHK(17) F 1700-
C COMMON /SPARAM/ WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CONTR,EROR,LECOF 180
1AK,RECH,SIP,U,SS,TT,TMIN,ETDIST,GET,ERR,TMAX,CDLT,HMAX,YDIM,WIDTH, COF 190
2NUMS,LSOR,ADI,DELT,SUM,SUMP,SUBS,STORE,TEST,ETQB,ETGD,FACTX,FACTY, COF 200
3IERR,KOUNT,IFINAL,NUMT,KT,KP,NPER,KTH,ITMAX,LENGTH,NWEL,NW,DIML,DICOF 210
4MW,JND1,IND1,R,P,PU,I,J,IDK1,IDK2,NSEQ,RCAL F 2200-
C COF 230
C DATA PIE/3.141593/ COF 235
C RETURN COF 240
C ..... COF 250
C COF 260
C ---COMPUTE COEFFICIENTS FOR TRANSIENT PART OF LEAKAGE TERM--- COF 270
C ***** COF 280
C ENTRY CLAY COF 290
C ***** COF 300
C TMIN=1.E30 COF 310
C TT=0.0 COF 320
C PRATE=0. COF 330
C DO 50 I=1,DIML COF 340
C DO 50 J=1,DIMW COF 350
C N=I+DIML*(J-1) COF 360
C COF 370
C ---SKIP COMPUTATIONS IF T, RATE OR M = 0, OR IF CONSTANT COF 380
C HEAD BOUNDARY--- COF 390
C IF (RATE(N).LE.0..OR.T(N).EQ.0..OR.M(N).EQ.0..OR.S(N).LT.0.) GO TOCOF 400
1 50 COF 410
C COF 420
C ---IF VALUE FOR TL(N ) WILL EQUAL VALUE FOR PREVIOUS NODE, COF 430
C SKIP PART OF COMPUTATIONS--- COF 440
C IF (RATE(N)*M(N).EQ.PRATE) GO TO 40 COF 450
C DIMT=RATE(N)*SUMP/(M(N)*M(N)*SS*3) COF 460
C IF (DIMT.GT.TT) TT=DIMT COF 470
C IF (DIMT.LT.TMIN) TMIN=DIMT COF 480
C PPT=PIE*PIE*DIMT COF 490
C COF 500
C ---RECOMPUTE PPT IF DIMT WITHIN RANGE FOR SHORT TIME COMPUTATION---COF 510
C IF (DIMT.LT.1.OE-03) PPT=1.0/DIMT COF 520
C CC=(2.3-PPT)/(2.*PPT) COF 530
C COF 540
C ---COMPUTE SUM OF EXPONENTIALS--- COF 550
C SUMN=0.0 COF 560

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	DO 20 K=1,200	COF 570
	POWER=K*K*PPT	COF 580
	IF (POWER.LE.150.) GO TO 10	COF 590
	POWER=150	COF 600
10	PEX=EXP(-POWER)	COF 610
	SUMN=SUMN+PEX	COF 620
	IF (PEX.GT.0.00009) GO TO 20	COF 630
	IF (K.GT.CC) GO TO 30	COF 640
20	CONTINUE	COF 650
C		COF 660
C	---COMPUTE DENOMINATER DEPENDING ON VALUE OF DMT---	COF 670
30	DENOM=1.0	COF 680
	IF (DMT.LT.1.0E-03) DENOM=SQRT(PIE*DMT)	COF 690
C		COF 700
C	---HEAD VALUES ARE NOT INCLUDED IN COMPUTATION OF Q FACTOR SINCE	COF 710
C	LEAKAGE IS CONSIDERED IMPLICITLY---	COF 720
40	Q1=RATE(N)/(M(N)*DENOM)	COF 730
	TL(N)=Q1+2.*Q1*SUMN	COF 740
	PRATE=RATE(N)*M(N)	COF 750
50	CONTINUE	COF 760
	TMIN=TMIN*3.0	COF 770
	TT=TT*3.0	COF 780
	RETURN	COF 790
C		COF 800
C	.....	COF 810
C	---COMPUTE TRANSMISSIVITY IN WT OR WT-ARTESIAN CONVERSION PROBLEM---	COF 820
C	*****	COF 830
	ENTRY TRANS	COF 840
C	*****	COF 850
	DO 60 I=1,DIML	COF 860
	DO 60 J=1,DIMW	COF 870
	N=I+DIML*(J-1)	COF 880
	IF (PERM(N).EQ.0.) GO TO 60	COF 890
	HED=PHI(N)	COF 900
	IF (CONVRT.EQ.CHK(7)) HED=AMIN1(SNGL(PHI(N)),TOP(N))	COF 910
	T(N)=PERM(N)*(HED-BOTTOM(N))	COF 920
	IF (T(N).GT.0.) GO TO 60	COF 930
	IF (WELL(N).LT.0.) GO TO 70	COF 940
C		COF 950
C	---THE FOLLOWING STATEMENTS APPLY WHEN NODES (EXCEPT WELL NODES)	COF 960
C	GO DRY---	COF 970
	PERM(N)=0.	COF 980
	T(N)=0.0	COF 990
	TR(N-DIML)=0.	COF1000
	TR(N)=0.	COF1010
	TC(N-1)=0.	COF1020
	TC(N)=0.	COF1030
	PHI(N)=SURI(N)	COF1040
	WRITE (P,150) I,J	COF1050
60	CONTINUE	COF1060
	IF (KT.EQ.0). RETURN	COF1070
	GO TO 90	COF1080
C		COF1090
C	---START PROGRAM TERMINATION WHEN A WELL GOES DRY---	COF1100
70	WRITE (P,120) I,J	COF1110
	WRITE (P,130)	COF1120
	IERR=1	COF1130
	CALL DRDN	COF1140
	DO 80 I=2,IND1	COF1150
	DO 80 J=2,JND1	COF1160

N=I+DIML*(J-1)	COF1170
80 PHI(N)=KEEP(N)	COF1180
SUM=SUM-DELT	COF1190
SUMP=SUMP-DELT	COF1200
KT=KT-1	COF1210
IF (KT.EQ.0) STOP	COF1220
IF (IDK2.EQ.CHK(15)) CALL DISK	COF1230
IF (PNCH.EQ.CHK(1)) CALL PUNCH	COF1240
IF (MOD(KT,KTH).EQ.0) STOP	COF1250
WRITE (P,140) KT,SUM	COF1260
CALL DRDN	COF1270
IF (CHCK.EQ.CHK(5)) CALL CWRITE	COF1280
STOP	COF1290
C	COF1300
C ---COMPUTE T COEFFICIENTS---	COF1310
C *****	COF1320
ENTRY TCOF	COF1330
C *****	COF1340
90 DO 110 I=1,IND1	COF1350
DO 110 J=1,JND1	COF1360
N=I+DIML*(J-1)	COF1370
NR=N+DIML	COF1380
NB=N+1	COF1390
IF (T(N).EQ.0.) GO TO 110	COF1400
IF (T(NR).EQ.0.) GO TO 100	COF1410
TR(N)=(2.*T(NR)*T(N))/(T(N)*DELX(J+1)+T(NR)*DELX(J))*FACTX	COF1420
100 IF (T(NB).EQ.0.) GO TO 110	COF1430
TC(N)=(2.*T(NB)*T(N))/(T(N)*DELY(I+1)+T(NB)*DELY(I))*FACTY	COF1440
110 CONTINUE	COF1450
RETURN	COF1460
C	F14601-
C	F14602-
C ---PREPARE A MATRIX WHICH WILL PUT RIVER SEGMENTS IN ORDER FROM	F14603-
C HIGHEST TO LOWEST RIVER HEADS---	F14604-
C *****	F14605-
ENTRY RSORT	F14606-
C *****	F14607-
DO 260 K=1,NSEG	F14608-
L=1	F14609-
DO 210 I=1,DIML	F14610-
DO 210 J=1,DIMW	F14611-
N=I+DIML*(J-1)	F14612-
IF (RIVER(N).EQ.0.) GO TO 210	F14613-
RR=RSEG(N)	F14614-
ISEG=INT(RR)	F14615-
IF (ISEG.NE.K) GO TO 210	F14616-
ISORT(L)=N	F14617-
L=L+1	F14618-
210 CONTINUE	F14619-
L=L-1	F14620-
LL=L-1	F14621-
LLL=L-1	F14622-
DO 240 II=1,LL	F14623-
DO 230 JJ=1,LLL	F14624-
IF (RIVER(ISORT(JJ+1)).GT.RIVER(ISORT(JJ))) GO TO 220	F14625-
GO TO 230	F14626-
220 LTEMP1=ISORT(JJ+1)	F14627-
LTEMP2=ISORT(JJ)	F14628-
ISORT(JJ)=LTEMP1	F14629-
ISORT(JJ+1)=LTEMP2	F14630-

230	CONTINUE	F14631-
240	CONTINUE	F14632-
	DO 250 LJ=1,L	F14633-
250	IRIV(ISORT(LJ))=LJ	F14634-
	NRSEQ(K)=L	F14635-
260	CONTINUE	F14636-
	RETURN	F14637-
C		COF1470
C	---FORMATS---	COF1480
C		COF1490
C	-----	COF1500
C		COF1510
C		COF1520
120	FORMAT ('-*****WELL', I3, ', ', I3, ' GOES DRY*****')	COF1530
130	FORMAT ('1', 50X, 'DRAWDOWN WHEN WELL WENT DRY')	COF1540
140	FORMAT ('1', 32X, 'DRAWDOWN FOR TIME STEP', I3, ', SIMULATION TIME =',	COF1550
	11PE15.7, ' SECONDS')	COF1560
150	FORMAT ('-', 20('*'), ' NODE ', I4, ', ', I4, ' GOES DRY ', 20('*'))	COF1570
	END	COF1580-

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SUBROUTINE CHECKI(PHI,KEEP,PHE,STRT,T,TR,TC,S,GRE,WELL,TL,PERM,BOTCHK 10
1TOM,SY,RATE,RIVER,M,TOP,GRND,DELX,DELY,PICK,PICKUP,RSEG,IRIV,NRSEGK 200-
2,FLOWIN,WIDE,SLOPE,IFLOUT,ROUGH,PREPIC,SL,FLOWAD) K 201-
C -----CHK 30
C COMPUTE A MASS BALANCE CHK 40
C -----CHK 50
C CHK 60
C SPECIFICATIONS: CHK 70
C REAL *8PHI,DBLE CHK 80
C REAL *4KEEP,M CHK 90
C INTEGER R,P,PU,DIML,DIMW,CHK,WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CHK 100
1CONTR,LEAK,RECH,SIP,ADI,RCAL CHK 110
C CHK 120
C DIMENSION PHI(IZ,JZ),KEEP(IZ,JZ),PHE(IZ,JZ),STRT(IZ,JZ),T(IZ,JCHK 130
1Z),TR(IZ,JZ),TC(IZ,JZ),S(IZ,JZ),GRE(IZ,JZ),WELL(IZ,JZ),TL(IZCHK 140
2,JZ),PERM(IZ,JZ),BOTTOM(IP,JP),SY(IP,JP),RATE(IR,JR),RIVER(IRCHK 150
3,JR),M(IR,JR),TOP(IC,JC),GRND(IL,JL),DELX(JZ),DELY(IZ),PICK(K 1600-
4IR,JR),PICKUP(IR,JR),RSEG(IR,JR),IRIV(IA,JA),NRSEG(1K),FLOWINK 1601-
5(1K),WIDE(1K),SLOPE(1K),IFLOUT(1K),ROUGH(1K),PREPIC(IA,JA),SK 1602-
6L(IZ,JZ),FLOWAD(1K) K 1603-
C CHK 170
COMMON /SARRAY/ VF4(11),CHK(17) K 1800-
COMMON /SPARAM/ WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CONTR,EROR,LECHK 190
1AK,RECH,SIP,U,SS,TT,TMIN,ETDIST,GET,ERR,TMAX,CDLT,HMAX,YDIM,WIDTH,CHK 200
2NUMS,LSOR,ADI,DELT,SUM,SUMP,SUBS,STORE,TEST,ETQB,ETGD,FACTX,FACTY,CHK 210
3IERR,KOUNT,IFINAL,NUMT,KT,KP,NPER,KTH,ITMAX,LENGTH,NWEL,NW,DIML,D1CHK 220
4MW,JND1,IND1,R,P,PU,I,J,1DK1,1DK2,NSEQ,RCAL K 2300-
COMMON /CK/ ETFLXT,STORT,GRET,CHST,CHDT,FLXT,PUMPT,CFLXT,FLXNT,1K 2400-
1RCHK,RAIN,PANEVA,IRCHK1 K 2401-
COMMON /ARSize/ IZ,JZ,IP,JP,IR,JR,IC,JC,IL,JL,IS,JS,IH,IMAX,IMX1,1K 2500-
1K,IA,JA K 2501-
COMMON /MPARAM/ FACTQ,NEWW,NEWG,ERLEAK,DAYS K 2502-
RETURN CHK 260
C .....CHK 270
C *****CHK 280
C ENTRY CHECK CHK 290
C *****CHK 300
C ---INITIALIZE VARIABLES---CHK 310
C PCHK=0.0 K 3101-
C PUMP=0. CHK 320
C STOR=0. CHK 330
C FLUXS=0.0 CHK 340
C CHD1=0.0 CHK 350
C CHD2=0.0 CHK 360
C GREFLX=0. CHK 370
C CFLUX=0. CHK 380
C FLUX=0. CHK 390
C ETFLUX=0. CHK 400
C FLXN=0.0 CHK 410
C .....CHK 420
C .....CHK 430
C ---COMPUTE RATES,STORAGE AND PUMPAGE FOR THIS STEP---CHK 440
C DO 240 I=2,DIML CHK 450
C DO 240 J=2,DIMW CHK 460
C IF (T(I,J).EQ.0.) GO TO 240 CHK 470
C AREA=DELX(J)*DELY(I) CHK 480
C IF (IRCHK.EQ.0) GO TO 235 K 4801-
C IF (S(I,J).GE.0.) GO TO 120 CHK 490
C .....CHK 500

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C	---COMPUTE FLOW RATES TO AND FROM CONSTANT HEAD BOUNDARIES---	CHK 510
	IF (S(I, J-1).LT.0..OR.T(I, J-1).EQ.0.) GO TO 30	CHK 520
	X=(STRT(I, J)-PHI(I, J-1))*TR(I, J-1)*DELY(I)	CHK 530
	IF (X) 10, 30, 20	CHK 540
10	CHD1=CHD1+X	CHK 550
	GO TO 30	CHK 560
20	CHD2=CHD2+X	CHK 570
30	IF (S(I, J+1).LT.0..OR.T(I, J+1).EQ.0.) GO TO 60	CHK 580
	X=(STRT(I, J)-PHI(I, J+1))*TR(I, J)*DELY(I)	CHK 590
	IF (X) 40, 60, 50	CHK 600
40	CHD1=CHD1+X	CHK 610
	GO TO 60	CHK 620
50	CHD2=CHD2+X	CHK 630
60	IF (S(I-1, J).LT.0..OR.T(I-1, J).EQ.0.) GO TO 90	CHK 640
	X=(STRT(I, J)-PHI(I-1, J))*TC(I-1, J)*DELX(J)	CHK 650
	IF (X) 70, 90, 80	CHK 660
70	CHD1=CHD1+X	CHK 670
	GO TO 90	CHK 680
80	CHD2=CHD2+X	CHK 690
90	IF (S(I+1, J).LT.0..OR.T(I+1, J).EQ.0.) GO TO 240	CHK 700
	X=(STRT(I, J)-PHI(I+1, J))*TC(I, J)*DELX(J)	CHK 710
	IF (X) 100, 240, 110	CHK 720
100	CHD1=CHD1+X	CHK 730
	GO TO 240	CHK 740
110	CHD2=CHD2+X	CHK 750
	GO TO 240	CHK 760
C		CHK 770
C	---RECHARGE AND WELLS---	CHK 780
120	GREFLX=GREFLX+GRE(I, J)*AREA	CHK 790
	IF (WELL(I, J)) 130, 150, 140	CHK 800
130	PUMP=PUMP+WELL(I, J)*AREA	CHK 810
	GO TO 150	CHK 820
140	CFLUX=CFLUX+WELL(I, J)*AREA	CHK 830
150	IF (EVAP.NE.CHK(6)) GO TO 190	CHK 840
C		CHK 850
C	---COMPUTE ET RATE---	CHK 860
	IF (PHI(I, J).GE.GRND(I, J)-ETDIST) GO TO 160	CHK 870
	ETQ=0.0	CHK 880
	GO TO 180	CHK 890
160	IF (PHI(I, J).LE.0RND(I, J)) GO TO 170	CHK 900
	ETQ=GET	CHK 910
	GO TO 180	CHK 920
170	ETQ=GET/ETDIST*(PHI(I, J)+ETDIST-0RND(I, J))	CHK 930
180	ETFLUX=ETFLUX-ETQ*AREA	CHK 940
C		CHK 950
C	---COMPUTE VOLUME FROM STORAGE---	CHK 960
190	STORE=S(I, J)	CHK 970
	IF (WATER.EQ.CHK(2)) STORE=SY(I, J)	CHK 980
	IF (CONVRT.NE.CHK(7)) GO TO 230	CHK 990
	X=KEEP(I, J)-PHI(I, J)	CHK1000
	IF (X) 200, 210, 210	CHK1010
200	HED1=PHI(I, J)	CHK1020
	HED2=KEEP(I, J)	CHK1030
	X=ABS(X)	CHK1040
	GO TO 220	CHK1050
210	HED1=KEEP(I, J)	CHK1060
	HED2=PHI(I, J)	CHK1070
220	STORE=S(I, J)	CHK1080
	IF (HED1-TOP(I, J).LE.0.) STORE=SY(I, J)	CHK1090
	IF ((HED1-TOP(I, J))*(HED2-TOP(I, J)).LT.0.0) STORE=(HED1-TOP(I, J))/CHK1100	

	1X*S(I,J)+(TOP(I,J)-HED2)/X*SY(I,J)	CHK1110
	230 STOR=STOR+STORE*(KEEP(I,J)-PHI(I,J))*AREA	CHK1120
C		CHK1130
C	---COMPUTE LEAKAGE RATE---	CHK1140
	235 IF (LEAK.NE.CHK(9)) GO TO 240	CHK1150
	IF (M(I,J).EQ.0.) GO TO 240	CHK1160
	HED1=STRT(I,J)	CHK1170
	IF (CONVRT.EQ.CHK(7)) HED1=AMAX1(STRT(I,J),TOP(I,J))	CHK1180
	HED2=PHI(I,J)	CHK1190
	IF (CONVRT.EQ.CHK(7)) HED2=AMAX1(SNGL(PHI(I,J)),TOP(I,J))	CHK1200
	XX=RATE(I,J)*(RIVER(I,J)-HED1)*AREA/M(I,J)	CHK1210
	YY=TL(I,J)*(HED1-HED2)*AREA	CHK1220
	FLUX=FLUX+XX	CHK1230
	XNET=XX+YY	CHK1240
	FLUXS=FLUXS+XNET	CHK1250
	IF (XNET.LT.0.) FLXN=FLXN-XNET	CHK1260
	IF (RCAL.EQ.CHK(17)) PREPIC(I,J)=PICK(I,J)	K12601-
	PICK(I,J)=XNET	K12602-
	IF (RCAL.NE.CHK(17)) PICKUP(I,J)=PICKUP(I,J)+PICK(I,J)*DELT	K12603-
	IF (RCAL.NE.CHK(17)) GO TO 240	K12604-
	PCHK=AMAX1(PCHK,ABS(PICK(I,J)-PREPIC(I,J)))	K12605-
	240 CONTINUE	CHK1270
	IF (RCAL.NE.CHK(17)) GO TO 245	K12701-
	WRITE (P,930) PCHK,ERLEAK	K12702-
	IF (PCHK.GT.ERLEAK) GO TO 250	K12703-
	IRCHK1=IRCHK	K12704-
	IRCHK=1	K12705-
C	.....	CHK1280
C		CHK1290
C	---COMPUTE CUMULATIVE VOLUMES, TOTALS, AND DIFFERENCES---	CHK1300
	245 IF (IRCHK1.EQ.0) GO TO 250	K13001-
	STORT=STORT+STOR	CHK1310
	STOR=STOR/DELT	CHK1320
	ETFLXT=ETFLXT-ETFLUX*DELT	CHK1330
	FLUXT=FLUXT+FLUXS*DELT	CHK1340
	FLXNT=FLXNT+FLXN*DELT	CHK1350
	FLXPT=FLUXT+FLXNT	CHK1360
	GRET=GRET+GREFLX*DELT	CHK1370
	CHDT=CHDT-CHD1*DELT	CHK1380
	CHST=CHST+CHD2*DELT	CHK1390
	PUMPT=PUMPT-PUMP*DELT	CHK1400
	CFLUXT=CFLUXT+CFLUX*DELT	CHK1410
	TOTL1=STORT+GRET+CFLUXT+CHST+FLXPT	CHK1420
	TOTL2=CHDT+PUMPT+ETFLXT+FLXNT	CHK1430
	SUMR=GREFLX+CFLUX+CHD2+CHD1+PUMP+ETFLUX+FLUXS+STOR	CHK1440
	DIFF=TOTL2-TOTL1	CHK1450
	PERCNT=0.0	CHK1460
	IF (TOTL2.EQ.0.) GO TO 250	CHK1470
	PERCNT=DIFF/TOTL2*100.	CHK1480
	250 RETURN	CHK1490
C	.....	CHK1500
C		CHK1510
C	---PRINT RESULTS---	CHK1520
C	*****	CHK1530
C	ENTRY CWRITE	CHK1540
C	*****	CHK1550
C		CHK1560
	IF (IRCHK1.EQ.0) GO TO 261	K15601-
	WRITE (P,260) STOR,GREFLX,STORT,CFLUX,GRET,PUMP,CFLUXT,ETFLUX,CHSTCHK1570	
	1,FLXPT,CHD2,TOTL1,CHD1,FLUX,FLUXS,ETFLXT,CHDT,SUMR,PUMPT,FLXNT,TOTCHK1580	

2L2, DIFF, PERCNT	CHK1590
261 IF (LEAK. NE. CHK(9)) GO TO 285	K15901-
IF (NSEQ. EQ. 0) GO TO 285	K15902-
WRITE (P, 280)	K15903-
DO 275 K=1, NSEQ	K15904-
PICSUM=0.	K15905-
PICKS=0.	K15906-
IF (RCAL. NE. CHK(17)) GO TO 262	K15907-
FLOSUM=0. 0	K15908-
NNODE=NRSEQ(K)	K15909-
DO 272 NN=1, NNODE	K15910-
262 DO 270 I=1, DIML	K15911-
DO 270 J=1, DIMW	K15912-
IF (RIVER(I, J). EQ. 0.) GO TO 270	K15913-
RR=RSEQ(I, J)	K15914-
ISEG=INT(RR)	K15915-
IF (ISEG. NE. K) GO TO 270	K15916-
IF (RCAL. NE. CHK(17)) GO TO 264	K15917-
IF (IRIV(I, J). NE. NN) GO TO 270	K15918-
264 RK=FLOAT(K)	K15919-
RRK=RR-RK	K15920-
RRK=RRK*10. 0+0. 1	K15921-
MR=INT(RRK)	K15922-
IF (MR. LT. 1) GO TO 269	K15923-
IF (RCAL. NE. CHK(17)) GO TO 266	K15924-
IF (NN. EQ. 1) FLOSUM=FLOWAD(K)	K15925-
FLOSUM=FLOSUM-PICK(I, J)	K15926-
IF (FLOSUM. LT. 0. 0. AND. MR. LT. 3) PICK(I, J)=0. 0	K15927-
IF (FLOSUM. LT. 0. 0) FLOSUM=0.	K15928-
PICKUP(I, J)=FLOSUM	K15929-
266 WRITE (P, 290) I, J, PICK(I, J), PICKUP(I, J)	K15930-
PICSUM=PICSUM+PICK(I, J)	K15931-
269 PICKS=PICKS+PICK(I, J)	K15932-
270 CONTINUE	K15933-
272 CONTINUE	K15934-
IF (PICSUM. NE. 0.) WRITE (P, 310) PICSUM	K15935-
PICOUT=-PICSUM	K15936-
IF (IRCHK. EQ. 1) WRITE (10, 940) DAYS, PICOUT	K15937-
275 WRITE (P, 300) K, PICKS	K15938-
285 RETURN	K15939-
C	K15940-
C	K15941-
C	K15942-
C	K15943-
C	K15944-
C	K15945-
C	K15946-
C	K15947-
IF (NSEQ. EQ. 0) GO TO 510	K15948-
DO 390 K=1, NSEQ	K15949-
390 FLOWAD(K)=FLOWIN(K)	K15950-
DO 500 K=1, NSEQ	K15951-
FLOW=0.	K15952-
TOTAR=0.	K15953-
NNODE=NRSEQ(K)	K15954-
DO 440 NN=1, NNODE	K15955-
DO 430 I=1, DIML	K15956-
DO 430 J=1, DIMW	K15957-
IF (RIVER(I, J). EQ. 0.) GO TO 430	K15958-
C	K15959-
--- <td></td>	

	RR=RSEG(I,J)	K15960-
	ISEG=INT(RR)	K15961-
	IF (ISEG.NE.K) GO TO 430	K15962-
C	---FIND THE FIRST NODE OF RIVER SEGMENT---	K15963-
	IF (IRIV(I,J).NE.NN) GO TO 430	K15964-
	IF (NN.GT.1) GO TO 400	K15965-
C	---FIND THE CALCULATION OPTION FOR THE RIVER SEGMENT---	K15966-
	GROUND=GRND(I,J)	K15967-
	POND=RIVER(I,J)	K15968-
	RK=FLOAT(K)	K15969-
	RRK=RR-RK	K15970-
	RRK=RRK*10.0+0.1	K15971-
	MR=INT(RRK)	K15972-
	MR=MR+1	K15973-
	400 GO TO (500,500,410,420),MR	K15974-
C	---RIVER SEGMENT---	K15975-
	410 IF (NN.EQ.1) FLOW=FLOWAD(K)	K15976-
	FLOW=FLOW-PICK(I,J)	K15977-
	IF (FLOW.LT.0.) FLOW=0.	K15978-
	PAY=FLOW*ROUGH(K)	K15979-
	PAYDA=1.486*WIDE(K)*(SQRT(SLOPE(K)))	K15980-
	DEPTH=(PAY/PAYDA)**0.6	K15981-
	RIVER(I,J)=GRND(I,J)+DEPTH	K15982-
	IF (DEPTH.GT.0.0) GO TO 430	K15983-
	RIVER(I,J)=GRND(I,J)	K15984-
	WRITE (P,320) I,J	K15985-
	GO TO 430	K15986-
C	---POND SEGMENT---	K15987-
	420 IF (NN.EQ.1) FLOW=FLOWAD(K)*DELT	K15988-
	IF (GRND(I,J).GT.GROUND) GO TO 425	K15989-
	GROUND=GRND(I,J)	K15990-
	POND=RIVER(I,J)	K15991-
	425 AREA=DELX(J)*DELY(I)	K15992-
	TOTAR=TOTAR+AREA	K15993-
	RAINP=RAIN*AREA*DELT	K15994-
	EVAPO=PAVEVA*AREA*DELT	K15995-
	FLOW=FLOW+RAINP-EVAPO-(PICK(I,J)*DELT)	K15996-
	IF (NN.EQ.1) FLEAK=FLOWAD(K)	K15997-
	FLEAK=FLEAK-PICK(I,J)	K15998-
	430 CONTINUE	K15999-
	440 CONTINUE	K16000-
	GO TO (500,500,490,450),MR	K16001-
C	---POND SEGMENT---	K16002-
	450 KK=IFLOUT(K)	K16003-
	IF (KK.EQ.0) GO TO 465	K16004-
	DO 460 I=1,DIML	K16005-
	DO 460 J=1,DIMW	K16006-
	IF (RIVER(I,J).EQ.0.) GO TO 460	K16007-
	RR=RSEG(I,J)	K16008-
	ISEG=INT(RR)	K16009-
	IF (ISEG.NE.KK) GO TO 460	K16010-
	IF (IRIV(I,J).NE.1) GO TO 460	K16011-
	IKK=I	K16012-
	JKK=J	K16013-
	460 CONTINUE	K16014-
	IF (POND.LT.GRND(IKK,JKK)) GO TO 465	K16015-
	FLOWR=(TOTAR*(RAIN-PAVEVA))+FLEAK	K16016-
	IF (FLOWR.LT.0.) GO TO 465	K16017-
	462 PAY=FLOWR*ROUGH(KK)	K16018-
	PAYDA=1.486*WIDE(KK)*(SQRT(SLOPE(KK)))	K16019-



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DST=(PAY/PAYDA)**0.6
PONDN=(3*DST/2)+GRND(IKK,JKK)
GO TO 467
465 DEPTH=FLOW/TOTAR
PONDN=POND+DEPTH
IF (KK.EQ.0) GO TO 467
IF (PONDN.LT.GRND(IKK,JKK)) GO TO 467
PONDIF=GRND(IKK,JKK)-POND
FLODIF=FLOW-(PONDIF*TOTAR)
FLOWR=FLODIF/DELT
GO TO 462
467 CONTINUE
DO 480 I=1,DIML
DO 480 J=1,DIMW
IF (RIVER(I,J).EQ.0.) GO TO 480
RR=RSEQ(I,J)
ISEG=INT(RR)
IF (ISEG.NE.K) GO TO 480
RIVER(I,J)=PONDN
IF (RIVER(I,J).LT.GRND(I,J)) GO TO 470
GO TO 480
470 RIVER(I,J)=GRND(I,J)
WRITE (P,330) I,J
480 CONTINUE
IF (KK.GT.0.AND.FLOWR.GT.0.0) FLOWAD(KK)=FLOWR
GO TO 500
490 IF (IFLOUT(K).NE.0) FLOWAD(IFLOUT(K))=FLOWIN(IFLOUT(K))+FLOW
500 CONTINUE
C
DO 505 I=1,DIML
DO 505 J=1,DIMW
IF (M(I,J).EQ.0.) GO TO 505
SL(I,J)=RATE(I,J)/M(I,J)*(RIVER(I,J)-STRT(I,J))
505 CONTINUE
DO 800 I=1,DIML
800 WRITE (P,990) I,(RIVER(I,J),J=1,DIMW)
510 RETURN
C
C ---FORMATS---
C
C -----
C
C
260 FORMAT ('0',10X,'CUMULATIVE MASS BALANCE:',16X,'L**3',23X,'RATES FCHK1670
10R THIS TIME STEP:',16X,'L**3/T',11X,24('-'),43X,25('-')//20X,'SOUCHK1680
2RCES:',69X,'STORAGE =',F20.4/20X,8('-'),68X,'RECHARGE =',F20.4/27XCHK1690
3,'STORAGE =',F20.2/35X,'CONSTANT FLUX =',F20.4/26X,'RECHARGE =',F2CHK1700
40.2/41X,'PUMPING =',F20.4/21X,'CONSTANT FLUX =',F20.2/30X,'EVAPOTRCHK1710
3ANSPIRATION =',F20.4/21X,'CONSTANT HEAD =',F20.2/34X,'CONSTANT HEACHK1720
6D:',27X,'LEAKAGE =',F20.2/46X,'IN =',F20.4/21X,'TOTAL SOURCES =',FCHK1730
720.2/45X,'OUT =',F20.4/96X,'LEAKAGE:',20X,'DISCHARGES:',45X,'FROM CHK1740
8PREVIOUS PUMPING PERIOD =',F20.4/20X,11('-'),68X,'TOTAL =',F20.4/1CHK1750
96X,'EVAPOTRANSPIRATION =',F20.2/21X,'CONSTANT HEAD =',F20.2/36X,'SCHK1760
$UM OF RATES =',F20.4/19X'QUANTITY PUMPED =',F20.2/27X,'LEAKAGE =',CHK1770
$F20.2/19X,'TOTAL DISCHARGE =',F20.2//17X,'DISCHARGE-SOURCES =',F20CHK1780
$.2/15X,'PER CENT DIFFERENCE =',F20.2//) CHK1790
280 FORMAT (1H1,///,60X,'LEAKAGE INTO (-) AND OUT OF (+) THE RIVER',/,K17901-
160X,41('-'),///,64X,'LEAKAGE RATE',10X,' CUMULATIVE FLOW ',/,42X,K17902-
2'I',9X,'J',13X,'(L**3/T)',18X,'(L**3/T)',/,40X,5('-'),5X,5('-'),5XK17903-
3.20('-'),5X,20('-'),//) K17904-

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290 FORMAT (41X, I3, 7X, I3, 11X, F10.4, 10X, F15.4) K17905-
300 FORMAT ('-', //, 78X, 'RIVER SEGMENT NUMBER =', I5, //, 74X, 'SUM OF THE SK17906-
2EEPAGE RATES =', F10.4, 2X, '(L**3/T)', //) K17907-
310 FORMAT ('-', //, 58X, 'TOTAL =', F10.4) K17908-
320 FORMAT ('-', 10X, '*****WARNING RIVER NODE', I5, ' ', ' ', I5, 'GOES DRYK17909-
1*****') K17910-
330 FORMAT ('-', 10X, '*****WARNING POND NODE', I5, ' ', ' ', I5, 'GOES DRYK17911-
1*****') K17912-
930 FORMAT ('-', 30X, 'MAXIMUM CHANGE IN LEAKAGE =', F10.4, 'ERROR CRITERIK17913-
ION =', F10.4) K17914-
990 FORMAT ('O', I2, 2X, 20F6.1/(5X, 20F6.1)) K17915-
END CHK1800-

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	SUBROUTINE PRNTAI(PHI, SURI, T, S, WELL, DELX, DELY)	PRN 10
C	-----	PRN 20
C	PRINT MAPS OF DRAWDOWN AND HYDRAULIC HEAD	PRN 30
C	-----	PRN 40
C		PRN 50
C	SPECIFICATIONS:	PRN 60
	REAL *8PHI, Z, XLABEL, YLABEL, TITLE, XN1, MESUR	PRN 70
	REAL *4K	PRN 80
	INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD,	PRN 90
	1CONTR, LEAK, RECH, SIP, ADI, RCAL	N 1000-
C		PRN 110
	DIMENSION PHI(IZ, JZ), SURI(IZ, JZ), S(IZ, JZ), WELL(IZ, JZ), DELX(JZ)	PRN 120
	1, DELY(IZ), T(IZ, JZ)	PRN 130
C		PRN 140
	COMMON /SARRAY/ VF4(11), CHK(17)	N 1500-
	COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LEPRN	PRN 160
	1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH,	PRN 170
	2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETGB, ETGD, FACTX, FACTY,	PRN 180
	3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DIPRN	PRN 190
	4MW, JNO1, INO1, R, P, PU, I, J, IDK1, IDK2, NSEG, RCAL	N 2000-
	COMMON /PR/ XLABEL(3), YLABEL(6), TITLE(5), XN1, MESUR, PRNT(122), BLANK	PRN 210
	1(60), DIGIT(122), VF1(6), VF2(6), VF3(7), XSCALE, DINCH, SYM(17), XN(100),	PRN 220
	2YN(13), NA(4), N1, N2, N3, YSCALE, FACT1, FACT2	PRN 230
	COMMON /ARSIZE/ IZ, JZ, IP, JP, IR, JR, IC, JC, IL, JL, IS, JS, IH, IMAX, IMX1, IN	PRN 2400-
	1K, IA, JA	N 2401-
	RETURN	PRN 250
C	.....	PRN 260
C		PRN 270
C	---INITIALIZE VARIABLES FOR PLOT---	PRN 280
C	*****	PRN 290
	ENTRY MAP	PRN 300
C	*****	PRN 310
10	XSF=DINCH*XSCALE	PRN 320
	YSF=DINCH*YSCALE	PRN 330
	NYD=YDIM/YSF	PRN 340
	IF (NYD*YSF. LE. YDIM-DELY(INO1)/2. ) NYD=NYD+1	PRN 350
	IF (NYD. LE. 12) GO TO 20	PRN 360
	DINCH=YDIM/(12. *YSCALE)	PRN 370
	WRITE (P, 310) DINCH	PRN 380
	IF (YSCALE. LT. 1. 0) WRITE (P, 320)	PRN 390
	GO TO 10	PRN 400
20	NXD=WIDTH/XSF	PRN 410
	IF (NXD*XSF. LE. WIDTH-DELX(JNO1)/2. ) NXD=NXD+1	PRN 420
	N4=NXD*N1+1	PRN 430
	N5=NXD+1	PRN 440
	N6=NYD+1	PRN 450
	N8=N2*NYD+1	PRN 460
	NA(1)=N4/2-1	PRN 470
	NA(2)=N4/2	PRN 480
	NA(3)=N4/2+3	PRN 490
	NC=(N3-NB-10)/2	PRN 500
	ND=NC+NB	PRN 510
	NE=MAX0(N5, N6)	PRN 520
	VF1(3)=DIGIT(ND)	PRN 530
	VF2(3)=DIGIT(ND)	PRN 540
	VF3(3)=DIGIT(NC)	PRN 550
	XLABEL(3)=MESUR	PRN 560
	YLABEL(6)=MESUR	PRN 570
	DO 40 I=1, NE	PRN 580

	NNX=N5-I	PRN 590
	NNY=I-1	PRN 600
	IF (NNY.GE.N6) GO TO 30	PRN 610
	YN(I)=YSF*NNY/YSF	PRN 620
30	IF (NNX.LT.0) GO TO 40	PRN 630
	XN(I)=XSF*NNX/YSF	PRN 640
40	CONTINUE	PRN 650
	RETURN	PRN 660
C	.....	PRN 670
C	*****	PRN 680
C	ENTRY PRNTA(NG)	PRN 690
C	*****	PRN 700
C	---VARIABLES INITIALIZED EACH TIME A PLOT IS REQUESTED---	PRN 710
	DIST=WIDTH-DELX(JND1)/2.	PRN 720
	JJ=JND1	PRN 730
	LL=1	PRN 740
	Z=NXD*XSF	PRN 750
	IF (NG.EQ.1) WRITE (P,280) (TITLE(I),I=1,2)	PRN 760
	IF (NG.EQ.2) WRITE (P,280) (TITLE(I),I=3,5)	PRN 770
	DO 270 I=1,N4	PRN 780
		PRN 790
C		PRN 800
C	---LOCATE X AXES---	PRN 810
	IF (I.EQ.1.OR.I.EQ.N4) GO TO 50	PRN 820
	PRNT(1)=SYM(12)	PRN 830
	PRNT(NB)=SYM(12)	PRN 840
	IF ((I-1)/N1*N1.NE.I-1) GO TO 70	PRN 850
	PRNT(1)=SYM(14)	PRN 860
	PRNT(NB)=SYM(14)	PRN 870
	GO TO 70	PRN 880
C		PRN 890
C	---LOCATE Y AXES---	PRN 900
	DO 60 J=1,NB	PRN 910
	IF ((J-1)/N2*N2.EQ.J-1) PRNT(J)=SYM(14)	PRN 920
	60 IF ((J-1)/N2*N2.NE.J-1) PRNT(J)=SYM(13)	PRN 930
C		PRN 940
C	---COMPUTE LOCATION OF NODES AND DETERMINE APPROPRIATE SYMBOL---	PRN 950
	70 IF (DIST.LT.0..OR.DIST.LT.Z-XN1*XSF) GO TO 220	PRN 960
	YLEN=DELY(2)/2.	PRN 970
	DO 200 L=2,IND1	PRN 980
	J=YLEN*N2/YSF+1.5	PRN 990
	IF (T(L,JJ).EQ.0.) GO TO 140	PRN1000
	IF (S(L,JJ).LT.0.) GO TO 190	PRN1010
	INDX3=0	PRN1020
	GO TO (80,90), NG	PRN1030
	80 K=(SURI(L,JJ)-PHI(L,JJ))*FACT1	PRN1040
C	-TO CYCLE SYMBOLS FOR DRAWDOWN, REMOVE C FROM COL. 1 OF NEXT CARD-	PRN1050
C	K=AMOD(K,10.)	PRN1060
	GO TO 100	PRN1070
	90 K=PHI(L,JJ)*FACT2	PRN1080
	100 IF (K) 110,140,120	PRN1090
	110 IF (J-2.GT.0) PRNT(J-2)=SYM(13)	PRN1100
	N=-K	PRN1110
	IF (N.LT.100) GO TO 130	PRN1120
	GO TO 170	PRN1130
	120 N=K	PRN1140
	IF (N.LT.100) GO TO 130	PRN1150
	IF (N.GT.999) GO TO 170	PRN1160
	INDX3=N/100	PRN1170
	IF (J-2.GT.0) PRNT(J-2)=SYM(INDX3)	PRN1180

	N=N-INDX3*100	PRN1190
130	INDX1=MOD(N,10)	PRN1200
	IF (INDX1.EQ.0) INDX1=10	PRN1210
C	-TO CYCLE SYMBOLS FOR DRAWDOWN, REMOVE C FROM COL. 1 OF NEXT CARD-	PRN1220
C	IF (NG.EQ.1) GO TO 150	PRN1230
	INDX2=N/10	PRN1240
	IF (INDX2.GT.0) GO TO 160	PRN1250
	INDX2=10	PRN1260
	IF (INDX3.EQ.0) INDX2=15	PRN1270
	GO TO 160	PRN1280
140	INDX1=15	PRN1290
150	INDX2=15	PRN1300
160	IF (J-1.GT.0) PRNT(J-1)=SYM(INDX2)	PRN1310
	PRNT(J)=SYM(INDX1)	PRN1320
	GO TO 200	PRN1330
170	DO 180 II=1,3	PRN1340
	JI=J-3+II	PRN1350
180	IF (JI.GT.0) PRNT(JI)=SYM(11)	PRN1360
190	IF (S(L,JJ).LT.0.) PRNT(J)=SYM(16)	PRN1370
200	YLEN=YLEN+(DELY(L)+DELY(L+1))/2.	PRN1380
210	DIST=DIST-(DELX(JJ)+DELX(JJ-1))/2.	PRN1390
	JJ=JJ-1	PRN1400
	IF (JJ.EQ.0) GO TO 220	PRN1410
	IF (DIST.GT.Z-XN1*XSF) GO TO 210	PRN1420
220	CONTINUE	PRN1430
C		PRN1440
C	---PRINT AXES, LABELS, AND SYMBOLS---	PRN1450
	IF (I-NA(LL).EQ.0) GO TO 240	PRN1460
	IF ((I-1)/N1*N1-(I-1)) 250,230,250	PRN1470
230	WRITE (P,VF1) (BLANK(J),J=1,NC), (PRNT(J),J=1,NB), XN(1+(I-1)/6)	PRN1480
	GO TO 260	PRN1490
240	WRITE (P,VF2) (BLANK(J),J=1,NC), (PRNT(J),J=1,NB), XLABEL(LL)	PRN1500
	LL=LL+1	PRN1510
	GO TO 260	PRN1520
250	WRITE (P,VF2) (BLANK(J),J=1,NC), (PRNT(J),J=1,NB)	PRN1530
C		PRN1540
C	---COMPUTE NEW VALUE FOR Z AND INITIALIZE PRNT---	PRN1550
260	Z=Z-2.*XN1*XSF	PRN1560
	DO 270 J=1,NB	PRN1570
270	PRNT(J)=SYM(15)	PRN1580
C		PRN1590
C	---NUMBER AND LABEL Y AXIS AND PRINT LEGEND---	PRN1600
	WRITE (P,VF3) (BLANK(J),J=1,NC), (YN(I),I=1,N6)	PRN1610
	WRITE (P,300) (YLABEL(I),I=1,6)	PRN1620
	IF (NG.EQ.1) WRITE (P,290) FACT1	PRN1630
	IF (NG.EQ.2) WRITE (P,290) FACT2	PRN1640
	RETURN	PRN1650
C		PRN1660
C	---FORMATS---	PRN1670
C		PRN1680
C	-----	PRN1690
C		PRN1700
C		PRN1710
280	FORMAT ('1',53X,4A8//)	PRN1720
290	FORMAT ('OEXPLANATION'//',11('-')//',R = CONSTANT HEAD BOUNDARY'//PRN1730	
1'	*** = VALUE EXCEEDED 3 FIGURES'//',MULTIPLICATION FACTOR ='//,FB.3)PRN1740	
300	FORMAT ('O',39X,6A8)	PRN1750
310	FORMAT ('O',25X,10('*')),' TO FIT MAP WITHIN 12 INCHES, DINCH REVISPRN1760	
1ED TO',	G15.7,1X,10('*'))	PRN1770
320	FORMAT ('O',45X,'NOTE: GENERALLY SCALE SHOULD BE > OR = 1.0')	PRN1780

```

END
BLOCK DATA
-----
C REAL *8XLABEL, YLABEL, TITLE, XN1, MESUR, RHO, B, D, F, H
C INTEGER R, P, PU, DIML, DIMW, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, BLD
1CONTR, LEAK, RECH, SIP, ADI, NEWW, NEWG, RCAL
C
COMMON /DPARAM/ RHO, B, D, F, H
COMMON /SARRAY/ VF4(11), CHK(17)
COMMON /MPARAM/ FACTG, NEWW, NEWG, ERLEAK, DAYS
COMMON /SPARAM/ WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, EROR, LEBLD
1AK, RECH, SIP, U, SS, TT, TMIN, ETDIST, GET, ERR, TMAX, CDLT, HMAX, YDIM, WIDTH, BLD
2NUMS, LSOR, ADI, DELT, SUM, SUMP, SUBS, STORE, TEST, ETGB, ETGD, FACTX, FACTY, BLD
3IERR, KOUNT, IFINAL, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, DIML, DIBLD
4MW, JNO1, INO1, R, P, PU, I, J, IDK1, IDK2, NSEQ, RCAL
COMMON /PR/ XLABEL(3), YLABEL(6), TITLE(5), XN1, MESUR, PRNT(122), BLANKBLD
1(60), DIGIT(122), VF1(6), VF2(6), VF3(7), XSCALE, DINCH, SYM(17), XN(100), BLD
2YN(13), NA(4), N1, N2, N3, YSCALE, FACT1, FACT2
COMMON /ARSize/ IZ, JZ, IP, JP, IR, JR, IC, JC, IL, JL, IS, JS, IH, IMAX, IMX1, ID
1K, IA, JA
C *****
C DATA IZ, JZ, IP, JP, IR, JR, IC, JC, IL, JL, IS, JS, IMAX/13*20/, IH/1/
DATA CHK/'PUNC', 'WATE', 'CONT', 'NUME', 'CHEC', 'EVAP', 'CONV', 'HEAD', 'BLD
1LEAK', 'RECH', 'SIP', 'LSOR', 'ADI', 'DK1', 'DK2', 'YES', 'CALC', 'R, P, D
2PU/5, 6, 7/, B, D, F, H/4*0. D0/
DATA SYM/'1', '2', '3', '4', '5', '6', '7', '8', '9', '0', '*', '!', '-', '+', 'BLD
1', 'R', 'W'
DATA PRNT/122* ' ', N1, N2, N3, XN1/6, 10, 133, . 8333333333D-1/, BLANK/60* 'BLD
1 ' ', NA(4)/1000/
DATA XLABEL/' X DIS-', 'TANCE IN', ' MILES', YLABEL/'DISTANCE', ' BLD
1FROM OR', 'IGIN IN', 'Y DIRECT', 'ION, IN', 'MILES', TITLE/'PLOT BLD
2OF ', 'DRAWDOWN', 'PLOT OF ', 'HYDRAULI', 'C HEAD'
DATA DIGIT/'1', '2', '3', '4', '5', '6', '7', '8', '9', '10', '11', '12', '13' BLD
1, '14', '15', '16', '17', '18', '19', '20', '21', '22', '23', '24', '25', '26', BLD
2'27', '28', '29', '30', '31', '32', '33', '34', '35', '36', '37', '38', '39', 'BLD
340', '41', '42', '43', '44', '45', '46', '47', '48', '49', '50', '51', '52', '58' BLD
43, '54', '55', '56', '57', '58', '59', '60', '61', '62', '63', '64', '65', '66' BLD
5, '67', '68', '69', '70', '71', '72', '73', '74', '75', '76', '77', '78', '79' BLD
6, '80', '81', '82', '83', '84', '85', '86', '87', '88', '89', '90', '91', '92' BLD
7, '93', '94', '95', '96', '97', '98', '99', '100', '101', '102', '103', '104' BLD
8, '105', '106', '107', '108', '109', '110', '111', '112', '113', '114', '115' BLD
9, '116', '117', '118', '119', '120', '121', '122'
DATA VF1/'(1H', ' ', ' ', ' ', ' ', 'A1, F', '10. 2', ' )'
DATA VF2/'(1H', ' ', ' ', ' ', ' ', 'A1, 1', 'X, A8', ' )'
DATA VF3/'(1H0', ' ', ' ', ' ', ' ', 'A1, F', '3. 1', ' ', '12F1', '0. 2'
DATA VF4/'(1H0', ' ', ' ', ' ', ' ', 'X, 12', '2X', '20F6', '1/(', ' ', 'X, 2' BLD
10, 'F6. 1', ' )'
C *****
C END
%%

```