Table 1.--Summary of aquifer-test analyses and results of methods used to estimate transmissivity--Continued

County	Owner's name	Other identification	Latitude	Longitude	Land-surface altitude (ft)	Well depth (ft)	Diameter of screens or open hole (in.)	Open interval(s) (ft below land surface)	Test date(s)	Test yield (gal/min)	Test duration (hours)	Transmissivity (ft^2/d)	Storage coefficient	Specific capacity [(gal/min)/ft]	Formation name or provincial stage of aquifer sediments	Method of analysis	ESTIMATED TRANSMISSIVITY (ft^2/d)			
																	Regression equation	Percent difference	Modified nonequilibrium equation	Percent difference
GEORGIA--Continued																				
Twiggs	J. M. Huber Corp.	DW-1, GGS1812, 18V007	32°41'13"	83°28'09"	326	225	18	85- 135 150- 185 195- 210	03-07-67 to 03-18-67	2,060	252	[1]36,900	--	52.8	Navarroan-Tayloran	Modified nonequilibrium formula[2]	25,300	-32	16,900	-54
Do.	do.	A-2, 18V017	32°41'26"	83°28'02"	320	225	4	0- 225	03-07-67 to 03-18-67	--	252	[6,13]34,000	8.2×10^{-4}	--	do.	Nonequilibrium formula[5]	--	--	--	--
Do.	do.	B-2, 18V018	32°41'22"	83°28'15"	338	225	4	0- 225	03-07-67 to 03-18-67	--	252	[1,13]31,800	8.0×10^{-4}	--	do.	do.	--	--	--	--
Do.	do.	C-2, 18V019	32°41'03"	83°28'27"	370	225	4	0- 225	03-07-67 to 03-18-67	--	252	[6,13]34,000	7.2×10^{-4}	--	do.	do.	--	--	--	--
Do.	do.	D-2, 18V020	32°41'00"	83°28'23"	345	225	4	0- 225	03-07-67 to 03-18-67	--	252	[6,13]34,400	8.1×10^{-4}	--	do.	do.	--	--	--	--
Do.	do.	E-2, 18V021	32°41'12"	83°28'08"	310	225	4	0- 225	03-07-67 to 03-18-67	--	252	[6,13]31,600	1.1×10^{-4}	--	do.	do.	--	--	--	--
Washington	Julian P. Veal	Test-well 2, 22Y007	33°02'36"	82°56'49"	248	114	8	36- 41 54- 69 104- 114	08-30-42 to 08-31-42	220	36	[1]2,680	--	4.0	Claibornian, Taylorian-Austinian	Modified nonequilibrium formula[2]	1,890	-29	2,300	-14
Do.	L. A. Wood	Test-hole 3, 22Y008	33°01'01"	82°58'24"	232	274	8	33- 43 48- 58 133- 138 190- 200	09-05-42 to 09-06-42	230	36	[1]718	--	4.4	do.	do.	2,080	190	1,200	67
Do.	American Industrial Clay	P-6, 22Y032	33°01'51"	82°52'34"	400	372	12, 10	280- 310 312- 342 352- 362	11-02-82	841	24	[1]7,100	--	17.1	Tayloran-Austinian	do.	8,140	15	4,850	-32
Do.	do.	P-5, 22Y029	33°01'54"	82°52'41"	420	410	10	278- 306 310- 340 390- 400	01-27-75	1,040	24.3	[1]7,340	--	22.1	do.	do.	10,500	43	6,300	-14
Wilkinson	Town of Toomsboro	No. 1, 21W004	32°45'32"	83°04'47"	235	310	8	225- 240 252- 257 268- 278 292- 302	08-30-82 to 08-31-82	300	24.5	[6]10,500	--	26.7	do.	do.	12,700	21	8,050	-23
Do.	J. M. Huber Corp.	X46.75, Y44, 19W004	32°48'50"	83°16'57"	312	215	18	115- 125 140- 150 180- 210	04-18-69 to 04-22-69	705	96	[1,15]3,300	--	7.3	do.	do.	3,460	5	2,010	-39
Do.	do.	X44Y44, 19W002	32°48'49"	83°16'59"	320	300	4	90- 300	04-18-69 to 04-22-69	--	96	[1,15]13,500	5.5×10^{-4}	--	do.	Nonequilibrium formula[5]	--	--	--	--
Do.	do.	X40Y38, 19W001	32°48'44"	83°16'57"	301	280	4	70- 280	04-18-69 to 04-22-69	--	96	[1,15]12,900	7.7×10^{-4}	--	do.	do.	--	--	--	--
Do.	do.	X44Y52, 19W003	32°48'52"	83°17'04"	319	300	4	90- 300	04-18-69 to 04-22-69	--	96	[1,15]6,270	4.3×10^{-4}	--	do.	do.	--	--	--	--
SOUTH CAROLINA																				
Aiken	Town of Burnettown	No. 1, AK-440	33°30'19"	81°50'50"	310	245	6	160- 170 180- 200	05-22-69	197	16	[6]12,200	--	11.8	do.	Modified nonequilibrium formula[2]	5,610	-54	3,420	-72
Do.	Savannah River Plant	66-H	33°17'11"	81°38'55"	303	863	--	Unknown	Unknown	1,535	24	[1]23,500	--	38.2	do.	do.	18,200	-22	11,690	-50
Do.	do.	905-82A, AK-452	33°20'16"	81°43'59"	375	710	10	445- 450 496- 506 511- 521 534- 544 560- 570 585- 600 610- 615 620- 630 638- 648 655- 665 680- 690	07-07-77	2,005	12	[6]8,740	--	34.6	Tayloran-Austinian	Modified nonequilibrium formula[2]	18,830	115	9,890	13
Do.	do.	24-F, LA-24	33°17'14"	81°40'11"	317	830	8	575- 585 595- 605 640- 660 680- 690 700- 720 780- 790 800- 820	09-29-51	1,506	8?	[6,16]33,700	6.6×10^{-4}	19.5	do.	Nonequilibrium formula[5]	9,290	-72	5,410	-83
Allendale	Creek Plantation	AL-66	33°06'55"	81°33'56"	210	785	8	390- 410 518- 523 595- 625 635- 680 690- 715	02-12-79	1,500	24	[6]7,100	--	16.2	Claibornian (390-410), Navarroan-Tayloran	Modified nonequilibrium formula[2]	7,710	9	4,730	-33
Do.	Town of Ulmer	AL-48	33°05'18"	81°14'29"	--	--	--	--	01-29-79	700	0.5	[1]3,920	--	17.9	Claibornian	do.	8,520	117	3,900	-1
Do.	Sandoz, Inc.	No. 1, AL-27	33°02'23"	81°29'19"	167	817	10	460- 470	09-14-77	70	7	[5]1,100	--	1.74	Claibornian	do.	819	-25	94	-91
								556- 566	09-12-77	59	20.3	[5]214	--	.42	Navarron-Tayloran	do.	197	-8	58	-73
								629- 639	09-11-77	50	6.8	[5]263	--	.29	do.	do.	136	-46	58	-78
Barnwell	Town of Williston	BW-79	33°23'48"	81°24'07"	360	685	10	490- 540 590- 600 640- 680	04- -81	1,404	12	[6]13,000	--	11.5	do.	do.	5,460	-58	3,090	-76
Do.	Savannah River Plant	43-H, LA-43	33°17'14"	81°38'22"	301	860	8	660- 690 750- 850	02-23-52	560	--	[6,16]26,300	--	46.9	do.	do.	22,400	-15	13,700	-48
Do.	Allied Gulf Nuclear Services	P-1, BW-72	33°14'55"	81°29'37"	256	985	10	Unknown	11-26-71 to 01-25-72	2,000	1,460	[6,17]22,800	--	28.2	Navarron-Tayloran-Austinian	do.	13,500	-41	10,140	-55
Do.	do.	O-1, BW-76	33°14'55"	81°29'33"	257	1,104	--	Unknown	11-26-71 to 01-25-72	2,000	1,460	[1,17]19,400	1.9×10^{-4}	--	do.	Nonequilibrium formula[5]	--	--	--	--
Do.	do.	do.	do.	do.	do.	do.	do.	do.	--	--	--	[6,17]20,300	2.5×10^{-4}	--	do.	do.	--	--	--	--
Do.	do.	do.	do.	do.	do.	do.	do.	do.	11-26-71	2,190	5.5	[1,17]19,800	--	--	do.	Modified nonequilibrium formula[2]	--	--	--	--

See footnotes at end of table.