

A COMPUTER PROGRAM FOR GEOCHEMICAL  
ANALYSIS OF ACID-RAIN AND OTHER  
LOW-IONIC-STRENGTH, ACIDIC WATERS

By Patricia A. Johnsson and Deborah G. Lord

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DONALD PAUL HODEL, Secretary  
U.S. GEOLOGICAL SURVEY  
Dallas L. Peck, Director

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For additional information  
write to:

District Chief  
Geological Survey  
Water Resources Division  
Mountain View Office Park  
810 Bear Tavern Road, Suite 206  
West Trenton, NJ 08628

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ABSTRACT

This paper describes ARCHEM, a computer program written in FORTRAN 77<sup>1</sup>, which is designed primarily for use in the routine geochemical interpretation of low-ionic-strength, acidic waters. On the basis of chemical analyses of the water and either laboratory or field determinations of pH, temperature, and dissolved oxygen, the program calculates the equilibrium distribution of major inorganic aqueous species and of inorganic aluminum complexes. The concentration of the organic anion is estimated from the dissolved organic carbon concentration, and the ratio of ferric to ferrous iron is calculated from the dissolved oxygen concentration. Ionic balances and comparisons of computed with measured specific conductance are performed as checks on the analytical accuracy of chemical analyses. ARCHEM may be tailored easily to fit different sampling protocols, and may be run on multiple sample analyses.

INTRODUCTION

Researchers of acidic deposition (acid rain) are commonly confronted with unique geochemical problems in data interpretation because of the low pH and low ionic strength of precipitation. In areas affected by acid rain, surface and ground waters are commonly acidified, and may even display some interesting geochemical properties such as negative alkalinities. Surface-water geochemistry can be particularly complex in areas such as the New Jersey Pinelands (Means and others, 1981), the North Carolina Sandhills region (J.K. Crawford, U.S. Geological Survey, Raleigh, N.C., oral commun., 1986), and the Bickford watershed, in Massachusetts (Eshleman and Hemond, 1985), where organic materials are present in high concentrations. Although there is a substantial library of geochemical computer models, including WATEQ<sup>2</sup> (Truesdell and Jones, 1974), SOLMENEQ<sup>3</sup> (Kharaka and Barnes, 1973), and MINEQL<sup>4</sup> (Westall and others, 1976), among others (see Nordstrom, 1979, for a review), the peculiarities of many low-ionic-strength waters require special modeling techniques.

ARCHEM<sup>5</sup>, a FORTRAN 77 computer program, was designed specifically to deal with geochemical factors such as: pH, alkalinity, organic-anion concentration, and aluminum speciation in a manner rigorous enough for use

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<sup>1</sup> Use of trade names in this report is for identification purposes only and does not constitute endorsement by the U.S. Geological Survey.

<sup>2</sup> WATEQ is the acronym for a computer program for calculating chemical equilibria of natural waters.

<sup>3</sup> SOLMENEQ is the acronym for a computer program for solution-mineral equilibrium computations.

<sup>4</sup> MINEQL is the acronym for a computer program for the calculation of chemical equilibrium composition of aqueous species.

<sup>5</sup> ARCHEM is the acronym for a computer program for geochemical analysis of acid-rain and other low-ionic-strength, acidic waters.

with low-ionic-strength waters. ARCHEM is not intended to be as sophisticated a model as WATEQ, SOLMENEQ, and MINEQL, nor does it give as detailed information on solution-mineral equilibria. The number of reactions considered by the model is limited, and a number of simplifications and estimation techniques are employed. However, the model may be used simply and effectively in the routine geochemical interpretation of low-ionic-strength, acidic water samples, and in the evaluation of their analytical accuracy. ARCHEM may be most useful for precipitation samples, which generally do not warrant calculations of mineral saturation indexes; for samples containing dissolved organics that can greatly complicate the geochemistry through interactions which are at present not well understood; and for performing checks on the analytical accuracy of large numbers of samples.

Like many existing geochemical computer programs, ARCHEM is based on an equilibrium model that uses both mass balance and mass action equations. The equations are solved through the method of successive iterations (Garrels and Thompson, 1962; Truesdell and Jones, 1974). The main body of the program calculates: (1) equilibrium molarities and activities of major aqueous species (see table 1), including an estimation of the organic-anion concentration; (2) equilibrium concentrations of major aluminum species (see table 2); and (3) ionic strength.

#### Purpose and Scope

This paper describes (1) the geochemical equations used to perform these calculations, (2) the iterative method for solving these equations, and (3) a number of calculations that aid in the interpretation of water chemistry. These calculations include (1) ion ratios, including a ferric to ferrous iron ratio computed from oxidation-reduction equations; (2) cation/anion balances based on analytical and computed data and inclusion of the organic-anion concentration as a component; and (3) specific conductance.

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### GEOCHEMICAL BASIS FOR COMPUTER PROGRAM

#### Major Equilibrium Equations

Table 1 is a list of the major, non-aluminum equilibrium relations considered in ARCHEM. Both the equations and their corresponding thermodynamic values are from Truesdell and Jones (1974, p. 234-240). For the major reactions in table 1, the equilibrium constants ( $K_T$ ) are calculated for input temperatures from 0° to 30°C. These calculations are based on the Van't Hoff equation at constant pressure:

$$d\ln K/dT = \Delta H/RT^2 \quad (1)$$

Table 1.--Major equilibrium relations considered  
by computer program  
[Adapted from Truesdell and Jones, 1974]

Reaction	$\log K^*$	$H_r^*$
$H_2CO_3 = HCO_3^- + H^+$	-6.379	1,976
$HCO_3^- = H^+ + CO_3^{-2}$	-10.330	3,550
$Mg^{+2} + HCO_3^- = MgHCO_3^+$	0.928	1.037
$Ca^{+2} + HCO_3^- = CaHCO_3^+$	1.260	6,331
$Mg^{+2} + SO_4^{-2} = MgSO_4^0$	2.238	4,920
$Ca^{+2} + SO_4^{-2} = CaSO_4^0$	2.309	1,650
$Mg^{+2} + CO_3^{-2} = MgCO_3^0$	3.398	58
$Ca^{+2} + CO_3^{-2} = CaCO_3^0$	3.200	3,130
$H_2O = H^+ + OH^-$	-13.998	13,345

\* K is the equilibrium constant at 25°C.  $H_r$  is the heat of reaction at 25°C (298°K).

where K is the equilibrium constant, T is the absolute temperature (degrees Kelvin), R is the ideal gas constant (1.99 calories/mole), and ΔH is the change in enthalpy of a reaction. From this equation, the expression for K at temperatures other than 25° Celsius can be derived:

$$K_t = K_{25} \times 10^{((\Delta H / (2.303 \times R)) \times ((T_2 - 298^\circ\text{K}) / (T_2 \times 298^\circ\text{K})))} \quad (2)$$

where  $K_{25}$  is the value of the equilibrium constant at 25°C (298°K) and  $K_t$  is the value of the equilibrium constant at the sample temperature,  $T_2$ , in degrees Kelvin.

The Van't Hoff equation, as presented above, assumes that the enthalpy change is independent of temperature. This assumption is not, in fact, correct for all of the reactions considered by ARCHEM. Although corrections for enthalpy changes can be made (see Stumm and Morgan, 1981, p. 69-71), ARCHEM uses the more simple equation presented above. According to Hem (1985), the use of the Van't Hoff equation as an approximation "is applicable over temperature ranges to be expected in most natural waters." The program is intended and designed for use on samples approaching standard pressure and temperature conditions, so that this approximation does not present additional limitations.

#### Aluminum Equilibria

ARCHEM also calculates the equilibrium concentrations of inorganic aluminum species (see table 2), because (1) aluminum species can act as the predominant buffering agents in low-ionic-strength waters (see, for example, Johnson and others, 1981), and (2) certain aluminum species may be toxic to fish populations (Driscoll and others, 1980) and may adversely affect tree growth (Ulrich and others, 1980). Table 2 is a list of the aluminum equilibrium equations and thermodynamic values utilized by ARCHEM. These values were chosen on the basis of (1) values prevalent in the recent acid-rain literature (see, for example, Johnson and others, 1981; Driscoll, 1984; and Cosby and others, 1985a) and (2) suggestions in Nordstrom and others (1984). An effort was made to maintain internal consistency within any one set of complexes (fluoride versus sulfate versus hydroxide) by choosing logK data from only one source for each of these sets (aluminum-fluoride complexes from Hem, 1968; aluminum-sulfate complexes from Behr and Wendt, 1962; and aluminum-hydroxide complexes from May and others, 1979). However, no attempt was made to maintain consistency between the sets of complexes.

Cozzarelli (U.S. Geological Survey, Reston, Va., written commun., 1987) cautions that the use of inconsistent thermodynamic data in the program may cause problems in the calculation of species' equilibrium distributions. The authors, therefore, strongly recommend that users perform a careful review of the recent literature before using the program. Nordstrom and others (1984), which is an excellent reference for such a review, provides a compilation of aluminum thermodynamic data along with recommendations for use, and a discussion of problems involving thermodynamic inconsistency. The responsibility for selection of thermodynamic data, for all of the species in the program, ultimately rests with the user. The thermodynamic values may be altered easily within the source code.

Table 2.--Aluminum equilibrium relations considered by computer program

Reaction	log K	H <sub>r</sub>	Data source*
Fluoride Complexes			
$Al^{+3} + F^{-} = AlF^{+2}$	7.01	1.10	1;2
$Al^{+3} + 2F^{-} = AlF_2^{+}$	12.75	2.00	1;2
$Al^{+3} + 3F^{-} = AlF_3^0$	17.02	2.50	1;2
$Al^{+3} + 4F^{-} = AlF_4^{-}$	19.72	2.20	1;2
$Al^{+3} + 5F^{-} = AlF_5^{-2}$	20.91	1.80	1;2
$Al^{+3} + 6F^{-} = AlF_6^{-3}$	20.86	0.10	1;3
Sulfate Complexes			
$Al^{+3} + SO_4^{-2} = AlSO_4^{+}$	3.20	2.29	4;5
$Al^{+3} + 2SO_4^{-2} = Al(SO_4)_2^{-}$	5.10	3.07	4;5
Hydroxide Complexes			
$Al^{+3} + H_2O = Al(OH)^{+2} + H^{+}$	-4.99	14.775	6;7
$Al^{+3} + 2H_2O = Al(OH)_2^{+} + 2H^{+}$	-10.13	22.0	6;3
$Al^{+3} + 3H_2O = Al(OH)_3^0 + 3H^{+}$	-16.76	33.0	6;3
$Al^{+3} + 4H_2O = Al(OH)_4^{-} + 4H^{+}$	-22.16	42.22	6;7
Total inorganic Aluminum = $[Al^{+3}] + [Al(OH)^{+2}] + [Al(OH)_2^{+}] + [Al(OH)_4^{-}] +$ $[Al(SO_4)^{+}] + [Al(SO_4)_2^{-}] + [AlF^{+2}] + [AlF_2^{+}] + [AlF_3^0] + [AlF_4^{-}] + [AlF_5^{-2}]$ $+ [AlF_6^{-3}]$			

\* Data Sources:

- 1 Hem, 1968.
- 2 Smith and Martell, 1976.
- 3 Nordstrom and others, 1984.
- 4 Behr and Wendt, 1962.
- 5 Izatt and others, 1969.
- 6 May and others, 1979.
- 7 Plummer and others, 1976.



If dissolved aluminum has been analytically fractionated into nonlabile monomeric aluminum (monomeric aluminorganic complexes) and labile monomeric aluminum (free aluminum and aluminosulfate, fluoride, and hydroxide complexes), then the program will subtract out organically bound aluminum before calculating concentrations of inorganic species. Otherwise, the programmer may choose between two options: (1) to calculate aluminum speciation treating the input value of aluminum as the total of all inorganic aluminum, or (2) to set the concentration of  $Al^{3+}$  equal to the input value of aluminum, disregarding speciation entirely. In many instances, option (1) may give a better value for the computed ion balance, because  $AlF_2^+$  is generally the dominant inorganic aluminum species (LaZerte, 1984). Aluminum fractionation by analytical means is strongly recommended, however, because the concentrations of dissolved inorganic aluminum species may be overestimated in waters containing organically-bound aluminum. A potential method for estimating the maximum quantity of aluminum that may be bound to organics is discussed below.

#### Organic-anion Concentration

Oliver and others (1983) showed that calculation of the concentration of the 'organic anion', which results from the dissociation of aquatic humic substances, can greatly improve ion balances for highly-colored natural waters. ARCHEM, therefore, performs an estimation of the organic-anion concentration, based on the equations derived by Oliver and others (1983) for "highly colored natural waters, where most of the organic carbon is humic material." First, an empirical expression is used to calculate the negative logarithm of the mass action quotient of humic and fulvic acids (the pK) from the pH:

$$pK = 0.96 + (0.90 \times pH) - (0.039 \times pH^2) \quad (3)$$

(Oliver and others, 1983, p.2033). Next, the concentration of organic acid ( $C_t$ ) is calculated by multiplying the dissolved organic carbon concentration (DOC) in milligrams per liter by  $10 \mu\text{eq}/\text{mg C}$  (microequivalents per milligram carbon)--the factor that Oliver and others (1983) found to be representative of humic substances from a variety of surface and ground waters in North America and Hawaii. This factor can be changed easily within the body of ARCHEM (see documentation in the source code) in instances where  $10 \mu\text{eq}/\text{mg C}$  is not a representative value. Finally, the values thus calculated are substituted into the following equation to determine the organic-anion concentration [OA]:

$$[OA] = K \times [C_t] / (K + [H^+]) \quad (\text{Oliver and others, 1983, p. 2034}). \quad (4)$$

#### Alkalinity Equations

The equation for alkalinity can be used along with mass action and mass balance equations in solving for the equilibrium concentrations of species. The equation for alkalinity must, however, be defined according to the specific chemical characteristics of any given system. A generalized

alkalinity equation was synthesized from the recent acid-rain literature. This equation is applicable to a wide range of conditions, including waters with negative values of alkalinity.

In ARCHEM, the concentrations of phosphate ion, of the organic anion, and of the major aluminum species as defined by Cosby and others (1985b, p. 1594) have been added to the standard form of the alkalinity equation (Stumm and Morgan, 1981, p. 188):

$$\text{Alk} = [\text{HCO}_3^-] + 2[\text{CO}_3^{2-}] + [\text{OH}^-] - [\text{H}^+] \quad (5)$$

to yield:

$$\begin{aligned} \text{Alk} = & [\text{HCO}_3^-] + 2[\text{CO}_3^{2-}] + [\text{OH}^-] + [\text{OA}^-] - 3[\text{Al}^{+3}] + [\text{Al}(\text{OH})_4^-] + 3[\text{PO}_4^{3-}] \\ & - [\text{H}^+] - 2[\text{AlOH}^{+2}] - [\text{Al}(\text{OH})_2^+] - 3[\text{AlF}^{+2}] - 3[\text{AlF}_2^+] - 3[\text{AlF}_3^0] \\ & - 3[\text{AlF}_4^-] - 3[\text{AlF}_5^{2-}] - 3[\text{AlF}_6^{3-}] - 3[\text{Al}(\text{SO}_4^+)] - 3[\text{Al}(\text{SO}_4)_2^-]. \end{aligned} \quad (6)$$

This equation can be rearranged and used to solve for the concentrations of the bicarbonate ( $[\text{HCO}_3^-]$ ) and carbonate ( $[\text{CO}_3^{2-}]$ ) ions. In these and future equations,  $[\ ]$  represents molar concentrations.

Alkalinity can also be defined as the sum of base cations ( $C_b$ ) minus the sum of strong acid anions ( $C_a$ ) (Stumm and Morgan, 1981, p. 182). ARCHEM, therefore, performs a second calculation of alkalinity according to the equation:

$$\begin{aligned} \text{Alk} = C_b - C_a = & [\text{Na}^+] + [\text{K}^+] + [\text{NH}_4^+] + 2[\text{Ca}^{+2}] + 2[\text{Mg}^{+2}] \\ & - [\text{Cl}^-] - [\text{NO}_3^-] - 2[\text{SO}_4^{2-}] - [\text{F}^-]. \end{aligned} \quad (7)$$

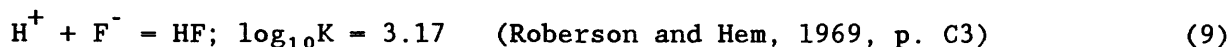
The value of alkalinity thus computed is reported in the output file but is not utilized in further equilibrium calculations. This value of alkalinity can, however, be used as a rough check on the analytical value of alkalinity, and can be used in future runs of the program as an estimate of the alkalinity when no analytical value is available.

### Fluoride Concentrations

Fluoride is a particularly important component of the equations considered by ARCHEM because of the role fluoride plays in complexing aluminum (see table 2). The program's treatment of fluoride depends on the method of analysis. If an ion-specific electrode was used, then the activity of the fluoride ion ( $\{F\}$ ) is set equal to the input value for fluoride. However, if only the concentration of total dissolved fluoride was determined, then an extra set of equations must be added to the equilibrium equations described above in order to solve for free fluoride,  $[F^-]$ . In this case, the assumption:

$$[\text{Total Fluoride}] = [\text{HF}] + [F^-] + [\text{AlF}^{+2}], \quad (8)$$

where



is a necessary simplification (LaZerte, 1984) that yields a linear expression and first approximation for  $[F^-]$ . The value of  $[F^-]$  determined from this equation is then substituted into the other equilibrium equations in order to solve for the concentrations of the various aluminum-fluoride components. The value of  $[F^-]$  is refined by the iterative procedure.

### Activity Coefficients and Ionic Strength

The reactions presented in tables 1 and 2 and equation 9 have corresponding mass action equations which may be used in solving for the concentrations of species at equilibrium. For a generalized reaction:



with an equilibrium constant K, the mass action equation would be:

$$\frac{\{A\}^a \{B\}^b}{\{C\}^c \{D\}^d} = K, \quad (11)$$

where {} symbolizes an activity. In order to utilize these mass action equations, ARCHEM must calculate the activity coefficients ( $\gamma_i$ s) of the various ionic species (where  $\{A\} = \gamma_a \times [A]$ ). The activity coefficients are dependent, in turn, on the ionic strength of the sample solution. The ionic strength (I) is calculated using the standard equation:

$$I = 1/2 \sum_{n=1}^i m_i z_i^2, \quad (12)$$

where n is the total number of ions in solution,  $m_i$  is the molarity of the i-th ion in the solution, and  $z_i$  is the ion's charge (Garrels and Christ, 1965, p. 56).

The following extended form of the Debye-Hückel expression, accurate for ionic strengths of less than 0.1 (Stumm and Morgan, 1981, p. 135), is used to calculate the ion activity coefficients ( $\gamma_i$ ) :

$$\log \gamma_i = -Az_i^2 I^{1/2} / (1 + \dot{a}_i B I^{1/2}) \quad (13)$$

Here,  $\dot{a}_i$  is a constant related to the 'effective hydrated diameter' of the ion in solution (Garrels and Christ, 1965, p. 61), and A and B are constants whose values depend on temperature and pressure. The values of  $\dot{a}_i$  used by ARCHEM are listed in table 3. Values of A and B were calculated using empirical expressions designed to duplicate the values reported in Garrels and Christ (1965, p. 61). The equations, along with their results compared to the Garrels and Christ values, are reported in table 4. The calculated values agree well with the values from Garrels and Christ over the temperature range considered (0 to 30°C).

Table 3.--Values of  $\dot{a}_i$  in the Debye-Hückel Equation  
 [Values from Klotz and Rosenberg, 1972.]

Species	$\dot{a}_i \times 10^8$
$\text{NH}_4^+$	2.5
$\left. \begin{array}{l} \text{K}^+ \\ \text{Cl}^- \\ \text{Br}^- \\ \text{I}^- \\ \text{NO}_3^- \end{array} \right\}$	3.0
$\left. \begin{array}{l} \text{SO}_4^{-2} \\ \text{PO}_4^{-3} \end{array} \right\}$	4.0
$\left. \begin{array}{l} \text{HCO}_3^- \\ \text{Na}^+ \end{array} \right\}$	4.0-4.5
$\text{CO}_3^{-2}$	4.5
$\left. \begin{array}{l} \text{Ca}^{+2} \\ \text{Mn}^{+2} \\ \text{Fe}^{+2} \end{array} \right\}$	6.0
$\text{Mg}^{+2}$	8.0
$\left. \begin{array}{l} \text{H}^+ \\ \text{Al}^{+3} \\ \text{Fe}^{+3} \end{array} \right\}$	9.0

Table 4.--Values of A and B in Debye-Hückel Equation \*

Temperature degrees C	Garrels and Christ A	Calculated A	Garrels and Christ B	Calculated B
0	0.4883	0.4880	0.3241	0.3241
5	0.4921	0.4921	0.3249	0.3249
10	0.4960	0.4962	0.3258	0.3257
15	0.5000	0.5003	0.3262	0.3265
20	0.5042	0.5044	0.3273	0.3273
25	0.5085	0.5085	0.3281	0.3281
30	0.5130	0.5126	0.3290	0.3289

\* Equations used to calculate A and B values:

$$A = 0.0082(T-5) + 0.4291$$

$$B = 0.3421 + 0.0008(T/5)$$

where T is the temperature in degrees Celsius.

The activity coefficients of the ionic aluminum species are calculated in the manner of Johnson and others (1981) by taking the average of the activity coefficients of other species with the same charge.

ARCHEM treats pH as the negative logarithm of the hydrogen-ion activity. For any individual sample, the hydrogen-ion activity remains constant throughout the program.

Activity coefficients of all non-ionic species, including water, are taken to be 1.

#### STRUCTURE OF COMPUTER PROGRAM

The equilibrium relations (mass-action equations, and the organic-anion, alkalinity, and fluoride equations), along with various mass-balance relationships, represent a group of simultaneous equations which can be solved through successive approximations. The equations are solved first using a carefully-chosen array of simplifications: the activity coefficients are set equal to 1, the sulfate concentration,  $[SO_4^{-2}]$  is set equal to 10 percent of the total sulfate, and bicarbonate is set equal to the alkalinity. The value,  $[SO_4^{-2}] = 0.10 \times \text{total sulfate}$ , is an arbitrary value that is refined by the program in future iterations. The molarity of free calcium,  $[Ca^{+2}]$  is then calculated from the expression:

$$[Ca^{+2}] = [\text{Total calcium}] / (1 + X + Y + Z) , \quad (14)$$

where  $X = (\gamma_{Ca} \times \gamma_{SO_4} \times [SO_4^{-2}]) / K_{CaSO_4}^{\circ}$ ,

$$Y = (\gamma_{HCO_3} \times \gamma_{Ca} \times [HCO_3^{-}]) / (K_{CaHCO_3}^{\circ} \times \gamma_{CaHCO_3}) ,$$

$$Z = (\gamma_{Ca} \times \gamma_{CO_3} \times [CO_3^{-2}]) / K_{CaCO_3}^{\circ} ,$$

and  $\gamma$  represents the appropriate activity coefficient.

Equation 14 is derived by substituting equilibrium mass action equations such as:

$$K_{CaSO_4}^{\circ} = \frac{\{Ca^{+2}\} \times \{SO_4^{-2}\}}{\{CaSO_4^{\circ}\}} , \quad (15)$$

where  $\{\}$  symbolizes an activity, into the mass-balance equation for calcium:

$$[\text{Total calcium}] = [CaSO_4^{\circ}] + [CaCO_3^{\circ}] + [CaHCO_3^{+}] + [Ca^{+2}] \quad (16)$$

and solving for  $[Ca^{+2}]$ .

Free magnesium,  $[Mg^{+2}]$  and free aluminum,  $[Al^{+3}]$  are both calculated in a similar fashion. Although equilibrium concentrations are normally written in terms of molalities, ARCHEM uses molarities. This

simplification is valid because for dilute waters, the differences between molality and molarity are small and generally can be neglected (Garrels and Christ, 1965; Hem, 1985).

The  $[Ca^{+2}]$ ,  $[Mg^{+2}]$ , and  $[Al^{+3}]$  values determined from equations similar to equation 14, are substituted back into mass-action equations such as equation 15 to calculate the concentrations of the various complexes. The ionic strength is calculated next, and is used to recalculate the activity coefficients of the separate ions (see equations 12 and 13). The bicarbonate concentration is recalculated from the alkalinity equation (see equation 6). The sulfate-ion concentration (old  $SO_4$ ) used in these calculations (where  $[SO_4^{-2}] = 0.10 \times \text{total sulfate}$ ) is then compared to the sulfate-ion concentration (new  $SO_4$ ) calculated from the mass-balance equation:

$$[SO_4^{-2}] = [\text{total sulfate}] - [CaSO_4] - [MgSO_4] - ([AlSO_4^+] + 2[Al(SO_4)_2^-]), \quad (17)$$

where the components in parentheses have values only if aluminum speciation is selected as an option. If these two sulfate values (old  $SO_4$  and new  $SO_4$ ) differ by less than 0.1 percent, then the iterations are halted and the various calculated concentrations are taken to be representative of the water sample, under equilibrium conditions. Otherwise, the sulfate ion concentration is increased by the amount  $(\text{old } SO_4 - \text{new } SO_4)/2$ , the calculations are performed again using the various refined values, and the loop is repeated until sulfate values converge. This convergence generally occurs within six iterations.

#### SPECIAL INTERPRETIVE FEATURES OF COMPUTER PROGRAM

After solving for equilibrium concentrations and activities, as described above, ARCHEM performs a series of calculations to assist in the interpretation of analytical and computed data. These calculations include ion ratios, cation/anion balances, and specific conductance. Ion ratios can be used to classify waters, to compare waters from similar or different geohydrologic sources, and in some instances, to determine the mineralogic sources of ions in solution (see Hem, 1985). Cation/anion balances and specific-conductance calculations can be used to evaluate the accuracy of water analyses. The analytical accuracy in turn limits the accuracy of all of the calculations performed by ARCHEM. As a further aid in the interpretation of water analyses, the input file for ARCHEM includes a section for identifying input values that are below the detection limit, estimated, or otherwise noteworthy. These 'flags,' which do not alter program functions, are included in the output file.

#### Ion Ratios

ARCHEM calculates the following ratios of analytical molarities: Na/Cl, Ca/Cl, Mg/Cl, K/Cl, Al/Cl,  $SO_4/Cl$ , Ca/Mg,  $SO_4/NO_3$ ,  $H^+/SO_4$ ,  $H^+/NO_3$ , and  $H^+/(SO_4 + NO_3)$ ; and of computed molarities: Ca/Cl, Mg/Cl,  $SO_4/Cl$ , and Al/Cl. The ratio of the logarithm of  $[Al^{+3}]$  to the pH is also calculated, because this ratio may be used in acid-rain studies to determine whether or not aluminum is in equilibrium with an  $Al(OH)_3$  mineral (Johnson and others,

1981, p. 1430-1431; Hooper and Shoemaker, 1985, p 463). Lastly, the ratio of ferric to ferrous iron is calculated from the dissolved oxygen concentration (DO) using oxidation-reduction equations. The DO, in mg/L (milligrams per liter), is first converted to the partial pressure of oxygen ( $pO_2$ ) using the equation:

$$pO_2 = DO/32000. \quad (18)$$

The value of  $pO_2$ , thus calculated, is then substituted into the equation for electron activity (Sato, 1960) to determine the electron activity (pE):

$$pE = 11.385 - pH + 1/4 \log(pO_2), \quad (19)$$

where 11.385 is the value of  $-\log K_{O_2}$  from Truesdell and Jones (1974, p. 239). This equation has been simplified by assuming that the activity of water is 1.

The ratio of ferric to ferrous iron is then calculated from the redox relation (Stumm and Morgan, 1981, p. 447):

$$pE = 13.01 + \log(Fe^{+3})/(Fe^{+2}) \quad (20).$$

#### Cation/anion Balances

ARCHEM performs two cation/anion balances; one based on analytical data, and the other on computed data. The formula used to calculate percent difference is:

$$\text{Percent difference} = \frac{\text{Sum of cations (eq/L)} - \text{sum of anions (eq/L)} \times 100}{\text{Sum of cations (eq/L)} + \text{sum of anions (eq/L)}} \quad (19)$$

where eq/L represents equivalents per liter. The cation/anion balances have a few special features: (1) both balances include the organic anion concentration, which is computed as outlined above; (2) the analytical ion balance treats all iron present as  $Fe^{+3}$ , whereas the computed ion balance uses either  $Fe^{+3}$  or  $Fe^{+2}$  according to the pE computed above; (3) for positive alkalinity, the analytical ion balance sets the bicarbonate-ion concentration equal to the alkalinity; for negative alkalinity, the bicarbonate-ion concentration is set to zero; and (4) in instances where aluminum speciation is not calculated, the computed ion balance treats all aluminum as  $Al^{+3}$ . An error statement is printed if the analytical ion balance is off by more than 5 percent but less than 10 percent. A separate message flags imbalances greater than 10 percent.

#### Specific Conductance

The specific conductance of a water sample depends on the types and concentrations of dissolved ionic substances, and on the sample temperature. Along with cation/anion balances, specific-conductance (SC) calculations can thus serve as data-quality checks in aqueous geochemical systems (American Public Health Association and others, 1975). Calculations of equivalent conductances were first incorporated into an equilibrium computer model by



Reynolds (1978, p. 589-590), and his approach is utilized here. The specific conductance of a solution at 25°C can be calculated using the Onsager Limiting Law (Harned and Owen, 1958):

$$SC = 1000 \sum_i m_i z_i \left( \lambda_{oi} - (.634 \lambda_{oi} |z_i| I)^{1/2} \right), \quad (22)$$

where  $m_i$  is the molarity of the  $i$ -th species in solution,  $z_i$  is the ion's charge, and  $I$  is the ionic strength of the solution. The values of  $\lambda_{oi}$  used by ARCHEM are presented in table 5.

For conductances measured on a meter that does not correct the reading to 25°C, the following equation is needed in order to compare calculated with measured conductance:

$$SCT = SC25/\exp(0.02x[25-T]), \quad (23),$$

where SC25 is the calculated conductance at 25°C and SCT is the conductance at the sample temperature, T (°C). This equation is based on the observation that conductance increases with temperature at a rate of about 2 percent per degree Celsius. Instructions for incorporating this equation are provided in the source code.

ARCHEM computes the percent difference between calculated and observed conductances according to the equation:

$$SC \text{ difference } (\%) = (SC_{calc} - SC_{obser}) / (SC_{calc} + SC_{obser}) \times 100 \% \quad (24).$$

An error flag is printed if the value of SC difference is greater than 5 percent, and a separate message is printed for a SC difference of more than 10 percent.

#### Component Flags

As a final interpretive feature, the program is designed to read an extra line of input containing single-digit, real numbers which can be used to 'flag' important information about any particular component. For example, '1.' may be used to symbolize a concentration below the detection limit; '2.' may represent an estimated value. These flags appear in a column of the output file, and can serve as useful indicators of the significance of values. The flags do not play an active role in determining program functions; the program uses whatever value is input, regardless of the flag. The treatment of detection-limit values and of missing values must be determined by the individual user.

#### LIMITATIONS OF COMPUTER PROGRAM

A number of factors limit the types of water samples that should be run on ARCHEM. The water temperature should be greater than 0° but less than 30°C (a temperature of 0.0° will cause mathematical problems), and the pH should be less than 10. Additionally, the ionic strength of the water should be less than 0.1, the maximum value permitted by the equation for the ion-activity coefficients (see equation 11). Lastly, the user should

Table 5.--Limiting ion conductances at 25°Celsius \*

Ion	lambda <sub>o</sub>
H <sup>+</sup>	349.82
K <sup>+</sup>	73.52
Na <sup>+</sup>	50.11
½ Ca <sup>+2</sup>	59.50
½ Mg <sup>+2</sup>	53.06
**CaHCO <sub>3</sub> <sup>+</sup>	45.
**MgHCO <sub>3</sub> <sup>+</sup>	45.
Cl <sup>-</sup>	76.34
Br <sup>-</sup>	78.4
NO <sub>3</sub> <sup>-</sup>	71.44
HCO <sub>3</sub> <sup>-</sup>	44.48
****½ CO <sub>3</sub> <sup>-2</sup>	97.
OH <sup>-</sup>	198.
½ SO <sub>4</sub> <sup>-2</sup>	79.8

\* Data from MacInnes, 1961, unless otherwise indicated.

\*\* Values estimated by Reynolds, 1978.

\*\*\*Value from the Handbook of Physics.

evaluate whether the chemical equations considered by ARCHEM and the constants such as those associated with complexing by organic material adequately describe the geochemical system and whether the species considered are likely to encompass the major species in solution.

Another important program limitation arises because the user must choose between laboratory and field data (pH, SC, and temperature) for use in calculating the equilibrium distribution of species and the value of SC difference. The program, therefore, must be run twice in order to compare equilibrium distribution of species under both field and laboratory conditions.

The following cautionary notes concern the use of the program: (1) the program assumes equilibrium conditions, and thus may yield results that are not representative of the water if nonequilibrium conditions exist; (2) the 10  $\mu\text{eq}/\text{mg C}$  conversion factor used in the organic-anion calculation may not be correct for a particular water sample and at best will yield only an estimate of the organic-anion concentration; (3) the treatment of iron is fairly crude, although the ferric to ferrous iron ratio should serve as an aid in detecting errors caused by this treatment; (4) although the program may be run on an incomplete data set, the results may be misleading; and (5) for samples that fail the analytical ion balance by greater than 10 percent, the calculated equilibrium concentrations may be erroneous due to analytical errors. Furthermore, the chemistry of the water sample may limit the usefulness of the specific conductance calculation. As the pH decreases, the utility of the specific conductance calculation decreases. At low pH, the hydrogen ion dominates the sample conductance, so that the calculated specific conductance provides less information about the other ions in solution, but is an excellent check on the pH measurement.

The use of specific conductance calculations also may be limited by the presence of ions such as aluminum and iron, for which the limiting ion conductances are not known (Cronan, 1978). ARCHEM has been tested on more than 200 surface- and ground-water samples from McDonalds Branch basin in Lebanon State Forest, N.J., where the surface and ground waters often have high concentrations of dissolved aluminum and iron. In spite of the high aluminum and iron concentrations, the calculated specific conductances, generally, were within 5 percent of the measured values. Furthermore, the sample with the highest combined aluminum and iron values, 10,000 and 370  $\mu\text{g}/\text{L}$  (D.G. Lord, U.S. Geological Survey, West Trenton, N.J., written commun., 1986), respectively, had a calculated specific conductance that differed from the measured value by only 6.4 percent.

ARCHEM may be run on data files containing from 1 to 50 sample analyses. The maximum number of samples may be reset using an available editor. Instructions for this procedure are outlined in the source code.

#### DATA INPUT

The format of sample input files is presented in Attachment A. In addition to the information contained in the input files, the program prompts the user for: (1) the name of the input file (up to 10 characters), (2) the name of the output file (up to 10 characters), (3) the date of the program run (up to 12 characters), and (4) the number of samples to be run

(up to 50 from any one file, in integer format). The maximum number of data files may be reset using an available editor. Instructions for this procedure are outlined in the source code.

#### TEST CASE

A sample output file is shown in Attachment B. This sample is from McDonalds Branch in Lebanon State Forest, N.J., and was obtained as part of a U.S. Geological Survey study of acidic deposition in McDonalds Branch basin. The waters of McDonalds Branch commonly have low pH, low alkalinity, and high concentrations of DOC, aluminum, and iron. The analytical ion balance for this sample has been improved significantly by the addition of the organic-anion concentration to the sum of anions. Without the organic-anion concentration, the percent difference in cations and anions would have been 13.2; with the organic-anion concentration, the percent difference is only 7.2. Despite the high concentrations of aluminum and iron (1,300 and 290  $\mu\text{g/L}$ , respectively) the percent difference in measured versus calculated specific conductance is only 3.1. Although aluminum fractionation was not performed on this sample, the equilibrium distribution of aluminum species has been calculated for display purposes. In some instances, ARCHEM may be used to estimate the maximum concentration of organically bound aluminum, by assuming that all of the calculated organic anion is balanced by aluminum (Thurman, E. M., U.S. Geological Survey Denver, Colo., oral commun., 1986). This approach is being evaluated presently by the authors.

#### SUMMARY

The computer program ARCHEM was designed for the routine geochemical interpretation of low-ionic-strength, acidic waters, as are commonly encountered in acid-rain studies. ARCHEM calculates equilibrium speciation, ionic strength, ion ratios, cation/anion balances, and specific conductance. The program has a number of special features, including a calculation of the organic-anion concentration, which can greatly improve cation/anion balances in some waters. Furthermore, the program allows for the input of negative alkalinity values. Lastly, ARCHEM may be run on files of multiple sample analyses.

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Attachment A. Sample Input File

S-7	' ' 2/19/1986'	3.7000	134.0000	0.0000	124.0000	0.5
290.0000	0.0887	4.6000	0.1000	0.0100	18.0000	
1300.0000	1.6000	1.0000	55.0000	2.8000	0.3100	
0.0000	0.0031	-0.2E-3	14.0000	10.50	3.9000	2.4791
0. 2. 2. 2. 1.						
0. 0. 0. 0. 1. 0. 0. 0. 0. 0. 0. 0. 3. 0. 2. 0. 0.						

Description of Format

- CARD 1 A17,1X,A12,1X,5(G10.4E2,1X) SITE ID,DATE,FIELD PH,FIELD SPECIFIC CONDUCTANCE(UMHOS),LAB PH, LAB SPECIFIC CONDUCT- AND(UMHOS),FIELD TEMPERATURE(DEGREES CELSIUS)
- CARD 2 6(G10.4E2,1X) IRON(UG/L),AMMONIUM(MG/L),CHLORIDE(MG/L), FLUORIDE(MG/L),BROMIDE(MG/L),SULFATE(MG/L)
- CARD 3 6(G10.4E2,1X) ALUMINUM(UG/L),CALCIUM(MG/L),MAGNESIUM(MG/L), MANGANESE(UG/L),SODIUM(MG/L),POTASSIUM(MG/L)
- CARD 4 5(G10.4E2,1X) NITRATE(MG/L),PHOSPHATE(MG/L),ALAKLINITY(EQ/L), DOC(MG/L),DO(MG/L)
- CARD 5 G10.4E2,4(1X,F1) CONCENTRATION OF ORGANICALLY-BOUND ALUM- INUM(UG/L),FLAG FOR LAB/FIELD DATA(1. OR 2.),FLAG FOR CALCULATION OF ALUMINUM SPECIATION(1. OR 2.),FLAG FOR FLUORIDE INPUT AS [F-] OR TOTAL FLUORIDE(1. OR 2.),FLAG TO INPUT CARD 1-5 DATA IN EQ/L INSTEAD OF MG/L OR UG/L (2. OR 1.).
- CARD 6 17(F1) FLAGS USED TO SIGNAL IMPORTANCE OF INPUT VALUE, IN FOLLOWING ORDER: AL,CA,MG,MN,NA,K,FE,NH4,CL,F,BR,SO4,NO3, PO4,ALKALINITY,DOC,DO  
(REPEAT CARDS 1-6 FOR REMAINING SAMPLES)



Attachment B. A sample output file.

1\*\*\*\*\*

SITE ID = S-7 DATE: 2/19/1986  
 DATE RUN ON ARCHEM.F77: 4/12/87

PHFLD= 3.700 TEMP= 0.500 SCFLD= 134.000  
 PHLAB= 0.000 TEMP= 25.000 SCLAB= 124.000

RATIO OF H+ ACTIVITY FIELD TO H+ ACTIVITY LAB= 0.0000  
 RATIO OF SC FIELD TO SC LAB= 1.08

FIELD DATA WERE USED

INPUT PARAMETERS				CALCULATED PARAMETERS		
	MG/L	MOLARITY	EQ/L	ACTIVITY	GAMMA	1.=<
H=		0.2058E-03	0.2058E-03	0.1995E-03	0.9695	
CA=	1.600	0.3992E-04	0.7984E-04	0.3438E-04	0.8804	0.
MG=	1.000	0.4113E-04	0.8226E-04	0.3590E-04	0.8825	0.
NA=	2.800	0.1218E-03	0.1218E-03	0.1179E-03	0.9682	1.
K=	0.3100	0.7927E-05	0.7927E-05	0.7671E-05	0.9678	0.
NH4=	0.8870E-01	0.4918E-05	0.4918E-05	0.4758E-05	0.9676	0.
CL=	4.600	0.1298E-03	0.1298E-03	0.1256E-03	0.9678	0.
F=	0.1000	0.5264E-05	0.5264E-05	0.1886E-07	0.9679	0.
BR=	0.1000E-01	0.1251E-06	0.1251E-06	0.1211E-06	0.9678	0.
SO4=	18.00	0.1874E-03	0.3748E-03	0.1589E-03	0.8786	0.
NO3=	0.0000	0.0000	0.0000	0.0000	0.9678	3.
PO4=	0.3100E-02	0.3264E-07	0.9793E-07	0.2440E-07	0.7474	0.
ALK=		-.2000E-03	-.2000E-03			2.
DOC=	14.00					0.
DO=	10.50					0.
	UG/L	MOLARITY	EQ/L	ACTIVITY	GAMMA	1.=<
AL=	1300.	0.4829E-04	0.1449E-03	0.2851E-04	0.7567	0.
MN=	55.00	0.1001E-05	0.2002E-05	0.8813E-06	0.8804	0.
FE=	290.0	0.5194E-05	0.1039E-04	0.4573E-05	0.8804	0.

ALL FE ASSIGNED TO +2 VALENCE AS FE+3/FE+2 RATIO  
 COMPUTED BELOW IS LESS THAN 1.

MOLARITIES CALCULATED  
 FROM EQUILIBRIUM SPECIATION EQUATIONS

CA= 0.3905E-04  
 MG= 0.4068E-04  
 SO4= 0.1808E-03  
 F= 0.1949E-07  
 HF= 0.5565E-08  
 OH= 0.6111E-11

SULFATE SPECIES

CASO4= 0.8534E-06  
 MGSO4= 0.4468E-06

CARBONATE SPECIES

CAHCO3= 0.1928E-07  
 MGHCO3= 0.4829E-08  
 CO3= 0.1242E-10  
 HCO3= 0.5358E-04  
 H2CO3= 0.5361E-01  
 CACO3= 0.3609E-12  
 MGCO3= 0.9711E-12

## ALUMINUM SPECIES

AL3+= 0.3768E-04  
 ALOH= 0.1554E-06  
 ALOH2= 0.1618E-08  
 ALOH3= 0.3167E-12  
 ALOH4= 0.1490E-14  
 ALF= 0.5238E-05  
 ALF2= 0.4273E-07  
 ALF3= 0.1341E-10  
 ALF4= 0.1374E-15  
 ALF5= 0.4814E-22  
 ALF6= 0.0000  
 ALSO4= 0.5119E-05  
 ALSO42= 0.5718E-07

## ION RATIOS FROM ANALYTICAL MOLARITIES=

NA/CL= 0.9386  
 CA/CL= 0.3076  
 MG/CL= 0.3170  
 K/CL= 0.6108E-01  
 AL/CL= 0.3722  
 SO4/CL= 1.444  
 CA/MG= 0.9706  
 SO4/NO3 = 0.0000  
 H/SO4= 1.065  
 H/NO3= 0.0000  
 H/(SO4+NO3)= 0.0000

## ION RATIOS FROM COMPUTED MOLARITIES

CA/CL= 0.3009  
 MG/CL= 0.3135  
 SO4/CL= 1.394  
 AL/CL= 0.2904

FE+3/FE+2= 0.6368E-06  
 PE= 6.814

RATIO (LOG ACTIVITY AL3+)/(LOG ACTIVITY OF H+)= 1.228

RECALCULATED TOTAL ALUMINUM, MOLES/L = 0.4830E-04  
 SATURATION INDEX FOR BASIC ALUMINUM SULFATE= 0.4550E-02

ORGANIC ANION CONC, EQ/L = 0.6549E-04

MEASURED ALKALINITY, EQ/L = -.2000E-03  
 NEWALK, ALKALINITY CALCULATED FROM Cb-Ca= -.1970E-03

IONIC STRENGTH= 0.8978E-03

SUM CATION EQ/L = 0.6587E-03  
 SUM ANION EQ/L = 0.5703E-03  
 ANALYTICAL PERCENT DIFFERENCE IN CATIONS VS ANIONS= 7.200

\*\*\* FAILS IONBAL AT 5% \*\*\*

SUM OF CATIONS= 0.6257E-03  
 SUM OF ANIONS= 0.6108E-03  
 COMPUTED PERCENT DIFFERENCE IN CATIONS VS ANIONS= 1.206

PREDICTED SC = 125.997  
 PERCENT DIFFERENCE IN SC MEASURED VS PREDICTED= 3.078

Attachment C. Source code.

(Copies of this source code on diskette can be purchased from the address given in the front of the book)

```

C      ARCHEM.F77, A FORTRAN 77 PROGRAM WRITTEN BY P.A. JOHNSON, WITH      1
C      D.G.LORD AT THE U.S. GEOL. SURVEY WRD TRENTON, NJ. THIS PROGRAM      2
C      TAKES CHEMICAL DATA IN MG/L AND UG/L AND CALCULATES MOLARITIES,      3
C      EQ/L, ORGANIC ANION CONCENTRATION, IONIC STRENGTH, CATION/ANION      4
C      BALANCE, AND PREDICTED SPECIFIC CONDUCTANCE.                          5
C      CALCULATION OF ALUMINUM SPECIATION IS OPTIONAL.                       6
C      ARCHEM.F77 WAS SPECIFICALLY FORMULATED FOR USE WITH LOW-PH, LOW      7
C      IONIC STRENGTH, ORGANIC-RICH WATERS, AS OCCUR IN THE NEW JERSEY      8
C      PINELANDS.                                                             9
C      PLEASE NOTE THAT THE CHEMICAL DATA MAY ALSO BE INPUT AS UEQ/L.      10
C      SEE EQGRAM(M), BELOW, AND LOOP FOLLOWING READ STATEMENTS.            11
C      SAMPLE INPUT FILE:                                                    12
C      CARD 1  A17,1X,A12,1X,5(G10.4E2,1X) SITE ID,DATE,FIELD PH,FIELD      13
C              SPECIFIC CONDUCTANCE(UMHOS),LAB PH, LAB SPECIFIC CONDUCT-    14
C              AND(UMHOS),FIELD TEMPERATURE(DEGREES CELSIUS)                15
C      CARD 2  6(G10.4E2,1X) IRON(UG/L),AMMONIUM(MG/L),CHLORIDE(MG/L),      16
C              FLUORIDE(MG/L),BROMIDE(MG/L),SULFATE(MG/L)                   17
C      CARD 3  6(G10.4E2,1X) ALUMINUM(UG/L),CALCIUM(MG/L),MAGNESIUM(MG/L),  18
C              MANGANESE(UG/L),SODIUM(MG/L),POTASSIUM(MG/L)                19
C      CARD 4  5(G10.4E2,1X) NITRATE(MG/L),PHOSPHATE(MG/L),ALAKLINITY(EQ/L), 20
C              DOC(MG/L),DO(MG/L)                                           21
C      CARD 5  G10.4E2,4(1X,F1) CONCENTRATION OF ORGANICALLY-BOUND ALUM-   22
C              INUM(UG/L),FLAG FOR LAB/FIELD DATA(1. OR 2.),FLAG FOR      23
C              CALCULATION OF ALUMINUM SPECIATION(1. OR 2.),FLAG FOR      24
C              FLUORIDE INPUT AS [F-] OR TOTAL FLUORIDE,FLAG FOR INPUT     25
C              AS MILLIGRAMS OR MICROEQUIVALENTS PER LITER (1. OR 2.).     26
C      CARD 6  17(F1) FLAGS USED TO SIGNAL IMPORTANCE OF INPUT VALUE, IN   27
C              FOLLOWING ORDER:  AL,CA,MG,MN,NA,K,FE,NH4,CL,F,BR,SO4,NO3,   28
C              PO4,ALKALINITY,DOC,DO                                         29
C                                                                              30
C              (REPEAT CARDS 1-6 FOR REMAINING SAMPLES)                       31
C                                                                              32
C      *****                                                                33
C      PARAMETER STATEMENT-- CHANGE M MANUALLY TO ALTER MAXIMUM            34
C      NUMBER OF SAMPLES THAT CAN BE RUN AT ONE TIME.  PRESENT MAXIMUM     35
C      IS 50.                                                                  36
C      *****                                                                37
C      PARAMETER (M = 50)                                                     38
C      *****                                                                39
C                                                                              40
C      .....INPUT FLAGS FOR LESS THAN VALUES (CARD 6 DATA)              41
C      REAL AZ1(M),AZ2(M),AZ3(M),AZ4(M),AZ5(M),AZ6(M),AZ7(M),              42
C      *      AZ8(M),AZ9(M),AZ10(M),AZ11(M),AZ12(M),AZ13(M),AZ14(M),        43
C      *      AZ15(M),AZ16(M),AZ17(M)                                         44

```

Attachment C. Source code-- continued.

C.....	INPUT PARAMETERS, IN MG/L	45
	REAL TCA(M), TMG(M), TSO4(M), NO3(M), NH4(M), NA(M), K(M), CL(M),	46
*	BR(M), F(M), DOC(M), PO4(M)	47
C.....	INPUT PARAMETERS, IN UG/L	48
	REAL FE(M), MN(M), AL(M)	49
C		50
C.....	INPUT PARAMETERS, IN EQ/L	51
	REAL ALK1(M)	52
C		53
C.....	OTHER INPUT PARAMETERS-- DISSOLVED OXYGEN, FIELD SPECIFIC	54
C.....	CONDUCTANCE, LAB SPECIFIC CONDUCTANCE, FIELD PH, LAB PH,	55
C	FIELD TEMPERATURE (DEG. CELSIUS).	56
C	CTEMP2 IS LAB TEMPERATURE AND IS AUTOMATICALLY PUT IN BY	57
C	ARCHEM AS 25 DEGREES CELSIUS.	58
	REAL DO(M), SCFLD(M), SCLAB(M), PH(M), PH2(M), CTEMP(M),	59
*	CTEMP2, SI(M)	60
C.....	CHARACTER INPUT SITE (17 CHARACTERS), DATE (12 CHARACTERS).	61
C.....	INPUT SHOULD INCLUDE SINGLE QUOTES.	62
	CHARACTER*17 SITE(M)	63
	CHARACTER*12 DATE(M)	64
C.....	CHARACTER INPUT CALLED FOR BY PROMPT. NAME OF INPUT FILE HAS	65
C	TEN CHARACTERS, NAME OF OUTPUT FILE HAS TEN CHARACTERS, TODAY'S	66
C	DATE HAS 12 CHARACTERS. NO SINGLE QUOTES NEEDED.	67
	CHARACTER INFILE*10, OUTFILE*10, TODAY*12	68
C.....	CALCULATED SPECIES, MOLARITIES	69
	REAL OH, CO3, ORG, HCO3, CA, MG, SO4, CASO4, MGSO4, CAHCO3, MGHCO3,	70
*	H2CO3, CACO3, MGC03, HF	71
C.....	A PARAMETERS ARE ACTIVITIES. ACTIVITIES OF UNCHARGED SPECIES ARE	72
C	TAKEN AS EQUAL TO 1.	73
	REAL ACA, AMG, ASO4, ANO3, ANH4, ANA, AK, ACL, ABR, AF, APO4,	74
*	AFE, AMN, AAL, ACO3, AHCO3, AOH	75
C.....	Z PARAMETERS ARE MOLARITIES	76
	REAL TCAZ, TMGZ, TSO4Z, NO3Z, NH4Z, NAZ, KZ, CLZ, BRZ, FZ, DOCZ, PO4Z,	77
*	FEZ, MNZ, ALZ, ALKZ	78
C.....	E PARAMETERS ARE EQ/L (FOR DI- AND TRI-VALENT SPECIES).	79
	REAL CAE, MGE, SO4E, PO4E, FEE, MNE, ALE	80
C.....	E2 PARAMETERS ARE UEQ/L	81
	REAL CAE2, MGE2, SO4E2, NO3E2, NH4E2, NAE2, KE2, CLE2, BRE2, FE2,	82
*	PO4E2, FEE2, MNE2, ALE2, OHE2, ORGE2,	83
*	EF	84
C.....	G PARAMETERS ARE ACTIVITY COEFFICIENTS, GAMMAS	85
	REAL GCA, GMG, GSO4, GHCO3, GCAHCO3, GMGHCO3, GOH, GH, GAL, GMN,	86
*	GFE, GPO4, GNA, GF, GK, GCL, GBR, GNO3, GNH4	87
C.....	SC PARAMETERS ARE EQUIVALENT CONDUCTANCES	88
	REAL SCCA, SCMG, SCH, SCNA, SCK, SCCAHCO3, SCMGHCO3, SCCO3, SCHCO3,	89
*	SCOH, SCCL, SCSO4, SCNH4, SCNO3, SCBR	90

Attachment C. Source code-- continued.

C.....K VALUES ARE EQUILIBRIUM EXPRESSIONS CORRECTED FOR TEMPERATURE.	91
REAL K1,K2,K3,K4,K5,K6,KW,K9,K10	92
C.....VALUES FOR ORGANIC ANION CALCULATION	93
REAL PK,KBAR,CBAR	94
C	95
C.....PARAMETERS FOR REDOX IRON CALCULATIONS (FROM STUMM AND	96
C    MORGAN)	97
REAL PO2,PE,FER,FEV2,FE3	98
C.....NEWALK IS THE ALKALINITY CALCULATED FROM THE ALTERNATIVE	99
C.....EQUATION FOR ALKALINITY:	100
C.....  ALK = Cb-Ca	101
C.....  WHERE Cb= 2*CA + 2*MG + NA + K + NH4	102
C.....  AND Ca= NO3 + 2*SO4 + CL + F	103
C.....  THE VALUE OF NEWALK CAN BE COMPARED TO THE MEASURED	104
C.....  VALUE OF ALKALINITY.	105
REAL NEWALK	106
C.....VALUES FOR SPECIFIC CONDUCTANCE CALCULATION	107
REAL SCT,SC25,SC25T,SCDIF	108
C.....VARIOUS CONSTANTS	109
REAL A,B,C,D,Z,KTEMP	110
C.....VALUES FOR LOOP	111
REAL L,MSO4,GMSO4,T,FZ2,FZM	112
C.....IONIC STRENGTH	113
REAL MU,MU2,MUF	114
C.....ION BALANCE	115
REAL CAT2,AN2,CATAN2,CAT,AN,CATAN	116
C.....R VALUES ARE ANALYTICAL ION RATIOS OF MOLARITIES	117
REAL RCA,RMG,RNA,RK,RAL,RSO4,RSO4NO3,RHSO4,RHNO3,RHSN	118
C.....R2 VALUES ARE COMPUTED ION RATIOS OF MOLARITIES	119
REAL R2CA,R2MG,R2AL,R2SO4	120
C.....VALUE OF LOG (ACTIVITY AL3+)/LOG(ACTIVITY H+)	121
REAL LRAL	122
C.....RATIO OF TDS TO SC.	123
REAL TDSRAT	124
C.....VALUES FOR LAB VERSUS FIELD DATA	125
REAL RATPH,RATSC,RPH1,RPH2	126
C.....FLAG FOR USE OF LAB OR FIELD DATA	127
C.....INPUT I=1. USES LAB DATA.  INPUT I = 2.	128
C.....USES FIELD DATA.	129
REAL LFI(M)	130
C.....FLAG FOR FLUORIDE INPUT.  FI(M) = 1. FOR ION-SPECIFIC ELECTRODE	131
C.....VALUE, WHERE FLUORIDE = {F-}.  FI(M) = 2. FOR FLUORIDE = TOTAL	132
C.....DISSOLVED FLUORIDE.	133
REAL FI(M)	134

Attachment C. Source code-- continued.

C.....	FLAG ALSP CALCULATES ALUMINUM SPECIATION. USE THIS OPTION	135
C.....	ONLY WHEN TEMP = 25 DEG C. IF YOU HAVE DATA FOR ORGANICALLY	136
C.....	BOUND ALUMINUM, INPUT THIS CONCENTRATION AS ORGAL. THIS VALUE IS	137
C.....	SUBTRACTED FROM TOTAL ALUMINUM IN THE SUBSEQUENT CALCULATIONS.	138
C.....	ALSP = 1. TO DELETE ALUMINUM SPECIATION. ALSP = 2. TO CALCULATE	139
C.....	ALUMINUM SPECIATION.	140
	REAL ALSP(M)	141
	REAL ORGAL(M)	142
C.....	FLAG FOR INPUT AS MILLIGRAMS PER LITER (1.) OR MICROEQUIVALENTS	143
C.....	PER LITER (2.)	144
	REAL EQGRAM(M)	145
C.....	MOLARITIES OF ALUMINUM SPECIES (AL3 IS ACTIVITY)	146
	REAL AL3,ALOH,ALOH2,ALOH3,ALOH4,ALF,ALF2,ALF3,ALF4,ALF5,ALF6,	147
*	ALSO4,ALSO42,TAL,AL3M	148
C.....	ACTIVITY COEFFICIENTS FOR ALUMINUM SPECIES, TAKEN AS THE	149
C.....	AVERAGE VALUE FOR MONO-, DI-, AND TRI- VALENT SPECIES IN	150
C.....	SOLUTION, AS IN JOHNSON ET. AL., 1981.	151
	REAL G1,G2,G3	152
C.....	EQUIVALENTS/LITER OF ALUMINUM SPECIES	153
	REAL AL3E,ALOHE,ALOH2E,ALOH4E,ALFE,ALF2E,ALF3E,ALF4E,ALF5E,	154
*	ALF6E,ALSO4E,ALSO42E,ALOH3E	155
C.....	SATURATION INDEX FOR BASIC ALUMINUM SULFATE (ALOHSO4)	156
	REAL ALSULF	157
C.....	VALUES OF EQUILIBRIUM CONSTANTS FOR ALUMINUM SPECIATION EQNS.,	158
C.....	AT 25C. VALUES FROM HEM, 1968; BEHR AND WENDT, 1962,	159
C.....	OR MAY ET. AL., 1968.	160
C.....	KSO IS FOR NATURAL GIBBSITE (MAY, ET AL., 1979)	161
	REAL KOH1,KOH2,KOH3,KOH4,KF1,KF2,KF3,KF4,KF5,KF6,KS1,KS2,KSO	162
	REAL DOH1,DOH4,DF1,DF2,DF3,DF4,DF5,DS1,DS2	163
	DATA KOH1/1.02E-05/,	164
*	KOH2/7.41E-11/,	165
*	KOH3/1.74E-17/,	166
*	KOH4/6.92E-23/,	167
*	KF1/1.023E+07/,	168
*	KF2/5.62E+12/,	169
*	KF3/1.047E+17/,	170
*	KF4/5.25E+19/,	171
*	KF5/8.32E+20/,	172
*	KF6/7.49E+20/,	173
*	KS1/1.58E+03/,	174
*	KS2/1.26E+05/,	175
*	KSO/5.89E+08/	176
C.....	VALUES OF DELTA H FOR AL-FLOURIDE SPECIES ARE FROM SMITH AND	177
C	MARTELL, 1976. VALUES FOR ALUMINUM SULFATE SPECIES ARE	178
C	FROM IZATT ET. AL., 1969. VALUES FOR ALUMINUM HYDROXIDES	179
C	ARE FROM NORDSTROM ET. AL., 1984 OR PLUMMER ET. AL., 1976.	180

Attachment C. Source code-- continued.

```

DATA DOH1/14.775/,
* DOH2/22.0/,
* DOH3/33.0/,
* DOH4/42.22/,
* DF1/1.100/,
* DF2/2.000/,
* DF3/2.500/,
* DF4/2.200/,
* DF5/1.800/,
* DF6/0.10/,
* DS1/2.290/,
* DS2/3.070/
CTEMP2 = 25.
C *****
C THIS PORTION OF THE PROGRAM READS IN DATA FROM KEYBOARD AND FILES.
C *****
C.....PROMPT FOR TODAY'S DATE, NAME OF INPUT FILE, NAME OF OUTPUT FILE
PRINT*, 'WELCOME TO ARCHEM.F77. PLEASE TYPE IN THE DATE'
READ '(A)', TODAY
PRINT*, 'TYPE IN NAME OF INPUT FILE'
READ '(A)', INFILE
PRINT*, 'TYPE IN NAME OF OUTPUT FILE'
READ '(A)', OUTFILE
PRINT*, 'TYPE IN NUMBER OF DATA FILES (UP TO 50)'
READ (1,*) NDAT
OPEN (20, FILE=INFILE)
OPEN (61, FILE=OUTFILE)
DO 500 IL = 1, NDAT
C READS DATA FROM INPUT FILE, CARDS 1-6 AS DESCRIBED ABOVE
READ (20,*) SITE(IL), DATE(IL), PH(IL), SCFLD(IL),
* PH2(IL), SCLAB(IL), CTEMP(IL), FE(IL), NH4(IL), CL(IL), F(IL),
* BR(IL), TSO4(IL), AL(IL), TCA(IL), TMG(IL), MN(IL), NA(IL), K(IL),
* NO3(IL), PO4(IL), ALK1(IL), DOC(IL), DO(IL)
READ(20,*) ORGAL(IL), LFI(IL), ALSP(IL), FI(IL), EQGRAM(IL)
READ (20,*) AZ1(IL), AZ2(IL), AZ3(IL), AZ4(IL), AZ5(IL),
* AZ6(IL), AZ7(IL), AZ8(IL), AZ9(IL), AZ10(IL), AZ11(IL),
* AZ12(IL), AZ13(IL), AZ14(IL), AZ15(IL), AZ16(IL), AZ17(IL)
C *****
C CHANGE FOR INPUTTING DATA AS UEQ/LITER. NOTE FE IS
C ASSUMED TO BE AS FE+3 IN DATA SET.
IF (EQGRAM(IL) .EQ. 2.) THEN
FE(IL) = FE(IL)/.05372
NH4(IL) = NH4(IL)*.001/.05544
CL(IL) = CL(IL)*.001/.02821
F(IL) = F(IL)*.001/.05264
BR(IL) = BR(IL)*.001/.01251

```

Attachment C. Source code-- continued.

```

TSO4(IL) = TSO4(IL)*.001/.02082      227
AL(IL) = AL(IL)/.11119                228
TCA(IL) = TCA(IL)*0.001/.04990       229
TMG(IL) = TMG(IL)*.001/.08226        230
MN(IL) = MN(IL)/.03640                231
NA(IL) = NA(IL)*.001/.04350          232
K(IL) = K(IL)*.001/.02557            233
NO3(IL) = NO3(IL)*.001/.01613        234
PO4(IL) = PO4(IL)*.001/.03159        235
ELSE                                    236
CONTINUE                                237
END IF                                  238
C.....COMPUTATION OF RATIOS: 1) HYDROGEN ION FROM FIELD DATA OVER 239
C HYDROGEN ION FROM LAB DATA AND 2) SCFIELD VERSUS SCLAB.          240
IF (PH(IL) .GT. 0. .AND. PH2(IL) .GT. 0.) THEN                          241
  RPH1 = 10.**(-(PH(IL)))                                                242
  RPH2 = 10.**(-(PH2(IL)))                                               243
  RATPH = RPH1/RPH2                                                      244
ELSE                                                                        245
CONTINUE                                                                    246
END IF                                                                        247
  RATSC = SCFLD(IL)/SCLAB(IL)                                             248
  CTEMP2 = 25.                                                            249
  WRITE (61,1) SITE(IL),DATE(IL),TODAY                                    250
  WRITE (61,2) PH(IL),CTEMP(IL),SCFLD(IL)                                251
  WRITE (61,3) PH2(IL),CTEMP2,SCLAB(IL)                                   252
  IF (LFI(IL) .EQ. 2.) THEN                                              253
    SCLAB(IL) = SCFLD(IL)                                                254
    CTEMP2 = CTEMP(IL)                                                   255
    PH2(IL) = PH(IL)                                                     256
  END IF                                                                    257
  IF (PH2(IL) .GE. 10.0) THEN                                             258
    WRITE (61,4)                                                           259
    WRITE (*,4)                                                            260
  END IF                                                                    261
  IF (CTEMP2 .LE. .1 .OR. CTEMP2 .GE. 100.0) THEN                       262
    WRITE (61,5)                                                           263
    WRITE (*,5)                                                            264
  END IF                                                                    265
  WRITE(61,6) RATPH,RATSC                                                 266
C.....CALCULATES TDS/S.C RATIO                                           267
  TDSRAT=((.001*AL(IL))+TCA(IL)+TMG(IL)+(.001*MN(IL))+NA(IL)+K(IL)      268
* +(.001*FE(IL))+NH4(IL)+CL(IL)+F(IL)+BR(IL)+TSO4(IL)+NO3(IL)+        269
* PO4(IL)+DOC(IL)+DO(IL))/SCLAB(IL)                                     270

```



Attachment C. Source code-- continued.

```

C.....CALCULATES VALUES OF FE+2 AND FE+3 FROM REDOX (STUMM AND MORGAN) 271
  IF (DO(IL) .NE. 0.) THEN 272
    PO2 = DO(IL)/32000 273
    PE = 11.385-PH2(IL) +(.25*LOG10(PO2)) 274
    FER = 10.**(PE-13.01) 275
    ELSE 276
    PE = 0. 277
    FER = 1. 278
  END IF 279
C.....Z PARAMETERS ARE MOLARITIES 280
C.....CONVERSION FACTORS ARE FROM USGS WATER SUPPLY PAPER 1473 281
  PO4Z = PO4(IL)*.001*.01053 282
  DOCZ = DOC(IL) 283
  TCAZ = TCA(IL)*.001*.02495 284
  TMGZ = TMG(IL)*.001*.04113 285
  TSO4Z = TSO4(IL)*.001*.01041 286
  NAZ = .001*NA(IL)*.04350 287
  CLZ = .001*CL(IL)*.02821 288
  NO3Z = .001*NO3(IL)*.01613 289
  FZ = .001*F(IL)*.05264 290
  FZ2 = FZ 291
  MNZ = MN(IL)*.001*.01820*.001 292
  KZ = K(IL)*.001*.02557 293
  BRZ = .001*BR(IL)*.01251 294
  ALKZ = ALK1(IL) 295
  FEZ = FE(IL)*.001*.01791*.001 296
  ALZ = AL(IL)*.001*.03715*.001 297
  NH4Z = NH4(IL)*.001*.05544 298
  ORGAL(IL) = ORGAL(IL)*.001*.03715*.001 299
C.....E PARAMETERS ARE EQ/LI 300
  ALE = ALZ*3. 301
  MNE = MNZ*2. 302
  IF (FER .GE. 1.) THEN 303
    FEE = FEZ*3. 304
    ELSE 305
    FEE = FEZ*2. 306
  END IF 307
  CAE =TCAZ*2. 308
  MGE = TMGZ*2. 309
  SO4E = TSO4Z*2. 310
  PO4E = PO4Z*3. 311
C.....SETS TEMPERATURE-DEPENDENT EQM. CONSTANTS. THERMODYNAMIC 312
C.....DATA FROM TRUESDELL AND JONES, 1974. 313
  KTEMP = CTEMP2 + 273.15 314
  C = ((1/KTEMP)-(3.35D-3)) 315

```

Attachment C. Source code-- continued.

```

D = (1.9D-3)*2.303                                316
K1 = (4.909D-3)*(10.**((1.65/D)*C))                317
K2 = (5.495*10.**(-2.))*(10.**((6.331/D)*C))      318
K3 = (5.8*10.**(-3.))*(10.**((4.92/D)*C))         319
K4 = (1.2*10.**(-1.))*(10.**((10.37/D)*C))        320
K5 = (6.3*10.**(-4.))*(10.**((3.13/D)*C))         321
K6 = (3.999*10.**(-4.))*(10.**((.058/D)*C))       322
KW = (1.0*10.**(-14.))*(10.**((-13.345/D)*C))    323
K9 = (4.677*10.**(-11.))*(10.**((-3.55/D)*C))    324
K10=(4.2*10.**(-7.))*(10.**((-1.976/D)*C))        325
C = (3.35D-3) - (1/KTEMP)                          326
KOH1 = KOH1*(10.**((DOH1/D)*C))                   327
KOH2 = KOH2*(10.**((DOH2/D)*C))                   328
KOH3 = KOH3*(10.**((DOH3/D)*C))                   329
KOH4 = KOH4*(10.**((DOH4/D)*C))                   330
KF1 = KF1*(10.**((DF1/D)*C))                       331
KF2 = KF2*(10.**((DF2/D)*C))                       332
KF3 = KF3*(10.**((DF3/D)*C))                       333
KF4 = KF4*(10.**((DF4/D)*C))                       334
KF5 = KF5*(10.**((DF5/D)*C))                       335
KS1 = KS1*(10.**((DS1/D)*C))                       336
KS2 = KS2*(10.**((DS2/D)*C))                       337
HCO3 = ALKZ                                         338
C.....SETS ACTIVITY COEFFICIENTS TO 1              339
GH = 1.                                             340
GOH = 1.                                           341
GSO4 = 1.                                          342
GCA = 1.                                           343
GMG = 1.                                           344
GCO3 = 1.                                          345
GHCO3 = 1.                                         346
GCAHCO3 = 1.                                       347
GMGHCO3 = 1.                                       348
GF = 1.                                             349
GAL = 1.                                           350
GMN = 1.                                           351
GFE = 1.                                           352
GPO4 = 1.                                          353
GNA = 1.                                           354
GK = 1.                                             355
GCL = 1.                                           356
GBR = 1.                                           357
GNO3 = 1.                                          358
GNH4 = 1.                                          359
C INITIALIZES [SO4] AS .1 X TSO4                   360
L = 1.*(10.**(-1.))                                361
SO4 = L*TSO4Z                                       362

```

Attachment C. Source code-- continued.

```

C      INITIALIZES HYDROGEN, HYDROXIDE, AND CARBONATE CONCENTRATIONS          363
63  HY = (10.**(-PH2(IL)))/GH                                                364
      H = HY*GH                                                                365
      HE2 = H*1000.*1000.                                                    366
      CO3 = K9*GHCO3*HCO3/(HY*GH*GCO3)                                       367
      OH = KW/(HY*GH*GOH)                                                    368
      OHE2 = OH*1000.*1000.                                                  369
C.....CALCULATES ORGANIC ANION(ORG) CONC.                                    370
C.....EQUATIONS FROM OLIVER, ET. AL., 1983.                                  371
C      TO CHANGE THE CONVERSION FACTOR FROM 10 UEG/MG DOC TO                 372
C      A VALUE APPROPRIATE FOR YOUR PARTICULAR WATERS,                       373
C      REPLACE THE 10. IN THE CBAR = LINE WITH THIS VALUE.                   374
      PK = .96 + (.9*PH2(IL)) - (.039*(PH2(IL)**2.))                         375
      KBAR = 10.**(-PK)                                                       376
      CBAR = DOCZ*(10.*(1.E-6))                                               377
      ORG = (KBAR*CBAR)/(KBAR + H)                                           378
      ORGE2 = ORG*(10.**6)                                                   379
C                                                                              380
C*****LOOP TO CALCULATE IONIC STRENGTH AND CARBONATE SPECIES             381
C                                                                              382
C      A AND B ARE FACTORS USED IN THE DEBYE-HUCKEL EQUATION.                383
      A = (.00082*((Ctemp2)-5.))+.4921                                       384
      B = (.3241+(.0008*(ctemp2/5.)))*(10.**(-8))                            385
      CA = TCAZ/(1.+(GCA*GSO4*SO4/K1)+(GHCO3*HCO3*GCA/(K2*GCAHCO3))+
*   (GCA*GCO3*CO3/K5))                                                       386
      MG = TMGZ/(1.+(GMG*GSO4*SO4/K3)+(GHCO3*HCO3*GMG/(K4*GMGHCO3))+
*   (GMG*GCO3*CO3/K6))                                                       387
      CASO4 = (CA*GCA*GSO4*SO4)/K1                                           388
      MGSO4 = (MG*GMG*GSO4*SO4)/K3                                           389
      CAHCO3 = (CA*GCA*GHCO3*HCO3)/(K2*GCAHCO3)                             390
      MGHCO3 = (MG*HCO3*GMG*GHCO3)/(K4*GMGHCO3)                             391
      CACO3 = GCA*CA*GCO3*CO3/K5                                             392
      MGCO3 = GMG*MG*GCO3*CO3/K6                                             393
C.....OPTIONAL AL SPECIATION CALCULATIONS                                   394
      IF (ALSP(IL) .EQ. 2.) THEN                                             395
          G1 = (GH+GNA+GK+GNH4+GCL+GF+GBR+GNO3)/8.                            396
          G2 = (GCA+GMG+GSO4+GMN)/4.                                          397
          G3 = (GPO4+GAL)/2.                                                  398
          AL3 = (ALZ - (ORGAL(IL)))/((1./GAL)+(KOH1/(GH*HY*G2)))+
*   (KOH2/(GH*GH*HY*HY*G1)) + (KOH3/(GH*GH*GH*HY*HY*HY))+
*   (KOH4/(HY*HY*HY*HY*GH*GH*GH*G1))+(FZ*GF*KF1/G2)+
*   (FZ*FZ*GF*GF*KF2/G1)+(FZ*FZ*FZ*GF*GF*GF*KF3) + (FZ*FZ*FZ*FZ*
*   GF*GF*GF*GF*KF4/G1)+(FZ*FZ*FZ*FZ*FZ*GF*GF*GF*GF*GF*KF5/G2)
*   + ((FZ**6)*(GF**6)*KF6/G3)+(SO4*GSO4*KS1/G1)+
*   ((SO4**2)*(GSO4**2)*(KS2/G1))                                           399
          400
          401
          402
          403
          404
          405
          406
          407

```

## Attachment C. Source code-- continued.

```

AL3M = AL3/GAL                                408
ALOH = (AL3*KOH1)/(HY*GH*G2)                  409
ALOH2 = (AL3*KOH2)/(HY*HY*GH*GH*G1)          410
ALOH3 = (AL3*KOH3)/(HY*HY*HY*GH*GH*GH)       411
ALOH4 = (AL3*KOH4)/((HY**4.)*(GH**4.)*G1)    412
ALF = (AL3*FZ*GF*KF1)/G2                      413
ALF2 = (AL3*FZ*FZ*GF*GF*KF2)/G1              414
ALF3 = (AL3*FZ*FZ*FZ*GF*GF*GF*KF3)           415
ALF4 = (AL3*FZ*FZ*FZ*FZ*GF*GF*GF*GF*KF4)/G1 416
ALF5 = (AL3*FZ*FZ*FZ*FZ*FZ*GF*GF*GF*GF*GF*KF5)/G2 417
ALF6 = (AL3*(FZ**6.)*(GF**6.)*KF6)/G3        418
ALSO4 = (AL3*SO4*GSO4*KS1)/G1                 419
ALSO42 = (AL3*SO4*SO4*GSO4*GSO4*KS2)/G1      420
C RECALCULATES [F-]                           421
  IF (FI(IL) .EQ. 2.) THEN                     422
    FZM =FZ2/(1.+(AL3*GF*KF1/G2)+(H*GF/(10.**(-3.17)))) 423
    HF = H*GF*FZ/(10.**(-3.17))               424
    FZ = FZM                                   425
    FZM = FZM+HF+ALF+(2.*ALF2)+(3.*ALF3)+(4.*ALF4)+(5.*ALF5)+ 426
    * (6.*ALF6)                                427
    ELSE                                       428
      FZ = FZ                                  429
    END IF                                     430
65 TAL =AL3M+ALOH+ALOH2+ALOH3+ALOH4+ALF+ALF2+ALF3+ALF4+ALF5+ALF6+ 431
* ALSO4+ALSO42                                432
  ELSE                                       433
    CONTINUE                                  434
  END IF                                     435
C CALCULATES IONIC STRENGTH                   436
MU=.5*((CA*4.)+(MG*4.)+(CO3*4.)+SO4*4.+CAHCO3+MGHCO3+FZ+PO4Z*9.+ 437
* HCO3)                                       438
  IF (FER .GE. 1.) THEN                       439
    MU = MU+(FEZ*9.)                          440
  ELSE                                         441
    MU = MU+(FEZ*4.)                          442
  END IF                                       443
MU2=MU+0.5*(BRZ+NAZ+(MNZ*4.)+KZ+HY+OH+NO3Z+NH4Z+CLZ+ORG) 444
  IF (ALSP(IL) .EQ. 1. ) THEN                 445
    MU2 = MU2+(.05*(ALZ*9.))                  446
  ELSE                                         447
    MU2 = MU2+(.05*(AL3M*9.)+(ALOH*4.)+ALOH2+ALOH4+(ALF*4.))+ 448
    * ALF2+ALF4+(ALF5*4.)+(ALF6*9.)+ALSO4+ALSO42) 449
  END IF                                       450
C CHECKS FOR CONVERGENCE OF SULFATE VALUES 451
  IF (SO4.GE.TSO4Z) THEN                      452
    GO TO 64                                   453

```

Attachment C. Source code-- continued

```

ELSE
MSO4 = TSO4Z - CASO4 - MGSO4-ALSO4-(2.*ALSO42)
END IF
IF(ABS((MSO4-SO4)/(MSO4+SO4)) .LE. .001) THEN
GO TO 64
ELSE
SO4 = ((MSO4 - SO4)/2.)+ SO4
C.....DEBYE-HUCKEL EQUATION USED TO COMPUTE ACTIVITY COEFFICIENTS.
C AN EXTENDED FORM OF THE DEBYE-HUCKEL EQUATION, GOOD FOR MU <
C .1 (STUMM AND MORGAN) IS USED:
C LOGF = -A*(Z**2)*(MU**.5)/(1.+B*a*(MU**.5))
C A AND B ARE COMPUTED ACCORDING TO CHANGES WITH TEMPERATURE.
MUF = MU2**.5
Z= (-A*(MUF))/(1.0+((9.0E+8)*B*(MUF)))
GH = 10.**Z
GOH = 10.**((-A*(MUF))/(1.0+(3.5E+8)*B*(MUF)))
GCA = 10.**((-A*4.*(MUF))/(1.0+(6.0E+8)*B*(MUF)))
GMG = 10.**((-A*4.*(MUF))/(1.0+(8.0E+8)*B*(MUF)))
GCAHCO3 = 10.**((-A*(MUF))/(1.0+(4.25E+8)*B*(MUF)))
GMGHCO3=GCAHCO3
GCO3 = 10.**((-A*4.*(MUF))/(1.0+(4.5E+8)*B*(MUF)))
GSO4 = 10.**((-A*4.*(MUF))/(1.0+(4.25E+8)*B*(MUF)))
GHCO3 = GCAHCO3
GAL = 10.**((-A*9.*(MUF))/(1.0+(9.0E+8)*B*(MUF)))
GMN = GCA
GPO4 = 10.**((-A*9.*(MUF))/(1.0+(4.25E+8)*B*(MUF)))
IF (FER .GE. 1.) THEN
GFE = GPO4
ELSE
GFE = GCA
END IF
GNA = GHCO3
GF = GOH
GK = 10.**((-A*(MUF))/(1.0+(3.0E+8)*B*(MUF)))
GCL = GK
GBR = GK
GNO3 = GK
GNH4 = 10.**(-A*(MUF)/(1.0+(2.5E+8)*B*(MUF)))
C CALCULATES HCO3 FROM ALKALINITY EQUATION
IF (ALSP(IL) .EQ. 1.) THEN
HCO3 = ALKZ-(2.*CO3)+HY-ORG-(3.*PO4Z)-OH+(3.*ALZ)
ELSE
HCO3 = ALKZ-(2.*CO3) + HY-ORG-(3.*PO4Z)-OH+(3.*AL3M)+
* (2.*(ALOH))+ALOH2)-ALOH4+(3.*ALF)+(3.*ALF2)+(3.*ALF3)+
* (3.*ALF4)+(3.*ALF5)+(3.*ALF6)+(3.*ALSO4)+(3.*ALSO42)

```

Attachment C. Source code-- continued.

```

        END IF
        H2CO3 = GH*HY*GHCO3*HCO3/K10
        GO TO 63
    END IF
C
64  CALCULATES ALKALINITY USING ALTERNATIVE METHOD Cb-Ca.
    NEWALK =(2.*CA)+(2.*MG)+NAZ+KZ+NH4Z-(NO3Z+(2.*SO4)+FZ+CLZ)
    IF (ALSP(IL) .EQ. 1.) THEN
        HCO3 = ALKZ-(2.*CO3)+HY-ORG-(3.*PO4Z)-OH+(3.*ALZ)
    ELSE
        HCO3 = ALKZ-(2.*CO3) + HY-ORG-(3.*PO4Z)-OH+(3.*AL3M)+
*           (2.*(ALOH))+ (ALOH2)-ALOH4
    END IF
    SO4 = MSO4
C
C*****END OF LOOP TO CALCULATE IONIC STRENGTH AND CARBONATE SPECIES.
C
C.....CALCULATION OF SPECIFIC CONDUCTANCE USING METHOD OF
C.....R.C. REYNOLDS (1978).
    SCCA=CA*2.*(59.5-(59.5*.634*2.*MUF))
    SCMG=MG*2.*(53.06-(53.06*.634*2.*MUF))
    SCH=HY*(349.82-(349.82*.634*MUF))
    SCNA=NAZ*(50.11-(50.11*.634*MUF))
    SCK =KZ*(73.52-(73.52*.634*MUF))
    SCCAICO3=CAHCO3*(45.-(45*.634*MUF))
    SCMGHCO3=MGHCO3*(45.-(45*.634*MUF))
    SCCO3=CO3*2.*(97.-(97*.634*2.*MUF))
    SCHCO3=HCO3*(44.48-(44.48*.634*MUF))
    SCOH=OH*(198-(198*.634*MUF))
    SCCL=CLZ*(76.34-(76.34*.634*MUF))
    SCSO4=SO4*2.*(79.8-(79.8*.634*2.*MUF))
    SCNH4=NH4Z*(73.4-(73.4*.634*MUF))
    SCNO3Z=NO3Z*(71.44-(71.44*.634*MUF))
    SCBR=BRZ*(78.4-(78.4*.634*MUF))
    SC25 = 1000.*(SCCA+SCMG+SCH+SCNA+SCK+SCCAHCO3+SCMGHCO3+SCBR)
    SC25T = SC25 +(1000.*(SCCO3+SCHCO3+SCOH+SCCL+SCSO4+SCNH4+SCNO3))
C.....FOR SOME SC METERS, THE FOLLOWING TEMPERATURE CORRECTION MAY BE
C      NEEDED.
C      SC25T = SC25T/(EXP(0.02*(25-CTEMP2)))
    SCDIF = ((ABS(SC25T-SCLAB(IL)))/(SC25T+SCLAB(IL)))*100.
C.....E2 PARAMETERS ARE UEQ/L (USED FOR GRAPHING)
    EF = 10.**6.
    CAE2 = CAE*EF
    MGE2 = MGE*EF
    NAE2 = NAZ*EF
    KE2 = KZ*EF
    NH4E2 = NH4Z*EF

```

Attachment C. Source code-- continued.

ALE2 = ALE*EF	545
MNE2 = MNE*EF	546
FEE2 = FEE*EF	547
PO4E2 = PO4E*EF	548
SO4E2 = SO4E*EF	549
BRE2 = BRZ*EF	550
IF (FI(IL) .EQ. 2.) THEN	551
FE2 = FZ2*EF	552
ELSE	553
FE2 = FZ*EF	554
END IF	555
CLE2 = CLZ*EF	556
NO3E2 = NO3Z*EF	557
C.....CALCULATES ACTIVITIES	558
ACA = CA*GCA	559
AMG = MG*GMG	560
ASO4 = SO4*GSO4	561
ANO3 = NO3Z*GNO3	562
ANH4 = NH4Z*GNH4	563
ANA = NAZ*GNA	564
AK = KZ*GK	565
ACL = CLZ*GCL	566
ABR = BRZ*GBR	567
AF = FZ*GF	568
APO4 = PO4Z*GPO4	569
AFE = FEZ*GFE	570
AMN = MNZ*GMN	571
AAL = AL3M*GAL	572
ACO3 = CO3*GCO3	573
AHCO3 = HCO3*GHCO3	574
AOH = GOH*OH	575
C.....CALCULATES ION RATIOS	576
RNA = NAZ/CLZ	577
RCA = TCAZ/CLZ	578
RMG = TMGZ/CLZ	579
RK = KZ/CLZ	580
RAL = ALZ/CLZ	581
RSO4 = TSO4Z/CLZ	582
IF (TSO4Z .NE. 0.0 .AND. NO3Z .NE. 0.0) THEN	583
RSO4NO3 = TSO4Z/NO3Z	584
RHNO3 = H/NO3Z	585
RHSN = H/(TSO4Z+NO3Z)	586
ELSE RHNO3 = 0.0	587
END IF	588
IF (TSO4Z .NE. 0.0) THEN	589
RHSO4 = H/TSO4Z	590

Attachment C. Source code-- continued.

```

END IF 591
R2CA = CA/CLZ 592
R2MG = MG/CLZ 593
R2SO4 = SO4/CLZ 594
R2AL = AL3M/CLZ 595
IF (AL(IL) .NE. 0. .AND. AL3 .NE. 0.) THEN 596
  LRAL =(LOG10(AL3))/(LOG10(H)) 597
END IF 598
C.....CALCULATES SATURATION INDEX FOR BASIC ALUMINUM SULFATE 599
ALSULF = (AL3*AOH*ASO4)/(5.89E-18) 600
C.....CALCULATES ION BALANCE FROM COMPUTED DATA, USING ORG. ANION AND 601
C.....CARBONATE SPECIES. 602
IF (ALSP(IL) .EQ. 2.) THEN 603
  CAT =(CA*2.)+(MG*2.)+HY+(NAZ)+(NH4Z)+ 604
* (KZ)+ 605
* (CAHCO3)+ 606
* (MGHCO3)+((MNZ*2.))+ 607
* (AL3M*3.)+(2.*ALOH) + (ALOH2) 608
  IF (FER .GE. 1.) THEN 609
    CAT = CAT+(FEZ*3.) 610
  ELSE 611
    CAT = CAT+(FEZ*2.) 612
  END IF 613
  AN =(CO3*2.)+(HCO3)+(OH)+(SO4*2.)+(PO4Z*3.) 614
* +(FZ)+(BRZ)+(NO3Z)+ORG+(CLZ)+ALOH4 615
  CATAN =((ABS(CAT-AN))/(CAT+AN))*100. 616
  ELSE 617
  CAT =(CA*2.)+(MG*2.)+HY+(NAZ)+(NH4Z)+ 618
* (KZ)+(CAHCO3)+(MGHCO3)+((MNZ*2.))+ (ALZ*3.) 619
  IF (FER .GE. 1.) THEN 620
    CAT = CAT+(FEZ*3.) 621
  ELSE 622
    CAT = CAT+(FEZ*2.) 623
  END IF 624
  AN =(CO3*2.)+(HCO3)+(OH)+(SO4*2.)+(PO4Z*3.)+ 625
* (FZ)+(BRZ)+(NO3Z)+ORG+(CLZ) 626
  CATAN =((ABS(CAT-AN))/(CAT+AN))*100. 627
  END IF 628
C.....CALCULATES ION BALANCE FROM ANALYTICAL DATA, USING ORG. ANION, AND 629
C BICARBONATE 630
CAT2=(TCAZ*2.)+(TMGZ*2.)+H+NAZ+KZ+(FEZ*3.)+(MNZ*2.)+ALZ*3.+NH4Z 631
AN2=OH+(TSO4Z*2.)+(PO4Z*3.)+FZ+BRZ+NO3Z+CLZ+ORG+ALK1(IL) 632
IF (ALK1(IL) .LE. 0. ) THEN 633
  AN2 = AN2 - ALK1(IL) 634
  ELSE 635
  AN2 = AN2 636

```



Attachment C. Source code-- continued.

```

END IF 637
CATAN2 = ((ABS(CAT2-AN2))/(CAT2+AN2))*100. 638
C 639
C.....WRITES OUTPUT FOR CREATING BAR GRAPHS 640
C.....OF UEQ/L FOR EACH CONSTITUENT. 641
C 642
C WRITE (62,130)SITE(IL),DATE(IL) 643
C WRITE (62,131) HE2,NAE2,CAE2,MGE2,KE2,NH4E2 644
C WRITE (62,132) 645
C WRITE (62,133) ALE2,MNE2,FEE2 646
C WRITE (62,132) 647
C WRITE (62,134) OHE2,NO3E2,PO4E2,ORGE2,SO4E2,CLE2,BRE2,FE2 648
C 649
C.....GENERATES OUTPUT TO SCREEN AND OUTPUT FILE 650
C 651
IF (LFI(IL) .EQ. 2.) THEN 652
WRITE(61,7) 653
ELSE 654
WRITE(61,8) 655
END IF 656
WRITE (61,9) 657
WRITE (61,10) HY,HY,H,GH 658
WRITE(61,11) TCA(IL),TCAZ,CAE,ACA,GCA,AZ2(IL) 659
WRITE (61,12) TMG(IL),TMGZ,MGE,AMG,GMG,AZ3(IL) 660
WRITE (61,13) NA(IL),NAZ,NAZ,ANA,GNA,AZ5(IL) 661
WRITE(61,14) K(IL),KZ,KZ,AK,GK,AZ6(IL) 662
WRITE(61,15) NH4(IL),NH4Z,NH4Z,ANH4,GNH4,AZ8(IL) 663
WRITE(61,16) CL(IL),CLZ,CLZ,ACL,GCL,AZ9(IL) 664
IF (FI(IL) .EQ. 2.) THEN 665
WRITE (61,17) F(IL),FZ2,FZ2,AF,GF,AZ10(IL) 666
ELSE 667
WRITE (61,18) F(IL),FZ,FZ,AF,GF,AZ10(IL) 668
END IF 669
WRITE(61,19) BR(IL),BRZ,BRZ,ABR,GBR,AZ11(IL) 670
WRITE (61,20) TSO4(IL),TSO4Z,SO4E,ASO4,GSO4,AZ12(IL) 671
WRITE (61,21) NO3(IL),NO3Z,NO3Z,ANO3,GNO3,AZ13(IL) 672
WRITE (61,22) PO4(IL),PO4Z,PO4E,APO4,GPO4,AZ14(IL) 673
WRITE (61,23) ALK1(IL),ALKZ,AZ15(IL) 674
WRITE (61,24) DOC(IL),AZ16(IL) 675
WRITE (61,25) DO(IL),AZ17(IL) 676
WRITE(61,26) 677
WRITE (61,27) AL(IL),ALZ,ALE,AAL,GAL,AZ1(IL) 678
WRITE (61,28) MN(IL),MNZ,MNE,AMN,GMN,AZ4(IL) 679
WRITE (61,29) FE(IL),FEZ,FEE,AFE,GFE,AZ7(IL) 680
IF (DO(IL) .EQ. 0.) THEN 681
WRITE (61,30) 682

```

## Attachment C. Source code-- continued.

```

FER = 0. 683
ELSE IF (FER .GE. 1.) THEN 684
WRITE(61,31) 685
ELSE 686
WRITE(61,32) 687
END IF 688
WRITE (61,33) 689
WRITE (61,34) CA,MG,SO4 690
IF (FI(IL) .EQ. 2.) THEN 691
WRITE (61,35) FZ,HF 692
ELSE 693
CONTINUE 694
END IF 695
WRITE (61,36) OH,CASO4,MGSO4 696
WRITE (61,37) CAHCO3,MGHCO3 697
WRITE (61,38) CO3,HCO3,H2CO3,CACO3,MGCO3 698
WRITE (61,39) AL3M,ALOH,ALOH2,ALOH3,ALOH4 699
WRITE (61,40) ALF,ALF2,ALF3,ALF4,ALF5,ALF6,ALSO4,ALSO42 700
WRITE (61,41) RNA,RCA,RMG,RK,RAL,RSO4,RSO4NO3,RHSO4,RHNO3, 701
* RHSN 702
WRITE (61,42) R2CA,R2MG,R2SO4,R2AL 703
WRITE (61,43) FER,PE 704
WRITE (61,44) LRAL 705
WRITE (61,45) TAL,ALSULF 706
WRITE (61,46) ORG 707
WRITE (61,47)ALKZ,NEWALK 708
WRITE (61,48) MU2 709
WRITE (61,49) TDSRAT 710
WRITE(61,50)CAT2,AN2 711
WRITE(61,51)CATAN2 712
IF (CATAN2 .GE. 10.) THEN 713
WRITE (61,52) 714
ELSE IF (CATAN2 .LE. 10. .AND. CATAN2 .GE. 5.) THEN 715
WRITE (61,53) 716
END IF 717
WRITE (61,54)CAT,AN 718
WRITE(61,55)CATAN 719
WRITE (61,56) SC25T 720
WRITE (61,57)SCDIF 721
IF (SCDIF .GE. 10.) THEN 722
WRITE (61,58) 723
ELSE IF (SCDIF .LE. 10. .AND. SCDIF .GE. 5.) THEN 724
WRITE (61,59) 725
END IF 726
500 CONTINUE 727
800 FORMAT (G10.4E2) 728

```

## Attachment C. Source code-- continued.

```

66  FORMAT (G10.4E2,G10.4E2,G10.4E2)          729
600  FORMAT (G10.4E2,G10.4E2)                730
C 130  FORMAT (A15,A15,'$',/, '0.0')        731
C 131  FORMAT (5(F7.2),/)                   732
C 132  FORMAT ('0.0',/)                     733
C 133  FORMAT (3(F7.2,/))                   734
C 134  FORMAT (7(F7.2,/))                   735
      1  FORMAT ('1',98('*'),//, ' SITE ID = ',A15,3X, 'DATE: ',A12,/,
      * ' DATE RUN ON ARCHEM.F77: ',A12,/)    736
      2  FORMAT(1X, 'PHFLD= ',F6.3,5X, ' TEMP= ',F6.3,5X, ' SCFLD= ',F7.3) 738
      3  FORMAT(1X, 'PHLAB= ',F6.3,5X, ' TEMP= ',F6.3,5X, ' SCLAB= ',F7.3,/) 739
      4  FORMAT ('***WARNING: THIS PROGRAM SHOULD ONLY BE USED FOR',/,
      * 'SAMPLES WITH PH LESS THAN 10.0***') 741
      5  FORMAT ('***WARNING: THIS PROGRAM SHOULD ONLY BE USED FOR',/,
      * 'TEMPERATURES IN THE RANGE OF 0.1 TO 100 DEGREES CENTIGRADE***') 743
      6  FORMAT(' RATIO OF H+ ACTIVITY FIELD TO H+ ACTIVITY LAB= ',
      * G10.4E2,/, ' RATIO OF SC FIELD TO SC LAB= ',F5.2,/) 745
      7  FORMAT (' FIELD DATA WERE USED',/,98('_'),/,/) 746
      8  FORMAT (' LAB DATA WERE USED',/,98('_'),/,/) 747
      9  FORMAT (1X, 'INPUT PARAMETERS',47X, 'CALCULATED PARAMETERS',
      * /,/,10X, 'MG/L ',9X, 'MOLARITY',
      * 7X, 'EQ/L ',20X, 'ACTIVITY',7X, 'GAMMA',9X, '1.=<') 750
     10  FORMAT (1X, 'H= ',20X,G10.4E2,5X,G10.4E2,15X,G10.4E2,5X,G10.4E2) 751
     11  FORMAT (' CA= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 752
     12  FORMAT (' MG= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 753
     13  FORMAT (' NA= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 754
     14  FORMAT (' K= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 755
     15  FORMAT (' NH4= ',4X,G10.4E2,2(5X,G10.4E2),10X,2(5X,G10.4E2),
      * 6X,F2.0) 757
     16  FORMAT (' CL= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 758
     17  FORMAT (' F= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 759
     18  FORMAT (' F= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 760
     19  FORMAT (' BR= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 761
     20  FORMAT (' SO4= ',4X,G10.4E2,2(5X,G10.4E2),10X,2(5X,G10.4E2),
      * 6X,F2.0) 763
     21  FORMAT (' NO3= ',4X,G10.4E2,2(5X,G10.4E2),10X,2(5X,G10.4E2),
      * 6X,F2.0) 765
     22  FORMAT (' PO4= ',4X,G10.4E2,2(5X,G10.4E2),10X,2(5X,G10.4E2),
      * 6X,F2.0) 767
     23  FORMAT (' ALK= ',4X,15X,G10.4E2,5X,G10.4E2,46X,F2.0) 768
     24  FORMAT (' DOC= ',4X,G10.4E2,76X,F2.0) 769
     25  FORMAT (' DO= ',5X,G10.4E2,76X,F2.0,/) 770
     26  FORMAT (10X, 'UG/L ',9X, 'MOLARITY',7X, 'EQ/L ',20X,
      * 'ACTIVITY',7X, 'GAMMA',9X, '1.=<') 772
     27  FORMAT (' AL= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 773
     28  FORMAT (' MN= ',3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0) 774

```

## Attachment C. Source code-- continued.

```
29 FORMAT (' FE=' ,3(5X,G10.4E2),10X,2(5X,G10.4E2),6X,F2.0,/, 775
* 98(' _'),/,) 776
30 FORMAT (/,' ALL FE ASSIGNED TO +3 VALENCE AND RATIO FE+3/FE+2'/, 777
* ' SET EQUAL TO 1 (SEE BELOW) AS INPUT VALUE OF DOX WAS 0.' ,/) 778
31 FORMAT (/,' ALL FE ]ASSIGNED TO +3 VALENCE AS FE+3/FE+2 RATIO' ,/, 779
* ' COMPUTED BELOW IS GREATER THAN 1.' ,/) 780
32 FORMAT (/,' ALL FE ASSIGNED TO +2 VALENCE AS FE+3/FE+2 RATIO' ,/, 781
* ' COMPUTED BELOW IS LESS THAN 1.' ,/) 782
33 FORMAT(1X,70(' _'),/,1X,'MOLARITIES CALCULATED' ,/ 783
* ' FROM EQUILIBRIUM SPECIATION EQUATIONS' ,/) 784
34 FORMAT (' CA= ',8X,G10.4E2,/, ' MG= ',8X,G10.4E2,/, ' SO4= ',7X, 785
* G10.4E2) 786
35 FORMAT (' F= ',9X,G10.4E2,/, ' HF= ',8X,G10.4E2) 787
36 FORMAT (' OH= ',8X,G10.4E2,/,/, ' SULFATE SPECIES' ,/,/' CASO4= ', 788
* 5X,G10.4E2,/, ' MGSO4= ',5X,G10.4E2) 789
37 FORMAT (/,' CARBONATE SPECIES' ,/,/' CAHCO3= ',4X,G10.4E2, 790
* /' MGHCO3= ',4X,G10.4E2) 791
38 FORMAT (' CO3= ',7X,G10.4E2,3X, 792
* /' HCO3= ',6X,G10.4E2,/,1X,'H2CO3= ',5X,G10.4E2,/, 793
* ' CACO3= ',5X,G10.4E2,/, ' MGCO3= ',5X,G10.4E2) 794
39 FORMAT (/,' ALUMINUM SPECIES' ,/,/, 795
* ' AL3+= ',6X,G10.4E2,/' ALOH= ',6X,G10.4E2,/' ALOH2= ',5X,G10.4E2, 796
* /,' ALOH3= ',5X,G10.4E2,/, ' ALOH4= ',5X,G10.4E2) 797
40 FORMAT (' ALF= ',7X,G10.4E2,/' ALF2= ',6X,G10.4E2,/' ALF3= ',6X, 798
* G10.4E2, 799
* /' ALF4= ',6X,G10.4E2,/' ALF5= ',6X,G10.4E2,/' ALF6= ',6X, 800
* G10.4E2,/, ' ALSO4= ',5X,G10.4E2,/' ALSO42= ',4X,G10.4E2) 801
41 FORMAT(/,1X,70(' _'),/,/' ION RATIOS FROM ANALYTICAL MOLARITIES=' , 802
* 1X,/, ' NA/CL= ',G10.4E2,/, ' CA/CL= ',G10.4E2,/, ' MG/CL= ', 803
* G10.4E2,/, ' K/CL= ',G10.4E2,/, ' AL/CL= ',G10.4E2,/, ' SO4/CL= ', 804
* G10.4E2,/, ' CA/MG= ',G10.4E2,/, ' SO4/NO3= ',G10.4E2,/, 805
* ' H/SO4= ',G10.4E2,/, ' H/NO3= ',G10.4E2,/, ' H/(SO4+NO3)= ', 806
* G10.4E2,/) 807
42 FORMAT (/,' ION RATIOS FROM COMPUTED MOLARITIES' ,/, ' CA/CL= ', 808
* G10.4E2,/, ' MG/CL= ',G10.4E2,/, ' SO4/CL= ',G10.4E2,/, ' AL/CL= ', 809
* G10.4E2,/) 810
43 FORMAT (/,' FE+3/FE+2= ',5X,G10.4E2,/, ' PE=' , 811
* 5X,G10.4E2,/) 812
44 FORMAT (' RATIO (LOG ACTIVITY AL3+)/(LOG ACTIVITY OF H+)= ', 813
* G10.4E2,/,1X,70(' _'),/) 814
45 FORMAT (/,' RECALCULATED TOTAL ALUMINUM, MOLES/L = ',G10.4E2, 815
* /,' SATURATION INDEX FOR BASIC ALUMINUM SULFATE= ',G10.4E2) 816
46 FORMAT (/,' ORGANIC ANION CONC, EQ/L = ',G10.4E2,/) 817
47 FORMAT (' MEASURED ALKALINITY, EQ/L = ',G10.4E2,/, 818
* ' NEWALK, ALKALINITY CALCULATED FROM Cb-Ca= ',G10.4E2,/) 819
48 FORMAT (' IONIC STRENGTH= ',G10.4E2,/) 820
```

Attachment C. Source code-- continued.

49	FORMAT(' RATIO TDS TO SC (GENERALLY .55 TO .75. USE WITH CAUTION	821
	* FOR VERY LOW I.S. SAMPLES)= ',2X,G10.4E2,/')	822
50	FORMAT(' SUM CATION EQ/L = ',G10.4E2,/' SUM ANION EQ/L = ',	823
	* G10.4E2)	824
51	FORMAT (' ANALYTICAL PERCENT DIFFERENCE IN CATIONS VS ANIONS= ',	825
	* F7.3,/')	826
52	FORMAT (' *** FAILS IONBAL AT 10% ***',/')	827
53	FORMAT (' *** FAILS IONBAL AT 5% ***',/')	828
54	FORMAT (' SUM OF CATIONS= ',G10.4E2,/' SUM OF ANIONS= ',	829
	* G10.4E2)	830
55	FORMAT (' COMPUTED PERCENT DIFFERENCE IN CATIONS VS ANIONS= ',	831
	* F7.3,/,/')	832
56	FORMAT (' PREDICTED SC =',F8.3)	833
57	FORMAT(' PERCENT DIFFERENCE IN SC MEASURED VS PREDICTED= ',F7.3)	834
58	FORMAT (/,' *** FAILS SC TEST AT 10% ***',/')	835
59	FORMAT (/,' *** FAILS SC TEST AT 5% ***',/')	836
C 65	FORMAT (/,' H/SC= ',G10.4E2,/, ' H/SCDIF= ',G10.4E2,/,	837
C	* ' ORG/H= ',G10.4E2,/, ' ORG/SCDIF= ',G10.4E2,/, ' ORG/SC= ',	838
C	* G10.4E2,/) GO TO 62	839
		840
60	WRITE (*,61)	841
61	FORMAT (' ERROR')	842
62	STOP	843
	END	844