

SOLMINEQ.88: A COMPUTER PROGRAM FOR GEOCHEMICAL
MODELING OF WATER-ROCK INTERACTIONS

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PREFACE

This report describes the theoretical aspects, the modeling capabilities and the limitations of the geochemical computer code SOLMINEQ.88. This code is the latest version of SOLMNEQ (Kharaka and Barnes, 1973), SOLMNEQF (Aggarwal and others, 1986), and several unpublished versions of this software package. The computer program can be used to model speciation, saturation, dissolution/precipitation, ion exchange/adsorption, mixing, boiling, and gas partitioning between water, oil, and gas phases. The program is comprehensive but it is especially useful for modeling water-rock interactions in sedimentary basins where high temperatures, pressures, salinities, and dissolved organic species prevail.

The user is requested to kindly notify the originating office of any errors found in this report or in the computer program. Updates may occasionally be made to both the report and the program. Users who wish to receive a copy of the computer program and report may send a request to the following addresses:

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CONVERSION FACTORS

Metric (International System) units are used in this report. For those readers who prefer to use inch-pound units, conversion factors for the terms used in this report are listed below:

<u>Multiply metric unit</u>	<u>by</u>	<u>To obtain inch-pound unit</u>
micrometer (μm)	0.03937	mil
centimeter	0.3937	inch
meter (m)	3.281	foot (ft)
square centimeter (cm^2)	0.1550	square inch (in^2)
cubic centimeter (cm^3)	0.06102	cubic inch (in^3)
cubic meter (m^3)	35.31	cubic feet (ft^3)
liter (l)	0.03531	cubic feet (ft^3)
microgram (μg)	1.543×10^{-5}	grain (gr)
milligram (mg)	1.543×10^{-2}	grain (gr)
gram (g)	2.205×10^{-3}	pound (lb)
kilogram (kg)	2.205	pound (lb)
milligram/liter (mg/l)	6.243×10^{-5}	pound/cubic foot (lb/ft^3)
atmosphere (atm)	14.70	pounds per square inch (psi)
bar	14.50	pounds per square inch (psi)
kilopascal (kPa)	0.1450	pounds per square inch (psi)
degree Celcius ($^{\circ}\text{C}$)	$1.8^{\circ}\text{C} + 32$	degree Fahrenheit ($^{\circ}\text{F}$)
degree Kelvin (K)	$(\text{K} - 273.15)1.8 + 32$	degree Fahrenheit ($^{\circ}\text{F}$)
calorie (cal)	3.968×10^{-3}	British thermal unit (Btu)
kilocalorie (kcal)	3.968	British thermal unit (Btu)

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ABSTRACT

Geochemical modeling based on equilibrium and irreversible thermodynamics has, in the last 20 years, become a well recognized tool for understanding the processes of water-rock interactions and predicting their consequences. SOLMINEQ.88 is the latest version of the 1973-computer program code SOLMNEQ and its various updated versions. This program is general and comprehensive, but is particularly useful for modeling geochemical interactions in sedimentary basins and petroleum reservoirs where petroleum, aqueous organic species, and subsurface pressure play an important role.

SOLMINEQ.88 is written in FORTRAN-77 and has an improved algorithm over that in previous versions for faster execution. This version has a revised thermodynamic database, more inorganic (260) and organic (80) aqueous species and minerals (220), computes the activity coefficients in brines using Pitzer equations, and computes pH and mineral solubilities at subsurface temperatures (0° to 350° C) and pressures (1 to 1,000 bars). New modeling options in SOLMINEQ.88 can be used to study the effects of boiling, mixing of solutions and partitioning of gases between water, oil and gas phases. SOLMINEQ.88 has several mass transfer options that can be used to predict the effects of ion exchange, adsorption/desorption, and dissolution/precipitation of solid phases. A user-friendly interactive code SOLINPUT is available for use to generate and update the input file for SOLMINEQ.88.

The numerous assumptions and limitations of geochemical models like SOLMINEQ.88 are described in detail because they indicate the range of conditions where the models can be used successfully. The limitations may be related to incomplete and/or unreliable chemical and mineral data as well as to uncertainties in equilibrium constants for aqueous species and minerals. The modeling capabilities and the limitations of the various options in this code are described with output from selected examples.

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INTRODUCTION

Water-rock interactions in natural systems comprise a combination of several physical and chemical processes, including (a) mineral dissolution and precipitation; (b) ion exchange and adsorption/desorption; (c) mixing of fluids; (d) gas separation by pressure-drawdown or boiling; and (e) organic/inorganic interactions. In the last 20 years, geochemical modeling based on equilibrium and irreversible thermodynamics has become a well recognized tool for understanding the processes of water-rock interaction and predicting their consequences. Numerous computer program codes are presently available for geochemical modeling of water-rock interactions (Nordstrom and others, 1979; Wolery, 1983; EPRI, 1984; Nordstrom and Munoz, 1985). The list of commonly used programs is large and expanding; it includes the following software packages:

1. PATHI and its modified versions (Helgeson and others, 1970; Perkins, 1980).
2. SOLMNEQ and its modified versions (Kharaka and Barnes, 1973; Aggarwal and others, 1986).
3. WATEQ and its modified versions (Truesdell and Jones, 1974; Plummer and others, 1984; Ball and others, 1987).
4. MINEQL (Westall and others, 1976).
5. EQ3/EQ6 (Wolery, 1979; 1983; 1984).
6. PHREEQE (Parkhurst and others, 1980).
7. GEOCHEM (Sposito and Mattigod, 1980).
8. SOLVEQ (Reed, 1982).
9. MINTEQ (Felmy and others, 1984).
10. DYNAMIX (Narasimhan and others, 1986)

The computer program code SOLMNEQ (Kharaka and Barnes, 1973) was originally written in PL/1 for the IBM 360 computers. The original program computed the equilibrium distribution of 162 inorganic aqueous species generally present in natural waters over the temperature range of 0° to 350 °C from the reported physical and chemical properties of the water and an internally consistent set of thermodynamic data. The program also computed the saturation states of 158 minerals commonly encountered in sedimentary rocks. SOLMNEQ has undergone continuous updating, additions and modifications. The additions and modifications were carried out to develop a general comprehensive computer program for geochemical modeling of water-rock interactions. This program, however, is particularly useful for modeling

interactions in sedimentary basins and in thermally stimulated oil reservoirs where petroleum and aqueous organic species play an important role.

The present version, renamed SOLMINEQ.88 (SOLution MINeral EQilibrium, 1988), is written in FORTRAN-77 and has an improved algorithm for faster execution. This version has a revised thermodynamic data base, more inorganic (260) and organic (80) aqueous species and minerals (220), and computes pH and mineral solubilities at subsurface temperatures and pressures. New modeling options have been added to SOLMINEQ.88 that can be used to study the effects of boiling, mixing of solutions, and partitioning of gases between water, oil and gas phases. SOLMINEQ.88 has mass-transfer capabilities that can be used to study the effects of ion exchange, adsorption/desorption, and dissolution/precipitation of solid phases.

This report documents the modeling capabilities of the computer code SOLMINEQ.88. It is intended as a user's guide, describing the assumptions underlying the various options and summarizing the mathematical and numerical techniques used. The thermochemical and other data used in the computations are tabulated. The fixed and optional data used to create the input file are described in detail. An interactive input program, SOLINPUT, is available to create or modify the input file. Output from several examples has been included to illustrate various applications of this code, and for comparison by users on other computer systems to verify that the program is functioning correctly.

Acknowledgments

This code has been greatly improved because of suggestions and corrections from many users including Bob Mariner, Randy Bassett, Jim Bishoff, Sheldon Sommer, Indu Mishri, Brian Hitchon, Gordon Bird, and several scientists at Alberta Research Council, and many students at the U.S. Geological Training Center in Denver, Colorado.

Dan Specht, Bob Hull, Ming Ko, and Pat Dorherty have made important contributions to the code. We are grateful for thorough reviews of this document by our colleagues Bob Mariner, Charly Alpers, Rich Wanty and Art White. Special thanks are due Jackie Hamilton for the many typings of this bulky report.

Table 1.

Glossary of Symbols Used in Text

a	Sum of the Goldschmidt radii
a	Stands for anion when used as a subscript
a, b, c, W, θ	Temperature-independent constants in eqn. 48
a_i	Activity of species i
$a_1, a_2, a_3, a_4, \theta, w, Q$	Constants used in eqn. 55
\bar{a}_i	Activity of species i at equilibrium
a_i^o	Ion size parameter of species i
A, B, C	Fitted pressure constants see appendix 1
A, B, C	Meyer-Kelley heat capacity temperature fit constants.
A	Chemical affinity
A_T	Total area of the exchanging surface per kg of water
A_γ	Debye-Hückel limiting law slope.
A^ϕ	Adjusted Debye-Hückel constant used in Pitzer eqn.
AP	Ion activity product
B_γ	Extended Debye-Hückel limiting law constant.
B^\bullet, B_u^*, B_m^*	Activity coefficient deviation functions subscripts for univalent and multivalent species.
B_{MX}, B'_{MX}	Cation-anion interaction coefficients in pitzer eqns.
c	Represents a cation when used as a subscript.
$C_{li}, C_{2i}, w_i, \theta_i$	Empirical constants in eqn. 47
C_p	Isobaric heat capacity
$\Delta C_{p,r}^o$	Standard state isobaric heat capacity of reaction
C_{MX}	Cation-anion interaction coefficient in pitzer eqns.
C_{MX}^ϕ	Cation-anion interaction parameter in pitzer eqns.
e	Electron charge, 1.602×10^{-19} coulomb
E	Equivalent fraction of surface sites occupied by a specific surface complex
E^o	Standard state potential

E_h	Oxidation potential referred to hydrogen half cell
$E_{\theta_{ij}}(I), E_{\theta'_{ij}}(I)$	Electrostatic effect of unsymmetrical unmixing used in Pitzer equations
F	Faraday constant, 9.648×10^4 coulomb mol ⁻¹
F	General Debye-Hückel interaction term used in Pitzer eqns.
$g(x), g'(x)$	Fitting functions used in Pitzer equations
ΔG_r°	Standard state Gibbs free energy of reaction
ΔG_{diff}	Gibbs free energy difference between the actual and equilibrium states of a mineral
ΔH_f°	Standard state enthalpy of formation
ΔH_r°	Standard state enthalpy of reaction
I	Ionic strength
k	Henry's Law coefficient in pure water
k_m	Henry's Law coefficient in a solution of molality m
K_i	Equilibrium constant of species i
ℓ	Refers to a liquid when used as a subscript or superscript
L	Number of ligands in eqns. 51 & 52
m_i	Molality of species i
$m_{i,t}$	Total analytical molality of component i
M	Represents positively charged species as a subscript
$M_{i,t}$	Total moles of substance i
N_A	Avogadro's number, 6.022×10^{23} mol ⁻¹
N_S	Number of sites per unit area of the mineral surface
N_a, N_c	Total number of the subscripted species
n	Number of electrons involved in redox reactions
$n_{i,j}$	Stoichiometric coefficient of component i in species j
p	Polarizability in eqn. 51
P	Pressure in bars
Q	Reaction quotient
R	Gas constant, 1.987 cal K ⁻¹ mol ⁻¹

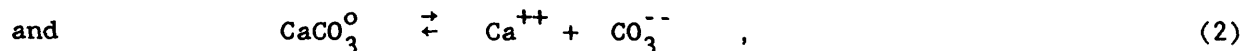
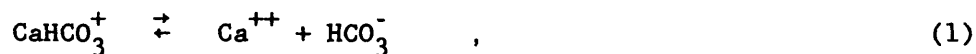
ΔS_r^o	Standard state entropy of reaction
SI	Saturation index
t	Temperature in degrees C
T	Temperature in degrees K
T_r	Reference temperature in degrees K
v	Refers to a vapor as a subscript or superscript
\bar{V}_i	Partial molal volume of aqueous species i
\bar{V}_i^v	Specific volume of gas i
ΔV_r^o	Standard state volume of reaction
W	Weight of a substance
x	Derivative of the variation of ϵ
X	Represents negatively charged ions when used as a subscript
Y_i	Tolerance factor for subscripted ion
z_i	Charge on species i
Z	Pitzer eqn. charge sum
Z	Compressibility factor
α	Charge fraction on surface sites
α_{MX}	Fitting parameter used in Pitzer equations
β	Coefficient of isothermal compressibility of water
$\beta_{MX}^{(0)}, \beta_{MX}^{(1)}, \beta_{MX}^{(2)}$	Pitzer cation-anion interaction parameters
γ_i	Activity coefficient of species i
$\gamma_{i,P}$	Activity coefficient of species i from Pitzer eqns.
ϵ	Dielectric constant of water
ϵ_o	Permittivity of the vacuum, 8.854×10^{-12} farad m^{-1}
θ_{ij}	Pitzer anion-anion/cation-cation interaction parameter
κ	Boltzman constant, 3.298×10^{-24} cal K^{-1}
ν_i	Number of moles of ions in component i
ρ	Density (g/cm^3)
σ_o, σ_d	Charge density at mineral surface (o) or diffuse layer (d)

ϕ_e	Osmotic coefficient of the subscripted electrolyte
$\Phi_{MM}, \Phi_{XX}, \Phi'_{MM}, \Phi'_{XX}$	Pitzer cation-cation/anion-anion interaction coefficients
χ	Fugacity coefficient
ψ	Surface potential
ψ_{ijk}	Pitzer cation-cation-anion/anion-anion-cation interaction parameters

METHOD OF COMPUTATION

The principal computations carried out by SOLMINEQ.88 are aqueous speciation and saturation states of minerals. This program computes the equilibrium distribution of more than 340 inorganic and organic aqueous species of major, minor and trace elements generally present in natural waters. The distribution of 54 organic species of acetate, oxalate, succinate and two user-defined (additional) organic anions has been included because organic species are important components of natural waters, especially those present in sedimentary basins (Carothers and Kharaka, 1978; Kharaka and others, 1986; MacGowan and Surdam, 1987; and many others). Although the total number of possible organic species is extremely large, the number of important anions in any given natural system in addition to acetate, oxalate and succinate is generally small (Kharaka and others, 1986; MacGowan and Surdam, 1987). Consequently, two additional user-defined organic anions together with their complexes with H^+ and 12 other cations usually are sufficient for modeling purposes. A user-defined cation together, with 13 complexes with anions, also was added to make the code of more general application.

The distribution of aqueous species for a given composition of water at specified pH and temperature (or temperatures) is computed using the same approach as in the original code (Kharaka and Barnes, 1973) by solving a set of mass-action, oxidation-reduction and mass-balance equations based on the ion-association aqueous model (Garrels and Christ, 1965; Helgeson, 1967). In this model, the dissociation reaction for each of the aqueous complexes (Table 2) has a corresponding mass-action equation. For example, the dissociation reactions for $CaHCO_3^+$ and $CaCO_3^0$ are



for which the respective mass-action equations are:

$$K_{CaHCO_3^+} = \frac{m_{Ca^{++}} \cdot \gamma_{Ca^{++}} \cdot m_{HCO_3^-} \cdot \gamma_{HCO_3^-}}{m_{CaHCO_3^+} \cdot \gamma_{CaHCO_3^+}} \quad , \quad (1)$$

$$K_{\text{CaCO}_3^0} = \frac{m_{\text{Ca}^{++}} \cdot \gamma_{\text{Ca}^{++}} \cdot m_{\text{CO}_3^{--}} \cdot \gamma_{\text{CO}_3^{--}}}{m_{\text{CaCO}_3^0} \cdot \gamma_{\text{CaCO}_3^0}}, \quad (2)$$

where m_i and γ_i are, respectively, the molality and activity coefficient of the subscripted species and K is the dissociation constant of the subscripted aqueous complex.

The mass-balance equations take the form:

$$m_{i,t} = \sum_{j=1}^j n_{i,j} m_j, \quad (3)$$

where $m_{i,t}$, $n_{i,j}$ and m_j are, respectively, the analytical (or total) molality of the component i , the stoichiometric coefficient of component i in species j , and the computed molality of species j . For a system of i components and j species, i mass-balance and $j-i$ mass-action equations can be written. With the additional constraints of specified pH and temperature, an iterative technique (see below) can be used to solve, simultaneously, the system of equations for the concentration of all species (Smith and Missin, 1982).

For aqueous species of Ca, for example, the mass-balance equation is

$$m_{\text{Ca},t} = m_{\text{Ca}^{++}} + m_{\text{CaHCO}_3^+} + m_{\text{CaCO}_3^0} + \dots \quad (4)$$

The mass-action and mass-balance equations are combined and rearranged after the activity coefficients have been computed (see below) to give the value of $m_{\text{Ca}^{++}}$ from the following:

$$m_{\text{Ca}^{++}} = \frac{m_{\text{Ca},t}}{1 + \gamma_{\text{Ca}^{++}} \cdot \Omega}, \quad (5)$$

$$\text{where } \Omega = \frac{m_{\text{HCO}_3^-} \cdot \gamma_{\text{HCO}_3^-}}{K_{\text{CaHCO}_3^+} \cdot \gamma_{\text{CaHCO}_3^+}} + \frac{m_{\text{CO}_3^{--}} \cdot \gamma_{\text{CO}_3^{--}}}{K_{\text{CaCO}_3^0} \cdot \gamma_{\text{CaCO}_3^0}} + \dots$$

$m_{\text{CaHCO}_3^+}$ and $m_{\text{CaCO}_3^0}$ are then computed from equations (1) and (2),

respectively, after substituting the computed $m_{\text{Ca}^{++}}$.

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data (see references at end of Table 3)

ID # and Name	Reaction	References
1 HCO_3^-	$\text{HCO}_3^- \rightleftharpoons \text{H}^+ + \text{CO}_3^{--}$	1a, 2a
2 H_2O^0	$\text{H}_2\text{O}^0 \rightleftharpoons \text{H}^+ + \text{OH}^-$	3a
3 H_4SiO_4^0	$\text{H}_4\text{SiO}_4^0 \rightleftharpoons \text{H}^+ + \text{H}_3\text{SiO}_4^-$	4a, 24a
4 Cu^{++}	$\text{Cu}^{++} + \text{Fe}^{++} \rightleftharpoons \text{Cu}^+ + \text{Fe}^{+3}$	5b
5 Fe^{+3}	$\text{Fe}^{+3} + \frac{1}{2}\text{H}_2\text{O} + \frac{1}{8}\text{HS}^- \rightleftharpoons \text{Fe}^{++} + \frac{1}{8}\text{SO}_4^{--} + \frac{9}{8}\text{H}^+$	6b
6 Hg^{++}	$2\text{Hg}^{++} + 2\text{Fe}^{++} \rightleftharpoons \text{Hg}_2^{++} + 2\text{Fe}^{+3}$	2c
7 Mn^{+3}	$\text{Mn}^{+3} + \text{Fe}^{++} \rightleftharpoons \text{Mn}^{++} + \text{Fe}^{+3}$	2b
8 H_2AsO_3^-	$\text{H}_2\text{AsO}_3^- \rightleftharpoons \text{H}^+ + \text{HASO}_3^{--}$	2a
9 AlF_5^{--}	$\text{AlF}_5^{--} \rightleftharpoons \text{Al}^{+3} + 5\text{F}^-$	2a
10 H_2S^0	$\text{H}_2\text{S}^0 \rightleftharpoons \text{H}^+ + \text{HS}^-$	7a, 64a
11 AlF^{++}	$\text{AlF}^{++} \rightleftharpoons \text{Al}^{+3} + \text{F}^-$	2a, 8a
12 AlF_2^+	$\text{AlF}_2^+ \rightleftharpoons \text{Al}^{+3} + 2\text{F}^-$	2a, 8a
13 AlF_3^0	$\text{AlF}_3^0 \rightleftharpoons \text{Al}^{+3} + 3\text{F}^-$	2a
14 AlF_4^-	$\text{AlF}_4^- \rightleftharpoons \text{Al}^{+3} + 4\text{F}^-$	2a
15 Al(OH)^{++}	$\text{Al(OH)}^{++} \rightleftharpoons \text{Al}^{+3} + \text{OH}^-$	9b
16 Al(OH)_2^+	$\text{Al(OH)}_2^+ \rightleftharpoons \text{Al}^{+3} + 2\text{OH}^-$	10e
17 Al(OH)_4^-	$\text{Al(OH)}_4^- \rightleftharpoons \text{Al}^{+3} + 4\text{OH}^-$	7a
18 $\text{Al(SO}_4)_2^+$	$\text{Al(SO}_4)_2^+ \rightleftharpoons \text{Al}^{+3} + \text{SO}_4^{--}$	2a
19 $\text{Al(SO}_4)_2^-$	$\text{Al(SO}_4)_2^- \rightleftharpoons \text{Al}^{+3} + 2\text{SO}_4^{--}$	2a
20 AgCl^0	$\text{AgCl}^0 \rightleftharpoons \text{Ag}^+ + \text{Cl}^-$	11a
21 AgCl_2^-	$\text{AgCl}_2^- \rightleftharpoons \text{Ag}^+ + 2\text{Cl}^-$	11a
22 AgCl_3^{--}	$\text{AgCl}_3^{--} \rightleftharpoons \text{Ag}^+ + 3\text{Cl}^-$	11a
23 AgCl_4^{-3}	$\text{AgCl}_4^{-3} \rightleftharpoons \text{Ag}^+ + 4\text{Cl}^-$	11a
24 $\text{Ag(SO}_4)_2^-$	$\text{Ag(SO}_4)_2^- \rightleftharpoons \text{Ag}^+ + \text{SO}_4^{--}$	2a
25 CH_3COOH^0	$\text{CH}_3\text{COOH}^0 \rightleftharpoons \text{H}^+ + \text{CH}_3\text{COO}^-$	12a
26 BaCO_3^0	$\text{BaCO}_3^0 \rightleftharpoons \text{Ba}^{++} + \text{CO}_3^{--}$	7f
27 $\text{Ba(HCO}_3)_2^+$	$\text{Ba(HCO}_3)_2^+ \rightleftharpoons \text{Ba}^{++} + \text{HCO}_3^+$	7f

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
28 Ba(OH) ⁺	Ba(OH) ⁺ ⇌ Ba ⁺⁺ + OH ⁻	9b
29 BaSO ₄ ⁰	BaSO ₄ ⁰ ⇌ Ba ⁺⁺ + SO ₄ ⁻⁻	7f
30 CaCO ₃ ⁰	CaCO ₃ ⁰ ⇌ Ca ⁺⁺ + CO ₃ ⁻⁻	1a, 7f
31 Ca(HCO ₃) ⁺	Ca(HCO ₃) ⁺ ⇌ Ca ⁺⁺ + HCO ₃ ⁻	1a, 13a
32 Ca(OH) ⁺	Ca(OH) ⁺ ⇌ Ca ⁺⁺ + OH ⁻	9b
33 CaPO ₄ ⁻	CaPO ₄ ⁻ ⇌ Ca ⁺⁺ + PO ₄ ⁻³	7a
34 CaHPO ₄ ⁰	CaHPO ₄ ⁰ ⇌ Ca ⁺⁺ + HPO ₄ ⁻⁻	7a
35 CaH ₂ PO ₄ ⁺	CaH ₂ PO ₄ ⁺ ⇌ Ca ⁺⁺ + H ₂ PO ₄ ⁻	7a
36 CaSO ₄ ⁰	CaSO ₄ ⁰ ⇌ Ca ⁺⁺ + SO ₄ ⁻⁻	14a
37 CuCl ⁰	CuCl ⁰ ⇌ Cu ⁺ + Cl ⁻	15a, 16a
38 CuCl ₂ ⁻	CuCl ₂ ⁻ ⇌ Cu ⁺ + 2Cl ⁻	7a
39 CuCl ₃ ⁻⁻	CuCl ₃ ⁻⁻ ⇌ Cu ⁺ + 3Cl ⁻	7a
40 CuCl ⁺	CuCl ⁺ ⇌ Cu ⁺⁺ + Cl ⁻	7a
41 CuCl ₂ ⁰	CuCl ₂ ⁰ ⇌ Cu ⁺⁺ + 2Cl ⁻	7a
42 CuCl ₃ ⁻	CuCl ₃ ⁻ ⇌ Cu ⁺⁺ + 3Cl ⁻	7a
43 CuCl ₄ ⁻⁻	CuCl ₄ ⁻⁻ ⇌ Cu ⁺⁺ + 4Cl ⁻	7a
44 Cu(OH) ⁺	Cu(OH) ⁺ ⇌ Cu ⁺⁺ + OH ⁻	9a
45 CuSO ₄ ⁰	CuSO ₄ ⁰ ⇌ Cu ⁺⁺ + SO ₄ ⁻⁻	2a
46 FeCl ⁺	FeCl ⁺ ⇌ Fe ⁺⁺ + Cl ⁻	17a
47 FeCl ₂ ⁰	FeCl ₂ ⁰ ⇌ Fe ⁺⁺ + 2Cl ⁻	17a
48 FeHPO ₄ ⁰	FeHPO ₄ ⁰ ⇌ Fe ⁺⁺ + HPO ₄ ⁻⁻	52c
49 H ₃ PO ₄ ⁰	H ₃ PO ₄ ⁰ ⇌ 3H ⁺ + PO ₄ ⁻³	24a
50 Fe(OH) ⁺	Fe(OH) ⁺ ⇌ Fe ⁺⁺ + OH ⁻	9b
51 Fe(OH) ₂ ⁰	Fe(OH) ₂ ⁰ ⇌ Fe ⁺⁺ + 2OH ⁻	9b
52 FeOOH ⁻	FeOOH ⁻ + 3H ⁺ ⇌ Fe ⁺⁺ + 2H ₂ O	9b
53 FeSO ₄ ⁰	FeSO ₄ ⁰ ⇌ Fe ⁺⁺ + SO ₄ ⁻⁻	2c
54 FeCl ⁺⁺	FeCl ⁺⁺ ⇌ Fe ⁺³ + Cl ⁻	7a, 8a
55 FeCl ₂ ⁺	FeCl ₂ ⁺ ⇌ Fe ⁺³ + 2Cl ⁻	7a, 8a

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
56 FeCl_3^0	$\text{FeCl}_3^0 \rightleftharpoons \text{Fe}^{+3} + 3\text{Cl}^-$	7a, 8a
57 FeCl_4^-	$\text{FeCl}_4^- \rightleftharpoons \text{Fe}^{+3} + 4\text{Cl}^-$	7a, 8a
58 $\text{Fe}(\text{SO}_4)^+$	$\text{Fe}(\text{SO}_4)^+ \rightleftharpoons \text{Fe}^{+3} + \text{SO}_4^{--}$	2c
59 $\text{Fe}(\text{SO}_4)_2^-$	$\text{Fe}(\text{SO}_4)_2^- \rightleftharpoons \text{Fe}^{+3} + 2\text{SO}_4^{--}$	18d
60 $\text{Fe}(\text{OH})^{++}$	$\text{Fe}(\text{OH})^{++} \rightleftharpoons \text{Fe}^{+3} + \text{OH}^-$	9b
61 $\text{Fe}(\text{OH})_2^+$	$\text{Fe}(\text{OH})_2^+ \rightleftharpoons \text{Fe}^{+3} + 2\text{OH}^-$	2e
62 $\text{Fe}(\text{OH})_3^0$	$\text{Fe}(\text{OH})_3^0 \rightleftharpoons \text{Fe}^{+3} + 3\text{OH}^-$	10f, 19f
63 $\text{Fe}(\text{OH})_4^-$	$\text{Fe}(\text{OH})_4^- \rightleftharpoons \text{Fe}^{+3} + 4\text{OH}^-$	19e
64 $\text{B}(\text{OH})_4^-$	$\text{B}(\text{OH})_4^- \rightleftharpoons \text{B}(\text{OH})_3^0 + \text{OH}^-$	20a
65 AlF_6^{-3}	$\text{AlF}_6^{-3} \rightleftharpoons \text{Al}^{+3} + 6\text{F}^-$	2b
66 H_3SiO_4^-	$\text{H}_3\text{SiO}_4^- \rightleftharpoons \text{H}^+ + \text{H}_2\text{SiO}_4^{--}$	2a
67 H_3AsO_3^0	$\text{H}_3\text{AsO}_3^0 \rightleftharpoons \text{H}^+ + \text{H}_2\text{AsO}_3^-$	24a
68 HAsO_4^{--}	$\text{HAsO}_4^{--} \rightleftharpoons \text{H}^+ + \text{AsO}_4^{-3}$	21c
69 H_2AsO_4^-	$\text{H}_2\text{AsO}_4^- \rightleftharpoons 2\text{H}^+ + \text{AsO}_4^{-3}$	24a
70 H_3AsO_4^0	$\text{H}_3\text{AsO}_4^0 \rightleftharpoons 3\text{H}^+ + \text{AsO}_4^{-3}$	24a
71 HF^0	$\text{HF}^0 \rightleftharpoons \text{H}^+ + \text{F}^-$	7a
72 H_2CO_3^0	$\text{H}_2\text{CO}_3^0 \rightleftharpoons \text{H}^+ + \text{HCO}_3^-$	1a, 7a
73 HPO_4^{--}	$\text{HPO}_4^{--} \rightleftharpoons \text{H}^+ + \text{PO}_4^{-3}$	7a
74 H_2PO_4^-	$\text{H}_2\text{PO}_4^- \rightleftharpoons 2\text{H}^+ + \text{PO}_4^{-3}$	24a
75 HS^-	$\text{HS}^- \rightleftharpoons \text{H}^+ + \text{S}^{--}$	7a
76 HSO_4^-	$\text{HSO}_4^- \rightleftharpoons \text{H}^+ + \text{SO}_4^{--}$	7a
77 HNO_3^0	$\text{HNO}_3^0 \rightleftharpoons \text{H}^+ + \text{NO}_3^-$	24a
78 HgCl^+	$\text{HgCl}^+ \rightleftharpoons \text{Hg}^{++} + \text{Cl}^-$	7c
79 HgCl_2^0	$\text{HgCl}_2^0 \rightleftharpoons \text{Hg}^{++} + 2\text{Cl}^-$	7c
80 HgCl_3^-	$\text{HgCl}_3^- \rightleftharpoons \text{Hg}^{++} + 3\text{Cl}^-$	7c
81 HgCl_4^{--}	$\text{HgCl}_4^{--} \rightleftharpoons \text{Hg}^{++} + 4\text{Cl}^-$	7c
82 HgSO_4^0	$\text{HgSO}_4^0 \rightleftharpoons \text{Hg}^{++} + \text{SO}_4^{--}$	18f, 22f

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
83 $\text{HgS}(\text{H}_2\text{S})_2^0$	$\text{HgS}(\text{H}_2\text{S})_2^0 + \text{H}^+ \rightleftharpoons \text{Hg}^{++} + 2\text{H}_2\text{S}^0 + \text{HS}^-$	23c
84 $\text{Hg}(\text{HS})_3^-$	$\text{Hg}(\text{HS})_3^- \rightleftharpoons \text{Hg}^{++} + 3\text{HS}^-$	17c
85 Hg^0	$\text{Hg}^0 + 2\text{Fe}^{+3} \rightleftharpoons \text{Hg}^{+2} + 2\text{Fe}^{++}$	23d
86 KCl^0	$\text{KCl}^0 \rightleftharpoons \text{K}^+ + \text{Cl}^-$	7a, 11a
87 KCO_3^-	$\text{KCO}_3^- \rightleftharpoons \text{K}^+ + \text{CO}_3^{--}$	31f
88 KHSO_4^0	$\text{KHSO}_4^0 \rightleftharpoons \text{K}^+ + \text{HSO}_4^-$	15c
89 KSO_4^-	$\text{KSO}_4^- \rightleftharpoons \text{K}^+ + \text{SO}_4^{--}$	7a
90 KHPO_4^-	$\text{KHPO}_4^- \rightleftharpoons \text{K}^+ + \text{HPO}_4^{--}$	7a
91 LiOH^0	$\text{LiOH}^0 \rightleftharpoons \text{Li}^+ + \text{OH}^-$	25c
92 LiSO_4^-	$\text{LiSO}_4^- \rightleftharpoons \text{Li}^+ + \text{SO}_4^{--}$	25
93 MgCO_3^0	$\text{MgCO}_3^0 \rightleftharpoons \text{Mg}^{++} + \text{CO}_3^{--}$	26d
94 MgHCO_3^+	$\text{MgHCO}_3^+ \rightleftharpoons \text{Mg}^{++} + \text{HCO}_3^-$	26d
95 MgF^+	$\text{MgF}^+ \rightleftharpoons \text{Mg}^{++} + \text{F}^-$	7a
96 MgOH^+	$\text{MgOH}^+ \rightleftharpoons \text{Mg}^{++} + \text{OH}^-$	9a
97 MgSO_4^0	$\text{MgSO}_4^0 \rightleftharpoons \text{Mg}^{++} + \text{SO}_4^{--}$	15, 27b
98 MgPO_4^-	$\text{MgPO}_4^- \rightleftharpoons \text{Mg}^{++} + \text{PO}_4^{-3}$	7a
99 MgHPO_4^0	$\text{MgHPO}_4^0 \rightleftharpoons \text{Mg}^{++} + \text{HPO}_4^{--}$	7a
100 $\text{MgH}_2\text{PO}_4^+$	$\text{MgH}_2\text{PO}_4^+ \rightleftharpoons \text{Mg}^{++} + \text{H}_2\text{PO}_4^-$	7a
101 MnCl^+	$\text{MnCl}^+ \rightleftharpoons \text{Mn}^{++} + \text{Cl}^-$	28d
102 MnCl_2^0	$\text{MnCl}_2^0 \rightleftharpoons \text{Mn}^{++} + 2\text{Cl}^-$	28d
103 MnCl_3^-	$\text{MnCl}_3^- \rightleftharpoons \text{Mn}^{++} + 3\text{Cl}^-$	28d
104 MnCl_4^{--}	$\text{MnCl}_4^{--} \rightleftharpoons \text{Mn}^{++} + 4\text{Cl}^-$	28d
105 MnHCO_3^+	$\text{MnHCO}_3^+ \rightleftharpoons \text{Mn}^{++} + \text{HCO}_3^-$	29d
106 MnSO_4^0	$\text{MnSO}_4^0 \rightleftharpoons \text{Mn}^{++} + \text{SO}_4^{--}$	25d
107 MnCl^{++}	$\text{MnCl}^{++} \rightleftharpoons \text{Mn}^{+3} + \text{Cl}^-$	15a
108 MnHPO_4^0	$\text{MnHPO}_4^0 \rightleftharpoons \text{Mn}^{++} + \text{HPO}_4^{--}$	52c
109 MnOH^+	$\text{MnOH}^+ \rightleftharpoons \text{Mn}^{++} + \text{OH}^-$	9c
110 NaCl^0	$\text{NaCl}^0 \rightleftharpoons \text{Na}^+ + \text{Cl}^-$	30a

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
111 NaCO_3^-	$\text{NaCO}_3^- \rightleftharpoons \text{Na}^+ + \text{CO}_3^{--}$	31c
112 NaHCO_3^0	$\text{NaHCO}_3^0 \rightleftharpoons \text{Na}^+ + \text{HCO}_3^-$	32, 22f
113 Na_2CO_3^0	$\text{Na}_2\text{CO}_3^0 \rightleftharpoons 2\text{Na}^+ + \text{CO}_3^{--}$	32, 33f
114 Na_2SO_4^0	$\text{Na}_2\text{SO}_4^0 \rightleftharpoons 2\text{Na}^+ + \text{SO}_4^{--}$	
115 NaSO_4^-	$\text{NaSO}_4^- \rightleftharpoons \text{Na}^+ + \text{SO}_4^{--}$	54a
116 NaHPO_4^-	$\text{NaHPO}_4^- \rightleftharpoons \text{Na}^+ + \text{HPO}_4^{--}$	35c
117 HgOH^+	$\text{HgOH}^+ \rightleftharpoons \text{Hg}^{++} + \text{OH}^-$	9b
118 NH_4OH^0	$\text{NH}_4\text{OH}^0 \rightleftharpoons \text{NH}_4^+ + \text{OH}^-$	7a
119 NaHS^0	$\text{NaHS}^0 \rightleftharpoons \text{Na}^+ + \text{HS}^-$	46a
120 NaF^0	$\text{NaF}^0 \rightleftharpoons \text{Na}^+ + \text{F}^-$	57c
121 PbCl^+	$\text{PbCl}^+ \rightleftharpoons \text{Pb}^{++} + \text{Cl}^-$	36a
122 PbCl_2^0	$\text{PbCl}_2^0 \rightleftharpoons \text{Pb}^{++} + 2\text{Cl}^-$	36a
123 PbCl_3^-	$\text{PbCl}_3^- \rightleftharpoons \text{Pb}^{++} + 3\text{Cl}^-$	36a
124 PbCl_4^{--}	$\text{PbCl}_4^{--} \rightleftharpoons \text{Pb}^{++} + 4\text{Cl}^-$	36a
125 PbSO_4^0	$\text{PbSO}_4^0 \rightleftharpoons \text{Pb}^{++} + \text{SO}_4^{--}$	15
126 $\text{Zn}(\text{CH}_3\text{COO})_2^0$	$\text{Zn}(\text{CH}_3\text{COO})_2^0 \rightleftharpoons \text{Zn}^{++} + 2\text{CH}_3\text{COO}^-$	18c, 38a
127 SrOH^+	$\text{SrOH}^+ \rightleftharpoons \text{Sr}^{++} + \text{OH}^-$	9b
128 SrCO_3^0	$\text{SrCO}_3^0 \rightleftharpoons \text{Sr}^{++} + \text{CO}_3^{--}$	40c
129 SrHCO_3^+	$\text{SrHCO}_3^+ \rightleftharpoons \text{Sr}^{++} + \text{HCO}_3^-$	40c
130 SrSO_4^0	$\text{SrSO}_4^0 \rightleftharpoons \text{Sr}^{++} + \text{SO}_4^{--}$	7a
131 ZnCl^+	$\text{ZnCl}^+ \rightleftharpoons \text{Zn}^{++} + \text{Cl}^-$	41a
132 ZnCl_2^0	$\text{ZnCl}_2^0 \rightleftharpoons \text{Zn}^{++} + 2\text{Cl}^-$	41a
133 ZnCl_3^-	$\text{ZnCl}_3^- \rightleftharpoons \text{Zn}^{++} + 3\text{Cl}^-$	41a
134 ZnCl_4^{--}	$\text{ZnCl}_4^{--} \rightleftharpoons \text{Zn}^{++} + 4\text{Cl}^-$	41a
135 ZnSO_4^0	$\text{ZnSO}_4^0 \rightleftharpoons \text{Zn}^{++} + \text{SO}_4^{--}$	42d
136 AsO_4^{-3}	$\text{AsO}_4^{-3} + 4\text{H}^+ + 2\text{Fe}^{++} \rightleftharpoons \text{H}_2\text{AsO}_3^- + 2\text{Fe}^{+3} + \text{H}_2\text{O}$	7a
137 $\text{Hg}(\text{OH})_2^0$	$\text{Hg}(\text{OH})_2^0 \rightleftharpoons \text{Hg}^{++} + 2\text{OH}^-$	9b

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
138 Fe^{++} to Fe^{+3}	$\text{Fe}^{++} \rightleftharpoons \text{Fe}^{+3} + \text{e}^-$	6b
139 Cu^+ to Cu^{++}	$\text{Cu}^+ \rightleftharpoons \text{Cu}^{++} + \text{e}^-$	5b
140 Hg_2^{++} to Hg^{++}	$\text{Hg}_2^{++} \rightleftharpoons 2\text{Hg}^{++} + 2\text{e}^-$	7c
141 Mn^{++} to Mn^{+3}	$\text{Mn}^{++} \rightleftharpoons \text{Mn}^{+3} + \text{e}^-$	7c
142 U^{+4} to UO_2^+	$\text{U}^{+4} + 2\text{H}_2\text{O} \rightleftharpoons \text{UO}_2^+ + 4\text{H}^+ + \text{e}^-$	43b
143 UO_2^+ to UO_2^{++}	$\text{UO}_2^+ \rightleftharpoons \text{UO}_2^{++} + \text{e}^-$	43b
144 V^{+3} to VO^{++}	$\text{V}^{+3} + \text{H}_2\text{O} \rightleftharpoons \text{VO}^{++} + 2\text{H}^+ + \text{e}^-$	44b, 2b
145 VO^{++} to VO_4^{-3}	$\text{VO}^{+3} + 2\text{H}_2\text{O} \rightleftharpoons \text{VO}_4^{-3} + 6\text{H}^+ + \text{e}^-$	44c, 45c
146 CaCl^+	$\text{CaCl}^+ \rightleftharpoons \text{Ca}^{++} + \text{Cl}^-$	46a
147 CaCl_2^0	$\text{CaCl}_2^0 \rightleftharpoons \text{Ca}^{++} + 2\text{Cl}^-$	79a
148 UOH^{+3}	$\text{UOH}^{+3} \rightleftharpoons \text{U}^{+4} + \text{OH}^-$	5b, 43b
149 U(OH)_2^{++}	$\text{U(OH)}_2^{++} \rightleftharpoons \text{U}^{+4} + 2\text{OH}^-$	5b, 43b
150 U(OH)_3^+	$\text{U(OH)}_3^+ + 3\text{H}^+ \rightleftharpoons \text{U}^{+4} + 3\text{H}_2\text{O}$	5b, 43b
151 U(OH)_4^0	$\text{U(OH)}_4^0 + 4\text{H}^+ \rightleftharpoons \text{U}^{+4} + 4\text{H}_2\text{O}$	5b, 43b
152 U(OH)_5^-	$\text{U(OH)}_5^- + 5\text{H}^+ \rightleftharpoons \text{U}^{+4} + 5\text{H}_2\text{O}$	47a
153 UF^{+3}	$\text{UF}^{+3} \rightleftharpoons \text{U}^{+4} + \text{F}^-$	5b, 43b
154 UF_2^{++}	$\text{UF}_2^{++} \rightleftharpoons \text{U}^{+4} + 2\text{F}^-$	5b, 43b
155 UF_3^+	$\text{UF}_3^+ \rightleftharpoons \text{U}^{+4} + 3\text{F}^-$	5b, 43b
156 UF_4^0	$\text{UF}_4^0 \rightleftharpoons \text{U}^{+4} + 4\text{F}^-$	5b, 43b
157 UF_5^-	$\text{UF}_5^- \rightleftharpoons \text{U}^{+4} + 5\text{F}^-$	5b, 43b
158 UF_6^{--}	$\text{UF}_6^{--} \rightleftharpoons \text{U}^{+4} + 6\text{F}^-$	5b, 43b
159 UCl^{+3}	$\text{UCl}^{+3} \rightleftharpoons \text{U}^{+4} + \text{Cl}^-$	5b, 43b
160 $\text{U(HPO}_4)_4^{++}$	$\text{U(HPO}_4)_4^{++} \rightleftharpoons \text{U}^{+4} + \text{HPO}_4^{--}$	2b, 43b
161 $\text{U(HPO}_4)_2^0$	$\text{U(HPO}_4)_2^0 \rightleftharpoons \text{U}^{+4} + 2\text{HPO}_4^{--}$	2b, 43b
162 $\text{U(HPO}_4)_3^{--}$	$\text{U(HPO}_4)_3^{--} + 3\text{H}^+ \rightleftharpoons \text{U}^{+4} + 3\text{H}_2\text{PO}_4^-$	2b, 43b
163 $\text{U(HPO}_4)_4^{-4}$	$\text{U(HPO}_4)_4^{-4} + 4\text{H}^+ \rightleftharpoons \text{U}^{+4} + 4\text{H}_2\text{PO}_4^-$	2b, 43b
164 $\text{U(SO}_4)_4^{++}$	$\text{U(SO}_4)_4^{++} \rightleftharpoons \text{U}^{+4} + \text{SO}_4^{--}$	5b, 43b

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

ID # and Name	Reaction	References
165 $\text{U}(\text{SO}_4)_2^0$	$\text{U}(\text{SO}_4)_2^0 \rightleftharpoons \text{U}^{+4} + 2\text{SO}_4^{--}$	5b, 43b
166 $\text{U}_6(\text{OH})_{15}^{+9}$	$\text{U}_6(\text{OH})_{15}^{+9} + 12\text{H}^+ \rightleftharpoons 6\text{U}^{+4} + 3\text{OH}^- + 12\text{H}_2\text{O}$	5b, 48b
167 $(\text{UO}_2)(\text{OH})^+$	$(\text{UO}_2)(\text{OH})^+ \rightleftharpoons \text{UO}_2^{++} + \text{OH}^-$	5b, 43b
168 $(\text{UO}_2)(\text{OH})_2^0$	$(\text{UO}_2)(\text{OH})_2^0 \rightleftharpoons \text{UO}_2^{++} + 2\text{OH}^-$	5b, 43b
169 $(\text{UO}_2)_2(\text{OH})_2^{++}$	$(\text{UO}_2)_2(\text{OH})_2^{++} \rightleftharpoons 2\text{UO}_2^{++} + 2\text{OH}^-$	5b, 43b
170 $(\text{UO}_2)_3(\text{OH})_5^+$	$(\text{UO}_2)_3(\text{OH})_5^+ + 5\text{H}^+ \rightleftharpoons 3\text{UO}_2^{++} + 5\text{H}_2\text{O}$	5b, 43b
171 $(\text{UO}_2)_3(\text{OH})_7^-$	$(\text{UO}_2)_3(\text{OH})_7^- + 7\text{H}^+ \rightleftharpoons 3\text{UO}_2^{++} + 7\text{H}_2\text{O}$	5b, 43b
172 $\text{UO}_2(\text{SO}_4)^0$	$\text{UO}_2(\text{SO}_4)^0 \rightleftharpoons \text{UO}_2^{++} + \text{SO}_4^{--}$	43b
173 $\text{UO}_2(\text{SO}_4)_2^{--}$	$\text{UO}_2(\text{SO}_4)_2^{--} \rightleftharpoons \text{UO}_2^{++} + 2\text{SO}_4^{--}$	5c, 45c
174 UO_2F^+	$\text{UO}_2\text{F}^+ \rightleftharpoons \text{UO}_2^{++} + \text{F}^-$	5b, 43b
175 UO_2F_2^0	$\text{UO}_2\text{F}_2^0 \rightleftharpoons \text{UO}_2^{++} + 2\text{F}^-$	5b, 43b
176 UO_2F_3^-	$\text{UO}_2\text{F}_3^- \rightleftharpoons \text{UO}_2^{++} + 3\text{F}^-$	5b, 43b
177 $\text{UO}_2\text{F}_4^{--}$	$\text{UO}_2\text{F}_4^{--} \rightleftharpoons \text{UO}_2^{++} + 4\text{F}^-$	5b, 43b
178 UO_2Cl^+	$\text{UO}_2\text{Cl}^+ \rightleftharpoons \text{UO}_2^{++} + \text{Cl}^-$	5b, 43b
179 $\text{UO}_2\text{H}_3\text{SiO}_4^+$	$\text{UO}_2\text{H}_3\text{SiO}_4^+ + \text{H}^+ \rightleftharpoons \text{UO}_2^{++} + \text{H}_4\text{SiO}_4^0$	5c, 45c
180 $\text{UO}_2(\text{HPO}_4)^0$	$\text{UO}_2(\text{HPO}_4)^0 \rightleftharpoons \text{UO}_2^{++} + \text{HPO}_4^{--}$	2b, 43b
181 $\text{UO}_2(\text{HPO}_4)_2^{--}$	$\text{UO}_2(\text{HPO}_4)_2^{--} \rightleftharpoons \text{UO}_2^{++} + 2\text{HPO}_4^{--}$	2b, 43b
182 $\text{UO}_2(\text{H}_2\text{PO}_4)^+$	$\text{UO}_2(\text{H}_2\text{PO}_4)^+ \rightleftharpoons \text{UO}_2^{++} + \text{HPO}_4^{--} + \text{H}^+$	2b, 43b
183 $\text{UO}_2(\text{H}_2\text{PO}_4)_2^0$	$\text{UO}_2(\text{H}_2\text{PO}_4)_2^0 \rightleftharpoons \text{UO}_2^{++} + 2\text{HPO}_4^{--} + 2\text{H}^+$	2b, 43b
184 $\text{UO}_2(\text{H}_2\text{PO}_4)_3^-$	$\text{UO}_2(\text{H}_2\text{PO}_4)_3^- \rightleftharpoons \text{UO}_2^{++} + 3\text{HPO}_4^{--} + 3\text{H}^+$	2b, 43b
185 $\text{UO}_2(\text{CO}_3)^0$	$\text{UO}_2(\text{CO}_3)^0 \rightleftharpoons \text{UO}_2^{++} + \text{CO}_3^{--}$	5b, 43b
186 $\text{UO}_2(\text{CO}_3)_2^{--}$	$\text{UO}_2(\text{CO}_3)_2^{--} \rightleftharpoons \text{UO}_2^{++} + 2\text{CO}_3^{--}$	5b, 43b
187 $\text{UO}_2(\text{CO}_3)_3^{-4}$	$\text{UO}_2(\text{CO}_3)_3^{-4} \rightleftharpoons \text{UO}_2^{++} + 3\text{CO}_3^{--}$	5b, 43b
188 HVO_4^{-2}	$\text{HVO}_4^{-2} \rightleftharpoons \text{VO}_4^{-3} + \text{H}^+$	43c
189 $\text{H}_2\text{VO}_4^{-1}$	$\text{H}_2\text{VO}_4^{-1} \rightleftharpoons \text{VO}_4^{-3} + 2\text{H}^+$	43c
190 H_3VO_4^0	$\text{H}_3\text{VO}_4^0 \rightleftharpoons \text{VO}_4^{-3} + 3\text{H}^+$	43c

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

ID # and Name	Reaction	References
191 H_4VO_4^+	$\text{H}_4\text{VO}_4^+ \rightleftharpoons \text{VO}_4^{-3} + 4\text{H}^+$	43c
192 NaHVO_4^-	$\text{NaHVO}_4^- \rightleftharpoons \text{Na}^+ + \text{VO}_4^{-3} + \text{H}^+$	2g
193 VO_2F^0	$\text{VO}_2\text{F}^0 \rightleftharpoons \text{VO}_2^+ + \text{F}^-$	15g
194 VO_2F_2^-	$\text{VO}_2\text{F}_2^- \rightleftharpoons \text{VO}_2^+ + 2\text{F}^-$	15g
195 $\text{V}(\text{OH})^{++}$	$\text{V}(\text{OH})^{++} \rightleftharpoons \text{V}^{+3} + \text{OH}^-$	43g
196 $\text{V}(\text{OH})_2^+$	$\text{V}(\text{OH})_2^+ \rightleftharpoons \text{V}^{+3} + 2\text{OH}^-$	43g
197 $\text{V}(\text{OH})_3^0$	$\text{V}(\text{OH})_3^0 \rightleftharpoons \text{V}^{+3} + 3\text{OH}^-$	43g
198 VOOH^+	$\text{VOOH}^+ \rightleftharpoons \text{VO}^{++} + \text{OH}^-$	43g
199 VOSO_4^0	$\text{VOSO}_4^0 \rightleftharpoons \text{VO}^{++} + \text{SO}_4^{--}$	2g
200 VOCl^+	$\text{VOCl}^+ \rightleftharpoons \text{VO}^{++} + \text{Cl}^-$	15g
201 VOF^+	$\text{VOF}^+ \rightleftharpoons \text{VO}^{++} + \text{F}^-$	2g
202 VOF_2^0	$\text{VOF}_2^0 \rightleftharpoons \text{VO}^{++} + 2\text{F}^-$	2g
203 $\text{UO}_2\text{CH}_3\text{COO}^+$	$\text{UO}_2\text{CH}_3\text{COO}^+ \rightleftharpoons \text{UO}_2^{++} + \text{CH}_3\text{COO}^-$	15c
204 $\text{UO}_2(\text{CH}_3\text{COO})_2^0$	$\text{UO}_2(\text{CH}_3\text{COO})_2^0 \rightleftharpoons \text{UO}_2^{++} + 2\text{CH}_3\text{COO}^-$	71c
205 UO_2^+	$\text{UO}_2^+ + \text{Fe}^{+3} \rightleftharpoons \text{UO}_2^{++} + \text{Fe}^{++}$	43b, 44b
206 U^{+4}	$\text{U}^{+4} + \text{Fe}^{+3} + 2\text{H}_2\text{O} \rightleftharpoons \text{UO}_2^+ + \text{Fe}^{++} + 4\text{H}^+$	43b, 44b
207 V^{+3}	$\text{V}^{+3} + \text{Fe}^{+3} + \text{H}_2\text{O} \rightleftharpoons \text{VO}^{++} + \text{Fe}^{++} + 2\text{H}^+$	2b, 44b
208 VO^{++}	$\text{VO}^{++} + \text{Fe}^{+3} + 3\text{H}_2\text{O} \rightleftharpoons \text{VO}_4^{-3} + \text{Fe}^{++} + 6\text{H}^+$	44c, 45c
209 $\text{AlCH}_3\text{COO}^{++}$	$\text{AlCH}_3\text{COO}^{++} \rightleftharpoons \text{Al}^{+3} + \text{CH}_3\text{COO}^-$	49
210 $\text{BaCH}_3\text{COO}^+$	$\text{BaCH}_3\text{COO}^+ \rightleftharpoons \text{Ba}^{++} + \text{CH}_3\text{COO}^-$	49c
211 $\text{CaCH}_3\text{COO}^+$	$\text{CaCH}_3\text{COO}^+ \rightleftharpoons \text{Ca}^{++} + \text{CH}_3\text{COO}^-$	50c
212 $\text{CuCH}_3\text{COO}^0$	$\text{CuCH}_3\text{COO}^0 \rightleftharpoons \text{Cu}^+ + \text{CH}_3\text{COO}^-$	49c
213 $\text{FeCH}_3\text{COO}^+$	$\text{FeCH}_3\text{COO}^+ \rightleftharpoons \text{Fe}^{++} + \text{CH}_3\text{COO}^-$	51a
214 $\text{Fe}(\text{CH}_3\text{COO})_2^0$	$\text{Fe}(\text{CH}_3\text{COO})_2^0 \rightleftharpoons \text{Fe}^{++} + 2\text{CH}_3\text{COO}^-$	51a
215 KCH_3COO^0	$\text{KCH}_3\text{COO}^0 \rightleftharpoons \text{K}^+ + \text{CH}_3\text{COO}^-$	52c, 53c
216 $\text{MgCH}_3\text{COO}^+$	$\text{MgCH}_3\text{COO}^+ \rightleftharpoons \text{Mg}^{++} + \text{CH}_3\text{COO}^-$	50c
217 $\text{NaCH}_3\text{COO}^0$	$\text{NaCH}_3\text{COO}^0 \rightleftharpoons \text{Na}^+ + \text{CH}_3\text{COO}^-$	52c, 53c

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
218 $\text{PbCH}_3\text{COO}^+$	$\text{PbCH}_3\text{COO}^+ \rightleftharpoons \text{Pb}^{++} + \text{CH}_3\text{COO}^-$	18c, 52c
219 $\text{Pb}(\text{CH}_3\text{COO})_2^0$	$\text{Pb}(\text{CH}_3\text{COO})_2^0 \rightleftharpoons \text{Pb}^{++} + 2\text{CH}_3\text{COO}^-$	18c, 52c
220 $\text{Pb}(\text{CH}_3\text{COO})_3^-$	$\text{Pb}(\text{CH}_3\text{COO})_3^- \rightleftharpoons \text{Pb}^{++} + 3\text{CH}_3\text{COO}^-$	18c, 52c
221 $\text{SrCH}_3\text{COO}^+$	$\text{SrCH}_3\text{COO}^+ \rightleftharpoons \text{Sr}^{++} + \text{CH}_3\text{COO}^-$	50c
222 $\text{ZnCH}_3\text{COO}^+$	$\text{ZnCH}_3\text{COO}^+ \rightleftharpoons \text{Zn}^{++} + \text{CH}_3\text{COO}^-$	18c, 38a
223 HC_2O_4^-	$\text{HC}_2\text{O}_4^- \rightleftharpoons \text{H}^+ + \text{C}_2\text{O}_4^{--}$	49c, 52c
224 $\text{H}_2\text{C}_2\text{O}_4^0$	$\text{H}_2\text{C}_2\text{O}_4^0 \rightleftharpoons 2\text{H}^+ + \text{C}_2\text{O}_4^{--}$	49c, 52c
225 AlC_2O_4^+	$\text{AlC}_2\text{O}_4^+ \rightleftharpoons \text{Al}^{+3} + \text{C}_2\text{O}_4^{--}$	49c, 59c
226 $\text{Al}(\text{C}_2\text{O}_4)_2^-$	$\text{Al}(\text{C}_2\text{O}_4)_2^- \rightleftharpoons \text{Al}^{+3} + 2\text{C}_2\text{O}_4^{--}$	49c, 59c
227 BaC_2O_4^0	$\text{BaC}_2\text{O}_4^0 \rightleftharpoons \text{Ba}^{++} + \text{C}_2\text{O}_4^{--}$	25c, 49c
228 CaC_2O_4^0	$\text{CaC}_2\text{O}_4^0 \rightleftharpoons \text{Ca}^{++} + \text{C}_2\text{O}_4^{--}$	25c, 49c
229 FeC_2O_4^0	$\text{FeC}_2\text{O}_4^0 \rightleftharpoons \text{Fe}^{++} + \text{C}_2\text{O}_4^{--}$	25c, 49c
230 FeC_2O_4^+	$\text{FeC}_2\text{O}_4^+ \rightleftharpoons \text{Fe}^{+3} + \text{C}_2\text{O}_4^{--}$	25c, 49c
231 KC_2O_4^-	$\text{KC}_2\text{O}_4^- \rightleftharpoons \text{K}^+ + \text{C}_2\text{O}_4^{--}$	25c, 49c
232 MgC_2O_4^0	$\text{MgC}_2\text{O}_4^0 \rightleftharpoons \text{Mg}^{++} + \text{C}_2\text{O}_4^{--}$	25c, 49c
233 MnC_2O_4^0	$\text{MnC}_2\text{O}_4^0 \rightleftharpoons \text{Mn}^{++} + \text{C}_2\text{O}_4^{--}$	49c, 52c
234 $\text{Mn}(\text{C}_2\text{O}_4)_2^{--}$	$\text{Mn}(\text{C}_2\text{O}_4)_2^{--} \rightleftharpoons \text{Mn}^{++} + 2\text{C}_2\text{O}_4^{--}$	49c, 52c
235 $\text{Mn}(\text{C}_2\text{O}_4)_3^{-4}$	$\text{Mn}(\text{C}_2\text{O}_4)_3^{-4} \rightleftharpoons \text{Mn}^{++} + 3\text{C}_2\text{O}_4^{--}$	49c, 52c
236 MnC_2O_4^+	$\text{MnC}_2\text{O}_4^+ \rightleftharpoons \text{Mn}^{+3} + \text{C}_2\text{O}_4^{--}$	49c, 52c
237 NaC_2O_4^-	$\text{NaC}_2\text{O}_4^- \rightleftharpoons \text{Na}^+ + \text{C}_2\text{O}_4^{--}$	25c, 49c
238 PbC_2O_4^0	$\text{PbC}_2\text{O}_4^0 \rightleftharpoons \text{Pb}^{++} + \text{C}_2\text{O}_4^{--}$	25f, 49f
239 SrC_2O_4^0	$\text{SrC}_2\text{O}_4^0 \rightleftharpoons \text{Sr}^{++} + \text{C}_2\text{O}_4^{--}$	25c, 49c
240 ZnC_2O_4^0	$\text{ZnC}_2\text{O}_4^0 \rightleftharpoons \text{Zn}^{++} + \text{C}_2\text{O}_4^{--}$	49c, 52c
241 $\text{H}(\text{C}_4\text{H}_4\text{O}_4)^-$	$\text{H}(\text{C}_4\text{H}_4\text{O}_4)^- \rightleftharpoons \text{H}^+ + \text{C}_4\text{H}_4\text{O}_4^{--}$	49c
242 $\text{H}_2(\text{C}_4\text{H}_4\text{O}_4)^0$	$\text{H}_2(\text{C}_4\text{H}_4\text{O}_4)^0 \rightleftharpoons 2\text{H}^+ + \text{C}_4\text{H}_4\text{O}_4^{--}$	49c
243 $\text{AlC}_4\text{H}_4\text{O}_4^+$	$\text{AlC}_4\text{H}_4\text{O}_4^+ \rightleftharpoons \text{Al}^{+3} + \text{C}_4\text{H}_4\text{O}_4^{--}$	49f, 59f

Table 2. -- Dissociation reactions for aqueous complexes and sources of thermochemical data -- (Continued)

ID # and Name	Reaction	References
244 $\text{Al}(\text{C}_4\text{H}_4\text{O}_4)_2^-$	$\text{Al}(\text{C}_4\text{H}_4\text{O}_4)_2^- \rightleftharpoons \text{Al}^{+3} + 2\text{C}_4\text{H}_4\text{O}_4^{--}$	49f, 59f
245 $\text{BaC}_4\text{H}_4\text{O}_4^0$	$\text{BaC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Ba}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
246 $\text{CaC}_4\text{H}_4\text{O}_4^0$	$\text{CaC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Ca}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
247 $\text{FeC}_4\text{H}_4\text{O}_4^0$	$\text{FeC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Fe}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25f, 49f
248 $\text{FeC}_4\text{H}_4\text{O}_4^+$	$\text{FeC}_4\text{H}_4\text{O}_4^+ \rightleftharpoons \text{Fe}^{+3} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
249 $\text{KC}_4\text{H}_4\text{O}_4^-$	$\text{KC}_4\text{H}_4\text{O}_4^- \rightleftharpoons \text{K}^+ + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
250 $\text{MgC}_4\text{H}_4\text{O}_4^0$	$\text{MgC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Mg}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
251 $\text{MnC}_4\text{H}_4\text{O}_4^0$	$\text{MnC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Mn}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
252 $\text{NaC}_4\text{H}_4\text{O}_4^-$	$\text{NaC}_4\text{H}_4\text{O}_4^- \rightleftharpoons \text{Na}^+ + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
253 $\text{PbC}_4\text{H}_4\text{O}_4^0$	$\text{PbC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Pb}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
254 $\text{SrC}_4\text{H}_4\text{O}_4^0$	$\text{SrC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Sr}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
255 $\text{ZnC}_4\text{H}_4\text{O}_4^0$	$\text{ZnC}_4\text{H}_4\text{O}_4^0 \rightleftharpoons \text{Zn}^{++} + \text{C}_4\text{H}_4\text{O}_4^{--}$	25c, 49c
256 FeF^{++}	$\text{FeF}^{++} \rightleftharpoons \text{Fe}^{+3} + \text{F}^-$	57c
257 SiF_6^{--}	$\text{SiF}_6^{--} + 4\text{OH}^- \rightleftharpoons \text{H}_4\text{SiO}_4^0 + 6\text{F}^-$	58c
258 $\text{Pb}(\text{HS})_2^0$	$\text{Pb}(\text{HS})_2^0 \rightleftharpoons \text{Pb}^{++} + 2\text{HS}^-$	2a, 55a, 56a
259 $\text{Pb}(\text{HS})_3^-$	$\text{Pb}(\text{HS})_3^- \rightleftharpoons \text{Pb}^{++} + 3\text{HS}^-$	2a, 55a
260 PbCO_3^0	$\text{PbCO}_3^0 \rightleftharpoons \text{Pb}^{++} + \text{CO}_3^{--}$	56a, 57a
261 PbOH^+	$\text{PbOH}^+ \rightleftharpoons \text{Pb}^{++} + \text{OH}^-$	52a, 56a
262 $\text{Zn}(\text{HS})_2^0$	$\text{Zn}(\text{HS})_2^0 \rightleftharpoons \text{Zn}^{++} + 2\text{HS}^-$	46a, 55a, 56a
263 $\text{Zn}(\text{HS})_3^-$	$\text{Zn}(\text{HS})_3^- \rightleftharpoons \text{Zn}^{++} + 3\text{HS}^-$	46a, 55a
264 ZnHCO_3^+	$\text{ZnHCO}_3^+ \rightleftharpoons \text{Zn}^{++} + \text{HCO}_3^-$	46a
265 ZnOH^+	$\text{ZnOH}^+ \rightleftharpoons \text{Zn}^{++} + \text{OH}^-$	46a
266 $\text{Zn}(\text{OH})_2^0$	$\text{Zn}(\text{OH})_2^0 \rightleftharpoons \text{Zn}^{++} + 2\text{OH}^-$	9a, 46a
267 $\text{Zn}(\text{HS})(\text{OH})^0$	$\text{Zn}(\text{HS})(\text{OH})^0 \rightleftharpoons \text{Zn}^{++} + \text{HS}^- + \text{OH}^-$	46a

Oxidation-Reduction Reactions

Oxidation-reduction reactions are used in conjunction with mass-action reactions and mass-balance expressions to compute the distribution of the multivalent elements Fe, Cu, Hg, Mn, U, and V where the Eh of the solution is known. The reaction for iron is



where e^{-} represents an electron. The concentrations of Fe^{++} and Fe^{+3} are related by

$$\text{Eh} = E^{\circ} + \frac{RT}{nF} \ln \left[\frac{m_{\text{Fe}^{+3}} \cdot \gamma_{\text{Fe}^{+3}}}{m_{\text{Fe}^{++}} \cdot \gamma_{\text{Fe}^{++}}} \right] \quad , \quad (6)$$

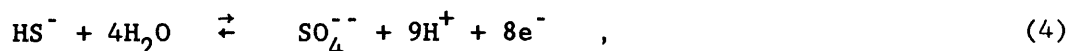
where Eh is the oxidation potential referred to the hydrogen half cell, E° is the standard state potential of the reaction, n is the number of electrons involved in the reaction, F is the Faraday constant and R is the gas constant. Values of E° at temperatures from 0° to 350 °C, are calculated from equation

$$E^{\circ} = \frac{\Delta G_r^{\circ}}{nF} \quad , \quad (7)$$

where the Gibbs standard state free energies for the oxidation-reduction reactions (ΔG_r°) are tabulated in the data files of the program (see below).

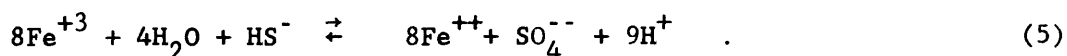
SOLMINEQ.88 will compute the Eh of a water sample at the desired temperature, if necessary, from the Emf of the Eh cell including the Calomel reference electrode (EHMC) or from the Emf of the Eh cell calibrated using Zobell's solution (EMFZSC). For a more detailed discussion of the theory of Eh, its field measurement and reduction, see Barnes and Back (1964), Barnes and Clarke (1969), Garrels and Christ (1965), and Thorstensen (1984).

Computations based on measured Eh have been kept to a minimum in SOLMINEQ.88 because of uncertainties in the measurement and interpretation of oxidation potentials (Barnes and Clarke, 1969; Wolery, 1983; Nordstrom and Munoz, 1985). However, the program can compute the distribution of species for elements with multiple redox states by assuming redox equilibrium between the species HS^{-} and SO_4^{--} . Kharaka and others (1980) have shown that oil field waters are strongly reducing ($\text{Eh} < -200$ mV) and that the sulfide-sulfate redox reaction



is probably the best of the possible redox couples for computing the Eh of these waters. However, in other natural systems alternative redox couples may be better indicators of the redox state of water (Freeze and Cherry, 1979; Kharaka and others, 1980; Nordstrom and Munoz, 1985).

The distribution of Fe species in SOLMINEQ.88 can be computed by combining $\text{HS}^-/\text{SO}_4^{--}$, and $\text{Fe}^{+3}/\text{Fe}^{++}$ couples (Reactions 3 and 4) to give the reaction



The distribution of species for the other multivalent elements can be computed by combining them with the $\text{Fe}^{+3}/\text{Fe}^{++}$ couple in reactions that eliminate the electron. In the case of Cu, for example, the reaction is



It must be emphasized in this section that the above computations assume a state of thermodynamic equilibrium that may not be applicable to many or all of the redox couples. For a detailed discussion of the real meaning of Eh, the related parameter pe and the numerous pitfalls and inconsistencies in their measurements and interpretations, the reader is referred to Barnes and Clarke (1969), Wolery (1983) and Thorstenson, (1984).

Speciation at Subsurface Conditions

The chemical compositions of subsurface water samples collected at the land surface may not correspond to their in-situ compositions. Volatile gases such as CO_2 , H_2S , and NH_3 may exsolve due to a pressure decrease. Loss of these gases may drastically change (by up to 3 pH units) the pH of the remaining fluids. Changes in temperature and pressure alone will result in pH changes due to variations in the stabilities of hydrogen-bearing aqueous species. Changes in pH, temperature, and pressure may result in precipitation of solid phases such as calcium carbonate and amorphous silica, among others. Increases in the Eh of waters containing Fe^{++} usually result in the precipitation of amorphous iron hydroxides and coprecipitation of trace metals.

The in situ water chemistry may be calculated for water-dominated geothermal and oil field systems where the amount and composition of gases

lost prior to water sampling are known. The main problem in these computations has been the estimation of an in situ pH which is critical to these computations. Two different approaches have been used (see Modeling Options) to compute the in-situ pH: (1) assuming equilibrium at subsurface conditions with a mineral (Merino, 1979) known to be present in the aquifer (calcite is generally selected), or (2) assuming mass balance for hydronium at surface and subsurface conditions (Truesdell and Singer, 1974; Kharaka and others, 1985).

SOLMINEQ.88 has options to compute the subsurface pH and resulting speciation and saturation states using either approach. The distribution of species in the mass-balance approach is carried out at surface conditions using the measured pH. The total hydrogen (m_{H,t,T_1}) and hydroxyl (m_{OH,t,T_1}) are then computed at the surface conditions from the equations

$$m_{H,t,T_1} = m_{H^+} + m_{HCO_3^-} + 2m_{H_2CO_3^0} + m_{HS^-} + 2m_{H_2S^0} + m_{CH_3COOH^0} + \dots, \quad (8)$$

$$m_{OH,t,T_1} = m_{OH^-} + m_{Ca(OH)^+} + m_{Mg(OH)^+} + m_{NH_4OH^0} + 2m_{Fe(OH)_2^0} + \dots \quad (9)$$

For samples where known quantities of CO_2 , H_2S , and NH_3 are lost prior to surface pH measurement, equations (8) and (9) are modified to include the lost gases. CO_2 , H_2S , and NH_3 are included as $2m_{H_2CO_3}$, $2m_{H_2S}$, and m_{NH_4OH} , respectively, in the computed value of m_{H,t,T_2} and m_{OH,t,T_2} (see Modeling Options).

The distribution of species is then computed at the subsurface temperature assuming that the subsurface pH is equal to the measured surface pH. The total molalities of hydrogen (m_{H,t,T_2}) and hydroxyl (m_{OH,t,T_2}) at subsurface temperature (T_2) are then computed. The value of the tolerance factor (Y_H) for the hydronium given by:

$$Y_H = 1 - \frac{(m_{H,t,T_2} - m_{OH,t,T_2})}{(m_{H,t,T_1} - m_{OH,t,T_1})}, \quad (10)$$

is then computed. The terms (m_{OH,t,T_1} and m_{OH,t,T_2}) are included in Equation (10) to account for the changes in the hydrogen mass-balance from hydrolysis

of water. Iterations are then carried out changing the pH by small increments (see below) until the value of Y is $\leq \pm 5 \times 10^{-5}$ (or another user-defined value). The final computed pH is then used to compute the distribution of species and the states of saturation of the solution with respect to minerals.

Iteration Techniques

The distribution of cations in SOLMINEQ.88 is carried out using equations that, throughout all computations, meet the requirement of mass-balance (Equation 3). In the case of anions, however, the total (analytical) molality of each anion is initially assigned to the primary (generally the predominant) species of that anion to compute the molalities of the other species. This generally results in a sum of computed molalities that after the first iteration is higher than the analytical molality. In the case of sulfate, for example, $m_{\text{SO}_4}^{--}$ is initially made equal to $m_{\text{SO}_4,t}$ resulting in

$$m_{\text{SO}_4,t} < m_{\text{SO}_4}^{--} + m_{\text{CaSO}_4}^0 + m_{\text{NaSO}_4}^- + \dots \quad (11)$$

SOLMINEQ.88 uses a back - substitution iterative procedure (see code listing in Appendix IV.) for the distribution of anions. Iterations are continued until the tolerance factor for the anion (Y_A) defined by the ratio of the analytical molality of the anion to the computed sum of its species and given by

$$Y_A = 1 - \frac{m_{i,t}}{\sum n_{i,j} m_{j,i}}, \quad (12)$$

is $\leq \pm 5 \times 10^{-5}$. Almost all waters examined to date have met these requirements within 10 iteration cycles. Iteration problems, however, may be encountered especially in solutions with many ions or high pH values, incorrect or incomplete chemical analysis, and in high salinity brines when using the Pitzer equations to compute the activity coefficients.

The iterative algorithm for hydronium mass-balance in SOLMINEQ.88 has been modified to utilize a polynomial interpolating technique. Initially, the pH is adjusted (the initial adjustment is 1.0 pH unit) until either convergence is achieved, (as defined by equation (10)), or the sign of Y_H is reversed. Once the sign of Y_H has reversed, values of pH and Y_H are fit to a

polynomial, the order of which is one less than the number of pH and Y_H values (up to a maximum of 6 points). The polynomial is then used to interpolate the value of pH where Y_H "should be" zero. This value is checked to insure that it is between the bracketing values. If it is not, a polynomial of decreased order is re-fit to the values and a new value of pH is obtained. This is continued until the pH is between the bracketing values. The aqueous species are then redistributed by iteration until Y_A is satisfied and a new value of Y_H obtained. This procedure continues until Y_H passes the convergence test. This technique results in a much faster solution than the back-substitution approach used in the original program, and allows imposition of a smaller tolerance factor. The smaller tolerance factor avoids an erroneous calculation of pH when one H^+ - or OH^- - bearing species is predominant in the solution (see Morel, 1983, p. 96-97).

All of the options which modify the solution composition and can be treated as a function of a single variable (addition/removal of a volatile, precipitation/dissolution of a mineral, etc.; see Modeling Options) use a similar procedure to obtain pH convergence; the only difference is the function for Y and the independent variable. For example, for mineral saturation, Y is a function of the saturation index (SI) of the minerals and it is varied as a function of the amount of material added to or removed from the solution.

Before the polynomial interpolation is used, the sign of Y must change. This is done by increasing or decreasing the independent variable. The choice of step size is critical. With the exception of the pH modification (discussed earlier), the step size is based on the difference between the current parameters (SI's, amount in solution, etc.), and the anticipated values of the parameter when convergence has been reached. If the first step does not cause Y to change sign, either the step size is increased or its direction reversed, depending on the current derivative. This process is continued until either Y changes sign, an impossible solution is reached (for example, negative mass of an element) or it can be demonstrated that no answer exists.

Saturation States of Minerals

The saturation state of a mineral in a given solution determines its interactions with that solution. In SOLMINEQ.88, two saturation indices are used to test for possible dissolution or precipitation of minerals. The program computes the Gibbs free energy difference (ΔG_{diff}) between the actual and equilibrium states of a mineral in a given subsurface water (equal to the chemical affinity A) as well as the saturation index SI given by:

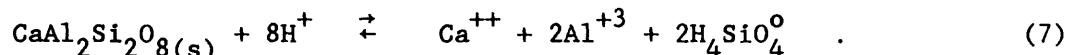
$$SI = \ln(Q/K) \quad . \quad (13)$$

ΔG_{diff} is given by:

$$\Delta G_{\text{diff}} = -RT \ln K - (-RT \ln Q) = RT \ln(Q/K) \quad , \quad (14)$$

where R is the gas constant, T is temperature in degrees Kelvin, Q is the reaction quotient (equal to the ion activity product (AP)), and K is the equilibrium constant at the specified temperature and pressure.

Mineral reactions used in SOLMINEQ.88 are for complete hydrolysis (Table 3); no incongruent reactions which require additional assumptions (e.g., conserving Al) are used. For anorthite, the reaction is



The reaction quotient (Q) for reaction (7) is given by:

$$Q_{\text{anorthite}} = \frac{a_{\text{Ca}^{++}} \cdot a_{\text{Al}^{+3}}^2 \cdot a_{\text{H}_4\text{SiO}_4^0}^2}{a_{\text{H}^+}^8 \cdot a_{\text{anorthite}}} \quad , \quad (15)$$

where (a) is the activity of the subscripted species at the specified temperature and pressure; $a_{\text{anorthite}}$ is the activity of anorthite. With the exception of minerals entered using the unknown mineral option, the activity of all minerals is assumed to be equal to 1.0 at any temperature and pressure.

At equilibrium, $Q = K$ and $\Delta G_{\text{diff}} = 0$. In this case, the subsurface water is in equilibrium with the mineral and no dissolution or precipitation should take place. Where $\Delta G_{\text{diff}} < 0$, anorthite cannot precipitate from that subsurface water because of undersaturation, but anorthite probably will dissolve if the mineral is present in the reservoir rocks. Where $\Delta G_{\text{diff}} > 0$, anorthite will not dissolve because of supersaturation, but rather will likely precipitate if kinetic factors allow.

Table 3. -- Reactions for the congruent dissolution of minerals
and sources of thermochemical data

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
1 Adularia	$\text{KAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{K}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	7a
2 Akermanite	$\text{Ca}_2\text{MgSi}_2\text{O}_7 + 6\text{H}^+ + \text{H}_2\text{O} \rightleftharpoons 2\text{Ca}^{++} + \text{Mg}^{++} + 2\text{H}_4\text{SiO}_4^0$	5b, 61b
3 Albite	$\text{NaAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{Na}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	5b, 61b
4 Albite, Low	$\text{NaAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{Na}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	5b, 61b
5 Albite, High	$\text{NaAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{Na}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	5b, 61b
6 Alunite	$\text{KAl}_3(\text{SO}_4)_2(\text{OH})_6 + 6\text{H}^+ \rightleftharpoons \text{K}^+ + 3\text{Al}^{+3} + 2\text{SO}_4^{--} + 6\text{H}_2\text{O}$	5b, 6b, 62b
7 Amesite, 14A	$\text{Mg}_2\text{Al}_2\text{SiO}_5(\text{OH})_4 + 10\text{H}^+ \rightleftharpoons 2\text{Mg}^{++} + 2\text{Al}^{+3} + \text{H}_4\text{SiO}_4^0 + 5\text{H}_2\text{O}$	66a
8 Analcime	$\text{NaAlSi}_2\text{O}_6 \cdot \text{H}_2\text{O} + 4\text{H}^+ + \text{H}_2\text{O} \rightleftharpoons \text{Na}^+ + \text{Al}^{+3} + 2\text{H}_4\text{SiO}_4^0$	6b, 72b
9 Andalusite	$\text{Al}_2\text{SiO}_5 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + \text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	5b, 6b
10 Andesine	$\text{Ca}_{.4}\text{Na}_{.6}\text{Al}_{1.4}\text{Si}_{2.6}\text{O}_8 \rightleftharpoons .4\text{CaAl}_2\text{Si}_2\text{O}_8 + .6\text{NaAlSi}_3\text{O}_8$	2a
11 Anhydrite	$\text{CaSO}_4 \rightleftharpoons \text{Ca}^{++} + \text{SO}_4^{--}$	39b, 63b
12 Annite	$\text{KFe}_3\text{AlSi}_3\text{O}_{10}(\text{OH})_2 + 10\text{H}^+ \rightleftharpoons \text{K}^+ + 3\text{Fe}^{++} + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6b, 72b
13 Anorthite	$\text{CaAl}_2\text{Si}_2\text{O}_8 + 8\text{H}^+ \rightleftharpoons \text{Ca}^{++} + 2\text{Al}^{+3} + 2\text{H}_4\text{SiO}_4^0$	6b, 72b
14 Apatite, Cl	$\text{Ca}_5(\text{PO}_4)_3\text{Cl} \rightleftharpoons 5\text{Ca}^{++} + 3\text{PO}_4^{--3} + \text{Cl}^-$	7a
15 Apatite, F	$\text{Ca}_5(\text{PO}_4)_3\text{F} \rightleftharpoons 5\text{Ca}^{++} + 3\text{PO}_4^{--3} + \text{F}^-$	2b, 6b
16 Apatite, OH	$\text{Ca}_5(\text{PO}_4)_3\text{OH} \rightleftharpoons 5\text{Ca}^{++} + 3\text{PO}_4^{--3} + \text{OH}^-$	6b, 61b
17 Aragonite	$\text{CaCO}_3 \rightleftharpoons \text{Ca}^{++} + \text{CO}_3^{--}$	35a
18 Augite	$\text{CaAl}_2\text{SiO}_6 + 8\text{H}^+ \rightleftharpoons \text{Ca}^{++} + 2\text{Al}^{+3} + \text{H}_4\text{SiO}_4^0 + 2\text{H}_2\text{O}$	6b, 72b
19 Azurite	$\text{Cu}_3(\text{CO}_3)_2(\text{OH})_2 \rightleftharpoons 3\text{Cu}^{++} + 2\text{CO}_3^{--} + 2\text{OH}^-$	6b, 72b

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
20 Barite	$\text{BaSO}_4 \rightleftharpoons \text{Ba}^{++} + \text{SO}_4^{--}$	6b, 63b
21 Boehmite	$\text{AlO(OH)} + 3\text{H}^+ \rightleftharpoons \text{Al}^{+3} + 2\text{H}_2\text{O}$	6b, 62b
22 Brucite	$\text{Mg(OH)}_2 \rightleftharpoons \text{Mg}^{++} + 2\text{OH}^-$	6b, 61b
23 Bytownite	$\text{Ca}_{.8}\text{Na}_{.2}\text{Al}_{1.8}\text{Si}_{2.2}\text{O}_8 \rightleftharpoons$ $.8\text{CaAl}_2\text{Si}_2\text{O}_8 + .2\text{NaAlSi}_3\text{O}_8$	2a
24 Calcite	$\text{CaCO}_3 \rightleftharpoons \text{Ca}^{++} + \text{CO}_3^{--}$	35a
25 Celestite	$\text{SrSO}_4 \rightleftharpoons \text{Sr}^{++} + \text{SO}_4^{--}$	6b, 61b
26 Chalcedony	$\text{SiO}_2 + 2\text{H}_2\text{O} \rightleftharpoons \text{H}_4\text{SiO}_4^0$	5b, 6b
27 Chamosite, 7A	$\text{Fe}_2\text{Al}_2\text{SiO}_5(\text{OH})_4 + 10\text{H}^+ \rightleftharpoons$ $2\text{Fe}^{++} + 2\text{Al}^{+3} + \text{H}_4\text{SiO}_4^0 + 5\text{H}_2\text{O}$	66a
28 Chlorite, 7A	$\text{Mg}_5\text{Al}_2\text{Si}_3\text{O}_{10}(\text{OH})_8 + 16\text{H}^+ \rightleftharpoons$ $5\text{Mg}^{++} + 2\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0 + 6\text{H}_2\text{O}$	5b, 6b
29 Chlorite, 14A	$\text{Mg}_5\text{Al}_2\text{Si}_3\text{O}_{10}(\text{OH})_8 + 16\text{H}^+ \rightleftharpoons$ $5\text{Mg}^{++} + 2\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0 + 6\text{H}_2\text{O}$	5b, 6b
30 Chrysotile	$\text{Mg}_3\text{Si}_2\text{O}_5(\text{OH})_4 + 6\text{H}^+ \rightleftharpoons 3\text{Mg}^{++} + 2\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 61b
31 Clinoenstatite	$\text{MgSiO}_3 + 2\text{H}^+ + \text{H}_2\text{O} \rightleftharpoons \text{Mg}^{++} + \text{H}_4\text{SiO}_4^0$	6b, 61b
32 Clinoptilolite Sodium	$\text{Na}_2\text{Al}_2\text{Si}_{10}\text{O}_{24} \cdot 8\text{H}_2\text{O} + 8\text{H}^+ + 8\text{H}_2\text{O} \rightleftharpoons$ $2\text{Na}^+ + 2\text{Al}^{+3} + 10\text{H}_4\text{SiO}_4^0$	76a
33 Clinoptilolite, Potassium	$\text{K}_2\text{Al}_2\text{Si}_{10}\text{O}_{24} \cdot 8\text{H}_2\text{O} + 8\text{H}^+ + 8\text{H}_2\text{O} \rightleftharpoons$ $2\text{K}^+ + 2\text{Al}^{+3} + 10\text{H}_4\text{SiO}_4^0$	76a
34 Clinoptilolite, Calcium	$\text{CaAl}_2\text{Si}_{10}\text{O}_{24} \cdot 8\text{H}_2\text{O} + 8\text{H}^+ + 8\text{H}_2\text{O} \rightleftharpoons$ $\text{Ca}^{++} + 2\text{Al}^{+3} + 10\text{H}_4\text{SiO}_4^0$	76a
35 Clinoptilolite, Magnesium	$\text{MgAl}_2\text{Si}_{10}\text{O}_{24} \cdot 8\text{H}_2\text{O} + 8\text{H}^+ + 8\text{H}_2\text{O} \rightleftharpoons$ $\text{Mg}^{++} + 2\text{Al}^{+3} + 10\text{H}_4\text{SiO}_4^0$	76a
36 Corundum	$\text{Al}_2\text{O}_3 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + 3\text{H}_2\text{O}$	5b, 6b
37 Cristobalite, α	$\text{SiO}_2 + 2\text{H}_2\text{O} \rightleftharpoons \text{H}_4\text{SiO}_4^0$	67a

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
38 Cristobalite, β	$\text{SiO}_2 + 2\text{H}_2\text{O} \rightleftharpoons \text{H}_4\text{SiO}_4^0$	67a
39 Dickite	$\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + 2\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 61b
40 Diopside	$\text{CaMgSi}_2\text{O}_6 + 4\text{H}^+ + 2\text{H}_2\text{O} \rightleftharpoons \text{Ca}^{++} + \text{Mg}^{++} + 2\text{H}_4\text{SiO}_4^0$	6b, 61b
41 Dolomite	$\text{CaMg}(\text{CO}_3)_2 \rightleftharpoons \text{Ca}^{++} + \text{Mg}^{++} + 2\text{CO}_3^{--}$	5b, 6b
42 Dolomite (DSORD)	$\text{CaMg}(\text{CO}_3)_2 \rightleftharpoons \text{Ca}^{++} + \text{Mg}^{++} + 2\text{CO}_3^{--}$	5b, 6b
43 Enstatite	$\text{MgSiO}_3 + 2\text{H}^+ + \text{H}_2\text{O} \rightleftharpoons \text{Mg}^{++} + \text{H}_4\text{SiO}_4^0$	5b, 6b
44 Epidote	$\text{Ca}_2\text{FeAl}_2\text{Si}_3\text{O}_{12}(\text{OH}) + 13\text{H}^+ \rightleftharpoons 2\text{Ca}^{++} + \text{Fe}^{+3} + 2\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 72b
45 Fayalite	$\text{Fe}_2\text{SiO}_4 + 4\text{H}^+ \rightleftharpoons 2\text{Fe}^{++} + \text{H}_4\text{SiO}_4^0$	6b, 61b
46 Fluorite	$\text{CaF}_2 \rightleftharpoons \text{Ca}^{++} + 2\text{F}^-$	68a
47 Forsterite	$\text{Mg}_2\text{SiO}_4 + 4\text{H}^+ \rightleftharpoons 2\text{Mg}^{++} + \text{H}_4\text{SiO}_4^0$	6b, 61b
48 Gibbsite, Am	$\text{Al}(\text{OH})_3 \rightleftharpoons \text{Al}^{+3} + 3\text{OH}^-$	7a
49 Gibbsite	$\text{Al}(\text{OH})_3 \rightleftharpoons \text{Al}^{+3} + 3\text{OH}^-$	6b, 62b
50 Greenalite	$\text{Fe}_3\text{Si}_2\text{O}_5(\text{OH})_4 + 6\text{H}^+ \rightleftharpoons 3\text{Fe}^{++} + 2\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	66a
51 Gypsum	$\text{CaSO}_4 \cdot 2\text{H}_2\text{O} \rightleftharpoons \text{Ca}^{+2} + \text{SO}_4^{-2} + 2\text{H}_2\text{O}$	6b, 63b
52 Halite	$\text{NaCl} \rightleftharpoons \text{Na}^+ + \text{Cl}^-$	6b, 61b
53 Halloysite	$\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + 2\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 61b
54 Heulandite	$\text{CaAl}_2\text{Si}_7\text{O}_{18} \cdot 6\text{H}_2\text{O} + 8\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{Ca}^{++} + 2\text{Al}^{+3} + 7\text{H}_4\text{SiO}_4^0$	6b, 78b
55 Huntite	$\text{CaMg}_3(\text{CO}_3)_4 \rightleftharpoons \text{Ca}^{++} + 3\text{Mg}^{++} + 4\text{CO}_3^{--}$	5b, 6b
56 Hydromagnesite	$\text{Mg}_5(\text{CO}_3)_4(\text{OH})_2 \cdot 3\text{H}_2\text{O} \rightleftharpoons 5\text{Mg}^{++} + 4\text{CO}_3^{--} + 2\text{OH}^- + 3\text{H}_2\text{O}$	6b, 69b
57 Hydrophilite	$\text{CaCl}_2 \rightleftharpoons \text{Ca}^{++} + 2\text{Cl}^-$	5b, 61b
58 Illite	$\text{K}_{.6}\text{Mg}_{.25}\text{Al}_{2.3}\text{Si}_{3.5}\text{O}_{10}(\text{OH})_2 + 8\text{H}^+ + 2\text{H}_2\text{O} \rightleftharpoons .6\text{K}^+ + .25\text{Mg}^{++} + 2.3\text{Al}^{+3} + 3.5\text{H}_4\text{SiO}_4^0$	7a

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
59 Kaolinite	$\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + 2\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 72b
60 Kenyaite	$\text{NaSi}_{11}\text{O}_{20.5}(\text{OH})_4 \cdot 3\text{H}_2\text{O} + \text{H}^+ + 16.5\text{H}_2\text{O} \rightleftharpoons$ $\text{Na}^+ + 11\text{H}_4\text{SiO}_4^0$	7e
61 K-Feldspar	$\text{KAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{K}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6b, 72b
62 Kyanite	$\text{Al}_2\text{SiO}_5 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + \text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 61b
63 Labradorite	$\text{Ca}_{.6}\text{Na}_{.4}\text{Al}_{1.6}\text{Si}_{2.4}\text{O}_8 \rightleftharpoons$ $.6\text{CaAl}_2\text{Si}_2\text{O}_8 + .4\text{NaAlSi}_3\text{O}_8$	2a
64 Larnite	$\text{Ca}_2\text{SiO}_4 + 4\text{H}^+ \rightleftharpoons 2\text{Ca}^{++} + \text{H}_4\text{SiO}_4^0$	5b, 61b
65 Laumontite	$\text{CaAl}_2\text{Si}_4\text{O}_{12} \cdot 4\text{H}_2\text{O} + 8\text{H}^+ \rightleftharpoons$ $\text{Ca}^{++} + 2\text{Al}^{+3} + 4\text{H}_4\text{SiO}_4^0$	5b, 61b
66 Leucite	$\text{KAlSi}_2\text{O}_6 + 4\text{H}^+ + 2\text{H}_2\text{O} \rightleftharpoons$ $\text{K}^+ + \text{Al}^{+3} + 2\text{H}_4\text{SiO}_4^0$	5b, 61b
67 Lime	$\text{CaO} + 2\text{H}^+ \rightleftharpoons \text{Ca}^{++} + \text{H}_2\text{O}$	5b, 61b
68 Magadite	$\text{NaSi}_7\text{O}_{13}(\text{OH})_3 \cdot 3\text{H}_2\text{O} + \text{H}^+ + 9\text{H}_2\text{O} \rightleftharpoons$ $\text{Na}^+ + 7\text{H}_4\text{SiO}_4^0$	7e
69 Magnesio- ferrite	$\text{MgFe}_2\text{O}_4 + 8\text{H}^+ \rightleftharpoons \text{Mg}^{++} + 2\text{Fe}^{+3} + 4\text{H}_2\text{O}$	7a
70 Magnesite	$\text{MgCO}_3 \rightleftharpoons \text{Mg}^{++} + \text{CO}_3^{--}$	6b, 69b
71 Chloro- magnesite	$\text{MgCl}_2 \rightleftharpoons \text{Mg}^{++} + 2\text{Cl}^-$	7a
72 Marialite	$(\text{NaAlSi}_3\text{O}_8)_3 \cdot \text{NaCl} + 12\text{H}^+ + 12\text{H}_2\text{O} \rightleftharpoons$ $4\text{Na}^+ + 3\text{Al}^{+3} + \text{Cl}^- + 9\text{H}_4\text{SiO}_4^0$	7a, 74a
73 Merwinite	$\text{Ca}_3\text{MgSi}_2\text{O}_8 + 8\text{H}^+ \rightleftharpoons 3\text{Ca}^{++} + \text{Mg}^{++} + 2\text{H}_4\text{SiO}_4^0$	5b, 61b
74 Microcline	$\text{KAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons$ $\text{K}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6b, 72b
75 Meionite	$(\text{CaAl}_2\text{Si}_2\text{O}_8)_3 \cdot \text{CaCO}_3 + 24\text{H}^+ \rightleftharpoons$ $4\text{Ca}^{++} + 6\text{Al}^{+3} + \text{CO}_3^{--} + 6\text{H}_4\text{SiO}_4^0$	6b, 75b

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

ID # and Name	Reaction	References
76 Mirabilite	$\text{Na}_2\text{SO}_4 \cdot 10\text{H}_2\text{O} \rightleftharpoons 2\text{Na}^+ + \text{SO}_4^{--} + 10\text{H}_2\text{O}$	2b, 5b
77 Monticellite	$\text{CaMgSiO}_4 + 4\text{H}^+ \rightleftharpoons \text{Ca}^{++} + \text{Mg}^{++} + \text{H}_4\text{SiO}_4^0$	5b, 6b
78 Mordenite, Na	$\text{NaAlSi}_5\text{O}_{12} \cdot 3\text{H}_2\text{O} + 4\text{H}^+ + 5\text{H}_2\text{O} \rightleftharpoons$ $\text{Na}^+ + \text{Al}^{+3} + 5\text{H}_4\text{SiO}_4^0$	76a
79 Mordenite, K	$\text{KAlSi}_5\text{O}_{12} \cdot 3\text{H}_2\text{O} + 4\text{H}^+ + 5\text{H}_2\text{O} \rightleftharpoons$ $\text{K}^+ + \text{Al}^{+3} + 5\text{H}_4\text{SiO}_4^0$	76a
80 Muscovite	$\text{KAl}_3\text{Si}_3\text{O}_{10}(\text{OH})_2 + 10\text{H}^+ \rightleftharpoons$ $\text{K}^+ + 3\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6b, 61b
81 Nahcolite	$\text{NaHCO}_3 \rightleftharpoons \text{Na}^+ + \text{HCO}_3^-$	5b, 71b
82 Nathermite	$\text{Na}_2\text{CO}_3 \cdot \text{H}_2\text{O} \rightleftharpoons 2\text{Na}^+ + \text{CO}_3^{--} + \text{H}_2\text{O}$	2b
83 Natron	$\text{Na}_2\text{CO}_3 \cdot 10\text{H}_2\text{O} \rightleftharpoons 2\text{Na}^+ + \text{CO}_3^{--} + 10\text{H}_2\text{O}$	5b, 71b
84 Nepheline	$\text{NaAlSiO}_4 + 4\text{H}^+ \rightleftharpoons \text{Na}^+ + \text{Al}^{+3} + \text{H}_4\text{SiO}_4^0$	6b, 72a
85 Nesquehonite	$\text{MgCO}_3 \cdot 3\text{H}_2\text{O} \rightleftharpoons \text{Mg}^{++} + \text{CO}_3^{--} + 3\text{H}_2\text{O}$	6b, 72b
86 Nontronite, Na	$\text{Na}_{.33}\text{Fe}_2\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $0.33\text{Na}^+ + 2\text{Fe}^{+3} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
87 Nontronite, K	$\text{K}_{.33}\text{Fe}_2\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $0.33\text{K}^+ + 2\text{Fe}^{+3} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
88 Nontronite, H	$\text{H}_{.33}\text{Fe}_2\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 6.99\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $2\text{Fe}^{+3} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
89 Nontronite, Ca	$\text{Ca}_{.165}\text{Fe}_2\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $0.165\text{Ca}^{++} + 2\text{Fe}^{+3} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
90 Nontronite, Mg	$\text{Mg}_{.165}\text{Fe}_2\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $0.165\text{Mg}^{++} + 2\text{Fe}^{+3} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
91 Oldhamite	$\text{CaS} + \text{H}^+ \rightleftharpoons \text{Ca}^{++} + \text{HS}^-$	7b
92 Oligoclase	$\text{Ca}_{.2}\text{Na}_{.8}\text{Al}_{1.2}\text{Si}_{2.8}\text{O}_8 \rightleftharpoons$ $.2\text{CaAl}_2\text{Si}_2\text{O}_8 + .8\text{NaAlSi}_3\text{O}_8$	2a

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
93 Paragonite	$\text{NaAl}_3\text{Si}_3\text{O}_{10}(\text{OH})_2 + 10\text{H}^+ \rightleftharpoons \text{Na}^+ + 3\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6a, 75a
94 Pargasite	$\text{NaCa}_2\text{Mg}_4\text{Al}_3\text{Si}_6\text{O}_{22}(\text{OH})_2 + 22\text{H}^+ \rightleftharpoons \text{Na}^+ + 2\text{Ca}^{++} + 4\text{Mg}^{++} + 3\text{Al}^{+3} + 6\text{H}_4\text{SiO}_4^0$	6b, 72b
95 Periclase	$\text{MgO} + 2\text{H}^+ \rightleftharpoons \text{Mg}^{++} + \text{H}_2\text{O}$	5b, 61b
96 Phillipsite	$\text{Na}_{.5}\text{K}_{.5}\text{AlSi}_3\text{O}_8 \cdot \text{H}_2\text{O} + 4\text{H}^+ + 3\text{H}_2\text{O} \rightleftharpoons .5\text{Na}^+ + .5\text{K}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	7a
97 Phlogopite, OH	$\text{KMg}_3\text{AlSi}_3\text{O}_{10}(\text{OH})_2 + 10\text{H}^+ \rightleftharpoons \text{K}^+ + 3\text{Mg}^{++} + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6b, 72b
98 Fluor- phlogopite	$\text{KMg}_3\text{AlSi}_3\text{O}_{10}\text{F}_2 + 8\text{H}^+ + 2\text{H}_2\text{O} \rightleftharpoons \text{K}^+ + 3\text{Mg}^{++} + \text{Al}^{+3} + 2\text{F}^- + 3\text{H}_4\text{SiO}_4^0$	5b, 61b
99 Portlandite	$\text{Ca}(\text{OH})_2 \rightleftharpoons \text{Ca}^{++} + 2\text{OH}^-$	5b, 61b
100 Potassium Oxide	$\text{K}_2\text{O} + 2\text{H}^+ \rightleftharpoons 2\text{K}^+ + \text{H}_2\text{O}$	5b, 61b
101 Prehnite	$\text{Ca}_2\text{Al}_2\text{Si}_3\text{O}_{10}(\text{OH})_2 + 10\text{H}^+ \rightleftharpoons 2\text{Ca}^{++} + 2\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	6b, 72b
102 Pyrophyllite	$\text{Al}_2\text{Si}_4\text{O}_{10}(\text{OH})_2 + 6\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons 2\text{Al}^{+3} + 4\text{H}_4\text{SiO}_4^0$	6b, 72b
103 Quartz	$\text{SiO}_2 + 2\text{H}_2\text{O} \rightleftharpoons \text{H}_4\text{SiO}_4^0$	70a
104 Sanidine, High	$\text{KAlSi}_3\text{O}_8 + 4\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons \text{K}^+ + \text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0$	5b, 61b
105 Saponite, Na	$\text{Na}_{.33}\text{Mg}_3\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons 0.33\text{Na}^+ + 3\text{Mg}^{++} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
106 Saponite, K	$\text{K}_{.33}\text{Mg}_3\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons 0.33\text{K}^+ + 3\text{Mg}^{++} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
107 Saponite, H	$\text{H}_{.33}\text{Mg}_3\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 6.99\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons 3\text{Mg}^{++} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
108 Saponite, Ca	$\text{Ca}_{.165}\text{Mg}_3\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $0.165\text{Ca}^{++} + 3\text{Mg}^{++} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
109 Saponite, Mg	$\text{Mg}_3.165\text{Al}_{.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $0.165\text{Mg}^{++} + 3\text{Mg}^{++} + 0.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	66a
110 Sepiolite	$\text{Mg}_4\text{Si}_6\text{O}_{15}(\text{OH})_2 \cdot 6\text{H}_2\text{O} + 8\text{H}^+ + \text{H}_2\text{O} \rightleftharpoons$ $4\text{Mg}^{++} + 6\text{H}_4\text{SiO}_4^0$	72a, 77a
111 Silica, Amorphous	$\text{SiO}_2 + 2\text{H}_2\text{O} \rightleftharpoons \text{H}_4\text{SiO}_4^0$	70a
112 Silica Gel	$\text{SiO}_2 + 2\text{H}_2\text{O} \rightleftharpoons \text{H}_4\text{SiO}_4^0$	7a
113 Sillimanite	$\text{Al}_2\text{SiO}_5 + 6\text{H}^+ \rightleftharpoons 2\text{Al}^{+3} + \text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 72b
114 Smectite, Ca	$\text{Ca}_{.167}\text{Al}_{2.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $.167\text{Ca}^{++} + 2.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	7a
115 Smectite, K	$\text{K}_{.33}\text{Al}_{2.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $.33\text{K}^+ + 2.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	7a
116 Smectite, Mg	$\text{Mg}_{.167}\text{Al}_{2.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $.167\text{Mg}^{++} + 2.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	7a
117 Smectite, Na	$\text{Na}_{.33}\text{Al}_{2.33}\text{Si}_{3.67}\text{O}_{10}(\text{OH})_2 + 7.32\text{H}^+ + 2.68\text{H}_2\text{O} \rightleftharpoons$ $.33\text{Na}^+ + 2.33\text{Al}^{+3} + 3.67\text{H}_4\text{SiO}_4^0$	7a
118 Sodium Monoxide	$\text{Na}_2\text{O} + 2\text{H}^+ \rightleftharpoons 2\text{Na}^+ + \text{H}_2\text{O}$	5b, 61b
119 Spinel	$\text{MgAl}_2\text{O}_4 + 8\text{H}^+ \rightleftharpoons \text{Mg}^{++} + 2\text{Al}^{+3} + 4\text{H}_2\text{O}$	5b, 61b
120 Stilbite	$\text{CaAl}_2\text{Si}_7\text{O}_{18} \cdot 7\text{H}_2\text{O} + 8\text{H}^+ + 3\text{H}_2\text{O} \rightleftharpoons$ $\text{Ca}^{++} + 2\text{Al}^{+3} + 7\text{H}_4\text{SiO}_4^0$	6b, 78b
121 Strengite	$\text{FePO}_4 \cdot 2\text{H}_2\text{O} \rightleftharpoons \text{Fe}^{+3} + \text{PO}_4^{-3} + 2\text{H}_2\text{O}$	7a
122 Strontianite	$\text{SrCO}_3 \rightleftharpoons \text{Sr}^{++} + \text{CO}_3^{-}$	40a
123 Sylvite	$\text{KCl} \rightleftharpoons \text{K}^+ + \text{Cl}^-$	6a, 61a
124 Talc	$\text{Mg}_3\text{Si}_4\text{O}_{10}(\text{OH})_2 + 6\text{H}^+ + 4\text{H}_2\text{O} \rightleftharpoons$ $3\text{Mg}^{++} + 4\text{H}_4\text{SiO}_4^0$	6a, 72b, 75b

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
125 Thenardite	$\text{Na}_2\text{SO}_4 \rightleftharpoons 2\text{Na}^+ + \text{SO}_4^{--}$	5b, 61b
126 Tremolite	$\text{Ca}_2\text{Mg}_5\text{Si}_8\text{O}_{22}(\text{OH})_2 + 14\text{H}^+ + 8\text{H}_2\text{O} \rightleftharpoons 2\text{Ca}^{++} + 5\text{Mg}^{++} + 8\text{H}_4\text{SiO}_4^0$	6b, 72b
127 Trona	$\text{Na}_2\text{CO}_3\text{NaHCO}_3 \cdot 2\text{H}_2\text{O} \rightleftharpoons 3\text{Na}^+ + \text{CO}_3^{--} + \text{HCO}_3^- + 2\text{H}_2\text{O}$	6b, 71b
128 Vivianite	$\text{Fe}_3(\text{PO}_4)_2 \cdot 8\text{H}_2\text{O} \rightleftharpoons 3\text{Fe}^{++} + 2\text{PO}_4^{--3} + 8\text{H}_2\text{O}$	7a
129 Wairakite	$\text{CaAl}_2\text{Si}_4\text{O}_{12} \cdot 2\text{H}_2\text{O} + 8\text{H}^+ + 2\text{H}_2\text{O} \rightleftharpoons \text{Ca}^{++} + 2\text{Al}^{+3} + 4\text{H}_4\text{SiO}_4^0$	6b, 72b
130 Witherite	$\text{BaCO}_3 \rightleftharpoons \text{Ba}^{++} + \text{CO}_3^{--}$	6b, 61b
131 Wollastonite	$\text{CaSiO}_3 + 2\text{H}^+ + \text{H}_2\text{O} \rightleftharpoons \text{Ca}^{++} + \text{H}_4\text{SiO}_4^0$	6b, 72b
132 Zoisite	$\text{Ca}_2\text{Al}_3\text{Si}_3\text{O}_{12}(\text{OH}) + 13\text{H}^+ \rightleftharpoons 2\text{Ca}^{++} + 3\text{Al}^{+3} + 3\text{H}_4\text{SiO}_4^0 + \text{H}_2\text{O}$	6b, 72b
133 Silver	$\text{Ag} + \text{Fe}^{+3} \rightleftharpoons \text{Ag}^+ + \text{Fe}^{++}$	5b, 61b
134 Cerargyrite	$\text{AgCl} \rightleftharpoons \text{Ag}^+ + \text{Cl}^-$	11a
135 Acanthite	$\text{Ag}_2\text{S} + \text{H}^+ \rightleftharpoons 2\text{Ag}^+ + \text{HS}^-$	5b, 61b
136 Copper, Native	$\text{Cu} + \text{Fe}^{+3} \rightleftharpoons \text{Cu}^+ + \text{Fe}^{++}$	5b, 6b
137 Malachite	$\text{Cu}_2\text{CO}_3(\text{OH})_2 \rightleftharpoons 2\text{Cu}^{++} + \text{CO}_3^{--} + 2\text{OH}^-$	6b, 61b
138 Tenorite	$\text{CuO} + 2\text{H}^+ \rightleftharpoons \text{Cu}^{++} + \text{H}_2\text{O}$	6b, 61b
139 Cuprite	$\text{Cu}_2\text{O} + 2\text{H}^+ \rightleftharpoons 2\text{Cu}^+ + \text{H}_2\text{O}$	5b, 6b
140 Covellite	$\text{CuS} + \text{H}^+ \rightleftharpoons \text{Cu}^{++} + \text{HS}^-$	6b, 61b
141 Chalcocite	$\text{Cu}_2\text{S} + \text{H}^+ \rightleftharpoons 2\text{Cu}^+ + \text{HS}^-$	6b, 61b
142 Chalcopyrite	$\text{CuFeS}_2 + 2\text{H}^+ \rightleftharpoons \text{Cu}^{++} + \text{Fe}^{++} + 2\text{HS}^-$	65a
143 Bornite	$\text{Cu}_5\text{FeS}_4 + 4\text{H}^+ \rightleftharpoons 4\text{Cu}^+ + \text{Cu}^{++} + \text{Fe}^{++} + 4\text{HS}^-$	5b, 6b
144 Lawrencite	$\text{FeCl}_2 \rightleftharpoons \text{Fe}^{++} + 2\text{Cl}^-$	7b
145 Molysite	$\text{FeCl}_3 \rightleftharpoons \text{Fe}^{+3} + 3\text{Cl}^-$	7b
146 Siderite	$\text{FeCO}_3 \rightleftharpoons \text{Fe}^{++} + \text{CO}_3^{--}$	5b, 6b
147 Ferrous Oxide	$\text{FeO} + 2\text{H}^+ \rightleftharpoons \text{Fe}^{++} + \text{H}_2\text{O}$	5b, 6b
148 Hematite	$\text{Fe}_2\text{O}_3 + 6\text{H}^+ \rightleftharpoons 2\text{Fe}^{+3} + 3\text{H}_2\text{O}$	5b, 6b

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
149 Maghemite	$\text{Fe}_2\text{O}_3 + 6\text{H}^+ \rightleftharpoons 2\text{Fe}^{+3} + 3\text{H}_2\text{O}$	7a
150 Magnetite	$\text{Fe}_3\text{O}_4 + 8\text{H}^+ \rightleftharpoons 2\text{Fe}^{+3} + \text{Fe}^{++} + 4\text{H}_2\text{O}$	5b, 6b
151 $\text{Fe}(\text{OH})_3$	$\text{Fe}(\text{OH})_3 \rightleftharpoons \text{Fe}^{+3} + 3\text{OH}^-$	7a
152 Goethite	$\text{FeOOH} + 3\text{H}^+ \rightleftharpoons \text{Fe}^{+3} + 2\text{H}_2\text{O}$	5b, 6b
153 Pyrrhotite	$\text{FeS} + \text{H}^+ \rightleftharpoons \text{Fe}^{++} + \text{HS}^-$	6b, 72b
154 Troilite	$\text{FeS} + \text{H}^+ \rightleftharpoons \text{Fe}^{++} + \text{HS}^-$	5b, 6b
155 Pyrite	$\text{FeS}_2 + \text{H}_2\text{O} \rightleftharpoons \text{Fe}^{++} + 1.75\text{HS}^- + 0.25\text{SO}_4^{--} + 0.25\text{H}^+$	5b, 6b
156 Greigite	$\text{Fe}_3\text{S}_4 + 4\text{H}^+ \rightleftharpoons 2\text{Fe}^{+3} + \text{Fe}^{++} + 4\text{HS}^-$	7a
157 Mercury (L)	$\text{Hg} + 2\text{Fe}^{+3} \rightleftharpoons \text{Hg}^{++} + 2\text{Fe}^{++}$	2b, 5b
158 Mercurous Chloride	$\text{HgCl}_2 \rightleftharpoons \text{Hg}^{++} + 2\text{Cl}^-$	7a
159 Calomel	$\text{Hg}_2\text{Cl}_2 \rightleftharpoons \text{Hg}_2^{++} + 2\text{Cl}^-$	7a
160 Montroydite	$\text{HgO} + 2\text{H}^+ \rightleftharpoons \text{Hg}^{++} + \text{H}_2\text{O}$	6b, 61b
161 Cinnabar	$\text{HgS} + \text{H}^+ \rightleftharpoons \text{Hg}^{++} + \text{HS}^-$	6b, 61b
162 Cinnabar, Meta-	$\text{HgS} + \text{H}^+ \rightleftharpoons \text{Hg}^{++} + \text{HS}^-$	6b, 61b
163 Scacchite	$\text{MnCl}_2 \rightleftharpoons \text{Mn}^{++} + 2\text{Cl}^-$	5b, 61b
164 Rhodochrosite	$\text{MnCO}_3 \rightleftharpoons \text{Mn}^{++} + \text{CO}_3^{--}$	5b, 61b
165 Manganosite	$\text{MnO} + 2\text{H}^+ \rightleftharpoons \text{Mn}^{++} + \text{H}_2\text{O}$	5b, 6b
166 Pyrolusite	$\text{MnO}_2 + \text{Mn}^{++} + 4\text{H}^+ \rightleftharpoons 2\text{Mn}^{+3} + 2\text{H}_2\text{O}$	5b, 6b
167 Alabandite	$\text{MnS} + \text{H}^+ \rightleftharpoons \text{Mn}^{++} + \text{HS}^-$	5b, 61b
168 Cotunnite	$\text{PbCl}_2 \rightleftharpoons \text{Pb}^{++} + 2\text{Cl}^-$	5b, 61b
169 Cerussite	$\text{PbCO}_3 \rightleftharpoons \text{Pb}^{++} + \text{CO}_3^{--}$	5b, 6b
170 Litharge	$\text{PbO} + 2\text{H}^+ \rightleftharpoons \text{Pb}^{++} + \text{H}_2\text{O}$	72a
171 Massicot	$\text{PbO} + 2\text{H}^+ \rightleftharpoons \text{Pb}^{++} + \text{H}_2\text{O}$	5b, 61b
172 Galena	$\text{PbS} + \text{H}^+ \rightleftharpoons \text{Pb}^{++} + \text{HS}^-$	46a
173 Anglesite	$\text{PbSO}_4 \rightleftharpoons \text{Pb}^{++} + \text{SO}_4^{--}$	6b, 63a
174 Smithsonite	$\text{ZnCO}_3 \rightleftharpoons \text{Zn}^{++} + \text{CO}_3^{--}$	46a

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
175 Zincite	$\text{ZnO} + 2\text{H}^+ \rightleftharpoons \text{Zn}^{++} + \text{H}_2\text{O}$	46a
176 Sphalerite	$\text{ZnS} + \text{H}^+ \rightleftharpoons \text{Zn}^{++} + \text{HS}^-$	46a
177 Zincosite	$\text{ZnSO}_4 \rightleftharpoons \text{Zn}^{++} + \text{SO}_4^{--}$	5b, 61b
178 Rutherfordine	$\text{UO}_2\text{CO}_3 \rightleftharpoons \text{UO}_2^{++} + \text{CO}_3^{--}$	6b, 44b, 61b
179 Uramphite	$(\text{NH}_4)_2(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $2\text{NH}_4^+ + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	2b, 45b, 61b
180 Przhevalskite	$\text{Pb}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Pb}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 7b, 44b
181 Torbernite	$\text{Cu}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Cu}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 45b, 61b
182 Saleeite	$\text{Mg}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Mg}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 45b, 74b
183 Autunite, Sr	$\text{Sr}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Sr}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 61b, 74b
184 Uranocircite	$\text{Ba}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Ba}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 45b, 61b
185 Bassetite	$\text{Fe}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Fe}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 44b, 45b
186 Clarkeite	$\text{UO}_3 + 2\text{H}^+ \rightleftharpoons \text{UO}_2^{++} + \text{H}_2\text{O}$	43b
187 Gummite	$\text{UO}_3 + 2\text{H}^+ \rightleftharpoons \text{UO}_2^{++} + \text{H}_2\text{O}$	43b, 45b
188 $\text{UO}_2(\text{OH})_2$	$\text{UO}_2(\text{OH})_2 \rightleftharpoons \text{UO}_2^{++} + 2\text{OH}^-$	5b, 45b
189 $\text{UF}_4 \cdot 2.5\text{H}_2\text{O}$	$\text{UF}_4 \cdot 2.5\text{H}_2\text{O} \rightleftharpoons \text{U}^{+4} + 4\text{F}^- + 2.5\text{H}_2\text{O}$	5b, 43b, 61b
190 $\text{U}(\text{HPO}_4)_2 \cdot 4\text{H}_2\text{O}$	$\text{U}(\text{HPO}_4)_2 \cdot 4\text{H}_2\text{O} \rightleftharpoons \text{U}^{+4} + 2\text{HPO}_4^{--} + 4\text{H}_2\text{O}$	5b, 43b, 61b
191 Ningyoite	$\text{CaU}(\text{HPO}_4)_2 \cdot 2\text{H}_2\text{O} + 2\text{H}^+ \rightleftharpoons$ $\text{Ca}^{++} + \text{U}^{+4} + 2\text{HPO}_4^{--} + 2\text{H}_2\text{O}$	5b, 45b, 61b
192 U_3O_8	$\text{U}_3\text{O}_8 + 4\text{H}^+ \rightleftharpoons \text{UO}_2^{++} + 2\text{UO}_2^+ + 2\text{H}_2\text{O}$	43b, 61b

Table 3. -- Congruent dissolution of minerals and sources
of thermochemical data -- (Continued)

<u>ID # and Name</u>	<u>Reaction</u>	<u>References</u>
193 Uraninite, Amorphous	$\text{UO}_2 + 4\text{H}^+ \rightleftharpoons \text{U}^{+4} + 2\text{H}_2\text{O}$	43b
194 Uraninite	$\text{UO}_2 + 4\text{H}^+ \rightleftharpoons \text{U}^{+4} + 2\text{H}_2\text{O}$	43b
195 U_4O_9	$\text{U}_4\text{O}_9 + 10\text{H}^+ \rightleftharpoons 2\text{U}^{+4} + 2\text{UO}_2^+ + 5\text{H}_2\text{O}$	43b, 61b
196 Coffinite	$\text{USiO}_4 + 4\text{H}^+ \rightleftharpoons \text{U}^{+4} + \text{H}_4\text{SiO}_4^0$	44b
197 Autunite, H	$\text{H}_2(\text{UO}_2)_2(\text{PO}_4)_2 \rightleftharpoons 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	44b
198 Autunite, Na	$\text{Na}_2(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $2\text{Na}^+ + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	2b, 61b
199 Autunite, K	$\text{K}_2(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $2\text{K}^+ + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 45b, 61b
200 Autunite	$\text{Ca}(\text{UO}_2)_2(\text{PO}_4)_2 + 2\text{H}^+ \rightleftharpoons$ $\text{Ca}^{++} + 2\text{UO}_2^{++} + 2\text{HPO}_4^{--}$	5b, 45b, 61b
201 Carnotite	$\text{K}_2(\text{UO}_2)_2(\text{VO}_4)_2 \rightleftharpoons 2\text{K}^+ + 2\text{UO}_2^{++} + 2\text{VO}_4^{-3}$	5b, 45b, 61b
202 Tyuyamunite	$\text{Ca}(\text{UO}_2)_2(\text{VO}_4)_2 \rightleftharpoons \text{Ca}^{++} + 2\text{UO}_2^{++} + 2\text{VO}_4^{-3}$	5b, 45b, 61b
203 Uranophane	$\text{Ca}(\text{UO}_2)_2(\text{HSiO}_4)_2 + 6\text{H}^+ \rightleftharpoons$ $\text{Ca}^{++} + 2\text{UO}_2^{++} + 2\text{H}_4\text{SiO}_4^0$	5b, 45b, 61b
204 Schoepite	$\text{UO}_2(\text{OH})_2 \cdot \text{H}_2\text{O} \rightleftharpoons \text{UO}_2^{++} + 2\text{OH}^- + \text{H}_2\text{O}$	43b, 61b
205 MgUO_4	$\text{MgUO}_4 + 4\text{H}^+ \rightleftharpoons \text{Mg}^{++} + \text{UO}_2^{++} + 2\text{H}_2\text{O}$	5b, 44b, 61b
206 CaUO_4	$\text{CaUO}_4 + 4\text{H}^+ \rightleftharpoons \text{Ca}^{++} + \text{UO}_2^{++} + 2\text{H}_2\text{O}$	5b, 44b, 61b
207 BaUO_4	$\text{BaUO}_4 + 4\text{H}^+ \rightleftharpoons \text{Ba}^{++} + \text{UO}_2^{++} + 2\text{H}_2\text{O}$	5b, 44b, 61b
208 UO_2F_2	$\text{UO}_2\text{F}_2 \rightleftharpoons \text{UO}_2^{++} + 2\text{F}^-$	5b, 44b, 61b
209 US_3	$\text{US}_3 + 2\text{H}_2\text{O} \rightleftharpoons \text{UO}_2^{++} + 3\text{HS}^- + \text{H}^+$	5b, 44b, 61b
210 Karelitanite	$\text{V}_2\text{O}_3 + 6\text{H}^+ \rightleftharpoons 2\text{V}^{+3} + 3\text{H}_2\text{O}$	2b, 45b
211 Vanadium Tetro-	$\text{V}_2\text{O}_4 + 4\text{H}^+ \rightleftharpoons 2\text{VO}^{++} + 2\text{H}_2\text{O}$	2b, 45b
212 Vanadium Pento-	$\text{V}_2\text{O}_5 + 3\text{H}_2\text{O} \rightleftharpoons 2\text{VO}_4^{-3} + 6\text{H}^+$	2b, 45b
213 $\text{VOSO}_4 \cdot 6\text{H}_2\text{O}$	$\text{VOSO}_4 \cdot 6\text{H}_2\text{O} \rightleftharpoons \text{VO}^{++} + \text{SO}_4^{--} + 6\text{H}_2\text{O}$	2b, 61b
214 $\text{Pb}_3(\text{VO}_4)_2$	$\text{Pb}_3(\text{VO}_4)_2 \rightleftharpoons 3\text{Pb}^{++} + 2\text{VO}_4^{-3}$	2b, 5b, 61b

Sources of Thermochemical Data for Reactions in Tables 2 and 3

- | | |
|--------------------------------------|--------------------------------------|
| 1) Plummer and Busenberg (1982) | 41) Ruaya and Seward (1986) |
| 2) Naumov and others (1974) | 42) Katayama (1976) |
| 3) Marshall and Frank (1981) | 43) Lemire and Tremaine (1980) |
| 4) Busey and Mesmer (1977) | 44) Hemingway (1982) |
| 5) Helgeson and others (1981) | 45) Langmuir (1978) |
| 6) Helgeson (1985 Version of SUPCRT) | 46) Bourcier and Barnes (1987) |
| 7) Kharaka and Barnes (1973) | 47) Tremaine and others (1981) |
| 8) Arnorsson and others (1982) | 48) Phillips (1982) |
| 9) Baes and Mesmer (1981) | 49) Martell and Smith (1977) |
| 10) May and others (1979) | 50) Nancollas (1956) |
| 11) Seward (1976) | 51) Palmer and Drummond (1988) |
| 12) Lown and others (1970) | 52) Wagman and others (1982) |
| 13) Jacobson and Langmuir (1974) | 53) Wagman and others (1976) |
| 14) Kalyanaraman and others (1973) | 54) Shanks and Bischoff (1977) |
| 15) Smith and Martell (1976) | 55) Giordano and Barnes (1981) |
| 16) Crerar and Barnes (1976) | 56) Wood and others (1987) |
| 17) Crerar and others (1978) | 57) Hogfeldt (1982) |
| 18) Wagman and others (1968; 1969) | 58) Roberson and Barnes (1978) |
| 19) Helgeson and others (1978) | 59) Bilinski and others (1986) |
| 20) Mesmer and others (1972) | 60) Daniele and others (1981) |
| 21) Helgeson (1969) | 61) Robie and others (1978) |
| 22) Bryzgalin and Rafelski (1982) | 62) Tremaine (1987) |
| 23) Barnes and others (1967) | 63) DeKock (1986) |
| 24) Smith and others (1986) | 64) Cobble and others (1982) |
| 25) Sillen and Martell (1964) | 65) Conard and others (1980) |
| 26) Siebert and Hostetler (1977) | 66) Wolery (1986) |
| 27) Wolley and Hepler (1977) | 67) Richet and others (1982) |
| 28) Kublanovskii (1977) | 68) Nordstrom and Jenne (1977) |
| 29) Harned and Owen (1958) | 69) Tanger and Helgeson (1988) |
| 30) Seward (1981) | 70) Fournier and Potter (1982) |
| 31) Drummond (1981) | 71) Vanderzee (1982) |
| 32) Lafon (1969) | 72) Tugarinov and others (1975) |
| 33) Reardon (1975) | 73) Hovey and others (1988) |
| 34) Lafon and Truesdell (1971) | 74) Zen (1972) |
| 35) Plummer and others (1984) | 75) Berman and others (1985) |
| 36) Seward (1984) | 76) Kerrisk (1983) |
| 37) Patterson and others (1982) | 77) Stoessell (1988) |
| 38) Giordano and Drummond (1987) | 78) Cho and others (1987) |
| 39) Møller (1988) | 79) Williams-Jones and Seward (1988) |
| 40) Busenberg and others (1984) | |

Letters following numerical references in Tables 2 and 3 refer to the method of computation used to calculate the equilibrium constants as described in the section, Equilibrium Constants.

ACTIVITY and ACTIVITY COEFFICIENTS

The activity of all minerals is assumed to be equal to unity, with the possible exception of the minerals entered using the unknown mineral option (see the description of the input file). The activity of water used in many equations is computed in SOLMINEQ.88 from the semiempirical expression given by Garrels and Christ (1965) as

$$a_{\text{H}_2\text{O}} = 1 - 0.017 \sum_i m_i \quad . \quad (16)$$

The summation covers the molalities (m_i) of all the species in solution.

Alternatively, a more accurate value for the activity of water can be obtained from the Pitzer expressions (Pitzer, 1973; 1981) where

$$\log (a_{\text{H}_2\text{O}}) = 0.007823 (\sum m_i) \phi \quad , \quad (17)$$

where ϕ is the osmotic coefficient of the solution. Values of ϕ are calculated by equations and parameters given by Pitzer (1973) and Pitzer (1981). Equations (16) and (17) give approximately the same value for the activity of water in NaCl solutions (0 - 6 molal) at temperatures of 25 °C to 200 °C; the activity of water is somewhat lower in CaCl_2 than in NaCl

solutions (see Table 6.2 in Kharaka and Mariner, 1989). The activity of water can be approximated for most natural waters using equation (16). Equation (17), however, should be used for waters where the concentrations of divalent cations comprise more than about 20 percent of the total cations.

The program uses equation (16), but the user can specify equation (17) by selecting the appropriate input switch. Values for the osmotic coefficients of NaCl, CaCl_2 and other electrolytes as a function of temperature and molality were obtained from Staples and Nuttall (1977), Holmes and others (1978, 1981) and Pitzer (1981).

The activities of aqueous species are computed from

$$a_i = m_i \gamma_i \quad , \quad (18)$$

where γ_i is the activity coefficient of species i . The standard state adopted for the aqueous species is that where the activity is equal to molality in a hypothetical infinitely dilute solution at any pressure and temperature.

Activity Coefficients for Neutral Species

Several methods are used by geochemists to calculate the activity coefficients of neutral species, each give different results. The activity coefficients of all neutral species are generally assumed equal to that of dissolved CO_2 in NaCl solutions (Helgeson, 1969). The activity coefficients for CO_2 (γ_{CO_2}) maybe calculated using:

$$\gamma_{\text{CO}_2}(T) = \frac{k_m}{k} \quad , \quad (19)$$

where k and k_m are the Henry's law coefficients (atm/mole) in pure water and sodium chloride solutions of molality m at temperature T ($^{\circ}\text{K}$). Values for k_m and k are available as a function of temperature (0° - 350°C) and molality of NaCl (0 - 6 molal) from Ellis and Golding (1963) and Drummond (1981). SOLMINEQ.88 has the option to compute γ_{CO_2} and all the other neutral species (except H_2S and H_4SiO_4) using a modified expression from Drummond (1981):

$$\begin{aligned} \ln k_{\text{CO}_2} = & 21.2752 - 0.0176036T - 1.0312m - \frac{3885.6}{T} + \frac{0.4445}{(m-1)} \\ & + 0.0012806 mT + \frac{255.9m}{T} - \frac{0.001606 T}{(m-1)} \quad . \end{aligned} \quad (20)$$

The activity coefficient for H_2S can be calculated from a similar expression, also modified from Drummond (1981) which is:

$$\begin{aligned} \ln k_{\text{H}_2\text{S}} = & 11.1255 - 0.0071704T + 0.2905T - \frac{2021.5}{T} + \frac{0.5705}{(m-1)} \\ & - 0.0001574mT - \frac{46.2m}{T} - \frac{0.001777T}{(m-1)} \quad . \end{aligned} \quad (21)$$

In both equations (20) and (21), m is the molality of NaCl.

The expressions of Marshall (1980) and Chen and Marshall (1982) are preferred for calculating the activity coefficient of H_4SiO_4^0 . Their activity coefficients for H_4SiO_4^0 were derived from data on the solubility of amorphous silica as a function of temperature (0° - 350°C), and NaCl salinity (0 - 6 molal). The expression is:

$$\log (\gamma_{\text{H}_4\text{SiO}_4^0}) = (0.00978 \times 10^{(280/T)}) \times m \quad . \quad (22)$$

Sodium and chloride are by far the dominant aqueous species in most formation waters from sedimentary basins (Kharaka and others, 1985), and equation (22) can be applied directly to these waters. However, the concentrations of other species, especially calcium, can be high, requiring modification of equation (22). Data in Marshall (1980) and Chen and Marshall (1982) show that equation (22) can be generalized to:

$$\log (\gamma_{\text{H}_4\text{SiO}_4^0}) = (0.00489 \times 10^{(280/T)}) \cdot \sum_i z_i^2 m_i \quad , \quad (23)$$

where z_i and m_i are the charge and molality of species (i). The summation includes all of the species in the formation water.

Activity Coefficients for Charged Species

In SOLMINEQ.88, the activity coefficients (γ) for the charged aqueous species are computed using B^* method (Lewis and Randall, 1961; Helgeson, 1969).

$$\log \gamma_i = \frac{-A_\gamma z_i^2 I^{1/2}}{1 + a_i^0 B_\gamma I^{1/2}} + B^* I \quad , \quad (24)$$

where a_i^0 is the ion size parameter, A_γ and B_γ are the molal Debye-Hückel coefficients (described below) at temperature T, z_i is the charge of the ith ion, I is the true ionic strength, and B^* is a deviation function. The ionic strength (I) of a given solution is given by:

$$I = 1/2 \sum_i n_i z_i^2 \quad . \quad (25)$$

The Debye-Hückel coefficients, A_γ and B_γ , are given by:

$$A_\gamma(T) = \frac{1.8248 \times 10^6 \rho^{1/2}}{(\epsilon T)^{3/2}} \quad , \quad (26)$$

and

$$B_\gamma(T) = \frac{50.29 \times 10^8 \rho^{1/2}}{(\epsilon T)^{1/2}} \quad , \quad (27)$$

where ρ and ϵ are the density and the dielectric constant of water at temperature T . The values of A_γ and B_γ in the above equations are given in Table 4 and are from Helgeson and others (1981). The density and dielectric constants are corrected for pressure using functions based on data in Helgeson and Kirkham (1974).

The a_i^0 values used (Appendix IA) are mainly from Kielland (1937), with unpublished data for U and V species from Goodwin (1982). Arbitrary a^0 values of 4.0, 5.0 and 6.0 were assigned, respectively, to those monovalent, divalent and trivalent species not reported in the literature; for U and V species, values of 4.5, 3.5, 2.5, 5.0 and 9.0 were assigned respectively to -2, -1, +1, +2, and +3 charged species as suggested by Goodwin (1982).

The values for the deviation function, B° , used in equation (24) vary as a function of temperature (Appendix ID) and are from Helgeson (1969). The B° values used are for NaCl solutions, a close approximation for most subsurface waters. The presence of appreciable amounts of divalent and trivalent cations and anions in solution with their higher degree of hydration will make the γ_i obtained lower than the true values. The B° option should not be used for waters with ionic strengths higher than about one molal. In these cases the Pitzer equations, as discussed in the following section, should be selected in the input file.

Table 4. Values of the Debye-Huckel coefficients
 A_γ and B_γ along the vapor pressure curve of water
(Helgeson and others, 1981).

t (°C)	A_γ ($\text{kg}^{1/2} \text{mole}^{-1/2}$)	B_γ ($\text{kg}^{1/2} \text{mole}^{-1} \text{cm}^{-1} \times 10^8$)
0	0.4913	0.3247
10	0.4976	0.3261
20	0.5050	0.3276
30	0.5135	0.3291
40	0.5231	0.3307
50	0.5336	0.3325
60	0.5450	0.3343
70	0.5573	0.3362
80	0.5706	0.3381
90	0.5848	0.3401
100	0.5998	0.3422
125	0.6417	0.3476
150	0.6898	0.3533
200	0.8099	0.3655
250	0.9785	0.3792
300	1.2555	0.3965
350	1.9252	0.4256

Pitzer Equations

SOLMINEQ.88 has an option to compute the activity coefficients of the aqueous species using Pitzer equations (Pitzer, 1981; Harvie and others, 1984). This modification was necessary because the B^{*} method used for calculating the activity coefficients (Helgeson, 1969) gives results that are much lower than the true values for solutions with salinities higher than about one molal (Figure 1). Pitzer equations are based on an ion-interaction or virial-coefficient model where the effects of ion association are implicitly incorporated in stoichiometric activity coefficients calculated by virial expansion of the Debye-Hückel theory (Pitzer, 1973, 1981; Silvester and Pitzer, 1978). A number of investigations (Whitfield, 1975; Harvie and Weare, 1980; Harvie and others, 1984; Gueddari and others, 1983) have shown that the use of the Pitzer equations has resulted in accurate predictions of mineral sequences in very concentrated brines at low temperatures.

The basic equations for the activity coefficients of positively (M) and negatively (X) charged species in terms of second and third virial coefficients (Pitzer, 1973; Harvie and others, 1984) are given below.

$$\ln \gamma_M = z_M^2 F + \sum_{a=1}^{N_a} m_a (2B_{Ma} + ZC_{Ma}) + \sum_{c=1}^{N_c} m_c (2\Phi_{Mc} + \sum_{a=1}^{N_a} m_a \psi_{Mca})$$

$$+ \sum_{a=1}^{N_a-1} \sum_{a'=a+1}^{N_a} m_a m_{a'} \psi_{aa'M} + |z_M| \sum_{c=1}^{N_c} \sum_{a=1}^{N_a} m_c m_a C_{ca} \quad , \quad (28)$$

$$\ln \gamma_X = z_X^2 F + \sum_{c=1}^{N_c} m_c (2B_{cX} + ZC_{cX}) + \sum_{a=1}^{N_a} m_a (2\Phi_{Xa} + \sum_{c=1}^{N_c} m_c \psi_{Xac})$$

$$+ \sum_{c=1}^{N_c-1} \sum_{c'=c+1}^{N_c} m_c m_{c'} \psi_{cc'X} + |z_X| \sum_{c=1}^{N_c} \sum_{a=1}^{N_a} m_c m_a C_{ca} \quad , \quad (29)$$

where m_c and z_c are the molality and charge of cation c and N_c is the total number of cations. Similar definitions apply for anions (subscript a). The following terms are defined for use in the above equations:

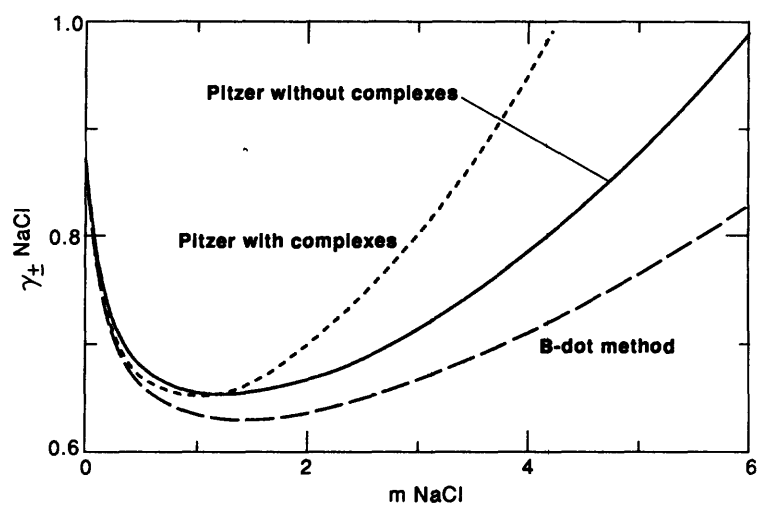


Figure 1. -- Pitzer and Ion Pair Activity Coefficients for NaCl solutions as a function of Ionic Strength.

$$F = -A^\phi \left[\frac{I^{1/2}}{1 + 1.2I^{1/2}} + \frac{2}{1.2} \ln(1 + 1.2I^{1/2}) \right] + \sum_{c=1}^{N_c} \sum_{a=1}^{N_a} m_c m_a B'_{ca} \\ + \sum_{c=1}^{N_c-1} \sum_{c'=c+1}^{N_c} m_c m_{c'} \Phi'_{cc'} + \sum_{a=1}^{N_a-1} \sum_{a'=a+1}^{N_a} m_a m_{a'} \Phi'_{aa'} \quad , \quad (30)$$

$$C_{MX} = C_{MX}^\phi / 2 |z_M z_X|^{1/2} \quad , \quad (31)$$

$$Z = \sum m_i |z_i| \quad , \quad (32)$$

and

$$A^\phi = \frac{2.303}{3.0} A_\gamma \quad , \quad (33)$$

where A_γ is the Debye-Huckel constant and I is the stoichiometric ionic strength. The second virial coefficients (B) and (Φ) are given the following ionic strength dependence:

$$B_{MX} = \beta_{MX}^{(0)} + \beta_{MX}^{(1)} g(\alpha_{MX} \sqrt{I}) + \beta_{MX}^{(2)} g(12\sqrt{I}) \quad , \quad (34)$$

$$B'_{MX} = \beta_{MX}^{(1)} g'(\alpha_{MX} \sqrt{I})/I + \beta_{MX}^{(2)} g'(12\sqrt{I})/I \quad , \quad (35)$$

$$\Phi_{ij} = \theta_{ij} + E_{\theta_{ij}}(I) \quad , \quad (36)$$

$$\Phi'_{ij} = E_{\theta'_{ij}}(I) \quad . \quad (37)$$

The functions, g and g' , are defined by the equations

$$g(x) = 2(1 - (1 + x)e^{-x})/x^2 \quad , \quad (38)$$

$$g'(x) = -2(1 - (1 + x + \frac{x^2}{2})e^{-x})/x^2 \quad , \quad (39)$$

where $x = \alpha_{MX} \sqrt{I}$ or $12 \sqrt{I}$. When either cation M or anion X is univalent,

$\alpha_{MX} = 2.0$. For 2 - 2, or higher valence pairs, $\alpha_{MX} = 1.4$. In most cases $\beta^{(2)}$ equals zero. The functions of $E_{\theta_{ij}}(I)$ and $E_{\theta'_{ij}}(I)$ account for the

electrostatic effects of unsymmetrical unmixing (Pitzer, 1981). They are only significant in complex 1-2 and 1-3 electrolytes at high ionic strength.

A relatively large and expanding database is now available to calculate the activities of alkali and alkaline earth metals in concentrated chloride and sulfate solutions at temperatures of up to at least 200 °C (Pitzer, 1981; Holmes and Mesmer, 1983; Pabalan and Pitzer, 1987; Møller, 1988; and many others).

The complete set of parameters required to calculate the activities of these species are: $\beta_{MX}^{(0)}$, $\beta_{MX}^{(1)}$, $\beta_{MX}^{(2)}$, and C_{MX}^{ϕ} for each cation-anion pair, θ_{ij} for each cation-cation and anion-anion pair; ψ_{ijk} for each cation-cation-anion and anion-anion-cation triplet. The interaction parameters for seven cations and four anions were calculated from various published data and are tabulated in the database of SOLMINEQ.88 (Appendix IG) at 25 °C intervals from 0° to 150 °C and at 50 °C intervals from 150 ° to 350 °C. The parameters are interpolated to the specified temperature (from 0° to 350 °C) by the Lagrange subroutine (TLUV) used to interpolate the K values (see below).

SOLMINEQ.88 has an option to compute the activity coefficients of the seven cations and four anions using Pitzer equations. It must be emphasized here that these equations are based on an ion interaction model that assumes no ion associations or complexing. The distribution of species in SOLMINEQ.88, on the other hand, is based on an ion association model. This inconsistency is resolved by incrementing the ion activity coefficients obtained from the Pitzer equations for these species so the final activity for the species is equal to that computed from Pitzer equations. In the case of Na, for example, the final value for γ_{Na^+} , is given by

$$\gamma_{Na^+} = \frac{m_{Na,t} \cdot \gamma_{Na,P}}{m_{Na^+}}, \quad (40)$$

where $\gamma_{Na,P}$ is the activity coefficient for Na obtained from the Pitzer equations. The activity coefficients for a large number of species and complexes in SOLMINEQ.88 can not be computed using Pitzer's equations because there are no published virial coefficients for them, especially at high temperatures. The activity coefficients for these species (γ_i) are calculated using a modified (B') equation given by:

$$\log \gamma_i = \frac{-z_i^2 A_\gamma I^{1/2}}{1 + a_i^o B_\gamma I^{1/2}} + B^*_i I \quad , \quad (41)$$

where B^* is a deviation function. The value of B^* used to calculate the activity coefficients for univalent cations, anions, and complexes (B_u^*) is obtained from:

$$B_u^* = \frac{1}{I} \left(\log \gamma_{Na^+} + \frac{A_\gamma I^{1/2}}{1 + 4.0 \times 10^{-8} B_\gamma I^{1/2}} \right) \quad , \quad (42)$$

where γ_{Na^+} is obtained for a hypothetical minor concentration of Na^+ equal to 0.01 m using Pitzer equations. The value of B_m^* used to calculate the activity coefficients for multivalent cations, anions and complexes with no virial coefficients data to calculate their activities by Pitzer equations is obtained from:

$$B_m^* = \frac{1}{I} \left(\log \gamma_{Ca^{++}} + \frac{4.0 A_\gamma I^{1/2}}{1 + 6.0 \times 10^{-8} B_\gamma I^{1/2}} \right) \quad , \quad (43)$$

where $\gamma_{Ca^{++}}$ is again obtained using Pitzer equations for a hypothetical 0.01 m concentrations of Ca^{++} . Hypothetical 0.01 concentrations of Na^+ and Ca^{++} are used because at concentrations higher than about 0.1 m, γ_i is a function of concentration (Pitzer, 1981; Tanger and Helgeson, 1988).

Using Na^+ and Ca^{++} as the "typical minor or trace" species to calculate the activity coefficients for the majority of the dissolved species is clearly not thermodynamically rigorous, but is an operational approach. However, comparison of values of activity coefficients obtained by this approach and by Pitzer equations for a number of dissolved species shows that this approach allows the operational B^* method (Helgeson, 1969) to be extended to about 3 to 6m solutions. Research to obtain virial coefficients for carbonate, aluminum and other important species is clearly needed.

EQUILIBRIUM CONSTANTS

The equilibrium constants (K) for the dissociation of aqueous complexes (Table 2) and congruent dissolution of minerals (Table 3) are the most important part of the database in geochemical codes such as SOLMINEQ.88. Examples of dissociation reactions (Reactions 1 and 2) and the corresponding equations (1 and 2) are given in an earlier section; the corresponding equation for the dissolution of anorthite reaction (7) is:

$$K_{an} = \frac{\bar{a}_{Ca^{++}} \cdot \bar{a}_{Al^{+3}}^2 \cdot \bar{a}_{H_4SiO_4^0}^2}{\bar{a}_{an} \cdot \bar{a}_{H^+}^8}, \quad (44)$$

where \bar{a}_i is the activity of the *i*th species at equilibrium. The equilibrium constants for the reactions shown in Tables 2 and 3 are in a data file labeled DATA.TBL. The K(T) values reported (Appendix IB and IC) at intervals of 25 °C from 0-150 °C and at intervals of 50 °C from 150°-350 °C were computed assuming a total pressure equal to the vapor pressure of water. (The correction for pressure is described in a following section.)

The equilibrium constants were obtained from references listed in Table 2 and by the methods described below, which are listed in decreasing order of reliability. The uncertainties in the computed equilibrium constants are generally higher for the aqueous species especially at temperatures higher than about 150 °C because their heat capacities can not be accurately estimated. In the case of minerals, if heat capacity functions are not available, they can be estimated from those of their oxides (Helgeson, 1969; Berman and others, 1985).

(a) Reported experimental data (solubility, free energy, and other data) or reported K values as a function of temperature over the temperature range of 25° to at least 200 °C. The values were extrapolated and interpolated to the temperature values used in this code.

(b) Computed using KELYCOB (Helgeson, 1971a) and SUPCRT (Helgeson, 1985), which computes the equilibrium constants of a given reaction ($\log K_r$) as a function of temperature and pressure. Generally the input to these programs for solids are the coefficients A, B, and C for the Maier-Kelley heat capacity power function (Kelly, 1960) given below

$$C_p = A + BT + \frac{C}{T^2}, \quad (45)$$

the standard state enthalpies of formation (H_f°), and the standard state entropies (S_i°) of all the components involved in the reaction. KELYCOB computes the $K(T)$ values from an integrated form of Van't Hoff's equation (Helgeson, 1969),

$$\begin{aligned} \log K(T) = & \log K_{298.15} - \frac{H_r^\circ}{2.303R} \left(\frac{1}{T} - \frac{1}{298.15} \right) \\ & - \frac{1}{2.303RT} \int_{298.15}^T \Delta C_{p,r}^\circ(T) dT \\ & + \frac{1}{2.303R} \int_{298.15}^T \Delta C_{p,r}^\circ(T) d\ln T \end{aligned} \quad (46)$$

The heat capacity of the aqueous species Na^+ , K^+ , Li^+ , Ag^+ , NH_4^+ , Cu^+ , Mg^{+2} , Ca^{+2} , Sr^{+2} , Ba^{+2} , Pb^{+2} , Zn^{+2} , Cu^{+2} , Hg^{+2} , Fe^{+2} , Mn^{+2} , Fe^{+3} , Al^{+3} , F^- , Cl^- , OH^- , HS^- , HCO_3^- , SO_4^{-2} , $NaCl^\circ$, and SiO_2° can be described by this equation (Helgeson and others, 1981; Helgeson, 1985):

$$C_p = C_{1i} + \frac{C_{2i}T}{T - \theta_i} - w_i T_x \quad (47)$$

where C_{1i} , C_{2i} , θ_i and w_i are empirical constants derived separately for each aqueous species, i , and x is the derivative of the variation of the dielectric constant of water, ϵ , with temperature (Helgeson and others, 1981).

A program called IONK was created which performs the function of KELYCOB, but uses the coefficients in equation (45) or those in equation (47) as input. IONK was used when the coefficients C_{1i} , C_{2i} , θ_i , and w_i were available.

KELYCOB and IONK were used to generate $\log K$ values at 25 °C intervals from 0° to 350 °C for most of the solubility reactions reported on Appendix IC. A number of $\log K$ values for the dissociation reactions of aqueous complexes were also obtained by this method.

The heat capacity power function for many minerals reported in this program are not known. They were approximated by summing up the heat capacity power functions for the oxides. The expression

$$(7.11 + .0082 T) \text{ cal mole}^{-1} \text{ deg}^{-1} \quad ,$$

(structural water) was used to represent H₂O in these approximations (Helgeson and others, 1978). For several ions (i.e., those containing U, V, or P) heat capacity was represented by a constant. The solubility constants of minerals containing these elements are only reliable below 200 °C (Langmuir, 1978).

(c) Computed using DQUANT (Helgeson, 1971b). This program requires only that $\Delta H_r^\circ(T_r)$ and $\Delta S_r^\circ(T_r)$ be known; it was used where no heat capacity data of any kind are available for one or more of the species involved in the reaction. This last condition covers many of the aqueous reactions reported in Table 2. DQUANT computes K(T) values by evaluating (Helgeson, 1967)

$$\log K(T) = \frac{\Delta S_r^\circ(T_r)}{2.303RT} \left[T_r - \frac{\theta}{W} (1 - \exp(\exp(b + aT) - c + \frac{(T - T_r)}{\theta})) \right] - \frac{\Delta H_r^\circ(T_r)}{2.303RT} \quad (48)$$

where θ , W, a, b, and c are temperature-independent constants characteristic of the solvent, and R is the gas constant.

DQUANT assumes that $\Delta C_{p,r}^\circ$ changes monotonically but nonlinearly with temperature. Dissociation constants computed from this program are often much closer approximations of actual dissociation constants at higher temperatures than those computed assuming $\Delta C_{p,r}^\circ(T) = 0$ or $\Delta C_{p,r}^\circ(T) = \text{a constant}$ (Helgeson, 1969). K(T) values obtained with DQUANT are reasonable approximations only to about 150 °C.

A correction factor was applied to some of the K(T) values generated with DQUANT at temperatures higher than 150 °C. These factors were generated either graphically by comparison with the K(T) values of similar complexes or by generating $\Delta C_{p,r}^\circ$ using K(T) values from 0° to 150 °C, then using them in equation (46). Even with the application of these correction factors, the errors involved in the values of K(T) at temperatures higher than 200 °C are large; this introduces large uncertainties in computations carried out with SOLMINEQ.88 at these high temperatures.

(d) Values for K are available at two or more generally low temperatures. Values for ΔH_r° and ΔS_r° are derived from this data using two equations of the form:

$$\frac{\log K(T)}{2.303RT} = \frac{\Delta H_r^0}{R} - T \frac{\Delta S_r^0}{R}, \quad (49)$$

and solving for ΔH_r^0 and ΔS_r^0 algebraically. This method was used only when ΔC_p^0 could not be derived from available data. Values for K at higher temperatures were calculated using Equation (48).

(e) Entropy was estimated by Arnorsson and others (1982) using correlation plots of the known entropies of ions as a function of molecular weight. Enthalpy was then calculated from the stability constant using Equation (49).

(f) A value for K is available only at 25 °C; it was extrapolated using the assumption that the curve of log K as a function of temperature is parallel to that of a similar species.

(g) A value for K is available only at 25 °C; it was extrapolated using Bryzgalin's method (Bryzgalin and Rafal'skiy, 1982):

$$-\log K(T) = \frac{298}{T} (-\log K(298)) + \frac{72600}{aT} \left(\frac{1}{\epsilon} - 0.0128 \right), \quad (50)$$

where

$$Z = Lz_C z_A - Qz_A^2 + \frac{pz_C^2 L}{2a^3} - \left[\frac{pz_C}{a^3} \right]^2 \frac{Q}{2}, \quad (51)$$

and

$$Q = \frac{3L^2 - 5L + 2}{8}, \quad (52)$$

ϵ is the dielectric constant of water, a is the sum of the Goldschmidt radii of the simple ions from which the ion complex is formed, z_A , and z_C are the charge of the anion and cation, respectively, L is the number of ligands (PbCl_3 has three ligands), and p is polarizability. Where p was not known it was assumed to be zero.

Equilibrium Constants at Desired Temperature

Values of log K for aqueous complexes and minerals at the desired temperature are interpolated from data in Appendix 1 by the subroutine TLUV. The interpolation of the log K values uses the cubic function:

$$Y = a + bX + cX^2 + dX^3, \quad (53)$$

where X is the independent variable (temperature at which K values are listed), Y is the dependent variable (log K values at the listed and specified sample temperature), and a, b, c, and d are constants. This subroutine calculates interpolated log K values between the reported intervals (25 °C from 0-150 °C and 50 °C from 150-350 °C) that are in good agreement with the original values.

Equilibrium Constants at Desired Pressure

The equilibrium constants (K) tabulated in SOLMINEQ.88 are computed at the vapor pressure of water. SOLMINEQ.88 has an option to compute the solubility of minerals at a specified pressure using data tabulated in Appendix 1E. The pressure dependence of the equilibrium constant is given by

$$\left(\frac{\partial \ln K}{\partial P} \right)_T = \frac{-\Delta V_r^0}{RT}, \quad (54)$$

where ΔV_r^0 is the volume change of the reaction in the standard state. Values of ΔV_r^0 at higher temperatures and pressures for the dissolution reactions of minerals can be obtained from the data of Helgeson and others (1978, 1981) and Robie and others (1978). However, ΔV_r^0 values at higher T and P for the dissociation reactions of most of the aqueous complexes are not available and, therefore, Equation (54) cannot be used to calculate K values at higher pressures for these complexes.

Correction of the solubility constants for pressure

Changes in the partial molal volume of aqueous species (\bar{V}) and water with pressure are the main contributors to the volume change in dissolution reactions (ΔV_r^0); minerals are assumed to be incompressible (Helgeson and others, 1981). Data on the molal volume of water were obtained from Helgeson and Kirkham (1974). Values for the partial molal volumes of aqueous species \bar{V}_i are sparse. They are calculated for the primary species using the data and equations reported in Helgeson and others (1981) and given by:

$$\bar{V}_i = a_{1i} + a_{2i}P + a_{3i}T + \frac{a_{4i}PT}{T - \theta_i} - w_iQ, \quad (55)$$

where a_{1i} is the intrinsic volume of species i which is independent of pressure and temperature; $w_i Q$ is the volume of solvation, the component of partial molal volume related to the orientation of water dipoles around the aqueous species. The remaining portion of Equation (55) is the volume of collapse, that is, the component of the partial molal volume related to the collapse of the water structure in the vicinity of the aqueous species. The constants a_{1i} , a_{2i} , a_{3i} , and a_{4i} are empirically derived; θ_i is a constant; P is in bars and T is in degrees K.

The pressure effect on the K values for minerals was estimated at 500 and 1,000 bars and temperatures of 100°, 150°, 200°, 300°, and 350 °C. The data were fit to a curve with the general formula

$$\log \left[\frac{K_p}{K} \right] = A + Bt + Ct^6 \quad , \quad (56)$$

where t is in °C, and the constants A , B and C were calculated for each solid phase at 500 and 1,000 bars. The term Ct^6 reflects the extreme changes in the partial molal volume (and therefore in K values) which occur above 300 °C. Values for the constants A , B and C for each mineral are listed in Appendix 1E.

The subroutine PCLOGK calculates solubility constants at selected pressure (P) below 500 bars using the following interpolation:

$$\log K_p = \log K + \frac{\Delta \log K_{500P}}{500} \quad , \quad (57)$$

and for pressures above 500 bars using:

$$\log K_p = \log K + \Delta \log K_{500} + \frac{(\Delta \log K_{1,000} - \Delta \log K_{500})(P - 500)}{500} \quad . \quad (58)$$

The pressure correction is significant when the pressure is several hundred bars or more, especially at temperatures above about 150 °C. For example, in Figure 2 it can be seen that at 1,000 bars the solubility product of anorthite is increased relative to saturation pressure of water by factors of about 30, 300 and 100,000,000, at 100°, 250° and 350 °C, respectively.

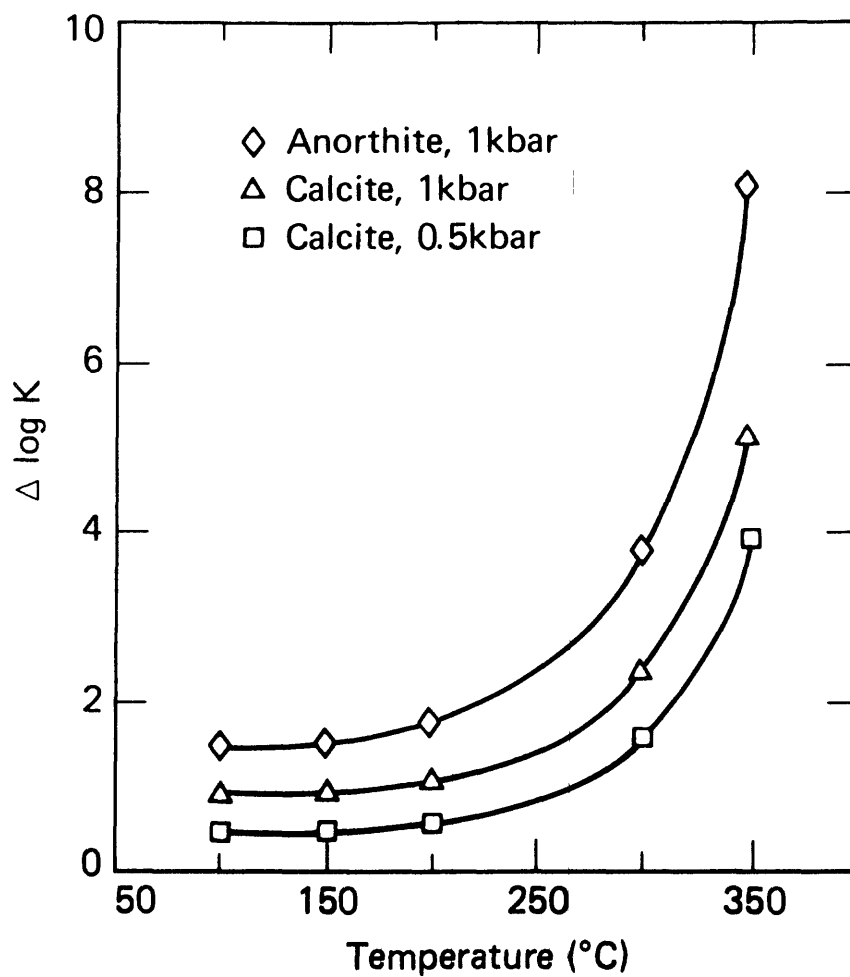


Figure 2. -- Effects of pressure on the solubilities of calcite and anorthite. Note that the difference between the solubilities of minerals at higher pressure and at vapor pressure of water ($\Delta \log K$) becomes very large at temperatures higher than about 200°C (Kharaka and others, 1985).

Correction of Dissociation Constants for Pressure

Values for the partial molal volume of most aqueous complexes are not available at high temperatures and pressures and, therefore, equation (54) can not be used to calculate K values at higher pressures. The pressure dependence of K for aqueous complexes in SOLMINEQ.88 is obtained by the method of Marshall and Mesmer (1981), in which K at pressure P is given by:

$$\ln K(P) = \ln K(S) - \frac{\Delta V(T)}{RT\beta} \ln \left(\frac{\rho(P)}{\rho(S)} \right), \quad (59)$$

where K(S) is the value of K at saturation water pressure and ρ is either the density of water at pressure (P) or at saturation vapor pressure of water (S); β is the coefficient of isothermal compressibility of water at temperature T; and $\Delta V(T)$ is the volume change of the dissociation reaction at temperature T and pressure S. It has been observed that the heat capacity and, by analogy, ΔV of "isocoulombic" reactions (reactions which are symmetrical with respect to the number of ions of each charge type) is nearly independent of temperature (Lindsay, 1980; Murray and Cobble, 1980). Thus, Equation (59) can be used with the 25 °C value of ΔV if the reaction is "isocoulombic", or is made so by the addition or subtraction of the dissociation reaction for water. For example, the dissociation reaction of the aqueous complex $H_2CO_3^0$:



can be written in the isocoulombic form as:



by combining reaction (8) with the ionization reaction of water



The equilibrium constant at higher pressures for (8) can be obtained from

$$\ln K_8(P) = \ln K_9(P) + \ln K_{10}(P), \quad (60)$$

and

$$\ln K_9(P)_T = \ln K_9(S)_T - \frac{n}{RT\beta} \ln \left(\frac{\rho(P)}{\rho(S)} \right), \quad (61)$$

where $n = \Delta V_8(S) - \Delta V_{10}(S)$ at 25 °C.

Values of $\Delta V_{10}(S)$ and of K_{10} at higher temperatures and pressures are well known and are incorporated in SOLMINEQ.88. Values of ΔV for dissociation

reactions even at 25 °C and saturation pressure are poorly known; however, they can be estimated from methods based on the electrostatic theory (Hemmes, 1972; Hemmes' method is based on the Fuoss (1958) equation), or empirical correlations (Millero, 1972; Swaddle and Mak, 1983). The ΔV values of dissociation reactions for 48 complexes used in SOLMINEQ.88 have been obtained either from available experimental data, or by estimation based on one of the above methods. They are tabulated in Appendix IF together with the number of water ionization reactions that must be added to convert the dissociation reaction or the complex to an "isocoulombic" form. The specific equations used to generate the data in Appendix IF and the original sources are detailed by Aggarwal and others (1989).

The dissociation constants generally increase with increasing pressures leading to an increase in the activity of the dissociated species and a decrease in the activity of the complexes. The increases are relatively high for the complexes of carbonate, bisulfide, ammonium and acetate species. The increase in the activity of dissociated species when the pressure effects are taken into account generally leads to reduced solubility products for minerals. In the case of calcite, for example, the increase in solubility shown in Figure 2 are reduced by more than a factor of 2 when the pressure effects on the dissociation of carbonate and calcium complexes are taken into account (see Aggarwal and others, 1989, for more details).

MODELING OPTIONS

SOLMINEQ.88 uses the chemical analysis of an aqueous fluid to calculate speciation-solubility relations at a given temperature and the vapor pressure of water or at a higher temperature and pressure with (1) a constant mass or with (2) a transfer of mass (Figure 3). The mass transfer options include:

- (a) addition of the gases, CO_2 , H_2S , NH_3 , CH_4 , which may have been lost prior to pH measurement,
- (b) partitioning of the gases CO_2 , H_2S , and CH_4 between water, oil and/or gas phases,
- (c) mixing with a second solution,
- (d) dissolution/precipitation of a given amount of a mineral; this may be continued to saturation with this or another mineral,
- (e) addition or subtraction of a given amount of one or more components of solution; this may be continued to saturation with a selected mineral,
- (f) boiling (formation of steam coupled with loss of volatiles into the steam), and
- (e) ion exchange and adsorption.

Calculations with a Constant Mass

The calculations with a constant mass can be carried out at a given temperature as well as at the subsurface (or experimental) temperature. These calculations can be performed with six options: (i) carbon; (ii) high-temperature carbon; (iii) pH; (iv) one or two additional (user defined) anions; (v) one additional cation; and (vi) one to five additional minerals.

Carbon Option

At a given pH, the distribution of carbonate species requires a value for any one of the following: (i) total inorganic carbon (TIC); (ii) bicarbonate and/or carbonate alkalinity (ALK); or (iii) total alkalinity (ALKTOT).

TIC, the sum of the concentrations of all aqueous species of inorganic carbon, is given as:

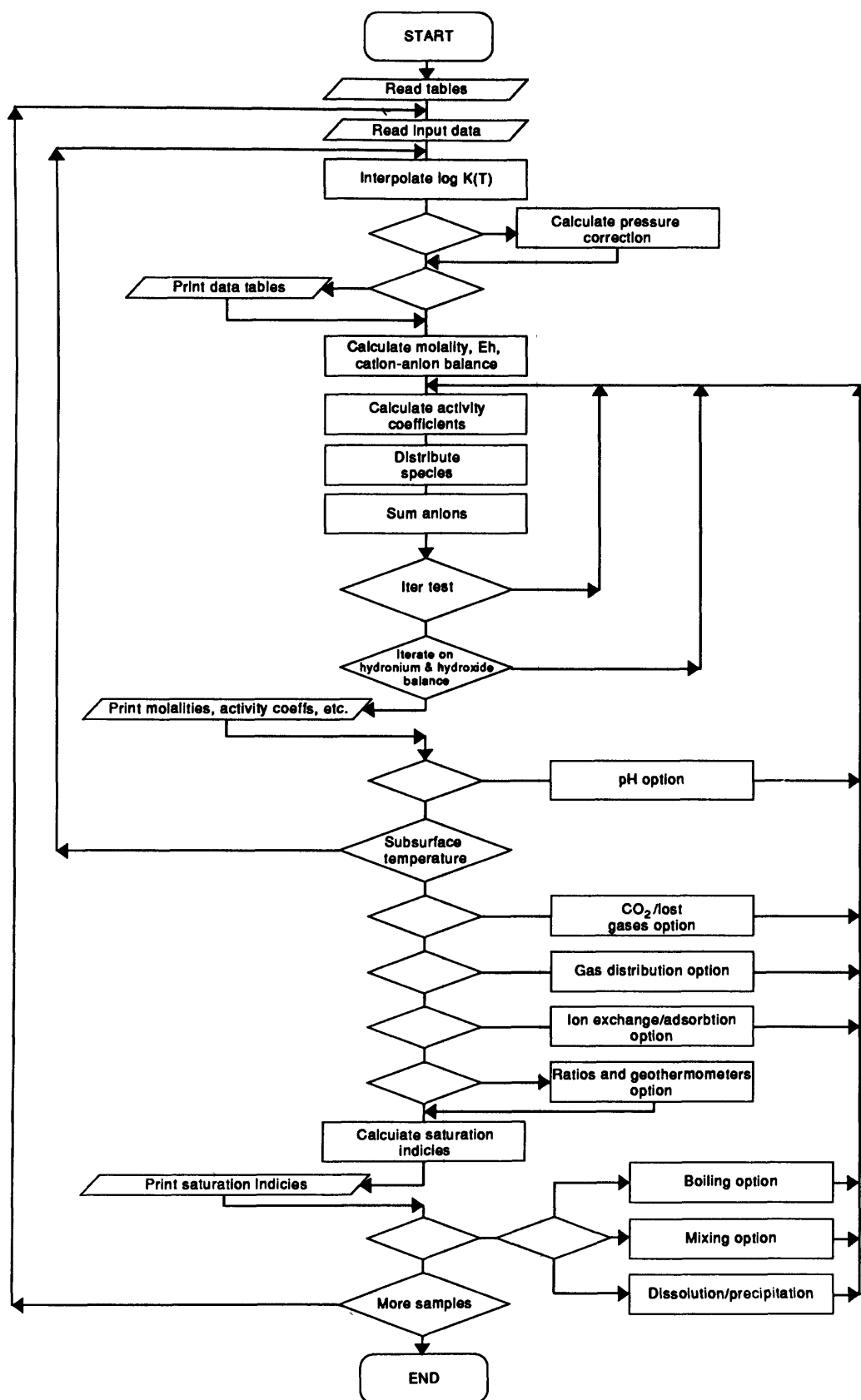


Figure 3. -- Flow Chart for SOLMINEQ.88

$$m_{TIC} = m_{H_2CO_3^0} + \sum m_{HCO_3^-} + \sum m_{CO_3^{--}}, \quad (62)$$

where the summation covers the species and complexes of the summed species.

ALK, the sum of the equivalents contributed to the alkalinity titration analysis by all the bicarbonate and carbonate species, is given as:

$$ALK = \sum m_{HCO_3^-} + \sum 2m_{CO_3^{--}}. \quad (63)$$

ALKTOT specifies that in addition to HCO_3^- and CO_3^{--} species, other inorganic and organic species (e.g., $Al(OH)_4^-$, $Ba(OH)^+$, CH_3COO^-) were also titrated during the alkalinity determination, and is given as:

$$ALKTOT = \sum m_{HCO_3^-} + \sum 2m_{CO_3^{--}} + \sum m_{CH_3COO^-} + m_{BaOH^+} + \dots \quad (64)$$

The carbon option in SOLMINEQ.88 is used to specify the criterion (TIC, ALK, or ALKTOT) for the distribution of carbonate species. The choice of any one of these criteria depends on the nature of the chemical analysis available. The other two are calculated and all three are printed in the output.

High-Temperature Carbon Option

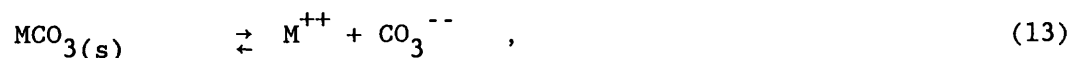
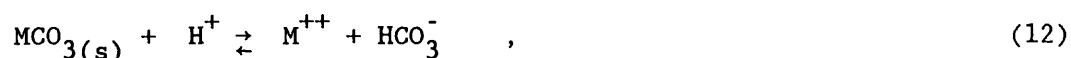
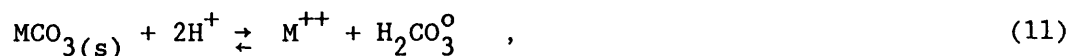
When a value for TIC is available, the distribution of carbonate species at a higher temperature is performed with a constant TIC. However, if a value for only ALK or ALKTOT is available, two alternatives exist for the distribution of carbonate species at high temperature: (a) constant alkalinity (ALK or ALKTOT) or (b) constant TIC. The value of TIC used at high temperature is calculated at the end of the low-temperature species distribution. If the high temperature calculations are carried out with a constant alkalinity, the resulting value of TIC in the solution may be significantly different from that at the low temperature because of the shift in carbonate equilibria with temperature. Similarly, a constant TIC at high temperature may result in a change in the value of calculated alkalinity.

pH Option

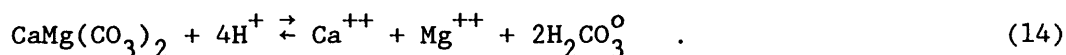
This option is most useful when the pH of the solution was not determined or may be in error, and the water is known to have been in equilibrium with a carbonate mineral. Formation water in reservoir rocks are often in equilibrium with calcite at depth; thus, this option can be used to calculate

the pH of this water. If it is known that the solution was in equilibrium with calcite, dolomite or siderite, then SOLMINEQ.88 will adjust the pH of the solution until $\log(AP/K)$ of the specified mineral is less than or equal to 0.05 (or to a value defined by the user = FSAT).

The equilibrium pH is guessed by SOLMINEQ.88, the distribution species is calculated, and the saturation index (SI) of the desired mineral is calculated. The SI is calculated in terms of the most abundant species of CO_2 , that is, the SI will be calculated according to one of the following reactions:



where $\text{MCO}_3(\text{s})$ is either of the carbonate minerals, calcite or siderite, and M is Ca^{++} or Fe^{++} , respectively. If saturation with dolomite is specified; reaction (11), for example, is written as



If the SI is not within the tolerance limit (0.05 log units or a value defined by the user), the pH is adjusted. The initial adjustment is determined through the use of reaction (11), (12), or (13). Subsequent adjustments increase either the size or direction of the pH step until the SI sign changes. Once this occurs, an interpolating polynomial in SI and pH is repeatedly used to obtain new values until the FSAT criterion is satisfied. Mineral saturation using the pH option is attempted within the pH limits of 0.0 and 14.0. The pH option is calculated after the initial distribution of species, and before the "HITEMP" calculation.

Additional Anions Option

SOLMINEQ.88 is particularly useful for modeling water-rock interactions in sedimentary basins where aqueous organic species may be present at high concentrations (up to 10,000 mg/L) (Figure 4) and can play an important role in these interactions. The total number of possible aqueous organic species is extremely large and it is not possible or even useful to incorporate all of them in this code. However, recent work (Carothers and Kharaka, 1978; Kharaka and others, 1986; Lundegard and Land, 1986; MacGowan and Surdam, 1988) has

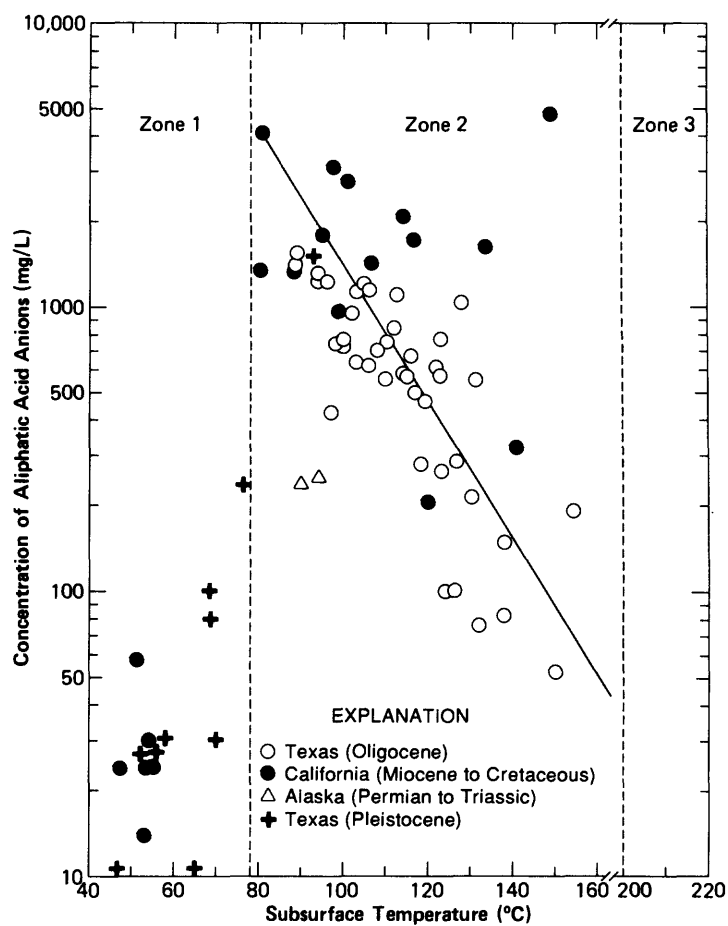
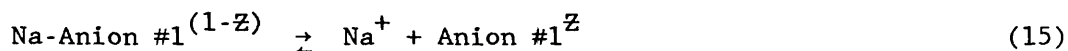


Figure 4. -- Distribution of organic species in oil field waters from United States of America. Note that the highest concentrations are in waters from reservoirs at temperatures of 80°C to 100°C.

shown that acetate, oxalate and succinate are the dominant organic species in oil field waters. These ligands and their complexes are incorporated in the code.

SOLMINEQ.88 has an option to add two user-defined organic ligands to the above three. This option is included because a total of five organic ligands is probably adequate to examine the role of organics on inorganic interactions in any natural-water system. The number of organic ligands examined can be increased as desired by making several runs of the program with the same input except for changing the list of the user-defined organic ligands in each run. This option has also been included because it is anticipated that potentially important new aqueous organics will be discovered in natural waters as better methods of sample preservation and analysis are used (Kharaka and others, 1986) and as more systems are studied.

The equations necessary for distribution of these user-defined ligands and their complexes with 14 inorganic cations are incorporated in SOLMINEQ.88. These ligands and their complexes are already included in the equations that compute titrated alkalinity and total hydronium. The ligands can have a charge of -1 to -4. Table 5 gives the identification number and the list of possible cations that may form complexes with these ligands. The dissociation constant for each complex must be supplied by the user. Otherwise, the complexes are treated as being unstable. In the case of Na-Anion #1, for example, the dissociation reaction, assuming Z charge for the ligand, is



The input subroutine to this code (see INPUT) prompts the user to provide the dissociation constants and other data necessary to implement this option.

Additional Cation Option

This option allows the user to study speciation-saturation states of one (during any one simulation) user-defined cation that is not in SOLMINEQ.88. As in the case of additional anions, all the equations necessary for the distribution of this cation and its complexes with all the anions (including the user defined anions) in the code are incorporated in SOLMINEQ.88. Again, the input subroutine to this code prompts the user to provide the dissociations constants and other data necessary to implement this option.

Table 5 Index numbers of user-defined anions and cations
and their complexes

1)	Anion#1	Anion#2	Cation
2)	H^+ - Anion#1	H^+ - Anion#2	Cation - Cl^-
3)	$2H^+$ - Anion#1	$2H^+$ - Anion#2	Cation - SO_4^{--}
4)	Al^{+3} - Anion#1	Al^{+3} - Anion#2	Cation - HCO_3^-
5)	Ba^{++} - Anion#1	Ba^{++} - Anion#2	Cation - OH^-
6)	Ca^{++} - Anion#1	Ca^{++} - Anion#2	Cation - PO_4^{-3}
7)	Cu^+ - Anion#1	Cu^+ - Anion#2	Cation - F^-
8)	Fe^{++} - Anion#1	Fe^{++} - Anion#2	Cation - CH_3COO^-
9)	K^+ - Anion#1	K^+ - Anion#2	Cation - CO_3^{--}
10)	Mg^{++} - Anion#1	Mg^{++} - Anion#2	Cation - HS^-
11)	Mn^{++} - Anion#1	Mn^{++} - Anion#2	Cation - $C_2O_4^{--}$
12)	Na^+ - Anion#1	Na^+ - Anion#2	Cation - $C_4H_4O_4^{--}$
13)	Pb^{++} - Anion#1	Pb^{++} - Anion#2	Cation - Anion#1
14)	Sr^{++} - Anion#1	Sr^{++} - Anion#2	Cation - Anion#2
15)	Zn^{++} - Anion#1	Zn^{++} - Anion#2	

Additional Minerals Option

SOLMINEQ.88 has 220 minerals in its data base. This number can be increased as this option allows the user to include up to five new minerals during any simulation. This option also can be used to input data for minerals present in the code in order to investigate the geochemical implications of using solubility constants that are different from those in the existing data base. This option should prove particularly useful in the study of the interactions of minerals with variable chemical composition (solid solutions). If the solubility constants for the end members are available in Appendix IC, the user can calculate the solubility of the impure phase assuming ideal mixing, then use the calculated values in the input for this option. The solubility constant for an ideal binary solid solution (K_1) is given by:

$$\log K_i = X \log K_1 + (1-X) \log K_2 + X \log X + (1-X) \log (1-X) \quad (65)$$

where K_1 and K_2 are the solubility constants for the end-member minerals and X and $(1-X)$ are the mole fractions of these end members in the phase. Most solid solutions, it should be noted, require a more rigorous treatment and additional parameters to calculate their solubility constants (Navrotsky, 1987).

The reactions for the congruent dissolution of optional minerals are completely general and may involve up to eight of the aqueous species in Table 6 together with a numerical constant. The numerical constant is included in the solubility reaction to simulate the effects of one or more aqueous species not present in Table 6 or in the user defined anions or cation. The input subroutine to SOLMINEQ.88 prompts the user to provide the solubility constants and the aqueous species and their stoichiometry to implement this option.

Calculations Involving Mass Transfer

Addition of Lost Gases

During sampling of subsurface fluids, volatiles (including CO_2 , H_2S , NH_3 , and CH_4) may be lost before the solution pH is measured. These gases can have a significant impact on the calculated, in-situ pH of the solution and must be included in the analyzed composition of the fluid. Three options are available in SOLMINEQ.88 which can be used for titrating the lost gases back into the solution (Figure 5): (a) gas-water option, (b) gas-water-oil option, and (c) CO_2 option.

(a) Gas-Water Option: this option is used when the amount of lost gases is known. The amount of a gas lost is added to the total concentration of its constituent component in the water and an equivalent amount is added to the summation of hydronium ions in the water as:

$$\text{TIC} = \text{TIC} + m_{\text{CO}_2} (\text{lost}) \quad (66)$$

$$m_{\text{H}_2\text{S},t} = m_{\text{H}_2\text{S},t} + m_{\text{H}_2\text{S}} (\text{lost}) \quad (67)$$

$$m_{\text{NH}_3,t} = m_{\text{NH}_3,t} + m_{\text{NH}_3} (\text{lost}) \quad (68)$$

and

$$\left(\sum m_{\text{H}^+}^f - \sum m_{\text{OH}^-}^f \right) = \left(\sum m_{\text{H}^+}^i - \sum m_{\text{OH}^-}^i \right) + 2m_{\text{CO}_2} + 2m_{\text{H}_2\text{S}} - m_{\text{NH}_3} \quad (69)$$

where the final (f) and initial (i) summations cover all the species with H^+ and OH^- . Methane, of course, does not affect the hydronium balance.

(b) Gas-Water-Oil Distribution Option: samples of oil-field waters for chemical analysis are generally collected after they have been separated from the oil phase. During the separation process, a gas phase (commonly containing CO_2 and CH_4 , but sometimes with H_2S) is also produced which may consist of gases derived from one or more of the three subsurface phases: oil, water, and natural gas. Because dissolved CO_2 gas has a significant impact on the in situ pH of the water, it is important to know the distribution of gas between the three phases in the in situ environment. The Gas-Water-Oil distribution option in SOLMINEQ.88 has been designed to perform such calculations. The necessary equations for equilibrium distribution of gases between oil (o),

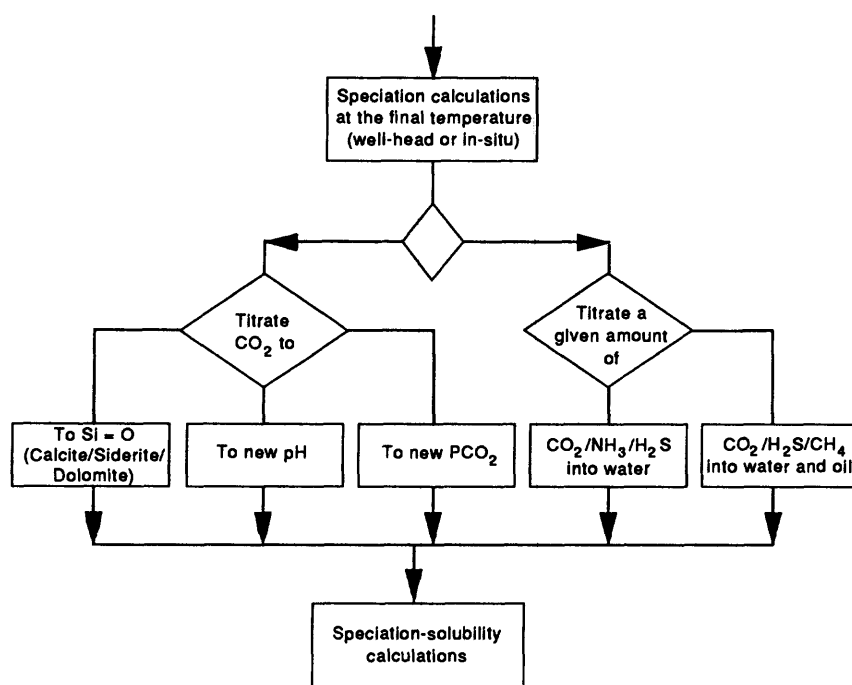


Figure 5. -- Flow chart for calculations with addition of gases to water and oil.

water (w), and natural gas (g) are as follows:

$$k_{\text{CO}_2, \text{w}} = \frac{P_{\text{CO}_2}}{m_{\text{CO}_2, \text{w}}} ; k_{\text{CH}_4, \text{w}} = \frac{P_{\text{CH}_4}}{m_{\text{CH}_4, \text{w}}} ; k_{\text{H}_2\text{S}, \text{w}} = \frac{P_{\text{H}_2\text{S}}}{m_{\text{H}_2\text{S}, \text{w}}} , \quad (70)$$

$$k_{\text{CO}_2, \text{o}} = \frac{P_{\text{CO}_2}}{m_{\text{CO}_2, \text{o}}} ; k_{\text{CH}_4, \text{o}} = \frac{P_{\text{CH}_4}}{m_{\text{CH}_4, \text{o}}} ; k_{\text{H}_2\text{S}, \text{o}} = \frac{P_{\text{H}_2\text{S}}}{m_{\text{H}_2\text{S}, \text{o}}} , \quad (71)$$

$$M_{\text{CO}_2, \text{t}} = C m_{\text{CO}_2, \text{o}} + m_{\text{CO}_2, \text{w}} + M_{\text{CO}_2, \text{g}} , \quad (72)$$

$$M_{\text{CH}_4, \text{t}} = C m_{\text{CH}_4, \text{o}} + m_{\text{CH}_4, \text{w}} + M_{\text{CH}_4, \text{g}} , \quad (73)$$

$$M_{\text{H}_2\text{S}, \text{t}} = C m_{\text{H}_2\text{S}, \text{o}} + m_{\text{H}_2\text{S}, \text{w}} + M_{\text{H}_2\text{S}, \text{g}} , \quad (74)$$

$$C = \frac{W_{\text{o}}}{W_{\text{w}}} , \quad (75)$$

$$\frac{M_{\text{CO}_2, \text{g}}}{P_{\text{CO}_2}} = \frac{M_{\text{CH}_4, \text{g}}}{P_{\text{CH}_4}} = \frac{M_{\text{H}_2\text{S}, \text{g}}}{P_{\text{H}_2\text{S}}} = \frac{M_{\text{H}_2\text{O}, \text{g}}}{P_{\text{H}_2\text{O}}} , \quad (76)$$

$$P_{\text{t}} = P_{\text{CH}_4} + P_{\text{CO}_2} + P_{\text{H}_2\text{S}} + P_{\text{H}_2\text{O}} , \quad (77)$$

where k is the Henry's law coefficient for the solubility of the subscripted gas in water or oil, m is the molality, M is total moles of a gas, C is the weight ratio of oil (W_{o}) to water (W_{w}), and P_{t} is the reservoir pressure.

Note that the Henry's law coefficients are expressed in the molality convention (moles of gas/Kg of water or oil) and not in the mole fraction convention (moles of gas/mole of fluid) because the term mole cannot be applied to oil which is a heterogeneous mixture of many compounds. The above equations are derived with the assumption that all gases (CO_2 , CH_4 , H_2S , H_2O), and their mixtures, behave as ideal gases (i.e., fugacity coefficients = 1).

The Henry's law constants for the water phase are calculated from Drummond's (1981) equations described in the section on the activity coefficients of neutral species. For the oil phase, the constants must be obtained and entered by the user. The user can calculate the Henry's law constants for oil (density range of 0.63 to 0.90 g/cm³) using the data (Figure 6) and equations summarized by ASTM (1985) and reported in Beerbower (1980). The density of oil at 15 °C (≈60 °F) in kg/L or its API gravity at 15 °C must be known by the user.

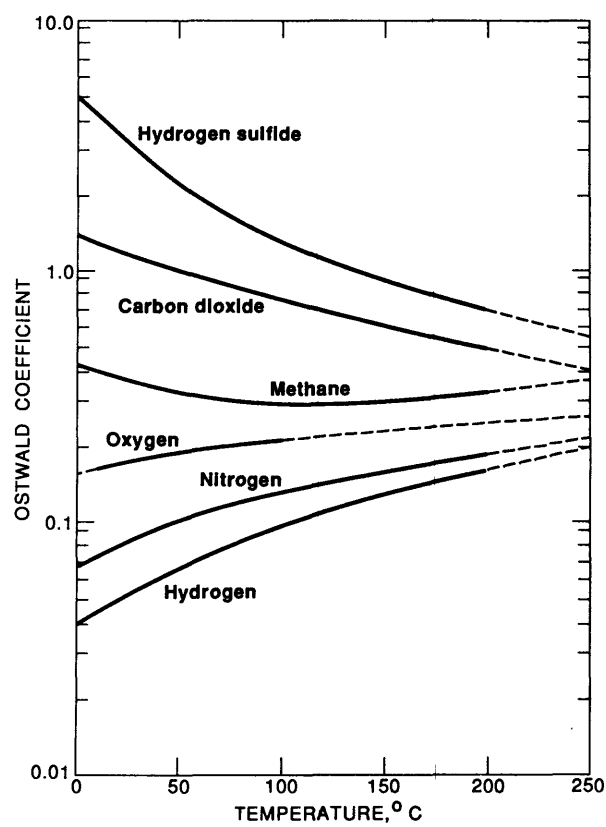


Figure 6. -- Solubility constants of selected gases in oil
(density = 0.85 g/ml at 15°C) modified from ASTM (1985)

Water samples are commonly collected from the test separator. If the separator pressure is greater than 1 atmosphere some dissolved gas will be lost during water sampling. To compensate for this, an additional SOLMINEQ.88 run must be made to equilibrate the water with the separator gas phase at the separator pressure by titrating CO_2 , H_2S and CH_4 back in. The concentrations of CO_2 , H_2S and CH_4 in the water must be calculated from equations (70-77). The CO_2 and H_2S options are then used to equilibrate the separator water at the separator pressure for the separator P_{CO_2} and $P_{\text{H}_2\text{S}}$. The user must then enter the modified $m_{\text{H}_2\text{S},w}$, $m_{\text{CH}_4,w}$, TIC and pH into SOLMINEQ.88, and activates the water-oil-gas distribution option which calculates the distribution of gases at reservoir pressure and temperature assuming that the gas phase in the separator was derived from only two phases, water and oil. If this assumption leads to the condition

$$P_{\text{CH}_4} + P_{\text{CO}_2} + P_{\text{H}_2\text{S}} + P_{\text{H}_2\text{O}} > P_t \quad , \quad (78)$$

then the third phase, vapor, is included in the distribution calculations. Once the pH and the distribution of the aqueous species are determined, SOLMINEQ.88 calculates the concentration of the volatiles in the water, oil, and vapor phases by simultaneously solving equations (70) to (77). At this point a check is made on the mass balance of the volatiles (including all their aqueous complexes). If not satisfied, the TIC, total H_2S and/or total CH_4 in the water are adjusted in the correct direction. A new pH and distribution of species is calculated. This cycle is repeated until mass balance is achieved.

(c) CO_2 Saturation Option: this option can be used for a variety of field and experimental conditions. In many cases, the amount of CO_2 lost from a subsurface fluid is not correctly known. However, it may be known that the fluid was in equilibrium with calcite, dolomite, or siderite. The CO_2 option can be used to determine the amount of CO_2 required to achieve saturation with the specified mineral and thus the subsurface pH of the solution. Another use of the CO_2 option is in the case of certain experiments where the amount of CO_2 exsolved between two pH measurements is not known; the CO_2 option can be used to determine the amount of CO_2 lost. A third use of the CO_2 option is in

calculating the pH and distribution of species in experimental solutions where the experiments were carried out at a constant P_{CO_2} . In some such cases, the pH of the solutions cannot be measured at the imposed pressure of CO_2 . However, it can be calculated using the CO_2 -option to achieve a specified P_{CO_2} or $m_{\text{H}_2\text{CO}_3}$ in solution.

The algorithm used for the CO_2 option is similar to that used in the pH option. The equilibrium test (FSAT) is formulated as one of the following relationships:

$$\text{FSAT} = \text{pH}_{(\text{desired})} - \text{pH}_{(\text{calculated})} \quad (79)$$

or

$$\text{FSAT} = m_{\text{H}_2\text{CO}_3}(\text{desired}) - m_{\text{H}_2\text{CO}_3}(\text{calculated}) \quad (80)$$

or

$$\text{FSAT} = P_{\text{CO}_2}(\text{desired}) - P_{\text{CO}_2}(\text{calculated}) \quad (81)$$

or

$$\text{FSAT} = \text{Saturation Index (SI) (calcite/siderite/dolomite)} \quad (82)$$

The saturation index of one of the carbonate minerals is calculated using the most abundant species of CO_2 , as discussed earlier in the pH option.

CO_2 is incremented, species distribution is recalculated and convergence is achieved in the aqueous model and on hydronium mass-balance. If the absolute value of FSAT is increasing, the step size or direction is modified such that the absolute value of FSAT decreases. Once the absolute value of FSAT is decreasing, step size is increased until FSAT changes sign. The value of FSAT and total CO_2 are then fit with a polynomial in order to interpolate to a new value of FSAT. This process is continued until FSAT is less than the user defined limit (default value = 0.05 log units).

Boiling Option

SOLMINEQ.88 may be used to predict the changes in solution composition and the saturation states of minerals as a consequence of boiling. There are two major effects of boiling:

1. Loss of steam.
2. Loss of gases such as CO_2 , H_2S , and NH_3 .

The loss of steam can be simulated by subtracting pure water of neutral pH from the solution. This is accomplished by multiplying the molality of each of the species and $(\Sigma m_{\text{H}^+} - \Sigma m_{\text{OH}^-})$ by the factor $1/(1 - X)$ where X is the fraction of water removed by boiling; and is given by

$$X = \frac{W_{\text{H}_2\text{O},v}}{W_{\text{H}_2\text{O},t}} = \frac{n_{\text{H}_2\text{O},v}}{n_{\text{H}_2\text{O},l} + n_{\text{H}_2\text{O},v}}, \quad (83)$$

where n = is the number of moles and W = the weight of water in the vapor (v), liquid (l), and total (t) system, respectively.

If the P-V-T relationships of all the gases are known, the amount of each gas lost due to boiling can be calculated. The partitioning of volatiles CO_2 , CH_4 , NH_3 , and H_2S is calculated following Drummond (1981) by making use of the volatility ratio, VR. For example, VR for CO_2 is calculated from:

$$\text{VR}_{\text{CO}_2} = \frac{55.51 k_H \bar{V}_{\text{H}_2\text{O}}^v}{x_{\text{CO}_2} Z_{\text{CO}_2} R T}, \quad (84)$$

where k_H is the Henry's Law constant given by $\frac{f_{\text{CO}_2}}{m_{\text{CO}_2}}$,

and $\bar{V}_{\text{H}_2\text{O}}^v$ is the specific volume of water vapor, and x and Z are the fugacity coefficient and compressibility factor of CO_2 , respectively. In the calculation, the product xZ is set equal to 1.0 which is a reasonable assumption at relatively low pressures. The VR is defined by:

$$VR_{CO_2} = \frac{n_{CO_2}^v}{n_{CO_2}^l} \cdot \frac{n_{H_2O}^l}{n_{H_2O}^v} = \frac{n_{CO_2}^v}{n_{CO_2}^l} \cdot \frac{(1-X)}{X}, \quad (85)$$

where n = number of moles of CO_2 or H_2O . Normalizing to 1000 grams of H_2O (i.e., assuming that 1,000 grams of H_2O are present in each of the liquid and vapor phases), equation (85) becomes:

$$VR = \frac{m_{CO_2}^v}{m_{CO_2}^l}, \quad (86)$$

where m is molality.

The boiling calculation is based on a system containing 1000 grams of water. Therefore the mass balance equation for CO_2 becomes

$$m_{CO_2}^{l,i} = n_{CO_2}^{l,i} = n_{CO_2}^l + n_{CO_2}^v, \quad (87)$$

where the superscript i refers to the molality or number of moles before any boiling occurs. For a given fraction of water, X , removed by boiling, equation (85) may be combined with equation (87) to give:

$$n_{CO_2}^v = \frac{m_{CO_2}^{l,i} VR_{CO_2}}{VR_{CO_2} + \frac{(1-X)}{X}}. \quad (88)$$

SOLMINEQ.88 solves for the partitioning of volatiles by estimating from equation (88) the amount lost to vapor. Because the effect of a change in pH is to increase or decrease the amount of $n_{CO_2}^l$ or $n_{NH_3}^l$ by reactions such as:



SOLMINEQ.88 then utilizes an iterative scheme by increasing or decreasing the total concentration of the volatile components in water (i.e. TIC); calculating the new pH and aqueous species distribution; and repartitioning the volatiles between vapor and liquid until the mass balance for volatiles in both phases (including all aqueous species) is achieved.

Mixing of Two Solutions Option

SOLMINEQ.88 has an option to mix two solutions in specified proportions (by weight) at constant or varying temperature. Mixing is performed based on analytical molalities. The mass-balance criteria for the mixture are formulated as follows:

$$\sum m_i (\text{mixture}) = X_1 \sum m_{i,1} + X_2 \sum m_{i,2} \quad , \quad (89)$$

$$(\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_{\text{mixture}} = X_1 (\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_1 + X_2 (\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_2 \quad , \quad (90)$$

where m_i is the analytical molality of the species of the i th element and X_1 and X_2 are the proportion of water (by weight) in which solutions 1 and 2 are to be mixed. The carbon mass-balance in the mixture is carried out using the TIC option.

Dissolution/Precipitation Option

The dissolution/precipitation option in SOLMINEQ.88 can be used to carry out the reactions listed below.

- 1-Dissolve/precipitate a given amount of mineral;
- 2-dissolve/precipitate a mineral to saturation;
- 3-dissolve/precipitate a mineral to saturation with an other mineral;
- 4-add/subtract aqueous components to saturation with a mineral; and
- 5-add/subtract components from a congruent, incongruent, or net reaction. Reaction may follow a kinetic rate law.

This option allows the user to titrate in (or out) a specified amount of aqueous components (see Table 6) (or of a titrant mineral) to (or from) the aqueous solution. The amount to be titrated may be specified by the user in moles of component per kilogram of solution. Alternatively, the amount may be determined by adding or subtracting the aqueous components (see Table 6) (or titrant mineral) until saturation is reached with any of the 214 minerals in the database of SOLMINEQ.88.

If a mineral is specified to be dissolved/precipitated, equilibration is achieved by dissolving (if the titrant mineral is undersaturated) or precipitating (if the titrant mineral is supersaturated) the titrant mineral. A series of reaction steps (i.e., moles of components or titrant mineral), initially based on the concentration of the least abundant component of the

Table 6 List of aqueous species components

No.	Species	No.	Species	No.	Species
1	Ca^{++}	2	Mg^{++}	3	Na^{+}
4	K^{+}	5	Cl^{-}	6	SO_4^{--}
7	HCO_3^{-}	8	H^{+}	9	OH^{-}
10	H_2O	12	$\text{SiO}_2(\text{aq})$	13	Ag^{+}
14	Al^{+3}	15	Ba^{++}	16	Cu^{+}
18	Fe^{++}	21	Hg^{++}	22	Li^{+}
23	Mn^{++}	25	Pb^{++}	26	Sr^{++}
27	Zn^{++}	28	$\text{H}_2\text{AsO}_3^{-}$	29	PO_4^{-3}
30	F^{-}	31	$\text{H}_3\text{BO}_3(\text{aq})$	32	$\text{NH}_3(\text{aq})$
33	$\text{H}_2\text{S}(\text{aq})$	48	$\text{CH}_3\text{COO}^{-}$	98	CO_3^{--}
136	NO_3^{-}	169	UO_2^{++}	210	VO_4^{-3}
246	$\text{C}_2\text{O}_4^{--}$	265	$\text{C}_4\text{H}_4\text{O}_4^{--}$	285	$\text{CH}_4(\text{aq})$

The species numbers in the input refer to the index number of selected species in the data file which are organized above. The species (with the exception of H^{+} and OH^{-}) are those normally entered in the input data file for SOLMINEQ.88, and are the only species allowed to be used in the dissolution/precipitation options and ion exchange/adsorption options. For the ion exchange/adsorption options, vacant surface site is assigned the number zero. Presently moles of H_2O is fixed in the program at 1 kilogram.

mineral to be saturated and its degree of departure from equilibrium (eg. saturation index, SI), are executed in order to find an interval where the SI changes its sign. An interpolating polynomial technique is then used to find the amount of mineral to be dissolved/precipitated for which SI is sufficiently close to zero.

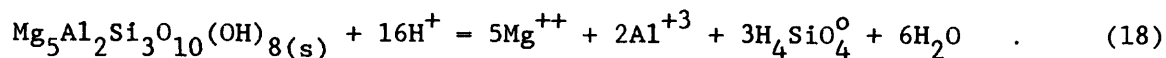
It is not always possible to achieve saturation with a mineral. Suppose the user wished to dissolve/precipitate gibbsite to reach saturation with kaolinite. If the SI of gibbsite is negative, it can only be dissolved. Dissolving gibbsite will increase the SI of kaolinite. If the SI of kaolinite is already positive, it will steadily increase as more gibbsite is dissolved into the aqueous phase. Clearly the SI of the kaolinite must be negative in order to reach a possible solution.

A mixture or solid which is not in the database can be titrated in and out by specifying its components (listed in Table 6). In this way a congruent or incongruent reaction can be followed. The reaction may be a simple one involving one or two minerals and aqueous components; or it may be the sum of several reactions (a net reaction) involving several minerals and aqueous components. The simple or net reaction may follow a rate law (user defined) which allows the knowledgeable user to compute changes in composition through time and/or space. The mass-balance criteria are formulated as:

$$\sum m_{i,t} = \sum (m_{i,\text{soln}} + A m_{i,j}) \quad , \quad (91)$$

$$(\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_t = (\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_{\text{soln}} + (\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_{\text{added}} \quad , \quad (92)$$

where m_i is the analytical molality of the species of the i^{th} element. $A m_{i,j}$ is the molality of the j^{th} species of i^{th} element to be added to the solution. To illustrate the use of this option for a congruent reaction of a mineral not in the database, let us consider the dissolution of one mole of clinocllore ($\text{Mg}_5\text{Al}_2\text{Si}_3\text{O}_{10}(\text{OH})_8(\text{s})$) according to the reaction:



For every mole of clinocllore dissolved, 5 moles of Mg, 2 moles of Al, and 3 moles of silica will be released and 16 moles of hydronium will be

consumed. The net hydronium balance of the solution will be decreased by only 4 moles of hydronium because H_4SiO_4^0 is included in the hydronium summation. Thus, the mixture would have the following constraints on the mass-balance that will be different from the original solution:

$$m_{\text{Al},t} = m_{\text{Al},\text{soln}} + 2 \quad , \quad (93)$$

$$m_{\text{Mg},t} = m_{\text{Mg},\text{soln}} + 5 \quad , \quad (94)$$

$$m_{\text{Si},t} = m_{\text{Si},\text{soln}} + 3 \quad , \quad (95)$$

$$(\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_t = (\sum m_{\text{H}^+} - \sum m_{\text{OH}^-})_{\text{soln}} - 4 \quad . \quad (96)$$

Note that the hydronium balance is decreased only by 4 because 12 of the 16 moles of hydronium lost will be added back by H_4SiO_4^0 .

If a mineral in the database is specified, SOLMINEQ.88 automatically determines the component stoichiometry to be added to the solution, saving time for the user.

Ion Exchange and Adsorption Option

Surface chemical processes can be simulated in SOLMINEQ.88 using two models: ion exchange and a preliminary adsorption option. The ion exchange model treats the exchange of cations or anions on a constant charge surface; the adsorption model simulates the exchange process on a surface where the surface charge is developed due to the ionization of surface sites at the solution-surface interface. The major distinction between the two models is in the treatment of the activity of aqueous species on the surface. In the ion-exchange model, the surface activity of aqueous species is considered to be the same as in the bulk solution. For the adsorption model, an electrical potential term is used to calculate the surface activity from the activity of the species in the bulk solution. Excellent discussions of the ion exchange and adsorption processes are given in several references (Hohl and others, 1980; Westall, 1980; Westall and Hohl, 1980; Bolt, 1982; James and Parks, 1982; Sposito, 1982) and the user should read these articles to understand the limitations inherent in modeling surface chemical processes and to obtain values for the selectivity constants to be used for modeling.

The ion exchange and adsorption models in SOLMINEQ.88 are completely general and can be used to simulate the interaction of any of the aqueous

species in the data file (Appendix IA) through the use of the appropriate components (Table 6). A maximum of 10 aqueous species (components) may be selected for each run to interact with a single surface of constant or varying charge. It is assumed that the activity coefficients of surface functional groups (X or SO⁻) and surface species (e.g. NaX or SONa) are equal to one. The ion exchange process, for example for a surface with no vacant sites and of constant charge exchanging with Na, Ca, and K, is given by the following reactions:



where X represents a surface site. These would be specified to SOLMINEQ.88 using the following three association reactions:



The cation exchange capacity (CEC) is the sum given by:

$$\text{CEC} = \text{NaX} + \text{KX} + 2\text{CaX}_2 \quad , \quad (97)$$

and is expressed in meq/kg of the solvent. The CEC is given by:

$$\text{CEC (meq/kg)} = \frac{A_T \cdot N_S \cdot 1000}{N_A} \quad , \quad (98)$$

where A_T is total area of the exchanging surface per kg of water, N_S is the number of sites per unit area of the surface, and N_A is Avogadro's number.

The equilibrium constants for reactions (21), (22), and (23) must sum to the equilibrium constants for reactions (19) and (20). They can be combined with equation (98) to solve for the concentration of surface and aqueous species by using an iterative technique similar to that used for the distribution of species.

The adsorption model in SOLMINEQ.88 is based on the Gouy-Chapman theory following Healy and White (1978) for the distribution of charge and potential at the solution-surface interface, which states that:

$$\sigma_o + \sigma_d = 0 \quad , \quad (99)$$

where σ is the charge density at the surface (o) or in the diffuse layer made up of coions and counterions (d). To illustrate the implementation of the Gouy-Chapman model, let us consider an amphoteric surface with ionizable

surface sites, SOH, in an NaCl solution. The intrinsic ionization of these sites is given as:



and the specific adsorption of ions as:



where the subscript "s" refers to the surface ions. The relation between the activities of ions in bulk solution and surface is given by

$$a_s = a_{aq} \exp(-z \cdot Y_o); Y_o = \frac{e \cdot \psi}{\kappa T} \quad , \quad (100)$$

where a_{aq} is the activity of an ion in the bulk solution, z is its charge, e is the electron charge, ψ is the surface potential, κ is Boltzman's constant and T is the temperature in Kelvin. The mass-action equations for (24) to (27), with the surface concentration described by equation (100), are:

$$K_{24} = \frac{E_{\text{SOH}} \cdot a_{\text{H}_s^+}}{E_{\text{SOH}_2^+}} \quad , \quad (101)$$

$$K_{25} = \frac{E_{\text{SO}^-} \cdot a_{\text{H}_s^+}}{E_{\text{SOH}}} \quad , \quad (102)$$

$$K_{26} = \frac{E_{\text{SONa}^0} \cdot a_{\text{H}_s^+}}{E_{\text{SOH}} \cdot a_{\text{Na}_s^+}} \quad , \quad (103)$$

$$K_{27} = \frac{E_{\text{SOH}_2\text{Cl}^0}}{a_{\text{H}_s^+} \cdot E_{\text{SOH}} \cdot a_{\text{Cl}_s^-}} \quad . \quad (104)$$

Now,

$$\sigma_o = e N_s A_T \alpha \quad , \quad (105)$$

LIMITATIONS OF GEOCHEMICAL MODELING

Geochemical models are extremely powerful and useful tools for understanding the processes of water-rock interactions and predicting their consequences. However, uncertainties involved in computations carried out using SOLMINEQ.88 and similar computer codes should be recognized by all users. Major uncertainties may be imposed by the amount and quality of thermochemical and other data used to calculate the equilibrium constants (K) for the dissociation of complexes and dissolution of minerals. Uncertainties in the computed activity coefficients of aqueous species are probably less severe except for those species (including aluminum and carbonate) that have no published Pitzer coefficients in concentrated brines at high temperatures. Usefulness of the results obtained is limited also by the completeness and reliability of the reported physical and chemical parameters used as input to the codes. It is also important to take the necessary precautions to insure that the sample is "representative" of the water in a specified part of the aquifer (Hull and others, 1985).

Physical Parameters

Accurate temperature and pressure values are needed to model water-rock interactions, especially in deep sedimentary basins where these values may be high. In these basins, oil and gas wells are the primary sources of temperature data. Unfortunately, the accuracy of temperatures obtained from oil wells varies widely (Meyer and McGee, 1985). Many operators do not recognize the importance of temperatures in exploration and production of petroleum and make no attempt to gather accurate data. Also, most temperatures are obtained from wells during drilling when the temperature distribution in the hole is under maximum thermal disturbance. The most reliable temperatures are those obtained from static bottom-hole pressure and temperature surveys generally conducted in production wells. Temperatures obtained from drill-stem tests are of intermediate accuracy. However, the majority of temperatures are obtained from electric log headings; these give the least reliable data, and are generally lower than the true subsurface values. Meyer and McGee (1985) showed that the discrepancy between log-header and static bottom-hole test temperatures from the Wattenberg field, Colorado, is large, ranging from 11 °C to 61 °C.

$$\alpha = \frac{E_{\text{SOH}_2^+} - E_{\text{SO}^-}}{E_{\text{SOH}_2^+} + E_{\text{SO}^-} + E_{\text{SONa}^0} + E_{\text{SOH}_2 \text{Cl}^0} + E_{\text{SOH}}} \quad (106)$$

where E refers to the equivalent fraction of surface sites occupied by the species. The dominator of equation (106) thus is unity and α is the fractional surface charge. Following Hunter (1981),

$$\sigma_d = \{2\epsilon_o \epsilon \kappa T \sum_i n_i (\exp(-Z_i \cdot Y_o) - 1)\}^{1/2} \quad (107)$$

where n_i is the number of ions of i per gram of the solution ($n_i = 1,000 N_A m_i$; m_i being the molality of each charged species in solution), ϵ_o is the permittivity of the vacuum, and ϵ is the dielectric constant of water.

Equations (99) and (101) to (107) are sufficient to uniquely solve for the concentrations of the surface species in equilibrium with the solution at a given pH, temperature and surface potential, ψ . The calculation routine in SOLMINEQ.88 satisfies equation (99) by iteratively changing the value of Y_o until its sign changes. An interpolation polynomial is then used to solve for the final value of Y_o .

Chemical geothermometers, based on the concentration of silica and proportions of sodium, potassium, lithium, calcium and magnesium in water from hot springs and geothermal wells, have been used successfully to estimate the subsurface temperatures of the reservoir rocks (Fournier and Truesdell, 1973; Fournier, 1981). Modified versions of these geothermometers and a new chemical geothermometer, based on the concentrations of magnesium and lithium (Table 7), were developed (Kharaka and others, 1985; Kharaka and Mariner, 1988) to estimate the subsurface temperatures (30 °C to 200 °C) in sedimentary basins where water salinities and hydraulic pressures are generally much higher than those in geothermal systems. SOLMINEQ.88 computes all the chemical geothermometer listed in Table 7.

Quartz, Mg-Li, Mg-corrected Na-K-Ca, and Na-Li geothermometers generally give concordant subsurface temperatures that are within 10 °C of the measured values for reservoir temperatures higher than about 70 °C. Mg-Li, Na-Li, and chalcedony geothermometers give the best results for reservoir temperatures from 30 °C to 70 °C. Subsurface temperatures calculated by chemical geothermometers are at least as reliable as those obtained by conventional methods. Chemical and conventional methods should be used together where reliable temperature data are required. The user then makes the selection of the temperature to be used for the high temperature option in SOLMINEQ.88. For more details see Kharaka and Mariner (1988).

Hydraulic pressure, as discussed earlier, is also an important parameter that affects the equilibrium constants for the aqueous species and minerals, especially at temperatures higher than about 150 °C. Assuming a hydrostatic pressure gradient of 0.45 psi/ft (10.2 kPa/m) is generally reasonable for petroleum wells immediately after drilling. However, in geopressured geothermal systems, initial hydraulic pressure gradients may reach lithostatic pressure gradient of 1.0 psi/ft (22.6 kPa/m). Production wells may have hydraulic pressures that are much lower than the original (virgin) shut-in pressure of the well. Accurate pressure readings at regular time intervals are generally available from the operator and should be extrapolated or interpolated to the time of sampling.

Table 7 Chemical Geothermometers in SOLMINEQ.88

(from Kharaka and Mariner, 1988)

Geothermometer	Equation
	(Concentrations are in mg/L; t in °C)
1. Quartz	$t = \frac{1309}{0.41 - \log(k \cdot pf)} - 273.15 ;$ $k = \frac{\alpha_{H_4SiO_4}}{\alpha_{H_2O}^2} ; \quad pf = (1 - 7.862 \times 10^{-5} e^{(3.61 \times 10^{-3} \cdot t)})_{p(\text{bar})}$
2. Chalcedony	$t = \frac{1032}{-0.09 - \log(k \cdot pf)} - 273.15$
3. Mg-Li	$t = \frac{2200}{\log(\sqrt{Mg/Li}) + 5.47} - 273.15$
4. Na-K	$t = \frac{1180}{\log(Na/K) + 1.31} - 273.15$
5. Na-K-Ca	$t = \frac{699}{\log(Na/K) + \beta [\log(\sqrt{Ca/Na}) + 2.06] + 0.489} - 273.15$ $\beta = 4/3 \text{ for } t < 100; = 1/3 \text{ for } t > 100$
6. Mg-Corrected, Na-K-Ca	$t = t_5 - \Delta t_{Mg} \quad \text{For } R \text{ values of } 0.5 \text{ to } 5.$ $\Delta t_{Mg} = 1.03 + 59.971 \log R + 145.05(\log R)^2$ $- 36711 (\log R)^2 / T(K) - 1.67 \times 10^7 \log(R/T^2);$ <p>For R values of 5 to 50</p> $\Delta t_{Mg} = 10.66 - 47415 R + 325.87(\log R)^2$ $- 1.032 \times 10^5 (\log R)^2 / T - 1.968 \times 10^7 (\log R)^2 / T^2$ $+ 1.605 \times 10^7 (\log R)^3 / T^2;$ <p>No correction should be attempted if $R > 50$.</p> $R = \frac{Mg}{Mg + 0.61 Ca + 0.31 K} \cdot 100$
7. Na/Li	$t = \frac{1590}{\log(Na/Li) + 0.779} - 273.15$

Chemical Analysis

Chemical data may be a major source of uncertainty in the computation of water-rock interactions. Uncertainty may result from:

1. Incomplete analyses. Chemical data collected by oil companies from wells drilled in search of, or for production of oil and gas are plentiful but almost always inadequate for these computations because data are available only for a limited number of major cations and anions. There are very few analyses of trace constituents from oil-field or geothermal waters. A major problem of almost all chemical data is the paucity of Al determinations that are essential for computing the states of reaction of water and aluminosilicates. Barnes (1975) showed that Al concentrations in natural waters at near-neutral pH values are generally less than 57 micrograms per liter ($\mu\text{g/l}$). Analyses of Al in oil-field and geothermal waters give values that are generally less than 20 $\mu\text{g/l}$ (Kharaka and others, 1985). Concentrations of this magnitude are difficult to determine reliably and some possibility exists that a portion of Al may have precipitated from water prior to sampling (MacGowan and Surdam, 1988).

Another major limitation of many chemical analyses is lack of data on the concentrations of dissolved organic species (Thurman, 1985). It is now generally accepted that mono- and dicarboxylic acid anions may be present at high concentrations (up to 10,000 mg/L) in waters from sedimentary basins (Carothers and Kharaka, 1978; Kharaka and others, 1986; MacGowan and Surdam, 1988). Detailed studies of organic species in oil field waters were initiated (Willey and others, 1975), to a large degree, because computations using SOLMNEQ (Kharaka and Barnes, 1973) had shown that oil field waters at Kettleman North Dome, California, were supersaturated by up to 3 kcal/mole with respect to calcite (Willey and others, 1975; Merino, 1975). Willey and others (1975) showed that the high supersaturation resulted because the alkalinities of the waters were attributed only to inorganic species (mainly HCO_3^- , CO_3^{2-} , and HS^-). They further showed that organic acid anions ($\text{C}_2 - \text{C}_5$) contributed up to 99 percent of the measured alkalinities. Carothers and Kharaka (1978) and Lundegard and Land (1986) showed that up to 100 percent of field determined alkalinities in oil field waters are contributed by organic species (Figure 7).

2. Unreliable chemical analyses. The reliability of many chemical analyses is uncertain because of the method of sample collection, treatment,

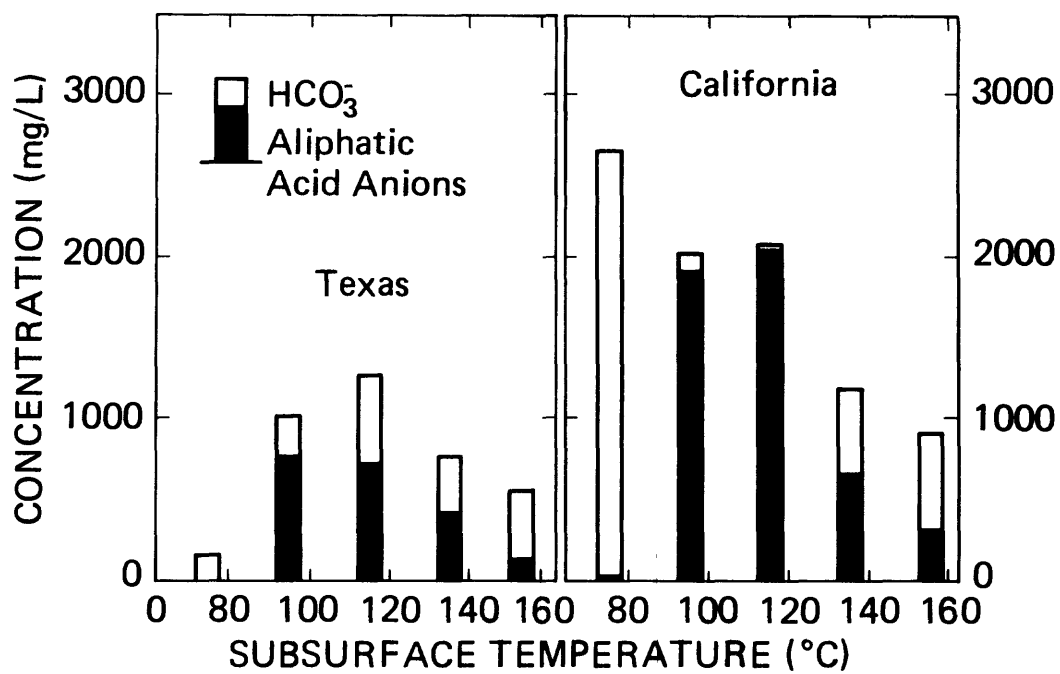


Figure 7. -- Average concentrations of aliphatic acid anions and bicarbonate in oil-field waters from Texas and California (from Carothers and Kharaka, 1978)

and analysis (Hem, 1985). Values of pH, alkalinity, H_2S , and NH_3 not determined in the field are always suspect (Presser and Barnes, 1974; Lico and others, 1982). Field treatment of the samples should include filtration through a 0.1 or 0.45 μm pore-size membrane filter for the major cations, anions, and organics and, in the case of cations, acidification with concentrated HCl to pH of about 2. An aliquot of the filtrate is diluted with distilled deionized water to decrease the silica concentration to less than 100 mg/L to prevent polymerization. Aluminum should be extracted in the field after filtration through a 0.1 μm filter (Barnes, 1975). Filtration through a 0.1 μm filter and acidification to pH 1.5 with high-purity nitric acid is also required for reliable determination of other trace metals (Kennedy and others, 1974). Mercuric chloride or sodium azide, and potassium permanganate should be added to preserve dissolved organics and mercury, respectively, (Hull and others, 1985).

Laboratory analyses require methodologies and instruments that give the best results for the samples selected. Analysis of cations is generally performed by atomic absorption (AA), flame emission spectrophotometry and inductively-coupled plasma atomic emission spectrometry (ICP-AES). Graphite-furnace AA with Zeeman background correction is used for the determination of most trace metals. An increasing number of anionic species, including sulfate, bromide, and iodide, are being determined by ion chromatographic techniques. Dissolved organics are determined by gas and ion chromatography and other instrumentation, such as mass spectrometry. The reader is referred to recent reviews by Parsons and others (1983) and Hull and others (1985).

A high level of analytical skill is required to obtain reliable data from the highly sophisticated instruments described above. Ellis (1976), in an international laboratory-comparison program, showed that the analytical precision for many chemical constituents was poor. The reported silica concentration of a geothermal sample, for example, ranged from 70 to 920 ppm. Lowest precisions were reported for geothermal and alkaline spring waters of unusual composition. Friedman and Erdmann (1982) provide some guidance for setting up a quality assurance program.

3. Incorrect interpretation of chemical determinations. We have already discussed the problems associated with assuming that alkalinities are contributed only by inorganic species. Similar problems may arise if the iodometric titration method, which measures the concentrations of bisulfides, sulfites, polysulfides and other oxidizable species, is assumed to titrate only the bisulfide species. In oil field waters, H_2S values obtained by

specific sulfide electrode are more accurate and are much lower (by a factor of up to 10) than those obtained by titration (Lico and others, 1982).

Equilibrium Constants

Reliability of equilibrium constants for the dissociation of complexes and dissolution of minerals is highly variable, depending on the quality and the nature of the thermochemical data used in these computations (Arnorsson and others, 1982; Nordstrom and Munoz, 1985; Apps and others, 1987). The range of available thermochemical data is large. The Gibbs free energy values reported for the same mineral may vary by more than 10 kcal/mole (Tardy and Garrels, 1974; Berman and others, 1985). For instance reported values of the equilibrium constant at 25 °C for fluorite range from 10^{-8} to 10^{-13} (Nordstrom and Jenne, 1977); those for the second dissociation constant of H_2S range from 10^{-12} to 10^{-19} (Schoonen and Barnes, 1988). Equilibrium constants computed from solubility or free energy determinations over the temperature range of interest are probably the most reliable. As discussed earlier, equilibrium constants for most minerals and a few aqueous complexes used in SOLMINEQ.88 are computed from an integrated form of the Van't Hoff equation (Equation 37). These equilibrium constants are the most reliable for the pure mineral samples used to generate thermochemical data in laboratory experiments. However, minerals in natural systems often show large variations in chemical composition, surface characteristics, degree of crystallinity, order-disorder, and lattice imperfections. Clays and zeolites are two major groups of minerals for which large uncertainties in equilibrium constants may result from these imperfections (Tardy and Garrels, 1974; Bassett and others, 1979; May and others, 1986).

Heat-capacity data are not available for most aqueous complexes. Equilibrium constants for these complexes are computed from empirical relation using a large number of assumptions and extrapolations (see previous section). Equilibrium constants calculated from these empirical equations, nonetheless, more closely approximate the actual values at higher temperatures than those computed assuming a constant or zero-heat capacity of reaction. However, very large errors may be present in log K values calculated from these equations, especially at temperatures above 200 °C (Apps and others, 1988). Equilibrium constants for many minerals and aqueous complexes (especially with organic ligands) are either not available or are available only at 25 °C.

Equilibrium constants are unquestionably the most important parameters used in geochemical codes like SOLMINEQ.88. However, these constants are subject to continuous refinements, modifications or major changes (Hovey and Tremaine, 1986; Apps and others, 1988), and the user should carry out literature searches to select the most reliable constants for the critical minerals and aqueous species in their study. SOLMINEQ.88 allows computations to be carried out using a set of up to six (at low and high temperatures) user selected equilibrium constants for minerals and aqueous complexes. The INPUT routine prompts the user to enter the desired equilibrium constants which will be used for any computations during that run. Permanent changes in the equilibrium constants, of course, can be made by changing the values for the desired complex or mineral in the permanent data file listed in Appendix IB and IC.

Limitations of Modeling Options

All of the modeling options in SOLMINEQ.88 have been designed to allow modification of the analyzed chemistry of a water sample to the in situ chemistry of the water and its mineral saturations. The options, also, can be used to study the consequences of the various hypothetical or planned water-rock interactions including sensitivity calculations.

The carbon option may be used to validate a chemical analysis if independent determinations of alkalinity and TIC exist. Given a value for one, SOLMINEQ.88 will calculate a value for the other. This can be compared to the analytical value (see Merino 1979 for examples). For high temperature calculations the assumption of constant TIC or constant alkalinity will affect the predictions differently. Constant alkalinity can only be enforced by allowing CO_2 to enter or leave the water, whereas constant TIC is a closed system. If CO_2 is known to have been lost from the system, it can be titrated back in with the gas-option. However, it is difficult to measure the ratio of gas/water in a flowing well. If the aim is to combine the masses of gas and water as they are in situ, large uncertainties exist because once gas separates from liquid water the two can travel at different velocities to the wellhead. If oil is present in the system, the gas lost from the oil must also be titrated back using the gas-water-oil option to reconstruct the in situ conditions. However, data on gas solubilities in oil have large uncertainties because of differences in the physical and chemical properties of oil. The gas-water-oil option will not run if the total pressure of the

gas phase (at high or low temperature) is less than the vapor pressure of water at that temperature and pressure. These calculations are carried out assuming that Henry's law does not vary with pressure and ideal mixing of gases. Although these assumption are good along the vapor pressure curve for water, significant errors will be introduced when pressures exceed several hundred bars at low temperatures; such conditions exist in deep wells in sedimentary basins. In addition, at high pressures, a significant mass of water vapor may exist in the natural gas phase which may condense in the well leading to erroneously low concentrations of dissolved species (Kharaka and others, 1985). Presently, all the water is assigned to the liquid phase in SOLMINEQ.88 except for the boiling option. The boiling and mixing options can handle loss or addition of water to in situ water, however, the fraction of boiling or the composition and amount of water mixing with the in situ water must be accurately known.

Minerals can also be used to compute the water chemistry at subsurface conditions. If the amount of gas which is lost is unknown, for example, an estimate can be made by assuming equilibrium with an in situ carbonate mineral using the CO_2 option; commonly equilibrium is assumed with calcite. If other minerals are controlling the water chemistry, a user specified set of components can be dissolved into or precipitated out of the water to reach saturation with a specified mineral. Even if the in situ mineralogy is known in detail, the extent to which a mineral controls the water chemistry depends on its surface area and reactivity, which are usually unknown. In addition, most minerals are solid solutions which are not presently included in the database of SOLMINEQ.88.

The mineral saturation option may be used to calculate the concentrations of unknown or suspect components. This option, for example, may be used to calculate the concentrations of SiO_2 (assuming quartz saturation) and Al (assuming equilibrium with kaolinite). This use of saturation options should only be used as a last resort because of the large uncertainties involved. If the pH is unknown or suspect, equilibrium with calcite is commonly assumed and the pH changed to attain equilibrium using the pH option. This case is only correct as long as significant amounts of the other ions in solution have not been added or subtracted at the same time the pH changed. Presently, SOLMINEQ.88 allows only equilibration with one mineral phase even when the reaction is incongruent, involving several minerals.

The water chemistry can also be changed by ion exchange or adsorption. Large uncertainties exist in the values for the ion exchange constants.

Consequently, in the ion exchange option, these constants must be specified by the user. Surface complexes are assumed to behave ideally. Smectites, the clays which control most of the ion exchange, are poorly characterized chemically. The double layer, one-site model chosen for adsorption calculations is probably too simple, but even this simple a model is difficult to use because of paucity of data. Consequently, mineral surface-water equilibrium calculations lag far behind mineral-water equilibrium predictions in accuracy.

The above discussion is included in this report because the uncertainties in the predictions made by these options can be large. The user should be cautioned to understand fully the assumptions and simplifications made in both the data and the calculations in order to use the model successfully.

INPUT FOR SOLMINEQ.88

The input to SOLMINEQ.88 consists of two sets of data: fixed and variable. The fixed set contains the chemical composition of an aqueous fluid and options for processing these data. The variable set consists of input data required for using the modeling options. Multiple samples may be processed during each run. The arrangement of input data is shown in Table 8. A list of input variable names and their description is given below. An interactive FORTRAN-77 program, SOLINPUT, is also available which can be used to generate or modify an input file. This program prompts the user for input data with a brief description of the required data. The user is prompted to press the "RETURN" key in cases where data are not available and where the default values are preferred. An abbreviated terminal session for building a data file using SOLINPUT is given in Appendix II. An interactive input-output management program (shell) that can be used with personal computers (PCs) is also available (Wiwchar and others, 1988) for SOLMINEQ.88

A. Input Data for the Fixed Set

TITLE	Sample identification and description.
TEMP	Temperature at which the pH of the solution was measured.
HITEMP	In-situ temperature, different from TEMP, at which a new pH is to be calculated.
DENS	Measured or desired density. If density is not entered, it is calculated based on the following empirical relationship (Kharaka, unpublished data): $\text{Density} = 1.0 + 6.88 \times 10^{-7} * \text{Total Dissolved Solids (mg/L)}$
PRESS	Total in-situ pressure (in bars). K values of the aqueous and mineral reactions will be adjusted for the pressure difference of $(\text{PRESS} - P_{\text{H}_2\text{O}})$. The K values are adjusted at only one temperature, TEMP or HITEMP. If PRESS is greater than $P_{\text{H}_2\text{O}}$ at TEMP and a value for HITEMP is entered, the K values are adjusted only at HITEMP.
PH	Measured pH of the solution.
EHM	Measured or calculated Eh relative to the hydrogen electrode potential in volts, otherwise a default value of 9.0 is entered by the program.

EHMC Measured Eh relative to the Calomel electrode potential in volts, otherwise a default value of 9.0 is entered by the program.

EMFZSC Measured Eh using Zobell's solution in volts, otherwise a default value of 9.0 is entered in the program.

UNITS Concentration units in which the chemical composition of the solution will be entered.

MG/L = milligrams/liter

PPM = parts per million

MOL/L = moles/liter (molar units)

MOL/K = moles/kg of solvent (molal units)

MEQ/L = milli-equivalents/liter

Total or analytical concentration of the specified component. The concentrations must be entered for the specified formula of the component (for example, sodium is entered as Na, silica as SiO₂, phosphorous as PO₄). The components are listed in Table 6.

TIC Concentration of total inorganic carbon in solution, if measured, in the same units used for the rest of the components. If UNITS is "MEQ/L", carbon concentration should not be entered as TIC; instead it should be entered as alkalinity (ALK).

ALK Criterion for the distribution of carbonate species.

"0" indicates that the entered concentration of HCO₃⁻ and for CO₃²⁻ represent "TOTAL ALKALINITY" that includes inorganic and organic species.

"1" indicates that the entered concentrations of HCO₃⁻ and for CO₃²⁻ represent "CARBONATE ALKALINITY" only.

"2" indicates that the entered concentrations of HCO₃⁻ and CO₃²⁻ represent "TIC".

It should be noted if ALK = 2 and TIC = 0.0, the entered concentration of HCO₃⁻ and CO₃²⁻ will be treated as TIC after conversion to the molality of carbon; if TIC is greater than 0.0, ALK will be set equal to 2 and the concentrations of HCO₃⁻ and CO₃²⁻, if entered, will be disregarded.

ITIC Criterion for the distribution of carbonate species at HITEMP "1" if this distribution is to be done with the value of TIC calculated at the end of low-temperature species distribution. Note that if a value for TIC is entered, ITIC will be automatically set equal to "1".

NUFLAG Sets the activity coefficients of neutral species;
 "1" for setting them equal to unity;
 "0" for setting them equal to the activity coefficient of aqueous CO₂.

IPIT Enter "1" if activity coefficients are to be calculated using the Pitzer equations.

FLAGS(I) Flags for the calculation of redox equilibria. If these flags are set equal to "1" the distribution of redox species will be calculated using the measured or calculated Eh and equations of the type:

$$\text{Fe}^{++} = \text{Fe}^{3+} + e^{-}$$

else, if equal to "0", the $\text{H}_2\text{S}^0/\text{SO}_4^{--}$ and $\text{Fe}^{++}/\text{Fe}^{+3}$, will be used to determine redox species distribution.

 FLAG(1) for Fe
 FLAG(2) for Cu
 FLAG(3) for Hg
 FLAG(4) for Mn
 FLAG(5) for U
 FLAG(6) for V

INFORM Flag for printing all the log K values in Tables 2 and 3. Set INFORM equal to "1" if you want the tables printed.

RATIO Flag for printing the analytical and calculated activity ratios of major elements. Set RATIO equal to "1" if you want the ratios printed.

GEOETH Flag for printing the temperature estimates from the chemical geothermometers. Set GEOETH equal to "1" if you want the geothermometers printed.

IPRIN1 Flag for printing the data on iteration of anions, set equal to "1" for output.

IPRIN2 Flag for printing the data on ($m_{\text{H},t,T} - m_{\text{OH},t,T}$) whenever a new pH is calculated. Set IPRIN2 equal to "1" to print data.

CONV1 Tolerance factor for convergence on distribution of anions. Enter the desired factor if different from a default value of 0.5E-4. Use of a lower value may result in greater accuracy but more computer time.

CONV2 Tolerance factor for pH calculation using hydronium mass-balance equation. Enter a desired factor if different from a default value of 0.5E-4. Use of a higher value may result in faster execution, but a larger pH difference between calculated and in situ.

OUTIN A restart file will be generated with the file name located in OUTIN. The restart file will contain data from the current SOLMINEQ.88 run. Leave blank if a restart file is not to be created.

B. Input for Gas, PH, and CO₂ options

DCO2 Concentration of CO₂ gas (moles/kg of water) that was lost before pH measurement.

DH2S Concentration of H₂S gas (moles/kg of water) that was lost before pH measurement.

DNH3 Concentration of NH₃ gas (moles/kg of water) that was lost before pH measurement.

DCH4 Concentration of CH₄ gas (moles/kg of water) that was lost before pH measurement.

ICCSAT Switch for the pH option (calculation of pH in equilibrium with carbonate mineral). "1" for calcite; "2" for dolomite; "3" for siderite. Default is "0"

IMCO3 Switch for the application of the CO₂ option.

"0" = do not use option (default).

"1" Enter for saturation with calcite.

"2" Enter for saturation with dolomite.

"3" Enter for saturation with siderite.

"4" for fixing a molality of H₂CO₃ specified by FIXIT.

"5" for fixing a pH specified by FIXIT.

"6" for fixing a P_{CO₂} specified by FIXIT.

FIXIT Specify the value to be fixed using the CO₂ option above if
IMCO3 = 4, 5, or 6.

FCCSAT Tolerance factor for satisfying the equilibrium criterion in the
PH and CO₂ options (default = 0.05). The equilibrium is tested
in log units.

C. Input for the Gas Distribution option

TCO2M Total moles of CO₂ (per kg of water) to be distributed between
Oil, Water, and Vapor.

TCH4M Total moles of CH₄ (per kg of water) to be distributed between
Oil, Water, and Vapor.

TH2SM Total moles of H₂S (per kg of water) to be distributed between
Oil, Water and Vapor.

WROIL Oil to water weight ratio.

KCO2OL Henry's law coefficient for the solubility of CO₂ in oil. If
value entered is "0", which is the default value, then the value
is calculated in the program.

KCH4OL Henry's law coefficient for the solubility of CH₄ in oil. If
value entered is "0", which is the default value, then the value
is calculated in the program.

KH2SOL Henry's law coefficient for the solubility of H₂S in oil. If
value entered is "0", which is the default value, then the value
is calculated in the program.

DSEP Density of oil at 15 °C needed to calculate Henry's law
coefficients for the solubility of gas in oil.

D. Input for the Ion Exchange or Adsorption Option

ADEX Flag for surface chemistry option:
"A" for adsorption, "E" for ion exchange.

CEC Cation exchange capacity in milliequivalents/kg of water.
Either a value for CEC or values for TAREA and SAREA must be
specified.

TAREA Site density per unit area (N_s) in sites/cm².

SAREA Total surface area per kilogram of solvent in cm^2 .

INSP Total number of surface species (10 maximum)

ISCHG(I) Charge of each surface site (e.g. ISCHG = 0 for NaX; -1 for X^-), where X represents vacant surface site.

MBASE(I) Equivalent fraction of surface sites occupied by each surface species. If vacant surface sites occupy an appreciable fraction of total, then a dummy reaction $\text{X} \rightleftharpoons \text{X}$ must be specified.

SPN(I) Name of each of the surface species.

KRXN(I) K_D for the association reaction of the surface species.

ISCOMP(I) Total number of components in the association reaction of SPN(I).

COEF(I,J) Stoichiometric coefficient of each of the reacting species (only those in Table 6) in the association reaction of SPN(I).

IDN(I,J) ID#s of the ISCOMP(I) components in the association reaction of SPN(I). It is important that the K_D and coefficients for the species be specified as for an association reaction; and that all association reactions use only the vacant surface site X as the reactant surface site.

E. Input for the Dissolution/Precipitation, Mixing, and Boiling Option

IBMIX Switch for the mixing and mass transfer option.
 "1" for dissolution/precipitation.
 "2" for mixing two solutions.
 "3" for boiling-off or adding steam.

ITMIX Total number of species to be added when IBMIX=1. If ITMIX is zero, it is used as the switch for the mineral saturation option. That is, if IBMIX = 1 and ITMIX = 0, then the program would look for the ID# of the mineral to be saturated. If ITMIX is not equal to zero, then a specified amount of mineral will be added if ITMIX = -1. If ITMIX = n, where n is greater than zero, then specified amounts of n aqueous components will be added.

IDSAT ID# (from 1 to 214) of the mineral to be equilibrated (i.e. SI=0). (See Table 3.)

IDDP ID # (from 1 to 214) of the mineral to be dissolved or precipitated. If IDDP equals "0", then a number of aqueous species are added or subtracted from the water.

ITT Total number of aqueous species to be added to or subtracted from the water.

DP Dissolution/precipitation switch. If DP is positive it will dissolve minerals or add aqueous components into solution; if negative, it will precipitate or subtract them out. The absolute value of DP is also used to scale the amount of material being added or subtracted. If the default value of zero is used then the program will determine the path to achieve equilibrium.

IRXDP(I) ID# of the aqueous species to be added (only the species listed in Table 6 can be used).

RXDP(I) Stoichiometric coefficient of the aqueous species to be added.

IDMIX(I) ID number of the aqueous species to be added (only the species listed in Table 6 can be used).

AMOL(I) Molality (Moles/kg of H₂O) of the aqueous or mineral species to be added.

INMIX Total number of mixtures of the two solutions to be mixed.

DFRAC1 Smallest fraction of solution 1 to be mixed with solution 2.

DINC Increment of solution 1 to be added (INMIX-1) times. For example, if INMIX = 3, DINC = 0.25 and DFRAC1 = 0.10, a total of THREE mixtures will be prepared with the following fractions of the two solutions:

(1) solution 1 = 0.10; solution 2 = 0.90

(2) solution 1 = 0.35; solution 2 = 0.65

(3) solution 1 = 0.60; solution 2 = 0.40

MIXFLE Name of second data file to form the mixture. No other mass transfer options can be executed as part of mixing.

FBOIL Fraction of the solution to be boiled-off as steam.

F. Input for variable K values at TEMP and then again at HIGHTEMP

ODUM(I) Switch for data base. If KT is for an aqueous complex dissociation reaction, enter "A"; if for a mineral dissociation reaction enter "M".

NDUM(I) ID# of the mineral (Table 3) or aqueous complex (Table 2) whose (KT) is to be changed.

XDUM(I) Log (KT) for the dissociation reaction specified in Tables 2 or 3.

G. Input for additional anions.

ANS1, ANS2 Switches for additional anion option. If ANS1 or ANS2 are not zero, the value of ANS1 or ANS2 is the number of lines (one line per complex with anion) to follow. If ANS1 = 0 (default option) and ANS2 = 0, skip option. If ANS1 > 0 and ANS2 = 0, or vice versa then add one additional anion. If ANS1 > 0 and ANS2 > 0, then add both additional anions.

PAGE1 Name of additional anions.

CUNITS Total concentration (same UNITS as other components) of additional anions.

GFW Gram formula weight of additional anion.

Z Charge of additional anion (-1 to -4).

DHA Debye Huckel radius of additional anion (default values are available).

NAME(I) Name of each complex formed by association with the additional anion.

INDEX(I) ID# of the dissociation reaction (Table 5) for the anion complex, NAME(I).

LOWKT(I) Low temperature log (KT) for the INDEX(I) dissociation reaction.

HIGHKT(I) High temperature log (KT) for the INDEX(I) dissociation reaction.

H. Input for additional cation.

NUMCOM Number of complexes entered for the additional cation.

Z Charge of additional cation (+1 to +4).

DHA Debye Huckel radius of additional cation (default values are available).

GFW Gram formula weight of additional cation.

CUNITS Total concentration (same UNITS as other components) of additional cation.

NAME(I) Name of each complex formed by association with the additional cation.

INDEX(I) ID# of the dissociation reaction (Table 5) for the cation complex, NAME(I).

LOWKT(I) Low temperature log K(T) for the INDEX(I) dissociation reaction.

HIGHKT(I) High temperature log K(T) for the INDEX(I) dissociation reaction.

J. Input for additional minerals.

NUMINS	Number of minerals to be added (up to 5 allowed)
LOWKT	Low temperature log $K(T)$ for the congruent dissolution of the mineral
HIGHKT	High temperature log $K(T)$ for the congruent dissolution of the mineral
ADDACT	An additional activity parameter which can be added to the dissolution reaction of mineral
NAME	Name of the mineral
COEFF(I)	Coefficient of aqueous species (I) in the dissolution reaction of the mineral.
INDEX(I)	Index number of aqueous species (I) in the dissolution reaction of the mineral

Table 8 Arrangement of data for input to SOLMINEQ.88.

Line	Variable	Format
1	TITLE	A80
2	TEMP, HITEMP, DENS, PRESS	4E10.4
3	PH, EHM, EHMC, EMFZSC, UNITS	4E10.4, A5
4	Total aqueous concentration of [Na, K, Li, Ca, Mg, Fe, Al]	7E10.4
5	Total aqueous concentration of [SiO ₂ , Cl, SO ₄ , H ₂ S, HCO ₃ , CO ₃ , TIC]	7E10.4
6	Total aqueous concentration of [F, PO ₄ , NO ₃ , NH ₃ , B, Sr, Ba]	7E10.4
7	Total aqueous concentration of [Pb, Zn, Cu, Mn, Hg, Ag]	6E10.4
8	Total aqueous concentration of [As, U, V]	3E10.4
9	Total aqueous concentration of [Acetate, Oxalate, Succinate, CH ₄]	4E10.4
10	Carbon, High Temperature Carbon Option ALK, ITIC	2I2
11	Gas Addition Option DCO2, DH2S, DNH3, DCH4	4E10.4
12	pH and CO ₂ Saturation Option ICCSAT, IMCO3, FIXIT, FCCSAT	2I2, 2E10.4
13	Gas-Water-Oil Option TCO2M, TCH4M, TH2SM, WROIL, KCO2OL, KCH4OL, KH2SOL, DSEP	8E10.4
14	Ion Exchange Option ADEX	A1
	if ADEX is "E" or "A", then	
	A. CEC, TAREA, SAREA, INSP	3E10.4, I3
	followed by INSP lines of	
	B. ISCHG(I), MBASE(I), SPN(I)	I4, E10.4, A10
	C. KRXN(I), ISCOMP(I), (COEF(I,J), IDN(I,J))	11(E10.4, I3)

15	Precipitation/Mixing/Boiling Options	
	IBMIX, ITMIX	2I2
	Dissolution/Precipitation Option:	
	If IBMIX = 1, then	
	(Dsl/Ppt a specific mineral amount)	
	If IBMIX = 1 and ITMIX < 0, then	
	A. IDDP, AMOL(1)	I4, E10.4
	(Dsl/Ppt a mineral to saturation)	
	Else If IBMIX = 1 and ITMIX = 0, then	
	A. IDSAT, IDDP, DP	2I4, E10.4
	(Add/Subtract aqueous species to saturation with a mineral)	
	If IDDP = 0, then	
	A. ITT	I4
	followed by ITT lines of	
	B. IRXDP(I), RXDP(I)	I4, E10.4
	(Add/Subtract a specific amount of aqueous species)	
	Else If IBMIX = 1 and ITMIX > 0, then	
	followed by ITMIX lines of	
	A. IDMIX(I), AMOL(I)	I4, E10.4
	Mixing Option:	
	Else If IBMIX = 2, then	
	A. INMIX, DFRAC1, DINC, MIXFLE	I4, 2E10.4, A80
	Boiling Option:	
	Else If IBMIX = 3, then	
	A. FBOIL	E10.4
16	Optional User Defined Log K at TEMP	
	A. ODUM(I), NDUM(I), XDUM(I)	6(A1, I4, E10.4)
17	Optional User Defined Log K at HITEMP	
	B. ODUM(I), NDUM(I), XDUM(I)	6(A1, I4, E10.4)

18	Additional Anions Option	
	ANS1, ANS2	2I2
	Skip if both ANS1 = 0 and ANS2 = 0.	
	If ANS1 > 0 or ANS2 > 0, then	
	A. CUNITS, GFW, Z, DHA, PAGE1	2E10.4, I2, E10.4, A8
	followed by ANS1 lines of	
	B. INDEX(I), DHA, LOWKT, HIGHKT, NAME(I)	I2, 3E10.4, A8
	If ANS1 > 0 and ANS2 > 0, then	
	A. CUNITS, GFW, Z, DHA, PAGE1	2E10.4, I2, E10.4, A8
	followed by ANS2 lines of	
	B. INDEX, DHA, LOWKT, HIGHKT, NAME	I2, 3E10.4, A8
19	Additional Cation Option	
	A. NUMCOM, Z, DHA, GFW, CUNITS, NAME	2I2, 3E10.4, A8
	followed by NUMCOM lines of	
	B. INDEX, DHA, LOWKT, HIGHKT, NAME	I2, 3E10.4, A8
20	Additional Minerals Option	
	NUMINS	I2
	followed by NUMINS lines of	
	B. LOWKT, HIGHKT, ADDACT, NAME	5E10.4, A8
	C. (COEFF(I), INDEX(I), I = 1, 8)	8(E10.4, I3)
21	NUFLAG, IPIT, (FLAGS(I), I = 1, 6)	8I2
22	INFORM, RATIO, GEOTH, IPRIN1, IPRIN2, OUTIN	5I2, A80
23	CONV1, CONV2	2E10.4

OUTPUT FROM SOLMINEQ.88

The results of the computations carried out by SOLMINEQ.88 and appearing in the printout (Appendix III) consist of a standard output which is similar to that from the original code and additional output which will depend on the options selected. The standard output consists of items listed below:

1. An input data echo that shows the values and options selected for each sample.
2. A table listing the calculated tolerance factor $(1 - Y_A)$ for successive iterations on the anions. Each set of iterations is completed at a fixed pH. At the end of each set or when the tolerance criteria are met, the current hydronium/hydroxyl summation $(m_{H,t,T} - m_{OH,t,T})$ is printed out along with the correct (desired) value. The printout of these numbers may be enabled by inputting $IPRIN1 = IPRIN2 = 1$. These data are used to verify the timely execution of the program and are not normally needed.
3. A list of input to SOLMINEQ.88, including sample description, pH, Eh (measured or computed, a dummy value of 9.0000 is printed when no Eh data are available) temperature, total milliequivalent of cations (MEQ/L CAT) and anions (MEQ/L AN) computed from the analytical data (ANAL...) and from the calculated molalities (CALC...), the true ionic strength of solution (I), the total pressure and the partial pressures, in atmospheres, of H_2O , CO_2 , H_2S , CH_4 , and NH_3 in the gas phase that is in equilibrium with the solution, the density of the solution, dissolved solids concentration and activity of water. The total hydronium and hydroxyl and their difference; the total alkalinity calculated as HCO_3^- , CO_3^{--} and $CaCO_3$; and the dissolved inorganic carbon (split up into HCO_3^- - alkalinity, H_2CO_3 , sum of all HCO_3^- species and the sum of all CO_3^{--} species) and total inorganic carbon are also printed out.
4. A table showing the distribution of species in solution. This consists of the index number (1 to 340) and name of the species which are present, reported and computed ppm, reported and computed mg/l, reported and computed molality, activity, activity coefficient, and -log activity. This table can be used to calculate the degree of complexing in the solution under study.
5. Ratios of a number of cations and anions of importance in geochemical processes. These consist of the mole ratios of cations and anions which may

aid in deciphering the origin of the water samples (White, 1965; Kharaka, 1985) and logs of the activity ratios of a number of cations used to study the stability fields of minerals. The subsurface temperature of a reservoir is computed by 12 different chemical geothermometers (see Table 7 for details of computations). A number of criteria for selecting the most probable temperature are also printed. (Fournier and Truesdell, 1973; Kharaka and Mariner, 1988). The computation and printout of these ratios and temperatures may be suppressed by inputting "RATIO = 0" and "GEOTH = 0" in the INPUT routine.

6. A table showing the states of reactions for minerals considered. The "DELG" column gives the (ΔG_{diff}), in kcal/mole. A positive (DELG) value indicates that the solution is supersaturated with respect to the given mineral; a negative (DELG) value indicates undersaturation with respect to it. This table also shows the mineral name and its ID numbers, log (AP), log (KT), and log (AP/KT). A mineral that contains a species not reported in the chemical analyses of the water sample will not appear in this table. The log (KT) of a number of minerals (for example, kenyaite, magadiite) is known only at 25 °C; it is assumed constant at other temperatures. The "DELG" values obtained for these minerals will not be significant if the temperature of the sample is outside the range of 15°-35 °C.

It is important to repeat here that (DELG) indicates that the reaction can proceed but does not mean that it will proceed in the specified direction. It is possible for a given solution to be supersaturated (unstable but persistent condition) with respect to a mineral by a number of kilocalories without precipitation. It is also important to note here that large uncertainties are involved in the computed log (KT) values for most aqueous complexes at temperatures higher than 200 °C.

Beside the standard output described above, implementation of various options will create additional output. This output is self-explanatory once the standard output format is understood. Selected examples are contained in Appendix III. The total number of possible options is large and could not be illustrated in this report. However, we have input/output from 20 different options that will be mailed, together with the source code, to those willing to implement this program.

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APPENDIX I. DATABASE

The database for SOLMINEQ.88 consists of physical parameters of the aqueous species, equilibrium constants (K) of the dissociation, redox, and dissolution reactions, constants for calculating the activity coefficients, and data for the extrapolation of the K values to higher pressures. The physical parameters are listed in Table IA. In this table, the name of the species is followed by its charge, hydrated radius (a^0), and molecular weight.

Tables IB and IC list the equilibrium constants at eleven temperatures from 0° to 350°C for the dissociation of aqueous complexes and redox reactions (IB), and dissolution reactions for the minerals (IC). The eleven constants are arranged in two lines for each of the species; the first line contains data for the temperatures (°C) 0, 25, 50, 75, 100, 125, and 150, and the second line for 200, 250, 300, and 350. The corresponding reactions together with the sources of thermochemical data are listed in Tables 2 and 3 of the main text.

Parameters and equations used for calculating the activity coefficients are given in the main text and Table ID. Table ID contains the B^* values for the specific temperatures used to calculate the activity coefficients of charged species by the equation (24).

Data for the pressure effects on K values are given in Tables IE and IF. Table IE contains the fit parameters for adjusting the K values of dissolution reactions of 158 minerals. These parameters have been obtained (see text for details) mainly by the regression of high temperature-high pressure values of K reported by Helgeson and others (1978).

Entries in Table IF consist of three parameters. The first refers to the number of the aqueous dissociation reaction from Table IB, the second to the ΔV of this reaction at 25°C, and the third to the number of water ionization reactions that must be added to convert the dissociation reaction to an "ISOCOULOMBIC" form. Table IG contains the Pitzer Coefficients used to calculate the activity of water and the activity coefficients of charged species. Table IH gives the aqueous species number and stoichiometry involved in the congruent dissolution of minerals. This table is used in the calculation of saturation states of minerals and reactions involving mass transfer between minerals and water.

Table IA. Physical Parameters of Aqueous Species.

	<u>Charge</u>	<u>a°</u>	<u>Molecular</u> <u>Weight</u>		<u>Charge</u>	<u>a°</u>	<u>Molecular</u> <u>Weight</u>
1 Ca ++	2	6.0	40.080	53 Ba(OH) +	1	5.0	154.347
2 Mg ++	2	8.0	24.312	54 BaSO4	0	0.0	233.402
3 Na +	1	4.0	22.990	55 CaCO3	0	0.0	100.089
4 K +	1	3.0	39.102	56 CaHCO3 +	1	6.0	101.097
5 Cl -	-1	3.0	35.453	57 Ca(OH) +	1	6.0	57.087
6 SO4 --	-2	4.0	96.062	58 CaPO4 -	-1	5.4	135.051
7 HCO3 -	-1	4.5	61.017	59 CaHPO4	0	0.0	136.059
8 H +	1	9.0	1.008	60 CaH2PO4+	1	5.4	137.067
9 OH -	-1	3.5	17.007	61 CaSO4	0	0.0	136.142
10 H2O	0	0.0	18.015	62 CuCl	0	0.0	98.993
11 H4SiO4	0	0.0	96.115	63 CuCl2 -	-1	4.0	134.446
12 SiO2	0	0.0	60.085	64 CuCl3 --	-2	5.0	169.899
13 Ag +	1	2.5	107.870	65 CuCl +	1	4.0	98.993
14 Al +3	3	9.0	26.982	66 CuCl2	0	0.0	134.446
15 Ba ++	2	5.0	137.340	67 CuCl3 -	-1	4.0	169.899
16 Cu +	1	2.5	63.540	68 CuCl4 --	-2	5.0	205.352
17 Cu ++	2	6.0	63.540	69 Cu(OH) +	1	4.0	80.547
18 Fe ++	2	6.0	55.847	70 CuSO4	0	0.0	159.602
19 Fe +3	3	9.0	55.847	71 FeCl +	1	4.0	91.300
20 Hg2 ++	2	4.0	401.180	72 FeCl2	0	0.0	126.753
21 Hg ++	2	5.0	200.590	73 FeHPO4	0	0.0	151.826
22 Li +	1	6.0	6.939	74 H3PO4	0	0.0	97.995
23 Mn ++	2	6.0	54.938	75 Fe(OH) +	1	5.0	72.854
24 Mn +3	3	9.0	54.938	76 Fe(OH)2	0	0.0	89.862
25 Pb ++	2	4.5	207.190	77 FeOOH -	-1	5.0	88.854
26 Sr ++	2	5.0	87.620	78 FeSO4	0	0.0	151.909
27 Zn ++	2	6.0	65.370	79 FeCl ++	2	5.0	91.300
28 H2AsO3-	-1	4.0	130.936	80 FeCl2 +	1	5.0	126.753
29 PO4 -3	-3	5.0	94.971	81 FeCl3	0	0.0	162.206
30 F -	-1	3.5	18.998	82 FeCl4 -	-1	4.0	197.659
31 B(OH)3	0	0.0	61.833	83 FeSO4 +	1	5.0	151.909
32 NH3	0	0.0	17.031	84 FeSO4)2-	-1	4.0	247.970
33 H2S	0	0.0	34.080	85 Fe(OH)++	2	5.0	72.854
34 AlF ++	2	5.4	45.980	86 Fe(OH)2+	1	5.4	89.862
35 AlF2 +	1	5.4	64.978	87 Fe(OH)3	0	0.0	106.869
36 AlF3	0	0.0	83.977	88 Fe(OH)4-	-1	5.4	123.877
37 AlF4 -	-1	4.5	102.975	89 B(OH)4 -	-1	2.6	78.840
38 Al(OH)++	2	5.4	43.989	90 H2SiO4--	-2	5.4	94.100
39 Al(OH)2+	1	5.4	60.996	91 H3SiO4 -	-1	4.0	95.108
40 Al(OH)4-	-1	4.5	95.011	92 HAsO3 --	-2	5.0	129.928
41 Al(SO4)+	1	4.5	123.043	93 HAsO4 --	-2	5.0	139.929
42 AlSO4)2-	-1	4.5	219.105	94 H2AsO4 -	-1	4.0	140.936
43 AgCl	0	0.0	143.323	95 H3AsO4	0	0.0	141.944
44 AgCl2 -	-1	4.0	178.776	96 HF	0	0.0	20.006
45 AgCl3 --	-2	5.0	214.229	97 H2CO3	0	0.0	62.025
46 AgCl4 -3	-3	6.0	249.682	98 CO3 --	-2	4.5	60.009
47 Ag(SO4)-	-1	4.0	203.932	99 HPO4 --	-2	5.0	95.979
48 CH3COO -	-1	4.5	59.045	100 H2PO4 -	-1	5.4	96.987
49 H3AsO3	0	0.0	125.944	101 HS -	-1	3.5	33.072
50 AsO4 -3	-3	6.0	138.921	102 S --	-2	5.0	32.064
51 BaCO3	0	0.0	197.349	103 HSO4 -	-1	4.5	97.070
52 BaHCO3 +	1	4.0	198.357	104 HNO3	0	0.0	63.013

	<u>Charge</u>	<u>a°</u>	<u>Molecular</u> <u>Weight</u>		<u>Charge</u>	<u>a°</u>	<u>Molecular</u> <u>Weight</u>
105 HgCl +	1	4.0	236.043	159 ZnCl2	0	0.0	136.276
106 HgCl2	0	0.0	271.496	160 ZnCl3 -	-1	4.0	171.729
107 HgCl3 -	-1	4.0	306.949	161 ZnCl4 --	-2	5.0	207.182
108 HgCl4 --	-2	5.0	342.402	162 ZnSO4	0	0.0	161.432
109 HgSO4	0	0.0	296.652	163 AlF5 --	-2	5.0	121.974
110 HgSH2S)2	0	0.0	300.814	164 AlF6 -3	-3	6.0	140.972
111 Hg(HS)3-	-1	4.0	299.806	165 HgOH +	1	4.0	217.597
112 Hg	0	0.0	200.590	166 Hg(OH)2	0	0.0	234.605
113 KCl	0	0.0	74.555	167 U +4	4	9.9	238.030
114 KCO3 -	-1	3.8	99.111	168 UO2 +	1	2.5	270.030
115 KHSO4	0	0.0	136.172	169 UO2 ++	2	6.0	270.030
116 KSO4 -	-1	5.4	135.164	170 UOH +3	3	9.0	255.040
117 KHPO4 -	-1	5.4	135.081	171 U(OH)2++	2	6.0	272.050
118 LiOH	0	0.0	23.946	172 U(OH)3 +	1	2.5	289.060
119 LiSO4 -	-1	5.0	103.001	173 U(OH)4	0	0.0	306.070
120 MgCO3	0	0.0	84.321	174 U(OH)5 -	-1	3.5	323.080
121 MgHCO3 +	1	4.0	85.329	175 UF +3	3	9.0	257.030
122 MgF +	1	4.5	43.310	176 UF2 ++	2	6.0	276.030
123 MgOH +	1	6.5	41.319	177 UF3 +	1	2.5	295.030
124 MgSO4	0	0.0	120.374	178 UF4	0	0.0	314.030
125 MgPO4 -	-1	5.4	119.283	179 UF5 -	-1	3.5	333.030
126 MgHPO4	0	0.0	120.291	180 UF6 --	-2	4.5	352.030
127 MgH2PO4+	1	5.4	121.299	181 UCl +3	3	9.0	273.480
128 MnCl +	1	4.0	90.391	182 UHPO4 ++	2	6.0	334.010
129 MnCl2	0	0.0	125.844	183 U(HPO4)2	0	0.0	429.990
130 MnCl3 -	-1	4.0	161.297	184 U(HPO4)3	-2	4.5	525.970
131 MnCl4 --	-2	5.0	196.750	185 U(HPO4)4	-4	6.0	621.960
132 MnHCO3 +	1	4.0	115.955	186 USO4 ++	2	6.0	334.090
133 MnSO4	0	0.0	151.000	187 U(SO4)2	0	0.0	430.150
134 MnHPO4	0	0.0	150.917	188 U6(OH)15	9	9.9	1683.330
135 MnOH +	1	4.0	71.945	189 UO2OH +	1	2.5	287.040
136 NO3 -	-1	3.0	62.005	190 UO2(OH)2	0	0.0	304.050
137 NaCl	0	0.0	58.443	191 UO2)2OH2	2	6.0	574.080
138 NaCO3 -	-1	5.4	82.999	192 UO2)3OH5	1	2.5	895.140
139 NaHCO3	0	0.0	84.007	193 UO2)3OH7	-1	3.5	929.160
140 Na2CO3	0	0.0	105.989	194 UO2SO4	0	0.0	366.090
141 Na2SO4	0	0.0	142.041	195 UO2SO4)2	-2	4.5	462.150
142 NaSO4 -	-1	5.4	119.051	196 UO2F +	1	2.5	289.030
143 NaHPO4 -	-1	5.4	118.969	197 UO2F2	0	0.0	308.030
144 NaF	0	0.0	41.988	198 UO2F3 -	-1	3.5	327.030
145 NaHS	0	0.0	56.062	199 UO2F4 --	-2	4.5	346.030
146 NH4 +	1	2.5	18.039	200 UO2Cl +	1	2.5	305.480
147 NH4OH	0	0.0	35.046	201 UH3SiO4+	1	2.5	265.140
148 PbCl +	1	4.0	242.643	202 UO2HPO4	0	0.0	366.010
149 PbCl2	0	0.0	278.096	203 UO2HPO42	-2	4.5	461.990
150 PbCl3 -	-1	4.0	313.549	204 UO2H2PO4	1	2.5	367.080
151 PbCl4 --	-2	5.0	349.002	205 UH2PO4)2	0	0.0	464.130
152 PbSO4	0	0.0	303.252	206 UH2PO4)3	-1	3.5	561.180
153 MnCl ++	2	5.0	90.391	207 UO2CO3	0	0.0	330.040
154 Sr(OH) +	1	5.0	104.627	208 UO2CO3)2	-2	4.5	390.050
155 SrCO3	0	0.0	147.629	209 UO2CO3)3	-4	6.0	450.060
156 SrHCO3 +	1	4.0	148.637	210 VO4 -3	-3	5.2	114.940
157 SrSO4	0	0.0	183.682	211 VO ++	2	5.0	66.940
158 ZnCl +	1	4.0	100.823	212 V +3	3	9.0	50.940

	<u>Charge</u>	<u>a°</u>	<u>Molecular</u> <u>Weight</u>		<u>Charge</u>	<u>a°</u>	<u>Molecular</u> <u>Weight</u>		
213	HVO4 --	-2	5.2	115.950	267	H2C4H4O4	0	0.0	118.088
214	H2VO4 -	-1	5.6	116.960	268	AlSuc +	1	4.5	143.054
215	H3VO4	0	0.0	117.970	269	AlSuc)2-	-1	4.5	143.054
216	H4VO4 +	1	4.0	118.980	270	BaSuc	0	0.0	253.412
217	NaHVO4 -	-1	4.0	138.940	271	CaSuc	0	0.0	156.152
218	VO2F	0	0.0	101.940	272	FeSuc	0	0.0	171.919
219	VO2F2 -	-1	4.0	120.940	273	FeSuc +	1	4.5	171.919
220	VOH ++	2	5.0	67.950	274	KSuc -	-1	4.5	155.174
221	V(OH)2 +	1	5.4	84.960	275	MgSuc	0	0.0	140.384
222	V(OH)3	0	0.0	101.970	276	MnSuc	0	0.0	171.010
223	VOOH +	1	2.5	83.950	277	NaSuc -	-1	4.5	139.062
224	VOSO4	0	0.0	163.000	278	PbSuc	0	0.0	323.262
225	VOC1 +	1	2.5	102.390	279	SrSuc	0	0.0	203.692
226	VOF +	1	2.5	85.940	280	ZnSuc	0	0.0	181.442
227	VOF2	0	0.0	104.940	281	CaCl +	1	4.0	75.533
228	CH3COOH	0	0.0	60.053	282	CaCl2	0	0.0	110.986
229	AlAce ++	2	4.5	86.027	283	FeF ++	2	5.0	74.845
230	BaAce +	1	4.5	196.385	284	SiF6 --	-2	5.0	142.076
231	CaAce +	1	4.5	99.125	285	CH4 Gas	0	0.0	16.043
232	CuAce +	1	4.5	122.585	286	Pb(HS)2	0	0.0	273.334
233	FeAce +	1	4.5	114.892	287	Pb(HS)3-	-1	4.0	306.416
234	Fe(Ace)2	0	0.0	173.937	288	PbCO3	0	0.0	267.199
235	KAce	0	0.0	98.147	289	PbOH +	1	4.0	224.197
236	MgAce +	1	4.5	83.357	290	Zn(HS)2	0	0.0	131.514
237	NaAce	0	0.0	82.035	291	Zn(HS)3-	-1	4.0	164.596
238	PbAce +	1	4.5	266.235	292	ZnHCO3 +	1	4.0	126.387
239	Pb(Ace)2	0	0.0	325.280	293	ZnOH +	1	4.0	82.377
240	Pb(Ace)3	-1	4.5	384.325	294	Zn(OH)2	0	0.0	99.385
241	SrAce +	1	4.5	146.665	295	ZnHSOH	0	0.0	115.449
242	UO2Ace +	1	3.5	329.075					
243	UO2Ace2	0	0.0	338.120					
244	ZnAce +	1	4.5	124.415					
245	Zn(Ace)2	0	0.0	183.460					
246	C2O4 --	-2	5.4	88.018					
247	HC2O4 -	-1	4.5	89.026					
248	H2C2O4	0	0.0	90.034					
249	AlOxy +	1	4.5	115.000					
250	AlOxy)2-	-1	4.5	203.018					
251	BaOxy	0	0.0	225.358					
252	CaOxy	0	0.0	128.098					
253	FeOxy	0	0.0	143.865					
254	FeOxy +	1	4.5	143.865					
255	KOxy -	-1	4.5	127.120					
256	MgOxy	0	0.0	112.330					
257	MnOxy	0	0.0	142.956					
258	MnOxy)2	-2	5.4	197.894					
259	MnOxy)3	-4	5.4	252.832					
260	MnOxy +	1	4.5	142.956					
261	NaOxy -	-1	4.5	111.008					
262	PbOxy	0	0.0	295.208					
263	SrOxy	0	0.0	175.638					
264	ZnOxy	0	0.0	153.388					
265	C4H4O4--	-2	5.4	116.072					
266	HC4H4O4-	-1	4.5	117.080					

Table IB. Equilibrium Constants of Dissociation, and
Redox Reactions at 0° to 350°C.

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
1 HCO ₃ -	-10.63 -10.78	-10.33 -11.29	-10.17 -11.88	-10.13 -12.53	-10.16	-10.25	-10.39
2 H ₂ O	-14.94 -11.31	-13.99 -11.20	-13.27 -11.33	-12.71 -11.88	-12.26	-11.91	-11.64
3 H ₄ SiO ₄	-10.28 -8.87	-9.83 -8.96	-9.49 -9.20	-9.26 -9.36	-9.09	-8.97	-8.90
4 Cu ++	-11.09 -7.21	-10.35 -6.66	-9.72 -6.20	-9.16 -5.80	-8.68	-8.25	-7.86
5 Fe +3	8.96 7.92	8.80 7.84	8.64 7.85	8.48 7.94	8.33	8.20	8.09
6 Hg ++	6.11 -0.97	4.67 -1.85	3.46 -2.56	2.44 -3.14	1.56	0.80	0.13
7 Mn +3	13.23 6.80	11.95 5.98	10.86 5.31	9.94 4.74	9.14	8.44	7.83
8 H ₂ AsO ₃ -	-12.68 -11.35	-12.13 -11.70	-11.74 -12.10	-11.47 -12.60	-11.30	-11.23	-11.20
9 AlF ₅ --	-20.39 -25.20	-20.40 -27.77	-20.61 -30.86	-20.99 -34.72	-21.54	-22.26	-23.16
10 H ₂ S	-7.40 -7.17	-7.00 -7.72	-6.75 -8.43	-6.63 -9.23	-6.61	-6.61	-6.75
11 AlF ++	-6.94 -8.78	-6.97 -9.69	-7.07 -10.94	-7.22 -11.93	-7.43	-7.71	-8.04
12 AlF ₂ +	-12.52 -15.88	-12.57 -17.53	-12.76 -19.64	-13.05 -21.60	-13.45	-13.93	-14.51
13 AlF ₃	-16.61 -20.82	-16.65 -22.94	-16.86 -25.42	-17.22 -28.21	-17.72	-18.34	-19.06
14 AlF ₄ -	-19.00 -23.89	-19.04 -26.08	-19.26 -28.87	-19.64 -32.02	-20.18	-20.88	-21.75
15 Al(OH)++	-9.17 -9.32	-9.04 -9.54	-8.96 -9.86	-8.97 -10.49	-9.00	-9.05	-9.13
16 Al(OH)2+	-18.08 -22.19	-18.06 -24.38	-18.22 -26.92	-18.57 -29.81	-19.05	-19.66	-20.40
17 Al(OH)4-	-33.72 -31.88	-32.77 -32.40	-32.20 -33.10	-31.84 -34.20	-31.67	-31.58	-31.59
18 Al(SO ₄)+	-2.88 -4.55	-3.00 -5.18	-3.16 -5.88	-3.34 -6.65	-3.54	-3.76	-4.01
19 AlSO ₄)2-	-4.72 -7.13	-4.89 -8.06	-5.10 -9.01	-5.35 -10.27	-5.64	-5.96	-6.32
20 AgCl	-3.70 -2.90	-3.32 -3.07	-3.07 -3.54	-2.94 -4.22	-2.88	-2.88	-2.88
21 AgCl ₂ -	-5.80 -4.58	-5.32 -4.86	-4.74 -5.42	-4.52 -6.52	-4.46	-4.46	-4.45
22 AgCl ₃ --	-6.30 -3.66	-5.10 -3.70	-4.40 -3.85	-4.00 -4.10	-3.85	-3.77	-3.73
23 AgCl ₄ -3	-5.80 -1.40	-3.90 -1.50	-3.10 -1.70	-2.40 -2.10	-1.94	-1.70	-1.60
24 Ag(SO ₄)-	-1.22 -2.23	-1.31 -2.69	-1.41 -3.44	-1.51 -5.02	-1.62	-1.75	-1.89
25 CH ₃ COOH	-4.77 -5.58	-4.76 -6.10	-4.78 -6.80	-4.85 -7.68	-4.79	-5.12	-5.31
26 BaCO ₃	-2.40 -3.60	-2.50 -4.10	-2.60 -4.70	-2.70 -5.30	-2.85	-3.00	-3.20

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
27 BaHCO ₃)+	-1.18 -3.62	-1.44 -4.60	-1.70 -5.60	-2.00 -6.80	-2.27	-2.60	-2.88
28 Ba(OH)+	-0.43 -1.86	-0.53 -2.30	-0.65 -2.83	-0.83 -3.68	-1.03	-1.22	-1.43
29 BaSO ₄	-2.39 -2.38	-2.31 -2.59	-2.26 -3.01	-2.23 -3.60	-2.23	-2.24	-2.26
30 CaCO ₃	-3.14 -5.44	-3.22 -6.30	-3.51 -7.24	-3.86 -8.28	-4.17	-4.32	-4.67
31 CaHCO ₃)+	-0.82 -2.33	-1.11 -2.64	-1.28 -2.90	-1.47 -3.10	-1.66	-1.83	-2.00
32 Ca(OH)+	-1.03 -2.51	-1.14 -2.91	-1.28 -3.44	-1.47 -4.24	-1.67	-1.87	-2.08
33 CaPO ₄ -	-6.31 -9.19	-6.47 -10.77	-6.69 -13.41	-6.95 -19.11	-7.23	-7.65	-8.09
34 CaHPO ₄	-2.41 -4.58	-2.61 -5.56	-2.82 -7.13	-3.05 -10.46	-3.29	-3.57	-3.87
35 CaH ₂ PO ₄ +	-1.23 -3.21	-1.44 -4.01	-1.65 -5.27	-1.87 -7.90	-2.10	-2.34	-2.60
36 CaSO ₄	-2.30 -3.60	-2.30 -4.10	-2.40 -4.50	-2.55 -5.00	-2.70	-2.90	-3.10
37 CuCl	-2.80 -2.25	-2.70 -2.20	-2.65 -2.40	-2.60 -2.70	-2.50	-2.45	-2.35
38 CuCl ₂ -	-4.99 -5.82	-4.94 -6.57	-4.94 -7.40	-4.98 -8.80	-5.06	-5.19	-5.35
39 CuCl ₃ --	-5.15 -6.36	-5.14 -7.25	-5.18 -8.30	-5.27 -10.50	-5.39	-5.56	-5.78
40 CuCl +	-0.53 -3.73	-0.02 -4.80	-0.54 -6.00	-1.04 -7.30	-1.54	-2.05	-2.58
41 CuCl ₂	1.38 -3.67	0.71 -4.90	0.08 -6.50	-0.53 -8.50	-1.13	-1.73	-2.34
42 CuCl ₃ -	3.18 -3.08	2.30 -4.60	1.49 -6.50	0.72 -9.00	-0.02	-0.76	-1.50
43 CuCl ₄ --	5.75 -2.04	4.60 -3.90	3.56 -6.10	2.58 -8.70	1.65	0.74	-0.16
44 Cu(OH)+	-6.19 -6.57	-6.06 -6.89	-6.06 -7.32	-6.02 -8.06	-6.08	-6.18	-6.30
45 CuSO ₄	-2.19 -3.26	-2.25 -3.84	-2.34 -4.79	-2.44 -6.84	-2.56	-2.70	-2.86
46 FeCl +	1.06 -1.58	0.53 -2.34	0.08 -2.33	-0.31 -2.00	-0.66	-0.69	-1.23
47 FeCl ₂	9.19 1.35	8.21 -0.61	7.23 -2.57	6.25 -4.53	5.27	4.29	3.31
48 FeHPO ₄	-3.49 -5.00	-3.60 -5.60	-3.72 -6.30	-3.89 -7.10	-4.09	-4.30	-4.56
49 H ₃ PO ₄	-21.97 -23.71	-21.69 -24.97	-21.63 -26.60	-21.80 -29.15	-22.02	-22.34	-22.73
50 Fe(OH) +	-4.54 -5.19	-4.50 -5.49	-4.50 -5.87	-4.57 -6.54	-4.66	-4.77	-4.90
51 Fe(OH) ₂	-7.28 -9.73	-7.39 -10.54	-7.57 -11.50	-7.87 -13.04	-8.20	-8.55	-8.94
52 FeOOH -	31.22 21.36	29.00 20.41	27.22 19.77	25.76 19.36	24.55	23.54	22.68
53 FeSO ₄	-2.41 -3.19	-2.43 -3.69	-2.48 -4.53	-2.54 -6.37	-2.63	-2.73	-2.86
54 FeCl ++	-0.98 -5.06	-1.47 -6.20	-1.96 -7.50	-2.45 -8.80	-2.94	-3.45	-3.97

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
55 FeCl ₂ +	-1.64 -5.87	-2.13 -7.11	-2.62 -8.46	-3.12 -9.89	-3.62	-4.16	-4.72
56 FeCl ₃	-0.48 -5.64	-1.13 -7.06	-1.75 -8.59	-2.37 -10.19	-2.99	-3.63	-4.30
57 FeCl ₄ -	1.67 -4.83	0.79 -6.49	-0.04 -8.24	-0.84 -10.05	-1.63	-2.42	-3.23
58 FeSO ₄ +	-3.77 -7.54	-4.14 -8.79	-4.54 -10.16	-4.96 -11.64	-5.42	-5.91	-6.42
59 FeSO ₄) ₂ -	5.16 8.61	5.42 10.40	5.72 13.40	6.07 20.89	6.45	6.89	7.38
60 Fe(OH)++	-12.10 -11.68	-11.86 -11.82	-11.69 -12.08	-11.60 -12.66	-11.55	-11.56	-11.58
61 Fe(OH) ₂ +	-21.14 -23.71	-20.88 -25.66	-20.75 -28.01	-20.89 -30.70	-21.17	-21.61	-22.19
62 Fe(OH) ₃	-30.28 -23.31	-28.50 -23.60	-27.01 -25.06	-25.90 -30.05	-24.97	-24.28	-23.79
63 Fe(OH) ₄ -	-34.92 -36.95	-34.06 -39.47	-33.70 -42.68	-33.64 -46.43	-33.83	-34.28	-34.95
64 H ₄ (BO ₄) -	-5.45 -2.27	-4.77 -1.98	-4.20 -1.80	-3.72 -1.70	-3.32	-2.99	-2.71
65 AlF ₆ -3	-20.97 -25.14	-20.88 -27.54	-21.00 -30.39	-21.30 -33.81	-21.18	-22.42	-23.25
66 H ₃ SiO ₄) -	-12.20 -11.00	-11.70 -11.50	-11.30 -12.00	-11.10 -13.00	-11.00	-11.00	-11.00
67 H ₃ AsO ₃	-9.70 -8.22	-9.29 -8.29	-8.94 -8.51	-8.67 -8.59	-8.49	-8.35	-8.27
68 HAsO ₄ --	-11.85 -11.50	-11.52 -11.90	-11.30 -12.40	-11.20 -12.90	-11.15	-11.20	-11.25
69 H ₂ AsO ₄ -	-18.79 -19.19	-18.46 -20.01	-18.24 -21.12	-18.20 -22.40	-18.24	-18.40	-18.61
70 H ₃ AsO ₄	-20.95 -22.60	-20.70 -23.57	-20.60 -25.49	-20.71 -27.40	-20.90	-21.23	-21.63
71 HF	-2.99 -4.86	-3.18 -5.40	-3.38 -5.95	-3.61 -6.50	-3.84	-4.09	-4.33
72 H ₂ CO ₃	-6.58 -7.23	-6.35 -7.79	-6.29 -8.40	-6.32 -8.26	-6.43	-6.58	-6.77
73 HPO ₄ --	-12.62 -12.45	-12.34 -12.80	-12.18 -13.30	-12.14 -13.80	-12.10	-12.14	-12.20
74 H ₂ PO ₄ -	-19.93 -20.35	-19.54 -21.16	-19.36 -22.26	-19.38 -24.20	-19.43	-19.58	-19.77
75 HS -	-17.50 -15.10	-17.00 -14.80	-16.70 -14.60	-16.30 -14.40	-16.10	-15.80	-15.40
76 HSO ₄ -	-1.63 -4.51	-1.95 -5.29	-2.29 -6.08	-2.64 -6.88	-3.00	-3.37	-3.74
77 HNO ₃	1.67 -0.49	1.43 -1.04	1.13 -1.66	0.85 -2.25	0.59	0.30	0.05
78 HgCl +	-6.59 -5.54	-6.25 -5.78	-5.99 -6.39	-5.80 -8.00	-5.65	-5.56	-5.51
79 HgCl ₂	-14.18 -10.36	-13.26 -10.34	-12.51 -10.84	-11.91 -12.63	-11.42	-11.03	-10.73
80 HgCl ₃ -	-16.40 -12.09	-15.35 -12.10	-14.50 -12.73	-13.81 -14.91	-13.26	-12.82	-12.48
81 HgCl ₄ --	-15.85 -12.34	-14.92 -12.58	-14.18 -13.53	-13.59 -16.35	-13.13	-12.79	-12.54
82 HgSO ₄	-1.20 -3.20	-1.40 -4.00	-1.60 -5.10	-1.90 -6.05	-2.10	-2.30	-2.60

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
83 HgSH ₂ S) ₂	-38.50 -25.15	-35.65 -24.04	-33.25 -23.83	-31.26 -25.50	-29.58	-28.16	-26.97
84 Hg(HS) ₃ -	-24.41 -9.79	-22.03 -7.15	-19.90 -5.31	-18.13 -6.16	-16.13	-14.43	-12.79
85 Hg	-3.28 -10.30	-4.06 -13.04	-5.61 -17.31	-6.42 -26.18	-7.28	-8.20	-9.19
86 KCl	1.00 -0.06	0.88 -0.34	0.77 -0.95	0.67 -1.90	0.57	0.46	0.34
87 KCO ₃ -	-1.04 -2.10	-1.07 -2.67	-1.14 -3.64	-1.24 -5.80	-1.37	-1.52	-1.96
88 KHSO ₄	-0.65 -1.80	-0.85 -2.20	-1.05 -2.60	-1.15 -3.20	-1.29	-1.39	-1.41
89 KSO ₄ -	-0.87 -1.74	-0.89 -2.21	-0.95 -3.00	-1.04 -4.78	-1.14	-1.27	-1.41
90 KHPO ₄ -	-0.11 -3.01	-0.29 -4.59	-0.51 -7.23	-0.77 -12.42	-1.05	-1.47	-1.91
91 LiOH	-0.26 -0.68	-0.18 -0.87	-0.20 -1.07	-0.26 -1.30	-0.34	-0.42	-0.50
92 Li(SO ₄)-	-0.64 -0.64	-0.64 -0.64	-0.64 -0.64	-0.64 -0.64	-0.64	-0.64	-0.64
93 MgCO ₃	-2.87 -4.40	-2.98 -4.98	-3.11 -5.65	-3.27 -6.37	-3.46	-3.66	-3.89
94 MgHCO ₃ +	-1.00 -1.77	-1.07 -2.04	-1.14 -2.34	-1.23 -2.67	-1.32	-1.42	-1.53
95 MgF +	-1.54 -3.70	-1.82 -4.40	-2.11 -5.29	-2.41 -6.27	-2.72	-3.00	-3.20
96 Mg(OH) +	-2.55 -4.04	-2.60 -4.59	-2.71 -5.03	-2.89 -5.82	-3.09	-3.32	-3.56
97 MgSO ₄	-2.34 -3.32	-2.40 -3.64	-2.49 -3.96	-2.60 -4.27	-2.73	-2.87	-3.02
98 MgPO ₄ -	-6.31 -9.19	-6.47 -10.77	-6.69 -13.41	-6.95 -19.11	-7.23	-7.65	-8.09
99 MgHPO ₄	-2.91 -5.08	-3.11 -6.06	-3.32 -7.63	-3.55 -11.00	-3.79	-4.07	-4.37
100 MgH ₂ PO ₄ +	-1.23 -3.21	-1.44 -4.01	-1.65 -5.27	-1.87 -7.90	-2.10	-2.34	-2.60
101 MnCl +	6.50 6.00	6.50 5.70	6.45 5.20	6.40 4.00	6.35	6.30	6.20
102 MnCl ₂	3.15 2.25	3.10 1.80	3.00 1.00	2.95 -0.70	2.90	2.80	2.65
103 MnCl ₃ -	1.80 0.40	1.70 -0.20	1.60 -1.20	1.50 -3.40	1.30	1.15	0.95
104 MnCl ₄ --	1.05 -1.00	0.80 -1.80	0.60 -3.10	0.40 -5.80	0.15	-0.15	-0.40
105 MnHCO ₃ +	-1.25 -2.54	-1.27 -3.02	-1.36 -3.51	-1.50 -4.00	-1.68	-1.87	-2.08
106 MnSO ₄	-2.03 -3.70	-2.26 -4.49	-2.40 -5.85	-2.56 -9.10	-2.74	-2.93	-3.15
107 MnCl ++	-2.12 -6.20	-2.61 -7.34	-3.10 -8.64	-3.59 -9.94	-4.08	-4.59	-5.11
108 MnHPO ₄	-3.47 -4.98	-3.58 -5.60	-3.70 -6.30	-3.87 -7.10	-4.07	-4.28	-4.55
109 MnOH +	-3.41 -4.64	-3.44 -5.17	-3.52 -5.91	-3.66 -7.24	-3.82	-4.00	-4.20
110 NaCl	1.00 0.15	0.85 -0.25	0.80 -0.95	0.70 -2.00	0.65	0.55	0.45

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
111 NaCO3 -	-0.71 -5.10	-1.27 -6.15	-1.81 -7.20	-2.35 -8.30	-2.89	-3.45	-4.04
112 NaHCO3	0.39 -0.68	0.25 -0.96	0.12 -1.40	-0.01 -1.80	-0.13	-0.25	-0.38
113 Na2CO3	1.00 -1.40	0.68 -2.20	0.40 -3.20	0.20 -4.30	-0.05	-0.40	-0.70
114 Na2SO4	999.99 999.99	999.99 999.99	999.99 999.99	999.99 999.99	999.99	999.99	999.99
115 NaSO4 -	-1.00 -2.20	-1.20 -2.60	-1.30 -3.00	-1.50 -3.80	-1.64	-1.80	-1.90
116 NaHPO4 -	-0.11 -3.01	-0.29 -4.59	-0.51 -7.23	-0.77 -12.42	-1.05	-1.47	-1.91
117 Hg(OH) +	-10.90 -10.08	-10.46 -10.79	-10.14 -12.29	-9.92 -15.93	-9.79	-9.74	-9.77
118 NH4OH	-4.87 -5.53	-4.75 -6.00	-4.70 -6.75	-4.75 -8.00	-4.85	-4.95	-5.10
119 NaHS	0.90 -0.06	0.83 -0.34	0.77 -0.95	0.69 -1.90	0.57	0.47	0.34
120 NaF	1.06 -0.22	0.88 -0.55	0.70 -0.93	0.54 -1.45	0.38	0.23	0.08
121 PbCl +	-1.39 -2.55	-1.41 -3.18	-1.47 -3.89	-1.55 -4.80	-1.67	-1.85	-2.09
122 PbCl2	-1.80 -4.00	-1.97 -4.98	-2.17 -6.26	-2.39 -8.20	-2.62	-2.89	-3.18
123 PbCl3 -	-1.64 -3.81	-1.66 -5.03	-1.70 -6.76	-1.91 -9.50	-2.21	-2.50	-2.84
124 PbCl4 --	-1.40 -2.14	-1.46 -2.14	-1.56 -2.14	-1.73 -2.14	-1.93	-2.14	-2.36
125 PbSO4	-2.75 -2.75	-2.75 -2.75	-2.75 -2.75	-2.75 -2.75	-2.75	-2.75	-2.75
126 Zn(AC)2	-1.02 -3.96	-1.35 -5.07	-1.72 -7.02	-2.04 -11.55	-2.33	-2.70	-3.07
127 Sr(OH) +	-0.57 -2.07	-0.69 -2.52	-0.83 -3.06	-0.99 -3.92	-1.22	-1.42	-1.63
128 SrCO3	-2.48 -5.90	-2.82 -7.40	-3.13 -9.24	-3.45 -11.65	-3.77	-4.18	-4.72
129 SrHCO3 +	-0.82 -4.14	-1.19 -5.35	-1.56 -6.88	-1.93 -8.86	-2.31	-2.70	-3.12
130 SrSO4	-2.12 -3.25	-2.20 -3.84	-2.29 -4.81	-2.40 -6.30	-2.52	-2.67	-2.84
131 ZnCl +	0.07 -4.01	-0.42 -5.21	-0.88 -6.55	-1.35 -8.00	-1.80	-2.34	-2.89
132 ZnCl2	-0.13 -3.98	-0.62 -5.70	-1.04 -7.51	-1.45 -9.54	-1.92	-2.37	-2.96
133 ZnCl3 -	-0.11 -3.00	-0.34 -3.89	-0.62 -4.86	-0.94 -5.85	-1.36	-1.69	-2.02
134 ZnCl4 --	1.07 -4.23	-0.18 -6.24	-1.03 -9.00	-1.63 -12.70	-2.04	-2.57	-3.21
135 ZnSO4	-2.10 -3.60	-2.21 -4.36	-2.35 -5.68	-2.50 -6.85	-2.67	-2.86	-3.07
136 AsO4 -3	6.05 6.33	5.21 7.75	4.62 9.80	4.53 12.60	4.73	5.00	5.30
137 Hg(OH)2	-22.99 -19.77	-21.87 -20.77	-21.02 -23.14	-20.38 -29.13	-19.94	-19.66	-19.54
138 Fe2-Fe3	17.10 22.33	17.75 23.92	18.38 26.01	19.01 29.87	19.64	20.29	20.94

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
139 Cu+-Cu2	3.77	4.25	4.65	5.00	5.32	5.61	5.89
	6.41	6.93	7.52	8.49			
140 Hg2-2Hg2	20.90	20.95	21.01	21.07	21.15	21.23	21.32
	21.56	21.90	22.47	23.78			
141 Mn2-Mn3	34.00	34.48	34.97	35.47	36.49	37.00	38.06
	28.80	28.60	28.50	28.30			
142 U4-UO2+	10.62	8.74	6.87	4.99	3.12	1.25	-0.61
	-4.35	-8.07	-11.79	-15.51			
143 UO2+-++	-3.76	-3.77	-3.83	-3.94	-4.08	-4.26	-4.48
	-5.01	-5.66	-6.42	-7.27			
144 V - VO	-6.72	-5.71	-4.87	-4.15	-3.53	-3.00	-2.53
	-1.74	-1.12	-0.61	-0.19			
145 VO - VO4	-48.37	-45.34	-42.90	-40.92	-39.45	-38.12	-37.19
	-36.21	-36.58	-39.28	-48.59			
146 CaCl +	-0.12	-0.42	-0.65	-0.87	-1.08	-1.25	-1.49
	-1.88	-2.04	-2.59	-2.91			
147 CaCl2	0.30	0.15	-0.02	-0.25	-0.51	-0.83	-1.15
	-1.82	-2.58	-3.44	-4.81			
148 UOH +3	-13.41	-13.27	-13.21	-13.19	-13.19	-13.21	-13.25
	-13.41	-13.69	-14.10	-14.66			
149 U(OH)2++	-26.29	-25.65	-25.24	-24.96	-24.78	-24.67	-24.64
	-24.78	-25.23	-25.99	-27.07			
150 U(OH)3 +	5.54	5.00	3.69	2.64	1.77	1.01	0.37
	-0.74	-1.60	-2.01	-0.93			
151 U(OH)4	10.25	8.57	7.13	6.05	5.18	4.47	3.88
	2.94	2.27	1.17	4.03			
152 U(OH)5 -	17.28	15.09	13.30	11.86	10.65	9.63	8.77
	7.44	6.57	6.14	10.06			
153 UF +3	-8.35	-8.66	-9.24	-9.51	-9.78	-10.03	-10.57
	-10.57	-11.16	-11.96	-13.55			
154 UF2 ++	-14.08	-14.49	-14.94	-15.40	-15.86	-16.33	-16.81
	-17.83	-19.01	-20.62	-23.85			
155 UF3 +	-18.86	-19.10	-19.48	-19.94	-20.45	-21.01	-21.63
	-23.07	-24.92	-27.71	-33.83			
156 UF4	-23.56	-23.72	-24.07	-24.54	-25.11	-25.72	-26.48
	-28.23	-30.57	-34.17	-42.23			
157 UF5 -	-25.19	-25.35	-25.72	-26.21	-26.78	-27.45	-28.21
	-30.09	-32.68	-36.85	-46.59			
158 UF6 --	-27.64	-27.68	-27.99	-28.45	-29.02	-29.69	-30.46
	-32.34	-34.88	-38.84	-47.78			
159 UC1 +3	-2.58	-2.59	-2.76	-3.03	-3.38	-3.79	-4.25
	-5.28	-6.45	-7.73	-9.12			
160 UHPO4 ++	-11.39	-12.06	-12.73	-13.41	-14.09	-14.75	-15.40
	-16.66	-17.86	-19.00	-20.08			
161 U(HPO4)2	-21.53	-21.99	-22.59	-23.29	-24.06	-24.88	-25.72
	-27.44	-29.18	-30.90	-32.57			
162 U(HPO4)3	-8.81	-9.06	-9.43	-9.79	-10.33	-10.74	-11.23
	-11.99	-12.67	-13.27	-13.63			
163 U(HPO4)4	-10.56	-9.86	-9.50	-9.24	-9.33	-9.34	-9.52
	-9.76	-10.05	-10.55	-10.54			
164 USO4 ++	-5.56	-5.54	-5.68	-5.92	-6.23	-6.59	-7.01
	-8.00	-9.21	-10.65	-12.34			
165 U(SO4)2	-9.61	-9.84	-10.25	-10.76	-11.32	-11.95	-12.63
	-14.22	-16.17	-18.55	-21.39			
166 U6(OH)15	-31.52	-24.80	-18.42	-12.06	-5.90	-0.09	5.55
	16.47	27.80	38.00	38.00			

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
167 UO2OH +	-8.42 -7.86	-8.23 -7.98	-8.10 -8.24	-8.01 -8.65	-7.94	-7.89	-7.85
168 UO2(OH)2	-16.71 -13.76	-16.05 -13.65	-15.54 -13.84	-15.11 -14.37	-14.74	-14.41	-14.14
169 UO2)2OH2	-23.42 -19.56	-22.43 -19.55	-21.68 -19.89	-21.08 -20.58	-20.60	-20.21	-19.91
170 UO2)3OH5	17.35 10.51	15.64 10.09	14.18 10.33	13.14 12.98	12.35	11.73	11.20
171 UO2)3OH7	33.97 15.81	30.80 12.82	27.84 10.00	25.36 12.22	23.14	21.10	19.24
172 UO2SO4	-2.72 -7.34	-2.93 -9.10	-3.33 -11.09	-3.84 -13.29	-4.43	-5.08	-5.78
173 UO2SO4)2	-3.81 -7.75	-4.18 -9.57	-4.57 -12.69	-4.99 -20.01	-5.43	-5.92	-6.46
174 UO2F +	-5.27 -6.01	-5.19 -6.54	-5.19 -7.32	-5.24 -8.94	-5.33	-5.46	-5.62
175 UO2F2	-9.04 -9.86	-8.92 -10.58	-8.91 -11.80	-8.96 -14.68	-9.06	-9.19	-9.37
176 UO2F3 -	-11.53 -11.72	-11.43 -12.29	-11.39 -13.57	-11.38 -17.36	-11.38	-11.40	-11.46
177 UO2F4 --	-12.71 -14.36	-12.54 -15.73	-12.55 -18.07	-12.66 -23.75	-12.85	-13.11	-13.45
178 UO2Cl +	-1.71 -6.83	-2.10 -8.45	-2.62 -10.14	-3.22 -11.91	-3.88	-4.57	-5.30
179 UH3SiO6+	2.62 1.51	2.40 1.37	2.21 1.25	2.06 1.15	1.92	1.80	1.69
180 UO2HPO4	-8.37 -10.19	-8.41 -10.86	-8.53 -11.55	-8.73 -12.23	-8.97	-9.24	-9.54
181 UO2HPO42	-18.73 -21.62	-18.25 -23.41	-18.16 -25.30	-18.36 -27.23	-18.77	-19.34	-20.02
182 UO2H2PO4	-10.22 -11.70	-10.15 -12.39	-10.20 -13.10	-10.44 -13.82	-10.54	-10.79	-11.07
183 UH4P2O10	-20.68 -20.17	-19.92 -20.99	-19.48 -21.92	-19.27 -22.92	-19.24	-19.34	-19.54
184 UH6P3O14	-30.18 -28.45	-28.80 -29.62	-27.94 -30.99	-27.48 -32.48	-27.32	-27.37	-27.61
185 UO2CO3	-10.41 -13.11	-10.04 -14.84	-10.00 -16.87	-10.20 -19.59	-10.55	-11.04	-11.65
186 UO2CO3)2	4.31 2.36	3.60 2.35	3.11 2.10	2.77 0.67	2.56	2.43	2.37
187 UO2CO3)3	9.42 7.54	9.55 6.36	9.51 4.62	9.36 1.03	9.12	8.81	8.45
188 HVO4 -3	-13.62 -14.14	-13.27 -15.53	-13.02 -17.60	-12.98 -20.48	-12.95	-13.21	-13.32
189 H2VO4 --	-21.92 -22.47	-21.33 -24.58	-20.94 -27.76	-20.73 -32.22	-20.74	-20.86	-21.24
190 H3VO4 -	-26.55 -22.93	-25.16 -25.94	-24.11 -28.85	-23.25 -32.85	-22.83	-22.55	-22.47
191 H4VO4	-29.76 -26.16	-28.38 -27.54	-27.33 -29.94	-26.57 -33.48	-26.06	-25.77	-25.69
192 NaHVO4 --	-0.20 -0.90	-0.30 -1.10	-0.40 -1.40	-0.40 -1.70	-0.50	-0.60	-0.70
193 VO2F	-27.17 -16.25	-24.96 -14.94	-23.10 -13.99	-21.51 -13.55	-20.16	-18.98	-17.95
194 VO2F2 -	-22.78 -15.13	-21.10 -14.55	-19.73 -14.48	-18.56 -15.70	-17.63	-16.82	-16.15

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
195 V(OH) ++	-11.88 -11.52	-11.73 -11.83	-11.48 -12.03	-11.40 -12.60	-11.32	-11.32	-11.38
196 V(OH)2 +	-23.48 -18.62	-22.13 -19.00	-21.07 -20.00	-20.18 -21.67	-19.62	-19.15	-18.83
197 V(OH)3	-32.69 -26.76	-30.92 -27.61	-29.55 -29.60	-28.40 -33.30	-27.73	-27.18	-26.85
198 VOOH +	-8.52 -8.87	-8.32 -9.31	-8.29 -9.82	-8.23 -10.57	-8.28	-8.38	-8.50
199 VOSO4	2.72 0.24	2.48 -0.69	2.18 -2.00	1.88 -3.10	1.57	1.23	0.92
200 VOCl +	0.13 -1.25	-0.04 -1.69	-0.21 -2.34	-0.36 -3.74	-0.54	-0.70	-0.87
201 VOF +	-3.39 -4.25	-3.30 -4.85	-3.28 -6.40	-3.43 -6.95	-3.56	-3.68	-3.86
202 VOF2	-5.61 -5.82	-5.46 -6.35	-5.37 -7.10	-5.30 -8.10	-5.34	-5.40	-5.50
203 UO2 Ace+	-2.23 -4.09	-2.39 -4.99	-2.57 -6.55	-2.76 -10.24	-2.96	-3.20	-3.46
204 UO2(Ace2	-4.41 -6.33	-4.51 -7.47	-4.64 -9.51	-4.81 -14.44	-5.03	-5.28	-5.57
205 UO2 +	10.66 8.33	10.24 8.10	9.87 8.00	8.53 8.04	9.22	8.95	8.71
206 U +4	5.19 12.68	6.62 13.86	7.84 14.96	8.89 16.04	9.81	10.62	11.37
207 VO ++	-7.11 -9.00	-7.44 -9.42	-7.73 -9.91	-7.94 -10.46	-8.20	-8.40	-8.60
208 VO4 -3	34.98 22.51	32.33 21.43	30.13 21.21	28.27 22.99	26.71	25.38	24.25
209 AlAce +	-2.86 -2.86	-2.86 -2.86	-2.86 -2.86	-2.86 -2.86	-2.86	-2.86	-2.86
210 BaAce +	-1.08 -1.80	-1.13 -2.20	-1.19 -2.85	-1.26 -3.60	-1.40	-1.40	-1.53
211 CaAce +	-1.18 -1.90	-1.23 -2.30	-1.29 -2.92	-1.36 -3.73	-1.44	-1.54	-1.64
212 CuAce +	-1.84 -2.74	-1.89 -3.25	-1.96 -4.17	-2.04 -6.36	-2.14	-2.26	-2.40
213 FeAce +	-0.60 -2.40	-0.87 -3.00	-1.10 -3.70	-1.38 -4.80	-1.60	-1.79	-2.00
214 FeAce)2	-1.70 -4.00	-1.89 -5.27	-2.10 -6.82	-2.34 -8.90	-2.60	-2.90	-3.20
215 KAce	0.31 0.13	0.39 0.13	0.13 0.13	0.13 0.13	0.13	0.13	0.13
216 MgAce +	-1.35 -0.86	-1.25 -0.82	-1.16 -0.80	-1.09 -0.81	-1.03	-0.97	-0.93
217 NaAce	0.33 0.11	0.23 0.11	0.11 0.11	0.11 0.11	0.11	0.11	0.11
218 PbAce +	-2.28 -2.71	-2.26 -3.10	-2.26 -3.83	-2.29 -5.63	-2.33	-2.39	-2.47
219 PbAce)2	-3.67 -4.36	-3.64 -4.98	-3.65 -6.14	-3.68 -9.02	-3.75	-3.85	-3.98
220 PbAce)3-	-3.82 -4.02	-3.72 -4.48	-3.67 -5.38	-3.65 -7.69	-3.66	-3.70	-3.77
221 SrAce +	-1.12 -1.70	-1.16 -2.10	-1.21 -2.64	-1.27 -3.37	-1.34	-1.42	-1.51
222 ZnAce +	-5.40 -5.10	-4.91 -5.53	-4.83 -6.53	-4.76 -9.19	-4.75	-4.78	-4.84

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
223 HC2O4 -	-1.32 -1.13	-1.25 -1.18	-1.20 -1.27	-1.17 -1.39	-1.14	-1.13	-1.12
224 H2C2O4	-4.23 -5.90	-4.31 -6.82	-4.43 -7.96	-4.58 -9.35	-4.77	-4.99	-5.26
225 AlOxy +	-6.00 -6.00	-6.00 -6.00	-6.00 -6.00	-6.00 -6.00	-6.00	-6.00	-6.00
226 AlOxy)2-	-11.00 -11.00	-11.00 -11.00	-11.00 -11.00	-11.00 -11.00	-11.00	-11.00	-11.00
227 BaOxy	-1.57 -1.57	-1.57 -1.57	-1.57 -1.57	-1.57 -1.57	-1.57	-1.57	-1.57
228 CaOxy	-3.00 -3.00	-3.00 -3.00	-3.00 -3.00	-3.00 -3.00	-3.00	-3.00	-3.00
229 FeOxy	-4.30 -5.80	-4.40 -6.70	-4.50 -7.70	-4.60 -9.00	-4.90	-5.00	-5.20
230 FeOxy +	-7.74 -7.74	-7.74 -7.74	-7.74 -7.74	-7.74 -7.74	-7.74	-7.74	-7.74
231 KOxy -	-0.70 -0.70	-0.70 -0.70	-0.70 -0.70	-0.70 -0.70	-0.70	-0.70	-0.70
232 MgOxy	-3.47 -3.47	-3.47 -3.47	-3.47 -3.47	-3.47 -3.47	-3.47	-3.47	-3.47
233 MnOxy	-3.93 -5.49	-4.00 -6.45	-4.10 -8.18	-4.29 -12.37	-4.41	-4.61	-4.86
234 MnOxy)2	-17.70 -18.70	-17.70 -19.20	-17.70 -20.20	-17.80 -22.70	-17.90	-18.00	-18.20
235 MnOxy)3	-19.50 -20.50	-19.50 -21.00	-19.50 -22.00	-19.60 -24.50	-19.70	-19.80	-20.00
236 MnOxy +	-11.00 -12.10	-11.10 -12.60	-11.10 -13.60	-11.20 -16.10	-11.30	-11.40	-11.60
237 NaOxy -	-0.90 -0.90	-0.90 -0.90	-0.90 -0.90	-0.90 -0.90	-0.90	-0.90	-0.90
238 PbOxy	-4.90 -4.90	-4.74 -5.31	-4.65 -5.89	-4.59 -6.62	-4.58	-4.61	-4.66
239 SrOxy	-2.54 -2.54	-2.54 -2.54	-2.54 -2.54	-2.54 -2.54	-2.54	-2.54	-2.54
240 ZnOxy	-4.78 -5.90	-4.90 -6.40	-4.90 -7.40	-5.00 -9.90	-5.10	-5.20	-5.40
241 HC4H4O4 -	-4.27 -4.80	-4.21 -5.33	-4.18 -6.04	-4.20 -6.92	-4.25	-4.34	-4.44
242 H2C4H4O4	-5.67 -6.89	-5.64 -7.77	-5.68 -8.91	-5.76 -10.31	-5.89	-6.07	-6.26
243 AlSuc +	-5.30 -5.30	-5.30 -5.30	-5.30 -5.30	-5.30 -5.30	-5.30	-5.30	-5.30
244 AlSuc)2-	-10.00 -10.00	-10.00 -10.00	-10.00 -10.00	-10.00 -10.00	-10.00	-10.00	-10.00
245 BaSuc	-2.02 -2.02	-2.02 -2.02	-2.02 -2.02	-2.02 -2.02	-2.02	-2.02	-2.02
246 CaSuc	-2.00 -2.00	-2.00 -2.00	-2.00 -2.00	-2.00 -2.00	-2.00	-2.00	-2.00
247 FeSuc	-2.00 -3.90	-2.20 -4.70	-2.40 -5.70	-2.60 -6.80	-2.80	-3.00	-3.30
248 FeSuc +	-7.00 -7.00	-7.00 -7.00	-7.00 -7.00	-7.00 -7.00	-7.00	-7.00	-7.00
249 KSuc -	-0.30 -0.30	-0.30 -0.30	-0.30 -0.30	-0.30 -0.30	-0.30	-0.30	-0.30
250 MgSuc	-2.05 -2.05	-2.05 -2.05	-2.05 -2.05	-2.05 -2.05	-2.05	-2.05	-2.05

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
251 MnSuc	-1.99	-2.17	-2.36	-2.57	-2.79	-3.03	-3.28
	-3.91	-4.71	-5.69	-6.84			
252 NaSuc +	-0.30	-0.30	-0.30	-0.30	-0.30	-0.30	-0.30
	-0.30	-0.30	-0.30	-0.30			
253 PbSuc	-3.20	-3.50	-3.70	-4.00	-4.30	-4.70	-5.00
	-5.90	-6.90	-8.20	-9.70			
254 SrSuc	-2.00	-2.00	-2.00	-2.00	-2.00	-2.00	-2.00
	-2.00	-2.00	-2.00	-2.00			
255 ZnSuc	-2.19	-2.46	-2.73	-3.02	-3.33	-3.67	-4.02
	-4.85	-5.92	-7.20	-8.72			
256 FeF ++	-5.82	-6.00	-6.20	-6.48	-6.81	-7.18	-7.60
	-8.50	-9.60	-10.70	-12.00			
257 SiF6 --	28.30	25.72	23.60	21.90	20.42	19.06	17.92
	15.41	12.92	10.75	10.33			
258 Pb(HS)2	-16.80	-15.90	-15.10	-14.50	-14.00	-13.50	-13.30
	-13.00	-13.40	-14.20	-15.30			
259 Pb(HS)3-	-18.58	-16.66	-15.23	-14.19	-13.46	-12.98	-12.71
	-12.66	-13.11	-13.93	-15.03			
260 PbCO3	-6.00	-7.00	-8.00	-8.80	-9.60	-10.30	-10.80
	-11.70	-12.40	-13.00	-13.51			
261 PbOH +	-8.00	-7.82	-7.68	-7.57	-7.48	-7.44	-7.42
	-7.51	-7.79	-8.33	-9.49			
262 Zn(HS)2	-14.14	-13.78	-12.75	-12.20	-12.30	-12.30	-12.30
	-12.90	-13.80	-15.00	-16.30			
263 Zn(HS)3-	-17.01	-15.95	-15.10	-14.50	-14.20	-14.20	-14.20
	-14.60	-15.30	-16.20	-17.10			
264 ZnHCO3 +	-1.35	-1.42	-1.55	-1.68	-1.82	-1.98	-2.20
	-2.71	-3.41	-4.55	-6.03			
265 ZnOH +	-5.14	-5.04	-5.06	-5.12	-5.27	-5.41	-5.58
	-5.96	-6.45	-7.16	-8.46			
266 Zn(OH)2	-10.50	-9.58	-8.96	-8.54	-8.32	-8.20	-8.13
	-8.25	-8.71	-9.70	-11.91			
267 ZnHSOH	-19.20	-18.40	-17.80	-17.30	-16.80	-16.30	-16.00
	-16.00	-16.40	-17.00	-17.80			

Table IC. Equilibrium Constants of Dissolution Reactions at 0° to 350°C

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
1 ADULARIA	2.16 -1.76	1.26 -2.14	0.54 -2.43	-0.35 -2.65	-0.51	-0.91	-1.24
2 AKERMANITE	50.13 26.35	45.46 23.28	41.41 20.58	37.93 19.03	34.94	32.35	30.10
3 ALBITE	3.63 -1.16	2.50 -1.75	1.75 -3.45	1.02 -4.90	0.46	-0.05	-0.48
4 ALBITE LOW	3.93 -0.76	3.11 -1.39	2.30 -2.11	1.58 -2.58	0.96	0.43	-0.02
5 ALBITE HIGH	5.42 -0.15	4.43 -0.90	3.47 -1.72	2.62 -2.27	1.89	1.27	0.73
6 ALUNITE	0.11 -17.11	-2.79 -20.99	-5.53 -26.54	-7.84 -40.08	-9.89	-11.80	-13.59
7 AMESITE	44.87 14.55	38.63 10.46	33.50 6.00	29.00 3.00	25.20	22.30	19.24
8 ANALCIME	7.33 0.83	6.05 -0.03	4.91 -1.15	3.93 -3.65	3.11	2.41	1.81
9 ANDALUSITE	20.16 2.42	16.57 -0.09	13.53 -2.89	10.97 -6.79	8.78	6.90	5.23
10 ANDESITE	15.12 2.91	12.73 1.28	10.64 -0.37	8.85 -1.61	7.30	5.97	4.82
11 ANHYDRITE	-4.14 -7.26	-4.33 -8.48	-4.64 -9.26	-5.00 -12.06	-5.40	-5.82	-6.26
12 ANNITE	33.22 12.16	29.14 9.22	25.48 5.88	22.39 -0.60	19.74	17.47	15.49
13 ANORTHITE	30.54 6.93	25.83 3.63	21.81 0.02	18.38 -6.45	15.44	12.91	10.69
14 APATITE	-64.90 -74.90	-66.15 -77.40	-67.40 -79.80	-68.65 -82.40	-69.90	-71.15	-72.40
15 APATITE	-68.56 -76.13	-68.34 -79.82	-68.74 -84.61	-69.50 -93.10	-70.50	-71.70	-73.04
16 APATITE	-59.89 -71.03	-60.39 -75.13	-61.41 -80.22	-62.70 -88.93	-64.15	-65.73	-67.41
17 ARAGONITE	-8.22 -11.23	-8.34 -12.59	-8.54 -14.14	-8.81 -15.84	-9.17	-9.59	-10.08
18 AUGITE	37.91 11.51	32.56 7.88	28.04 4.00	24.22 -2.66	20.96	18.14	15.68
19 AZURITE	-39.86 -40.68	-39.46 -41.89	-39.36 -44.14	-39.38 -50.00	-39.50	-39.68	-39.94
20 BARITE	-10.50 -10.31	-9.96 -10.80	-9.69 -11.57	-9.58 -13.00	-9.59	-9.69	-9.88
21 BOEHMITE	8.70 0.23	6.95 -0.96	5.50 -2.33	4.27 -4.85	3.24	2.35	1.56
22 BRUCITE	-11.54 -12.89	-11.47 -13.83	-11.53 -15.12	-11.65 -16.79	-11.85	-12.00	-12.24
23 BYTOWNITE	22.18 4.20	18.60 2.96	15.51 -0.60	12.89 -2.44	10.62	8.69	6.97
24 CALCITE	-8.38 -11.29	-8.48 -12.64	-8.66 -14.18	-8.93 -15.84	-9.27	-9.68	-10.16
25 CELESTITE	-6.51 -8.35	-6.43 -9.41	-6.53 -10.30	-6.71 -12.15	-6.95	-7.23	-7.56
26 CHALCEDONY	-4.21 -2.26	-3.73 -2.05	-3.38 -1.88	-3.10 -1.80	-2.88	-2.69	-2.53
27 CHAM, 7A	34.60 7.23	29.03 3.43	24.50 -0.80	20.05 -3.50	17.00	14.00	11.54

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
28 CHLOR, 7A	81.86 32.96	71.94 26.43	63.47 19.41	56.30 9.99	50.24	45.06	40.53
29 CHLOR, 14A	78.30 30.39	68.57 23.97	60.28 17.04	53.70 7.70	47.32	42.25	37.80
30 CRYSTIL	35.65 17.68	32.03 15.53	28.89 13.74	26.23 14.50	23.97	22.04	20.39
31 C-ENSTATIT	12.63 5.67	11.29 4.75	10.10 3.91	9.08 3.32	8.20	7.44	6.77
32 C-PTIL, Na	-8.10 -10.20	-7.90 -10.70	-8.10 -11.90	-8.55 -13.80	-9.00	-9.35	-9.70
33 C-PTIL, K	-16.00 -13.80	-15.00 -14.00	-14.55 -15.00	-14.25 -16.90	-14.10	-13.95	-13.90
34 C-PTIL, Ca	-9.20 -13.10	-9.30 -14.40	-9.60 -15.50	-10.10 -16.80	-10.60	-11.10	-11.70
35 C-PTIL, Mg	-4.20 -11.50	-5.00 -13.00	-5.80 -15.30	-7.00 -18.00	-8.10	-9.10	-10.00
36 CORUNDUM	25.60 5.37	21.40 2.58	17.91 -0.45	15.00 -4.47	12.53	10.40	8.53
37 CRISTOBA	-3.80 -2.13	-3.54 -1.91	-3.27 -1.77	-3.01 -1.76	-2.80	-2.61	-2.43
38 CRISTOBB	-3.13 -2.09	-2.94 -1.90	-2.76 -1.79	-2.59 -1.78	-2.54	-2.34	-2.23
39 DICKITE	8.34 -2.07	6.17 -3.35	4.32 -4.61	2.78 -3.98	1.48	0.38	-0.54
40 DIOPSIDE	21.69 10.88	19.63 9.47	17.79 8.16	16.19 7.45	14.81	13.63	12.59
41 DOLOMITE	-17.75 -25.19	-18.06 -28.36	-18.68 -32.77	-19.50 -39.61	-20.42	-21.45	-22.60
42 DSORD	-16.01 -24.44	-16.52 -27.74	-17.30 -32.26	-18.26 -39.18	-19.31	-20.45	-21.69
43 ENSTATITE	12.82 5.77	11.47 4.85	10.27 4.00	9.23 3.40	8.34	7.57	6.90
44 EPIDOTE	38.04 7.74	31.99 3.45	26.79 -1.47	22.37 -10.99	18.61	15.37	12.54
45 FAYALITE	21.91 9.28	19.43 7.61	17.27 6.10	15.42 5.19	13.84	12.47	11.27
46 FLUORITE	-11.32 -10.71	-10.96 -10.95	-10.73 -11.24	-10.59 -11.57	-10.53	-10.52	-10.55
47 FORSTERITE	32.49 15.30	29.07 13.08	26.13 11.07	23.63 9.69	21.48	19.62	18.00
48 GIBBS AM	-34.29 -30.70	-34.42 -31.29	-32.41 -32.60	-31.80 -36.22	-31.23	-30.89	-30.60
49 GIBBSITE	-34.95 -31.11	-34.92 -31.75	-32.70 -33.22	-32.09 -37.00	-31.64	-31.31	-31.13
50 GREENALITE	25.28 11.34	22.58 9.42	20.21 7.30	18.16 4.36	16.41	14.89	13.56
51 GYPSUM	-4.65 -5.88	-4.60 -6.50	-4.70 -7.67	-4.85 -8.48	-4.98	-5.16	-5.37
52 HALITE	1.50 1.24	1.59 0.89	1.62 -0.41	1.62 -0.20	1.57	1.52	1.44
53 HALLOYSITE	11.35 -0.46	8.91 -1.93	6.83 -3.33	5.08 -2.84	3.61	2.36	1.29
54 HEULANDITE	3.00 -6.26	1.41 -7.61	-0.20 -9.57	-1.63 -14.80	-2.86	-3.91	-4.80
55 HUNTITE	-28.79 -39.91	-30.62 -42.13	-32.33 -44.85	-33.88 -50.13	-35.26	-36.53	-37.08

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
56 HYDRMAGN	-36.72 -48.79	-38.53 -51.65	-40.34 -55.68	-41.99 -64.64	-43.49	-44.89	-45.21
57 HYPHILIT	13.03 4.92	11.80 3.09	10.64 0.86	9.56 -3.18	8.55	7.60	6.69
58 ILLITE	13.52 -1.03	10.34 -2.59	7.75 -3.79	5.61 -4.74	3.82	2.31	1.03
59 KAOLINITE	8.55 -2.82	6.23 -4.44	4.25 -6.50	2.58 -11.08	1.17	-0.03	-1.07
60 KENYAITE	-25.00 -25.00	-25.00 -25.00	-25.00 -25.00	-25.00 -25.00	-25.00	-25.00	-25.00
61 K-SPAR	-0.18 -2.82	-0.55 -3.31	-0.99 -4.12	-1.40 -6.42	-1.76	-2.07	-2.34
62 KYANITE	17.85 1.36	14.48 -0.87	11.64 -3.13	9.24 -5.12	7.21	5.46	3.93
63 LABRADOR	19.29 3.92	16.25 2.26	14.28 -0.18	11.31 -1.89	9.43	7.77	6.32
64 LARNITE	42.58 23.94	38.88 21.56	35.71 19.51	32.99 18.38	30.66	28.64	26.87
65 LAUMONTITE	17.05 2.66	14.17 0.99	11.63 -0.39	9.46 -2.20	7.63	6.08	4.76
66 LEUCITE	7.75 1.31	6.52 0.44	5.42 -0.46	4.46 -0.97	3.64	2.93	2.32
67 LIME	35.76 20.34	32.66 18.38	30.04 16.72	27.81 15.65	25.89	24.23	22.78
68 MAGADITE	-14.34 -14.34	-14.34 -14.34	-14.34 -14.34	-14.34 -14.34	-14.34	-14.34	-14.34
69 MgFe2O4	25.60 3.48	21.10 0.46	17.31 -2.51	14.12 -4.75	11.39	9.04	6.97
70 MAGNESITE	-7.58 -10.43	-8.05 -11.00	-8.50 -11.71	-8.89 -13.07	-9.25	-9.57	-9.87
71 MgCl2	24.57 10.70	22.15 8.44	20.00 6.44	18.09 4.65	16.34	14.76	13.30
72 MARIALITE	4.05 -8.04	1.71 -9.57	-0.45 -11.28	-2.25 -13.80	-3.63	-5.15	-6.37
73 MERWINITE	75.05 40.31	68.17 35.86	62.24 31.97	57.17 29.75	52.82	49.05	45.77
74-MICROCLN	-0.18 -2.84	-0.55 -3.33	-0.99 -4.13	-1.41 -6.41	-1.77	-2.09	-2.36
75 MIEONITE	83.98 -0.78	69.95 -16.72	57.12 -34.00	45.48 -60.60	34.86	25.08	15.99
76 MIRABILT	-2.36 4.52	-1.09 5.73	-0.02 7.33	0.92 15.95	1.76	2.53	3.24
77 MONTICEL	33.28 16.81	30.15 14.51	27.40 12.42	25.02 11.07	22.96	21.14	19.54
78 MORD, Na	-4.00 -5.10	-3.90 -5.50	-4.04 -6.00	-4.22 -6.60	-4.40	-4.60	-4.80
79 MORD, K	-8.00 -6.90	-7.60 -7.00	-7.30 -7.30	-7.13 -7.80	-7.10	-7.03	-7.00
80 MUSCOVITE	16.51 -1.34	12.88 -3.68	9.76 -6.10	7.12 -7.07	4.89	3.00	1.37
81 NACHOLIT	-0.71 1.23	-0.43 1.53	-0.16 1.60	0.10 0.87	0.35	0.59	0.82
82 NATRTHRM	0.08 -2.39	-0.01 -3.26	-0.21 -4.14	-0.48 -5.02	-0.80	-1.17	-1.56
83 NATRON	-1.93 3.70	-0.88 4.74	0.01 6.38	0.76 15.88	1.47	2.10	2.66

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
84 NEPHALINE	15.63	13.52	11.73	10.21	8.92	7.82	6.87
	5.28	3.89	2.37	-0.47			
85 NESQUHON	-4.14	-5.35	-5.32	-5.22	-5.04	-4.96	-4.90
	-4.86	-4.86	-5.07	-6.01			
86 NONT, Na	-10.88	-11.48	-11.90	-13.17	-13.18	-13.58	-13.95
	-14.59	-15.35	-16.83	-19.90			
87 NONT, K	-11.30	-11.81	-12.17	-13.38	-13.35	-13.72	-14.06
	-14.66	-15.40	-16.85	-19.90			
88 NONT, H	-11.94	-12.50	-12.92	-14.21	-14.26	-14.73	-15.16
	-15.95	-16.90	-18.54	-21.76			
89 NONT, Ca	-10.84	-11.54	-12.05	-13.40	-13.48	-13.96	-14.38
	-15.13	-16.00	-17.58	-20.77			
90 NONT, Mg	-10.81	-11.56	-12.12	-13.49	-13.61	-14.11	-14.56
	-15.35	-16.25	-17.87	-21.10			
91 OLDHAMIT	13.19	11.90	10.75	9.71	8.77	7.90	7.10
	5.66	4.40	3.27	2.26			
92 OLIGOCLA	10.40	8.73	7.22	5.91	4.79	3.82	2.99
	1.63	0.47	0.44	-1.46			
93 PARAGONI	18.42	14.39	10.95	8.03	5.57	3.47	1.65
	-1.41	-4.20	-7.61	-14.89			
94 PARAGASI	114.71	100.79	88.81	78.61	69.89	62.38	55.83
	44.82	35.35	25.38	8.34			
95 PERICLAS	23.92	21.51	19.46	17.74	16.26	14.98	13.86
	12.00	10.48	9.14	8.19			
96 PHILLIPS	3.30	3.30	3.30	3.30	3.30	3.30	3.30
	3.30	3.30	3.30	3.30			
97 PHLOGPITE	42.10	37.22	32.91	29.21	26.09	23.41	21.06
	17.25	13.75	10.11	3.20			
98 PHLOGPTF	20.52	16.73	13.25	10.19	7.49	5.10	2.94
	-0.91	-4.59	-8.84	-14.53			
99 PORTLAN	-5.25	-5.42	-5.71	-6.04	-6.38	-6.73	-7.09
	-7.90	-8.92	-10.51	-14.25			
100 POTASSI	90.96	84.12	78.33	73.39	69.13	65.41	62.15
	56.69	52.32	48.79	46.58			
101 PREHNITE	36.87	32.02	27.82	24.24	21.19	18.56	16.27
	12.41	9.00	5.16	-2.13			
102 PYROPHYL	1.42	-0.10	-1.61	-2.90	-4.02	-4.98	-5.82
	-7.27	-8.65	-10.54	-15.09			
103 QUARTZ	-4.24	-3.93	-3.63	-3.35	-3.10	-2.88	-2.68
	-2.36	-2.11	-1.94	-1.90			
104 SANIDINE	1.74	1.18	0.58	0.03	-0.45	-0.86	-1.22
	-1.82	-2.36	-3.00	-3.35			
105 SAPO, Na	30.19	26.88	23.91	21.32	19.14	17.26	15.61
	12.87	10.50	7.85	4.07			
106 SAPO, K	29.78	26.55	23.65	21.11	18.97	17.12	15.50
	12.80	10.45	7.82	4.08			
107 SAPO, H	28.16	25.85	22.91	20.33	18.15	16.26	14.61
	11.84	9.43	6.75	2.97			
108 SAPO, Ca	30.23	26.82	23.76	21.09	18.84	16.89	15.18
	12.33	9.85	7.09	3.20			
109 SAPO, Mg	30.26	26.80	23.71	21.00	18.72	16.74	15.01
	12.12	9.61	6.82	2.89			
110 SEPIOLITE	34.56	31.52	28.70	26.60	25.00	23.60	22.20
	20.10	18.36	17.10	16.40			
111 SILICAAM	-2.88	-2.70	-2.52	-2.37	-2.23	-2.10	-1.99
	-1.81	-1.67	-1.59	-1.54			

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
112 SILICGEL	-2.94	-2.71	-2.52	-2.36	-2.20	-2.06	-1.93
	-1.74	-1.53	-1.30	-0.95			
113 SILLIMAN	19.39	15.73	12.63	10.02	7.79	5.86	4.18
	1.31	-1.24	-4.09	-9.28			
114 SMEC Ca	9.14	6.14	3.70	1.68	-0.01	-1.44	-2.65
	-4.60	-6.07	-7.20	-8.10			
115 SMEC K	8.67	5.86	3.57	1.69	0.12	-1.21	-2.33
	-4.12	-5.47	-6.51	-7.32			
116 SMEC Mg	9.08	6.04	3.57	1.51	-0.02	-1.64	-2.87
	-4.83	-6.32	-7.47	-8.36			
117 SMEC Na	9.01	6.12	3.77	1.83	0.22	-1.14	-2.29
	-4.13	-5.51	-6.57	-7.39			
118 Na2O	73.09	67.43	62.69	58.65	55.20	52.25	49.59
	45.27	41.86	39.12	37.47			
119 SPINEL	42.49	36.46	31.44	27.24	23.68	20.63	17.99
	13.58	9.88	6.36	3.56			
120 STILBITE	3.00	1.41	-0.20	-1.63	-2.86	-3.91	-4.80
	-6.26	-7.61	-9.57	-14.80			
121 STRENGIT	-27.31	-27.20	-27.41	-27.76	-28.22	-28.69	-29.36
	-30.66	-32.03	-33.43	-34.84			
122 SrCO3	-9.34	-9.27	-9.37	-9.59	-9.90	-10.28	-10.70
	-11.64	-12.65	-13.70	-14.72			
123 SYLVITE	0.60	0.91	1.12	1.26	1.35	1.39	1.40
	1.29	1.02	0.61	0.04			
124 TALC	23.59	21.13	18.83	16.84	15.11	13.62	12.32
	10.16	8.27	6.14	1.98			
125 THENARDI	-0.33	-0.29	-0.37	-0.52	-0.71	-0.94	-1.19
	-1.84	-2.71	-4.09	-7.25			
126 TREMOLITE	67.53	60.89	54.87	49.62	45.10	41.19	37.78
	32.06	27.15	21.83	12.15			
127 TRONA	-0.65	-0.63	-1.56	-2.21	-2.70	-3.04	-3.23
	-3.29	-2.92	-2.16	-1.32			
128 VIVIANIT	-36.00	-36.00	-36.00	-36.00	-36.00	-36.00	-36.00
	-36.00	-36.00	-36.00	-36.00			
129 WAIRAKITE	21.05	17.33	14.05	11.22	8.79	6.70	4.87
	1.80	-0.92	-4.04	-10.17			
130 WITHERITE	-8.96	-8.63	-8.78	-9.05	-9.42	-9.88	-10.41
	-11.70	-13.31	-15.25	-17.55			
131 WOLLASTO	14.82	12.60	12.50	11.55	10.73	10.01	9.39
	8.34	7.79	6.58	5.21			
132 ZOISITE	49.21	42.10	36.03	30.89	26.46	22.66	19.39
	13.76	8.83	3.37	-6.69			
133 SILVER	-1.53	-0.50	0.35	1.09	1.73	2.31	2.83
	2.75	4.58	5.43	6.69			
134 AgCl	-10.82	-9.73	-8.86	-8.15	-7.65	-7.19	-6.81
	-6.33	-6.10	-6.43	-6.97			
135 Ag2S	-39.90	-36.26	-33.18	-30.52	-28.20	-26.16	-24.35
	-21.30	-18.89	-16.99	-15.53			
136 COPPER	3.78	4.25	4.65	5.00	5.31	5.61	5.89
	6.41	6.93	7.52	8.49			
137 MALACHITE	-33.55	-33.58	-32.03	-31.76	-31.65	-31.70	-31.90
	-32.71	-34.16	-36.77	-43.08			
138 CuO	8.70	7.67	6.80	6.07	5.44	4.91	4.44
	3.66	2.98	2.23	0.90			
139 Cu2O	-2.35	-1.90	-1.50	-1.11	-0.73	-0.36	-0.01
	0.65	1.25	1.72	1.86			

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
140 CuS	-24.48	-22.83	-21.50	-20.41	-19.50	-18.75	-18.10
	-17.16	-16.64	-16.70	-18.15			
141 Cu ₂ S	-38.29	-34.95	-32.17	-29.79	-27.74	-25.96	-24.39
	-21.82	-19.86	-18.40	-17.38			
142 CuFeS ₂	-36.32	-34.07	-32.32	-30.90	-29.76	-28.83	-28.08
	-27.09	-26.77	-27.45	-30.99			
143 BORNITE	-111.09	-102.51	-95.49	-89.60	-84.60	-80.33	-76.67
	-70.88	-67.01	-65.43	-69.17			
144 FeCl ₂	9.12	7.90	6.76	5.70	4.70	3.76	2.88
	1.24	-0.24	-1.60	-2.55			
145 FeCl ₃	14.65	12.34	10.23	8.30	6.51	4.84	3.28
	0.42	-2.13	-4.45	-6.57			
146 FeCO ₃	-10.34	-10.54	-10.84	-11.21	-11.57	-11.96	-12.38
	-13.27	-14.28	-15.48	-17.32			
147 FeO	15.19	13.50	12.07	10.15	9.81	8.91	8.91
	6.79	5.66	4.55	2.93			
148 Fe ₂ O ₃ HEM	2.14	0.04	-1.69	-3.13	-4.34	-5.37	-6.28
	-7.85	-9.36	-11.30	-15.55			
149 Fe ₂ O ₃ MGH	6.40	6.40	6.40	6.40	6.40	6.40	6.40
	6.40	6.40	6.40	6.40			
150 Fe ₃ O ₄	14.28	10.75	7.82	5.36	3.28	1.51	-0.04
	-2.64	-4.92	-7.26	-8.92			
151 Fe(OH) ₃	-38.67	-37.20	-36.10	-35.30	-34.73	-34.34	-34.10
	-33.92	-34.04	-34.35	-34.79			
152 GOETHITE	1.49	0.48	-0.33	-1.00	-1.60	-2.08	-2.50
	-3.20	-3.83	-4.47	-4.50			
153 FeSPYRHO	-3.69	-3.76	-3.90	-4.06	-4.24	-4.44	-4.66
	-5.19	-5.86	-6.89	-9.24			
154 FeSTROLT	-3.78	-3.87	-4.02	-4.20	-4.38	-4.59	-4.81
	-5.33	-5.99	-7.01	-9.36			
155 FeS ₂ PYR	-26.54	-24.71	-23.34	-22.28	-21.46	-20.82	-20.36
	-19.88	-20.00	-21.05	-25.35			
156 GREIGITE	-45.00	-45.00	-45.00	-45.00	-45.00	-45.00	-45.00
	-45.00	-45.00	-45.00	-45.00			
157 Hg(L)	-4.25	-2.84	-1.69	-0.70	0.18	0.96	1.68
	2.98	4.16	5.38	7.11			
158 HgCl ₂ (C)	-15.11	-14.11	-13.30	-12.64	-12.10	-11.66	-11.32
	-10.88	-10.79	-11.25	-12.99			
159 Hg ₂ Cl ₂ (C)	-19.49	-17.84	-16.43	-15.23	-14.19	-14.27	-12.46
	-11.08	-9.95	-8.97	-8.04			
160 HgO	2.83	2.44	2.11	1.86	1.67	1.53	1.43
	1.31	1.25	1.19	1.53			
161 CINNABAR	-43.32	-39.86	-37.02	-34.64	-32.62	-30.90	-29.44
	-27.14	-25.53	-24.94	-23.94			
162 CINABMET	-41.84	-38.58	-35.89	-33.64	-31.74	-30.12	-28.75
	-26.60	-25.11	-25.26	-23.25			
163 MnCl ₂	9.89	8.79	7.75	6.77	5.85	4.99	4.16
	2.54	0.84	-1.30	-5.35			
164 MnCO ₃	-10.52	-10.54	-10.70	-10.94	-11.21	-11.54	-11.92
	-12.81	-13.91	-15.43	-18.26			
165 MnO	19.62	17.70	16.08	14.72	13.56	12.56	11.70
	10.28	9.13	8.13	7.56			
166 MnO ₂	-7.79	-8.33	-8.75	-9.11	-9.42	-9.68	-9.90
	-10.23	-10.36	-10.06	-7.29			
167 MnS	-0.13	-0.47	-0.82	-1.16	-1.50	-1.82	-2.16
	-2.87	-3.70	-4.67	-5.82			

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
168 PbCl2	-5.31	-4.82	-4.51	-4.31	-4.19	-4.14	-4.15
	-4.35	-4.86	-5.94	-8.92			
169 PbCO3	-13.37	-12.89	-12.62	-12.48	-12.40	-12.42	-12.51
	-12.88	-13.52	-14.58	-16.85			
170 PbOLITHR	13.60	12.55	11.67	10.90	10.25	9.66	9.18
	8.62	8.33	7.64	8.97			
171 PbOMASIC	13.76	12.69	11.80	11.07	10.48	9.99	9.59
	8.98	8.53	8.19	8.34			
172 PbS GALN	-16.30	-14.78	-13.59	-12.90	-12.34	-11.83	-11.42
	-10.93	-10.72	-10.82	-11.10			
173 PbSO4	-8.07	-7.80	-7.70	-7.69	-7.74	-7.84	-7.98
	-8.43	-9.15	-10.45	-13.74			
174 ZnCO3	-9.20	-9.87	-10.50	-10.15	-11.72	-12.22	-12.66
	-13.34	-13.83	-14.22	-14.63			
175 ZnO	12.90	11.20	9.70	8.30	7.17	6.10	5.38
	4.42	4.02	4.02	4.23			
176 ZnS	-12.42	-11.79	-11.32	-11.00	-10.82	-10.65	-10.54
	-10.60	-10.83	-11.05	-10.95			
177 ZnSO4	4.71	3.54	2.38	1.30	0.30	-0.66	-1.58
	-3.36	-5.23	-7.57	-11.95			
178 RUTHERFO	-17.11	-16.88	-16.81	-16.89	-17.03	-17.26	-17.57
	-18.33	-19.31	-20.54	-22.47			
179 URAMPHIT	-27.44	-27.07	-27.04	-27.25	-27.64	-28.17	-28.80
	-30.26	-31.89	-33.62	-35.39			
180 PRZHEVAL	-18.49	-19.52	-20.62	-21.75	-22.89	-24.03	-25.17
	-27.42	-29.65	-31.86	-34.06			
181 TOBERNIT	-19.02	-20.37	-21.82	-23.33	-24.87	-26.41	-27.96
	-31.04	-34.09	-37.11	-40.13			
182 SALEEITE	-16.92	-18.73	-20.28	-21.62	-22.80	-23.83	-24.76
	-26.36	-27.81	-29.16	-30.47			
183 SR AUTUN	-18.31	-19.52	-20.77	-22.02	-23.26	-24.48	-25.69
	-28.06	-30.38	-32.69	-34.99			
184 URANOCIR	-18.77	-19.70	-20.84	-22.12	-23.49	-24.90	-26.34
	-29.29	-32.27	-35.27	-38.28			
185 BASSETIT	-17.94	-19.55	-21.23	-22.94	-24.64	-26.33	-28.00
	-31.30	-34.53	-37.72	-40.87			
186 UO3 (C)	9.05	7.76	6.66	5.71	4.88	4.16	3.51
	2.41	1.50	0.75	0.11			
187 UO3 (AM)	10.99	10.45	9.14	8.01	7.02	6.16	5.39
	4.09	3.02	2.13	1.38			
188 UO2(OH)2	-23.06	-22.12	-21.47	-21.00	-20.68	-20.47	-20.36
	-20.38	-20.78	-21.54	-22.64			
189 UF4*2.5W	-27.66	-27.61	-27.70	-27.89	-28.15	-28.48	-28.89
	-29.96	-31.41	-33.29	-35.61			
190 UHP)2*4W	-26.69	-26.74	-27.06	-27.56	-28.19	-28.92	-29.71
	-31.40	-33.09	-34.41	-32.18			
191 NINGYOIT	-28.73	-29.19	-29.85	-30.63	-31.50	-32.42	-33.38
	-35.39	-37.49	-39.66	-41.89			
192 U3O8	0.30	-1.00	-2.08	-2.99	-3.76	-4.42	-5.00
	-5.93	-6.67	-7.26	-7.73			
193 UO2(AM)	2.81	0.92	-0.68	-2.05	-3.22	-4.25	-5.15
	-6.66	-7.87	-8.85	-9.68			
194 UO2(C)	-3.40	-4.66	-5.72	-6.61	-7.39	-8.06	-8.65
	-9.64	-10.42	-11.07	-11.60			
195 U4O9	-13.61	-16.33	-18.54	-20.36	-21.86	-23.11	-24.16
	-25.79	-26.95	-27.78	-28.37			

	<u>0/200</u>	<u>25/250</u>	<u>50/300</u>	<u>75/350</u>	<u>100</u>	<u>125</u>	<u>150</u>
196 USIO4	-7.44	-8.30	-9.06	-9.72	-10.31	-10.81	-11.05
	-11.96	-12.51	-12.95	-13.33			
197 H AUTUNI	-22.78	-23.40	-24.01	-24.64	-25.24	-25.83	-26.41
	-27.52	-28.58	-29.57	-30.51			
198 NA AUTUN	-22.04	-22.49	-22.95	-23.41	-23.85	-24.29	-24.71
	-25.51	-26.29	-27.06	-27.83			
199 K AUTUNI	-23.27	-23.28	-23.40	-23.58	-23.81	-24.07	-24.35
	-24.94	-25.58	-26.25	-26.95			
200 AUTUNITE	-18.30	-19.62	-20.85	-22.00	-23.05	-24.03	-24.96
	-26.69	-28.31	-29.86	-31.40			
201 K2U2V2Ox	-57.98	-56.45	-55.26	-54.32	-53.58	-52.99	-52.51
	-51.87	-51.51	-51.39	-51.58			
202 CAU2V2OX	-53.28	-53.02	-52.94	-52.97	-53.08	-53.25	-53.47
	-54.03	-54.72	-55.62	-57.11			
203 URANOPHA	17.38	17.38	17.38	17.38	17.38	17.38	17.38
	17.38	17.38	17.38	17.38			
204 SCHOEPIT	-24.46	-23.38	-22.60	-22.02	-21.59	-21.28	-21.07
	-20.91	-21.07	-21.72	-23.17			
205 MGUO4	26.42	23.22	20.51	18.21	16.23	14.51	13.01
	10.51	8.49	6.85	6.56			
206 CAUO4	17.01	14.89	13.12	11.63	10.38	9.32	8.41
	6.94	5.82	5.00	5.58			
207 BAUO4	19.75	17.64	15.88	14.41	13.16	12.09	11.18
	9.71	8.60	7.83	8.56			
208 UO2F2	-6.79	-7.30	-7.82	-8.33	-8.83	-9.33	-10.87
	-10.78	-12.05	-13.66	-16.88			
209 US3	-19.33	-18.41	-17.83	-17.53	-17.41	-17.45	-17.63
	-18.32	-19.51	-21.59	-27.48			
210 V2O3	12.50	9.83	7.61	5.74	4.16	2.80	1.62
	-0.30	-1.80	-2.99	-3.94			
211 V2O4	10.47	8.53	6.98	5.73	4.71	3.88	3.20
	2.19	1.51	1.06	0.78			
212 V2O5	-33.26	-31.82	-30.60	-29.55	-28.64	-27.85	-27.15
	-25.98	-25.03	-24.24	-23.58			
213 VOSO4*6W	-5.10	-4.68	-4.64	-4.85	-5.26	-5.81	-6.49
	-8.14	-10.13	-12.14	-15.01			
214 PB3VO4)2	-52.49	-50.84	-49.52	-48.39	-47.39	-46.51	-45.72
	-44.41	-43.47	-43.11	-44.37			

Table ID. Parameters for Calculating Activity Coefficients
by the B^{*} Method (Helgeson, 1969).

Temperature	B [*]	Temperature	B [*]
0.0	0.038	200.0	0.047
25.0	0.041	250.0	0.034
50.0	0.043	270.0	0.015
100.0	0.046	300.0	0.000
150.0	0.047	350.0	0.000

Table IE. Fit Parameters for Calculating the Equilibrium Constants of Dissolution Reactions at Higher Pressures.

	<u>500 bars</u>			<u>1000 bars</u>		
	A	Bx10 ⁴	Cx10 ¹⁶	A	Bx10 ⁴	Cx10 ¹⁶
1	0.623	-5.380	12.260	2.275	-22.600	16.490
2	0.038	17.930	10.050	0.059	28.706	12.710
3	0.584	-4.260	11.170	1.057	-1.960	14.986
4	0.705	-10.557	15.702	1.388	-24.487	24.043
5	0.709	-10.696	15.144	1.390	-24.371	24.005
6	1.847	32.520	75.360	3.717	42.296	96.763
7	1.603	-20.100	59.016	2.810	-14.920	80.253
8	0.491	-2.578	12.683	0.869	-1.719	15.855
9	0.537	-0.576	21.450	0.930	3.320	26.929
10	0.769	-7.714	20.010	1.441	-14.938	27.290
11	0.423	-1.000	16.176	0.729	1.576	20.302
12	0.871	-3.512	28.668	1.506	0.512	35.887
13	0.865	-3.449	26.480	1.520	-0.614	32.160
14	1.380	0.000	0.000	2.750	0.000	0.000
15	1.380	0.000	0.000	2.750	0.000	0.000
16	1.380	0.000	0.000	2.750	0.000	0.000
17	0.473	-1.575	17.190	0.846	0.108	21.650
18	0.000	0.000	0.000	0.000	0.000	0.000
19	1.701	-28.676	27.076	3.206	-44.737	38.138
20	0.394	-1.119	15.305	0.674	1.229	19.202
21	0.193	-0.145	10.250	0.288	3.732	13.108
22	0.484	-1.633	18.297	0.840	0.681	23.004
23	0.833	-4.871	24.320	1.494	-5.389	30.540
24	0.514	-1.970	17.096	0.928	-0.790	21.485
25	0.417	-1.015	15.819	0.720	1.324	19.876
26	0.111	-0.963	0.435	0.210	-1.617	0.575
27	0.913	-13.266	29.151	1.646	-14.039	39.787
28	0.000	0.000	0.000	0.000	0.000	0.000
29	0.000	0.000	0.000	0.000	0.000	0.000
30	0.432	1.186	17.613	0.661	7.287	21.954
31	0.188	0.084	6.001	0.313	1.520	7.530
32	0.000	0.000	0.000	0.000	0.000	0.000
33	0.000	0.000	0.000	0.000	0.000	0.000
34	0.000	0.000	0.000	0.000	0.000	0.000
35	0.000	0.000	0.000	0.000	0.000	0.000
36	0.413	0.634	20.940	0.690	5.624	26.290
37	0.135	-1.345	0.584	0.268	-2.402	0.583
38	0.150	-1.600	0.480	0.288	-2.940	0.621
39	0.162	28.640	16.790	0.900	5.826	27.260
40	0.422	-0.558	21.130	0.638	1.832	13.700
41	0.982	-3.101	35.360	1.749	0.756	44.430
42	0.921	-15.653	9.425	1.747	-26.193	13.480
43	0.188	0.084	6.001	0.313	1.520	7.530
44	1.221	-12.484	36.876	2.180	-8.362	50.108
45	0.349	-1.967	11.190	0.610	-0.943	14.060
46	0.399	-0.047	17.580	0.682	3.602	22.020
47	0.302	0.224	11.630	0.476	3.687	14.510
48	0.773	-2.712	29.530	1.373	0.453	37.140
49	0.773	-2.712	29.530	1.373	0.453	37.140
50	0.645	-7.980	14.829	1.156	-7.986	20.008

<u>500 bars</u>				<u>1000 bars</u>		
	A	Bx10 ⁴	Cx10 ¹⁶	A	Bx10 ⁴	Cx10 ¹⁶
51	0.328	0.589	16.120	0.553	4.785	20.180
52	0.120	-2.333	6.703	0.192	-2.372	10.020
53	0.540	0.126	21.850	0.897	5.936	27.290
54	1.282	-10.518	23.935	2.343	-7.283	31.729
55	1.942	-5.414	71.810	3.447	3.294	90.210
56	2.218	10.018	73.150	3.960	-5.114	92.040
57	0.301	0.321	15.168	0.514	3.745	19.007
58	1.195	-3.120	27.430	2.167	0.492	33.510
59	0.540	0.139	21.840	0.902	5.834	27.290
60	0.000	0.000	0.000	0.000	0.000	0.000
61	0.572	-3.745	10.640	1.037	-1.236	14.246
62	0.494	-0.082	21.500	0.839	4.588	27.000
63	0.801	-6.292	22.170	1.467	-10.163	28.910
64	0.313	-0.730	9.450	0.521	-0.985	11.843
65	0.848	-2.231	27.360	1.545	2.523	34.230
66	0.506	-2.701	12.135	0.907	-2.396	12.230
67	0.122	-0.348	4.519	0.196	0.548	5.695
68	0.000	0.000	0.000	0.000	0.000	0.000
69	1.175	-10.520	25.750	2.165	-15.470	32.590
70	0.464	-0.684	18.160	-0.198	79.600	10.345
71	0.243	1.783	16.182	0.405	6.100	20.350
72	0.000	0.000	0.000	0.000	0.000	0.000
73	0.665	-1.940	20.071	2.013	-42.620	29.840
74	0.600	-3.402	12.610	1.080	-3.414	15.770
75	3.298	-40.570	75.131	6.054	-46.600	102.888
76	0.010	4.441	13.900	-0.118	12.740	17.310
77	0.340	-0.910	10.583	0.559	1.329	13.210
78	0.000	0.000	0.000	0.000	0.000	0.000
79	0.000	0.000	0.000	0.000	0.000	0.000
80	0.897	-0.853	33.490	1.532	-0.853	33.490
81	0.270	0.000	0.000	0.540	0.000	0.000
82	1.790	-6.960	15.300	3.470	-9.280	22.520
83	1.790	-6.960	15.310	3.470	-9.280	22.520
84	0.381	-1.777	12.251	0.660	-0.203	15.327
85	0.690	-4.549	18.330	0.476	54.330	12.490
86	0.000	0.000	0.000	0.000	0.000	0.000
87	0.000	0.000	0.000	0.000	0.000	0.000
88	0.000	0.000	0.000	0.000	0.000	0.000
89	0.000	0.000	0.000	0.000	0.000	0.000
90	0.000	0.000	0.000	0.000	0.000	0.000
91	0.256	-3.080	9.658	0.419	1.628	12.010
92	0.737	-9.135	17.860	1.414	-19.712	25.670
93	0.994	-10.189	30.429	1.786	-6.568	41.289
94	1.963	-17.122	59.240	3.416	-5.334	80.087
95	0.232	-1.814	5.702	0.404	-1.879	7.131
96	0.933	-7.970	13.700	2.097	-23.500	20.250
97	0.846	-6.644	25.840	1.449	-10.942	34.783
98	1.570	-10.500	42.430	3.903	-25.200	54.210
99	0.528	-2.789	17.224	0.935	-1.821	21.710
100	1.659	-86.100	11.590	-0.030	1.101	1.788

500 bars				1000 bars			
	A	Bx10 ⁴	Cx10 ¹⁶		A	Bx10 ⁴	Cx10 ¹⁶
101	1.435	-32.900	38.060	1.932	-7.150	39.750	
102	0.783	-1.869	22.750	1.374	1.858	28.420	
103	0.111	-0.936	0.453	0.208	-1.530	0.559	
104	0.632	-5.382	12.265	2.275	-22.630	16.490	
105	0.000	0.000	0.000	0.000	0.000	0.000	
106	0.000	0.000	0.000	0.000	0.000	0.000	
107	0.000	0.000	0.000	0.000	0.000	0.000	
108	0.000	0.000	0.000	0.000	0.000	0.000	
109	0.000	0.000	0.000	0.000	0.000	0.000	
110	0.164	-1.848	0.495	0.313	3.366	0.634	
111	0.118	-0.936	0.453	0.216	-1.530	0.559	
112	0.000	0.000	0.000	0.000	0.000	0.000	
113	0.537	-0.576	21.450	0.926	3.447	26.880	
114	1.687	-2.840	26.970	3.160	0.915	33.390	
115	1.430	11.450	25.790	1.700	8.230	34.040	
116	1.420	11.690	25.690	1.600	1.216	34.260	
117	1.420	10.620	25.500	1.600	-5.920	34.210	
118	0.111	-5.330	2.757	-0.066	-7.940	6.728	
119	0.540	0.599	26.580	0.884	7.127	33.330	
120	2.591	-24.662	58.576	4.697	-18.025	78.189	
121	0.560	0.000	0.000	1.130	0.000	0.000	
122	0.528	-2.590	16.820	0.951	-1.671	21.140	
123	0.919	-42.710	11.120	0.144	2.149	7.550	
124	0.682	-1.479	18.610	1.125	3.350	23.110	
125	0.313	-0.813	14.140	0.524	1.988	17.690	
126	1.644	-4.370	40.530	2.790	2.628	50.680	
127	0.770	0.000	0.000	1.550	0.000	0.000	
128	0.000	0.000	0.000	0.000	0.000	0.000	
129	1.522	32.050	33.180	0.793	82.000	19.150	
130	0.523	-3.039	16.310	0.936	-2.343	20.500	
131	0.237	-1.350	4.990	0.317	4.920	7.330	
132	1.090	-1.000	41.850	1.815	8.850	52.300	
133	0.000	0.000	0.000	0.000	0.000	0.000	
134	0.055	0.658	6.124	0.081	2.613	7.689	
135	0.075	-0.017	6.804	0.108	1.843	8.524	
136	-0.056	-1.220	-3.224	-0.095	-2.810	-4.000	
137	0.866	2.034	35.420	1.887	-4.074	45.700	
138	0.413	-6.360	5.423	0.754	-9.060	7.200	
139	0.481	-23.710	8.307	0.600	-25.920	-9.942	
140	0.213	-0.334	10.590	0.331	3.695	13.060	
141	0.183	-1.730	7.770	0.316	-1.113	9.756	
142	0.422	-0.588	21.130	0.737	3.213	26.530	
143	0.810	-3.689	36.971	1.423	0.869	46.525	
144	0.247	0.130	16.070	0.340	-2.840	19.790	
145	0.429	0.547	25.870	0.734	6.011	32.390	
146	0.495	-2.141	18.000	0.897	-7.380	22.640	
147	0.123	-0.665	5.394	0.202	0.330	6.734	
148	0.472	-0.912	19.790	0.813	2.430	24.840	
149	0.427	-0.912	19.790	0.813	2.430	24.840	
150	0.610	-1.692	25.150	1.054	2.029	31.620	

<u>500 bars</u>				<u>1000 bars</u>			
	A	Bx10 ⁴	Cx10 ¹⁶		A	Bx10 ⁴	Cx10 ¹⁶
151	0.000	0.000	0.000	0.000	0.000	0.000	
152	0.266	-0.456	9.895	0.468	1.215	12.420	
153	0.200	-0.500	10.440	0.570	-13.900	16.150	
154	0.200	-0.500	10.440	0.570	-13.900	16.150	
155	0.257	0.376	16.920	0.390	6.890	21.580	
156	0.000	0.000	0.000	0.000	0.000	0.000	
157	-0.174	4.580	-7.010	-0.263	4.295	-8.800	
158	0.000	0.000	0.000	0.000	0.000	0.000	
159	0.000	0.000	0.000	0.000	0.000	0.000	
160	0.134	-1.463	4.317	0.282	-4.143	5.732	
161	0.210	-0.849	9.432	0.372	0.173	11.897	
162	0.218	-1.114	9.478	0.382	0.026	11.920	
163	0.217	1.652	15.730	0.354	6.450	19.660	
164	0.482	-2.991	18.350	0.853	-1.391	23.100	
165	0.082	0.153	5.148	0.122	1.805	6.407	
166	0.000	0.000	0.000	0.000	0.000	0.000	
167	0.150	0.954	10.255	0.224	4.054	12.830	
168	0.226	0.812	14.580	0.417	2.367	17.990	
169	0.507	-2.940	16.660	0.924	-2.370	20.970	
170	0.137	-1.400	4.039	0.034	14.200	2.259	
171	0.123	-0.828	4.090	0.015	14.870	2.083	
172	0.202	-0.663	9.142	0.359	0.548	11.497	
173	0.398	-1.417	15.660	0.699	0.496	19.700	
174	0.468	-1.760	18.010	0.833	4.472	22.620	
175	0.339	-2.930	4.950	0.663	-4.240	5.850	
176	0.198	0.094	10.490	0.340	2.350	13.170	
177	0.409	-1.110	17.050	0.699	2.090	21.330	

Table IF. Data for Calculating the Effect of Pressure
on Aqueous Dissociation Reactions.

	<u>ΔV @25°C</u>	<u># Water Ionization Reactions</u>
1	-28.7	1.0
3	-37.9	1.0
10	-13.0	1.0
15	-22.4	1.0
16	-43.2	2.0
17	-64.3	3.0
25	-11.2	1.0
26	-7.5	2.0
27	-34.3	1.0
28	-19.74	1.0
29	-7.1	2.0
30	-10.6	2.0
31	-31.6	1.0
32	-19.74	1.0
36	-25.0	2.0
44	-19.74	1.0
45	-7.1	2.0
50	-19.74	1.0
51	-5.7	2.0
53	-7.1	2.0
54	-4.6	1.0
60	-22.4	1.0
61	-43.5	2.0
62	-64.6	3.0
63	-85.7	4.0
64	-35.5	0.0
72	-27.2	1.0
73	-35.96	1.0
74	-25.85	1.0
76	-14.81	1.0
87	-19.8	1.0
93	-9.8	2.0
94	-31.5	1.0
96	-19.74	1.0
97	-7.4	2.0
105	-34.0	1.0
106	-7.1	2.0
110	-13.7	1.0
111	-23.1	1.0
112	-13.8	1.0
114	-7.1	2.0
115	-15.8	1.0
118	-28.8	1.0
127	-19.74	1.0
128	-9.12	2.0
129	-31.5	1.0
130	-7.1	2.0
135	-7.6	2.0

Table IG. Pitzer Coefficients

M	X	t	$\beta^{(0)}$	$\beta^{(1)}$	C^ϕ	M	X	t	$\beta^{(0)}$	$\beta^{(1)}$	C^ϕ
Na	Cl	0	0.0532	0.2496	0.00441	K	Cl	0	0.0296	0.1621	0.00119
		25	0.0765	0.2664	0.00127			25	0.0485	0.2122	-0.00084
		50	0.0903	0.2846	-0.00095			50	0.0596	0.2429	-0.00205
		75	0.0978	0.3041	-0.00250			75	0.0662	0.2705	-0.00277
		100	0.1012	0.3250	-0.00354			100	0.0698	0.2977	-0.00318
		125	0.1017	0.3472	-0.00420			125	0.0715	0.3250	-0.00340
		150	0.1003	0.3707	-0.00457			150	0.0721	0.3527	-0.00350
		200	0.0938	0.4218	-0.00469			200	0.0710	0.4084	-0.00349
		250	0.0838	0.4738	-0.00429			250	0.0677	0.4640	-0.00322
		300	0.0708	0.5401	-0.00357			300	0.0621	0.5188	-0.00264
		350	0.0546	0.6073	-0.00268			350	0.0534	0.5724	-0.00162
Na	SO ₄	0	-0.08601	0.892	0.0353	K	SO ₄	0	-0.04138	0.7830	0.0172
		25	0.01864	1.096	0.00555			25	0.00000	1.1023	0.0188
		50	0.06264	1.213	-0.00303			50	0.02771	1.2578	0.0174
		75	0.0888	1.285	-0.00839			75	0.04888	0.3704	0.0137
		100	0.1057	1.330	-0.0123			100	0.06819	0.4637	0.00811
		125	0.1175	1.357	-0.0153			125	0.0887	1.5510	0.00098
		150	0.1266	1.374	-0.0178			150	0.1124	1.6415	-0.00741
		200	0.1415	1.444	-0.0213			200	0.1743	1.8578	-0.0271
		250	0.1546	1.856	-0.0235			250	0.2596	2.1511	-0.0499
		300	0.1656	3.730	-0.0249			300	0.3701	2.5460	-0.0749
		350	0.1723	12.550	-0.0256			350	0.5058	3.0590	-0.1015
Na	HCO ₃	25	0.0277	0.0411	0.0000	K	HCO ₃	25	0.0296	-0.013	-0.0080
Na	CO ₃	25	0.0399	1.389	0.0044	K	CO ₃	25	0.1488	1.430	-0.0015
Ca	SO ₄	25	0.200	3.1973	0.0000	H	Cl	25	0.1775	0.2945	0.0008
Ca	HCO ₃	25	0.400	2.977	0.0000	H	SO ₄	25	0.0298	0.000	0.0438
Zn	Cl	25	0.2602	1.6425	-0.08798	Al	Cl	25	0.6993	5.845	0.00273

M	X	τ	$\beta^{(0)}$	$\beta^{(1)}$	C^ϕ	M	X	τ	$\beta^{(0)}$	$\beta^{(1)}$	C^ϕ		
Ca	Cl	0	0.318	1.500	0.00155	Mg	Cl	0	0.368	1.55	0.00700		
		25	0.3159	1.6140	-0.00034			25	0.3524	1.682	0.00519		
		50	0.313	1.800	-0.0033			50	0.338	1.85	0.00325		
		75	0.310	1.980	-0.0058			75	0.324	2.03	0.00125		
		100	0.305	2.170	-0.0080			100	0.311	2.23	-0.00025		
		125	0.299	2.400	-0.0098			125	0.300	2.45	-0.00138		
		150	0.291	2.600	-0.0113			150	0.289	2.65	-0.00238		
		200	0.272	3.100	-0.0138			200	0.269	3.15	-0.00388		
		250	0.230	3.830	-0.0133			250	0.230	3.88	-0.00513		
		300	0.244	5.250	-0.0143			300	0.244	5.30	-0.00613		
350	0.369	8.300	-0.0232	350	0.369	8.35	-0.00700						
Ba	Cl	0	0.385	2.10	-0.0154	Mg	SO ₄	0	0.1866	3.039	0.00979		
		25	0.350	2.00	-0.0193			25	0.2150	3.365	0.00699		
		50	0.314	1.92	-0.0222			50	0.2275	3.163	0.00494		
		75	0.292	1.90	-0.247			75	0.2372	3.843	0.00290		
		100	0.276	1.92	-0.261			100	0.2489	4.410	0.00079		
		125	0.263	2.00	-0.263			125	0.2640	4.805	-0.00130		
		150	0.252	2.22	-0.258			150	0.2856	5.912	-0.00353		
		200	0.235	2.87	-0.229			200	0.3785	9.736	-0.0115		
		250	0.219	3.83	-0.0168			250	0.6489	7.532	-0.0364		
		300	0.210	5.25	-0.0122			300	1.334	9.736	-0.1046		
350	0.206	8.30	-0.0067	350	2.806	12.57	-0.2575						
Sr	Cl	0	0.460	2.35	0.0100	Mg	HCO ₃	25	0.329	0.6072	0.0000		
		25	0.381	2.22	-0.0013								
		50	0.344	2.20	-0.0080			Mn	SO ₄	25	0.201	2.98	0.0182
		75	0.320	2.13	-0.0115								
		100	0.302	2.10	-0.0139								
		125	0.290	2.16	-0.0156								
		150	0.278	2.30	-0.0167								
		200	0.264	2.90	-0.0180								
		250	0.258	3.83	-0.0191								
		300	0.256	5.25	-0.0198								
350	0.2555	8.30	-0.0203										

<u>i j</u>	<u>t</u>	<u>θ</u>	<u>k l</u>	<u>t</u>	<u>θ</u>
Na Ca	0	-0.0085	Cl SO ₄	25	0.02
	25	-0.0078			
	50	-0.00726	Cl HCO ₃	25	0.03
	75	-0.00696			
	100	-0.0068	Cl CO ₃	25	-0.02
	125	-0.0069			
	150	-0.0074	Cl OH	25	-0.05
	200	-0.0099			
	250	-0.0128	SO ₄ HCO ₃	25	0.01
	300	-0.0155			
	350	-0.0180	SO ₄ CO ₃	25	0.02
Na K	25	-0.012	SO ₄ OH	25	-0.01
Na Mg	25	0.070	HCO ₃ CO ₃	25	-0.04
Na H	25	0.036	CO ₃ OH	25	0.01
K Ca	25	0.032			
K H	25	0.005			
Ca Mg	25	0.007			
Ca H	25	0.092			
Mg H	25	0.100			

<u>i</u>	<u>j</u>	<u>k</u>	<u>t</u>	<u>ψ</u>	<u>k</u>	<u>l</u>	<u>i</u>	<u>t</u>	<u>ψ</u>
Na	Ca	Cl	0	0.0044	Cl	SO ₄	Na	25	0.0014
			25	0.0029					
			50	0.0015	Cl	SO ₄	Ca	25	-0.018
			75	0.00066					
			100	0.00042	Cl	SO ₄	Mg	25	-0.004
			125	0.00035					
			150	0.00035	Cl	HCO ₃	Na	25	-0.015
			200	0.00035					
			250	0.00035	Cl	HCO ₃	Mg	25	-0.096
			300	0.00035					
			350	0.00035	Cl	CO ₃	Na	25	0.0085
Na	K	Cl	25	-0.0018	Cl	CO ₃	K	25	0.004
Na	K	SO ₄	25	-0.01	Cl	OH	Na	25	-0.006
Na	K	HCO ₃	25	-0.003	Cl	OH	K	25	-0.006
Na	K	CO ₃	25	0.003	Cl	OH	Ca	25	-0.025
Na	Ca	SO ₄	25	-0.055	SO ₄	HCO ₃	Na	25	-0.005
Na	Mg	Cl	25	-0.012	SO ₄	HCO ₃	Mg	25	-0.161
Na	Mg	SO ₄	25	-0.015	SO ₄	CO ₃	Na	25	-0.005
Na	H	Cl	25	-0.004	SO ₄	CO ₃	K	25	-0.009
Na	H	SO ₄	25	-0.012	SO ₄	OH	Na	25	-0.009
K	Ca	Cl	25	-0.025	SO ₄	OH	K	25	-0.05
K	Mg	Cl	25	-0.022	HCO ₃	CO ₃	Na	25	0.002
K	Mg	SO ₄	25	-0.048	HCO ₃	CO ₃	K	25	0.0129

<u>i</u>	<u>j</u>	<u>k</u>	<u>t</u>	<u>ψ</u>	<u>k</u>	<u>l</u>	<u>i</u>	<u>t</u>	<u>ψ</u>
K	H	Cl	25	-0.011	CO ₃	OH	Na	25	-0.017
K	H	SO ₄	25	0.197	CO ₃	OH	K	25	-0.01
Ca	Mg	Cl	25	-0.012					
Ca	Mg	SO ₄	25	0.024					
Ca	H	Cl	25	-0.015					
Mg	H	Cl	25	-0.011					

Table IH. Table of congruent dissolution of minerals listing the aqueous species number and stoichiometry.

1,	1.0,4,1.0,14,3.0,11,-4.0,8,-4.0,10,
2,	2.0,1,1.0,2,2.0,11,-6.0,8,-1.0,10,
3,	1.0,3,1.0,14,3.0,11,-4.0,8,-4.0,10,
4,	1.0,3,1.0,14,3.0,11,-4.0,8,-4.0,10,
5,	1.0,3,1.0,14,3.0,11,-4.0,8,-4.0,10,
6,	1.0,4,3.0,14,2.0,6,-6.0,8,6.0,10,
7,	2.0,2,2.0,14,1.0,11,-10.0,8,5.0,10,
8,	1.0,3,1.0,14,2.0,11,-4.0,8,-1.0,10,
9,	2.0,14,1.0,11,-6.0,8,1.0,10,
10,	0.4,1.0,6,3,1.4,14,2.6,11,-5.6,8,-2.4,10,
11,	1.0,1,1.0,6,
12,	1.0,4,3.0,18,1.0,14,3.0,11,-10.0,8,
13,	1.0,1,2.0,14,2.0,11,-8.0,8,
14,	5.0,1,3.0,29,1.0,5,
15,	5.0,1,3.0,29,1.0,30,
16,	5.0,1,3.0,29,1.0,9,
17,	1.0,1,1.0,98,
18,	1.0,1,2.0,14,1.0,11,-8.0,8,2.0,10,
19,	3.0,17,2.0,98,2.0,9,
20,	1.0,15,1.0,6,
21,	1.0,14,2.0,10,-3.0,8,
22,	1.0,2,2.0,9,
23,	0.8,1.0,2,3,1.8,14,2.2,11,-7.2,8,-0.8,10,
24,	1.0,1,1.0,98,
25,	1.0,26,1.0,6,
26,	1.0,11,-2.0,10,
27,	2.0,18,2.0,14,1.0,11,-10.0,8,5.0,10,
28,	5.0,2,2.0,14,3.0,11,6.0,10,-16.0,8,
29,	5.0,2,2.0,14,3.0,11,6.0,10,-16.0,8,
30,	3.0,2,2.0,11,-6.0,8,1.0,10,
31,	1.0,2,1.0,11,-2.0,8,-1.0,10,
32,	2.0,3,2.0,14,10.0,11,-8.0,8,-8.0,10,
33,	2.0,4,2.0,14,10.0,11,-8.0,8,-8.0,10,
34,	1.0,1,2.0,14,10.0,11,-8.0,8,-8.0,10,
35,	1.0,2,2.0,14,10.0,11,-8.0,8,-8.0,10,
36,	2.0,14,3.0,10,-6.0,8,
37,	1.0,11,-2.0,10,
38,	1.0,11,-2.0,10,
39,	2.0,14,2.0,11,-6.0,8,1.0,10,
40,	1.0,1,1.0,2,2.0,11,-4.0,8,-2.0,10,
41,	1.0,1,1.0,2,2.0,98,
42,	1.0,1,1.0,2,2.0,98,
43,	1.0,2,1.0,11,-2.0,8,-1.0,10,
44,	2.0,1,1.0,19,2.0,14,3.0,11,-13.0,8,1.0,10,
45,	2.0,18,1.0,11,-4.0,8,
46,	1.0,1,2.0,30,
47,	2.0,2,1.0,11,-4.0,8,
48,	1.0,14,3.0,9,
49,	1.0,14,3.0,9,
50,	3.0,18,2.0,11,-6.0,8,1.0,10,
51,	1.0,1,1.0,6,2.0,10,
52,	1.0,3,1.0,5,
53,	2.0,14,2.0,11,-6.0,8,1.0,10,
54,	1.0,1,2.0,14,7.0,11,-8.0,8,-4.0,10,
55,	1.0,1,3.0,2,4.0,98,

56, 5.0,2,4.0,98,2.0,9,3.0,10,
 57, 1.0,1,2.0,5,
 58, 0.6,4,0.25,2,2.3,14,3.5,11,-8.0,8,-2.0,10,
 59, 2.0,14,2.0,11,-6.0,8,1.0,10,
 60, 1.0,3,11.0,11,-1.0,8,-16.5,10,
 61, 1.0,4,1.0,14,3.0,11,-4.0,8,-4.0,10,
 62, 2.0,14,1.0,11,-6.0,8,1.0,10,
 63, 0.6,1,0.4,3,1.6,14,2.4,11,-6.6,8,-1.6,10,
 64, 2.0,1,1.0,11,-4.0,8,
 65, 1.0,1,2.0,14,4.0,11,-8.0,8,
 66, 1.0,4,1.0,14,2.0,11,-4.0,8,-2.0,10,
 67, 1.0,1,1.0,10,-2.0,8,
 68, 1.0,3,7.0,11,-1.0,8,-9.0,10,
 69, 1.0,2,2.0,19,4.0,10,-8.0,8,
 70, 1.0,2,1.0,98,
 71, 1.0,2,2.0,5,
 72, 4.0,3,3.0,14,9.0,11,1.0,5,-12.0,8,-12.0,10,
 73, 3.0,1,1.0,2,2.0,11,-8.0,8,
 74, 1.0,4,1.0,14,3.0,11,-4.0,8,-4.0,10,
 75, 4.0,1,6.0,14,6.0,11,1.0,98,-24.0,8,
 76, 2.0,3,1.0,6,10.0,10,
 77, 1.0,1,1.0,2,1.0,11,-4.0,8,
 78, 1.0,3,1.0,14,5.0,11,-4.0,8,-5.0,10,
 79, 1.0,4,1.0,14,5.0,11,-4.0,8,-5.0,10,
 80, 1.0,4,3.0,14,3.0,11,-10.0,8,
 81, 1.0,3,1.0,7,
 82, 2.0,3,1.0,98,1.0,10,
 83, 2.0,3,1.0,98,10.0,10,
 84, 1.0,3,1.0,14,1.0,11,-4.0,8,
 85, 1.0,2,1.0,98,3.0,10,
 86, 0.33,3,2.0,19,0.33,14,3.67,11,-7.32,8,-2.68,10,
 87, 0.33,4,2.0,19,0.33,14,3.67,11,-7.32,8,-2.68,10,
 88, 2.0,19,0.33,14,3.67,11,-6.99,8,-2.68,10,
 89, 0.165,1,2.0,19,0.33,14,3.67,11,-7.32,8,-2.68,10,
 90, 0.165,2,2.0,19,0.33,14,3.67,11,-7.32,8,-2.68,10,
 91, 1.0,1,1.0,101,-1.0,8,
 92, 0.2,1,0.8,3,1.2,14,2.8,11,-4.8,8,-3.2,10,
 93, 1.0,3,3.0,14,3.0,11,-10.0,8,
 94, 1.0,3,2.0,1,4.0,2,3.0,14,6.0,11,-22.0,8,
 95, 1.0,2,-2.0,8,1.0,10,
 96, 0.5,3,0.5,4,1.0,14,3.0,11,-4.0,8,-3.0,10,
 97, 1.0,4,3.0,2,1.0,14,3.0,11,-10.0,8,
 98, 1.0,4,3.0,2,1.0,14,3.0,11,2.0,30,-8.0,8,-2.0,10,
 99, 1.0,1,2.0,9,
 100, 2.0,4,-2.0,8,1.0,10,
 101, 2.0,1,2.0,14,3.0,11,-10.0,8,
 102, 2.0,14,4.0,11,-6.0,8,-4.0,10,
 103, 1.0,11,-2.0,10,
 104, 1.0,4,1.0,14,3.0,11,-4.0,8,-4.0,10,
 105, 0.33,3,3.0,2,0.33,14,3.67,11,-7.32,8,-2.68,10,
 106, 0.33,4,3.0,2,0.33,14,3.67,11,-7.32,8,-2.68,10,
 107, 3.0,2,0.33,14,3.67,11,-6.99,8,-2.68,10,
 108, 0.165,1,3.0,2,0.33,14,3.67,11,-7.32,8,-2.68,10,
 109, 0.165,2,3.0,2,0.33,14,3.67,11,-7.32,8,-2.68,10,
 110, 4.0,2,6.0,11,-8.0,8,-1.0,10,
 111, 1.0,11,-2.0,10,
 112, 1.0,11,-2.0,10,
 113, 2.0,14,1.0,11,-6.0,8,1.0,10,

114, 0.167,1,2.33,14,3.67,11,-7.32,8,-2.68,10,
 115, 0.33,4,2.33,14,3.67,11,-7.32,8,-2.68,10,
 116, 0.167,2,2.33,14,3.67,11,-7.32,8,-2.68,10,
 117, 0.33,3,2.33,14,3.67,11,-7.32,8,-2.68,10,
 118, 2.0,3,-2.0,8,1.0,10,
 119, 1.0,2,2.0,14,4.0,10,-8.0,8,
 120, 1.0,1,2.0,14,7.0,11,-8.0,8,-3.0,10,
 121, 1.0,19,1.0,29,2.0,10,
 122, 1.0,26,1.0,98,
 123, 1.0,4,1.0,5,
 124, 3.0,2,4.0,11,-6.0,8,-4.0,10,
 125, 2.0,3,1.0,6,
 126, 2.0,1,5.0,2,8.0,11,-14.0,8,-8.0,10,
 127, 3.0,3,1.0,7,1.0,98,2.0,10,
 128, 3.0,18,2.0,29,8.0,10,
 129, 1.0,1,2.0,14,4.0,11,-8.0,8,-2.0,10,
 130, 1.0,15,1.0,98,
 131, 1.0,1,1.0,11,-2.0,8,-1.0,10,
 132, 2.0,1,3.0,14,3.0,11,-13.0,8,1.0,10,
 133, 1.0,13,1.0,18,-1.0,19,
 134, 1.0,13,1.0,5,
 135, 2.0,13,1.0,101,-1.0,8,
 136, 1.0,16,1.0,18,-1.0,19,
 137, 2.0,17,1.0,98,2.0,9,
 138, 1.0,17,-2.0,8,1.0,10,
 139, 2.0,16,-2.0,8,1.0,10,
 140, 1.0,17,1.0,101,-1.0,8,
 141, 2.0,16,1.0,101,-1.0,8,
 142, 1.0,17,1.0,18,2.0,101,-2.0,8,
 143, 4.0,16,1.0,17,1.0,18,4.0,101,-4.0,8,
 144, 1.0,18,2.0,5,
 145, 1.0,19,3.0,5,
 146, 1.0,18,1.0,98,
 147, 1.0,18,-2.0,8,1.0,10,
 148, 2.0,19,3.0,10,-6.0,8,
 149, 2.0,19,3.0,10,-6.0,8,
 150, 2.0,19,1.0,18,4.0,10,-8.0,8,
 151, 1.0,19,3.0,9,
 152, 1.0,19,2.0,10,-3.0,8,
 153, 1.0,18,1.0,101,-1.0,8,
 154, 1.0,18,1.0,101,-1.0,8,
 155, 1.0,18,1.75,101,0.25,6,0.25,8,-1.0,10,
 156, 2.0,19,1.0,18,4.0,101,-4.0,8,
 157, 1.0,21,2.0,18,-2.0,19,
 158, 1.0,21,2.0,5,
 159, 1.0,20,2.0,5,
 160, 1.0,21,-2.0,8,1.0,10,
 161, 1.0,21,1.0,101,-1.0,8,
 162, 1.0,21,1.0,101,-1.0,8,
 163, 1.0,23,2.0,5,
 164, 1.0,23,1.0,98,
 165, 1.0,23,-2.0,8,1.0,10,
 166, 2.0,24,2.0,10,-1.0,23,-4.0,8,
 167, 1.0,23,1.0,101,-1.0,8,
 168, 1.0,25,2.0,5,
 169, 1.0,25,1.0,98,
 170, 1.0,25,-2.0,8,1.0,10,
 171, 1.0,25,-2.0,8,1.0,10,

172, 1.0,25,1.0,101,-1.0,8,
 173, 1.0,25,1.0,6,
 174, 1.0,27,1.0,98,
 175, 1.0,27,-2.0,8,1.0,10,
 176, 1.0,27,1.0,101,-1.0,8,
 177, 1.0,27,1.0,6,
 178, 1.0,169,1.0,98,
 179, -2.0,8,2.0,169,2.0,99,2.0,146,
 180, -2.0,8,2.0,169,2.0,99,1.0,25,
 181, -2.0,8,2.0,169,2.0,99,1.0,17,
 182, -2.0,8,2.0,169,2.0,99,1.0,2,
 183, -2.0,8,2.0,169,2.0,99,1.0,26,
 184, -2.0,8,2.0,169,2.0,99,1.0,15,
 185, -2.0,8,2.0,169,2.0,99,1.0,18,
 186, 1.0,169,-2.0,8,1.0,10,
 187, 1.0,169,-2.0,8,1.0,10,
 188, 1.0,169,2.0,9,
 189, 1.0,167,2.5,10,4.0,30,
 190, 2.0,99,1.0,167,4.0,10,
 191, -2.0,8,1.0,167,2.0,99,2.0,10,1.0,1,
 192, 1.0,169,2.0,168,-4.0,8,2.0,10,
 193, 1.0,167,-4.0,8,2.0,10,
 194, 1.0,167,-4.0,8,2.0,10,
 195, 2.0,167,2.0,168,-10.0,8,5.0,10,
 196, -4.0,8,1.0,167,1.0,11,
 197, 2.0,169,2.0,99,
 198, -2.0,8,2.0,3,2.0,169,2.0,99,
 199, -2.0,8,2.0,4,2.0,169,2.0,99,
 200, -2.0,8,1.0,1,2.0,169,2.0,99,
 201, 2.0,4,2.0,169,2.0,210,
 202, 1.0,1,2.0,169,2.0,210,
 203, -6.0,8,1.0,1,2.0,169,2.0,11,
 204, 1.0,169,2.0,9,1.0,10,
 205, 1.0,169,1.0,2,-4.0,8,2.0,10,
 206, 1.0,169,1.0,1,-4.0,8,2.0,10,
 207, 1.0,169,1.0,15,-4.0,8,2.0,10,
 208, 1.0,169,2.0,30,
 209, 1.0,169,3.0,101,1.0,8,-2.0,10,
 210, 2.0,212,3.0,10,-6.0,8,
 211, 2.0,211,-4.0,8,2.0,10,
 212, 2.0,210,6.0,8,-3.0,10,
 213, 1.0,211,1.0,6,6.0,10,
 214, 2.0,210,3.0,25,

APPENDIX II. An abbreviated version of the interactive input routine SOLINPUT

SOLMINEQ_88 Input Data File Creation Program

Sample 1

MAIN MENU

- 1) Create/Edit Current Sample Data
- 2) Read an Existing Input File
- 3) Go to Next Sample
- 4) Go to Previous Sample
- 5) Write All Samples to an Input File
- 6) Exit Program

Enter Choice (1-6)

1

OPTIONS MENU

- 1) Enter Basic Parameters
- 2) Enter Program Option Flags
- 3) Enter Gas, pH, and CO2 Options
- 4) Enter Gas Distribution Option
- 5) Enter Ion Exchange or Adsorption Option
- 6) Enter Precipitation/Mixing/Boiling Option
- 7) Enter User Log K Option
- 8) Enter Additional Anions/Cation/Minerals Option
- 9) Return to Main Menu

Enter Choice (1-9)

1

BASIC PARAMETERS MENU

- 1) Enter Title and Units
- 2) Enter Temperatures, Density, and Pressure
- 3) Enter pH, and Eh
- 4) Enter Concentrations for Major Species
- 5) Enter Concentrations for Minor Species
- 6) Enter Concentrations for Organic Species
- 7) Return to Options Menu

Enter Choice (1-7)

Enter the title of this sample

[SAMPLE # 1]

Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C

Enter Concentration Units (Mg/l, PPM, Mol/l, Mol/K, Meq/l)

[MG/L]

ppm

Enter the pH

[Current = 7.0000]

8.2

Enter Eh in Volts

[Current = 9.0000]

0.5

- 1) ENTER: Na, K, Li, Ca, Mg, Fe, Al
- 2) ENTER: SiO₂, Cl, SO₄, H₂S, HCO₃, CO₃, TIC
- 3) Return to Basic Parameters Menu

Enter Choice (1-3)

Enter Concentration of Na [Current = 0.0000E-01]

10770

Enter Concentration of K [Current = 0.0000E-01]

399.1

Enter Concentration of Li [Current = 0.0000E-01]

0.181

Enter Concentration of Ca [Current = 0.0000E-01]

412.3

Enter Concentration of Mg [Current = 0.0000E-01]

1292

Enter Concentration of Fe [Current = 0.0000E-01]

0.002

Enter Concentration of Al [Current = 0.0000E-01]

0.002

Enter Concentration of SiO₂ [Current = 0.0000E-01]

4.28

Enter Concentration of Cl [Current = 0.0000E-01]

0.1935E+05

Enter Concentration of SO₄ [Current = 0.0000E-01]

2712

Enter Concentration of H2S [Current = 0.0000E-01]

Enter Alkalinity as HCO3 [Current = 0.0000E-01]
123.4

Enter Alkalinity as CO3 [Current = 0.0000E-01]

Enter TIC [Current = 0.0000E-01]

1) ENTER: F, PO4, NO3, NH3, B, Sr, Ba

2) ENTER: Pb, Zn, Cu, Mn, Hg, Ag

3) ENTER: As, U, V

4) Return to Basic Parameters Menu

Enter Choice (1-4)

Enter Concentration of F [Current = 0.0000E-01]
1.39

Enter Concentration of PO4 [Current = 0.0000E-01]
0.06

Enter Concentration of NO3 [Current = 0.0000E-01]
.29

Enter Concentration of NH3 [Current = 0.0000E-01]
.03

Enter Concentration of B [Current = 0.0000E-01]
4.45

Enter Concentration of Sr [Current = 0.0000E-01]
8.14

Enter Concentration of Ba [Current = 0.0000E-01]
.02

Enter Concentration of Pb [Current = 0.0000E-01]
0.5E-4

Enter Concentration of Zn [Current = 0.0000E-01]
0.0049

Enter Concentration of Cu [Current = 0.0000E-01]
0.0007

Enter Concentration of Mn [Current = 0.0000E-01]
0.0002

Enter Concentration of Hg [Current = 0.0000E-01]

Enter Concentration of Ag [Current = 0.0000E-01]
0.004

OPTIONS MENU

- 1) Enter Basic Parameters
 - 2) Enter Program Option Flags
 - 3) Enter Gas, pH, and CO₂ Options
 - 4) Enter Gas Distribution Option
 - 5) Enter Ion Exchange or Adsorption Option
 - 6) Enter Precipitation/Mixing/Boiling Option
 - 7) Enter User Log K Option
 - 8) Enter Additional Anions/Cation/Minerals Option
 - 9) Return to Main Menu
- Enter Choice (1-9)

2

FLAGS MENU

- 1) Enter Carbonate Distribution
 - 2) Enter Activity Coefficient Control
 - 3) Enter Redox Equilibria
 - 4) Enter Printout Control
 - 5) Enter Tolerance Control
 - 6) Return to Options Menu
- Enter Choice (1-6)

What does the concentration of bicarbonate/carbonate refer to:

- 0 - Total Alkalinity as HCO₃/CO₃?
 - 1 - Carbonate Alkalinity as HCO₃/CO₃?
 - 2 - Total Inorganic Carbon (TIC)?
- [Current = 0]

2

Do you wish to use TIC for the distribution of carbonate species at high temperature? (Y/N)

[Current = N]

Do you want to distribute Fe using Eh? (Y/N)

[Current = N]

y

Do you want to distribute Cu using Eh? (Y/N)

[Current = N]

y

Do you want to distribute Hg using Eh? (Y/N)

[Current = N]

y

Do you want to distribute Mn using Eh? (Y/N)

[Current = N]

y

Do you want to distribute U using Eh? (Y/N)

[Current = N]

Do you want to distribute V using Eh? (Y/N)

[Current = N]

Do you want to print the aqueous log K values in the
data base at the temperatures of interest ? (Y/N)

[Current = N]

Do you want to print out the analytical and calculated
activity ratios of the major elements? (Y/N)

[Current = N]

y

Do you want to print out the temperature estimates
from the chemical geothermometers? (Y/N)

[Current = N]

y

Do you want to print out the data on the iteration
of the anions? (Y/N)

[Current = N]

Do you want to print out the data on the mass balance
on Hydrogen whenever a new pH is calculated? (Y/N)

[Current = N]

Name of a new input file to be created based upon
the output of this sample.

[Current =]

Sample 1

MAIN MENU

- 1) Create/Edit Current Sample Data
- 2) Read an Existing Input File
- 3) Go to Next Sample
- 4) Go to Previous Sample
- 5) Write All Samples to an Input File
- 6) Exit Program

Enter Choice (1-6)

5

What do you want to call this file?

[Current = SOLMINEQ.IN]

SOLMINEQ.IN

already exists. Do you wish to overwrite?

y

Will write out 1 sample(s).

Enter a <CR> for ok or a number indicating how many
samples you want written out.

Writing file ...

Sample 1

MAIN MENU

- 1) Create/Edit Current Sample Data
- 2) Read an Existing Input File
- 3) Go to Next Sample
- 4) Go to Previous Sample
- 5) Write All Samples to an Input File
- 6) Exit Program

Enter Choice (1-6)

6

**** STOP

Input File Created

Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C

0.2500E+020.0000E+000.0000E+000.0000E+00

0.8200E+010.5000E+000.9000E+010.9000E+01PPM

0.1077E+050.3991E+030.1810E+000.4123E+030.1292E+040.2000E-020.2000E-02

0.4280E+010.1935E+050.2712E+040.0000E+000.1234E+030.0000E+000.0000E+00

0.1390E+010.6000E-010.2900E+000.3000E-010.4450E+010.8140E+010.2000E-01

0.5000E-040.4900E-020.7000E-030.2000E-030.3000E-040.4000E-04

0.4000E-020.0000E+000.0000E+00

0.0000E+000.0000E+000.0000E+000.0000E+00

2 0

0.0000E+000.0000E+000.0000E+000.0000E+00

0 00.0000E+000.5000E-01

0.0000E+000.0000E+000.0000E+000.0000E+000.0000E+000.0000E+000.0000E+000.0000E+00

0 0

00.0000E+00 00.0000E+00 00.0000E+00 00.0000E+00 00.0000E+00

00.0000E+00

00.0000E+00 00.0000E+00 00.0000E+00 00.0000E+00 00.0000E+00

00.0000E+00

0 0

0

0

1 0 1 1 1 1 0 0

0 1 1 0 0

0.5000E-040.5000E-04

APPENDIX III. Output Examples

The output from four test cases are given below. These cases were selected to illustrate several of the main options in this code and to be used for comparison of results by those who acquire and implement this program. The number of possible options in this code is extremely large and can not be adequately illustrated in this report.

Test sample #1 gives the chemical composition of modified sea water (Nordstrom and others, 1979) to which has been added 0.1 ppm acetate, oxalate, and succinate. The output gives the distribution of all the inorganic and organic species and the saturation states of all the minerals in the database with the exception of those for U and V. The activity coefficients for the charged species are calculated using the B^{*} method and those for neutral species are made equal to the activity coefficient of dissolved CO₂. The printing options selected display the iterations for anions (total = 6), the ratios for cations and anions, and the chemical geothermometers.

The mixing option in SOLMINEQ.88 is illustrated with the test sample #2. This case is a real world test involving the mixing of formation water from the McMurray formation, Alberta, Canada, and high pH flood water. The mixing proportions specified in this case are 50/50%, but the number of the mixtures and the mixing proportions can be varied by the user for any one run. Speciation and saturation computations are carried out and results are listed for each end member as well as for the specified mixture or mixtures.

Test sample #3 illustrates one of the dissolution/precipitation options in SOLMINEQ.88. In this case the mineral anorthite (index number = 13) is to be dissolved/precipitated until the sea water of test sample #1 is at equilibrium with the mineral gibbsite (index number = 49). The program initially carries out speciation and saturation computations for sea water (printout not shown, but is similar to that shown on pages 2-10 of test sample #1). Results of speciation and saturation computations after equilibration with gibbsite are then printed.

The amount of anorthite precipitated to achieve equilibrium with gibbsite ($SI \leq 0.05$) is -3.076×10^{-8} moles. The "thinking" geochemist should realize that the program (which obeys all commands!) is performing an impossible task. The saturation states of anorthite and gibbsite in sea water are -6.782 and 0.917 kcal/mole, respectively. Thus, in order to equilibrate with gibbsite, anorthite must precipitate from this sea water sample. Precipitation of

anorthite from a solution that is undersaturated with respect to it is, of course, thermodynamically impossible. This example illustrates the fact that the user (not the code) is responsible for all the results of computations carried out by this program.

The ion exchange option is illustrated with the test sample #4. In this case 100 g of smectite, with cation exchange capacity (CEC) of 100 meq per 100 g and with its sites filled with an equal amount of Ca and Mg, is added to one liter of sea water. We assume that the selectivity constant of smectite for divalent cations relative to monovalent cations is so high that we can neglect any exchange with monovalent cations in sea water. We assume, also, that the selectivity of smectite for Ca and Mg is equal to one.

The program initially computes the distribution of species and the saturation states of minerals (printout deleted as it is similar to that of test sample #1). The program then computes the final distribution of Ca and Mg on the smectite surface and the new distribution of species and saturation state of minerals in the resulting sea water sample. The output shows that 424 ppm Ca has been transferred from the smectite surface to the sea water and 257 ppm Mg from sea water to the smectite surface. The saturation states of all the Ca and Mg minerals, of course, are changed from the initial conditions.

***** INPUT DATA ECHO *****

TITLE : Test Sample #1 for SOLMINEq.88 - Modified Seawater at 25 C

TEMP	HITEMP	DENS	PRESS
0.2500E+02	0.0000E+00	0.1023E+01	0.0000E+00
PH	EHM	EHMC	EMFZSC
0.8200E+01	0.5000E+00	0.9000E+01	0.9000E+01

CONCENTRATION UNITS : PPM

Na	K	Li	Ca	Mg	Fe	Al
0.1077E+05	0.3991E+03	0.1810E+00	0.4123E+03	0.1292E+04	0.2000E-02	0.2000E-02
SiO2	Cl	SO4	H2S	HCO3	CO3	TIC
0.4280E+01	0.1935E+05	0.2712E+04	0.0000E+00	0.1234E+03	0.0000E+00	0.0000E+00
F	PO4	NO3	NH3	B	Sr	Ba
0.1390E+01	0.6000E-01	0.2900E+00	0.3000E-01	0.4450E+01	0.8140E+01	0.2000E-01
Pb	Zn	Cu	Mn	Hg	Ag	
0.5000E-04	0.4900E-02	0.7000E-03	0.2000E-03	0.3000E-04	0.4000E-04	
As	U	V				
0.4000E-02	0.0000E+00	0.0000E+00				
Acetate	Oxalate	Succinate	CH4			
0.1000E+00	0.1000E+00	0.1000E+00	0.1000E+00			

ALK ITIC

Z 0

DCO2 DH2S DNH3 DCH4

0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

ICCSAT IMCO3 FIXIT FCCSAT

0 0 0.0000E+00 0.0500

TCO2M TCH4M TH2SM WROIL

0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

KCO2OL KCH4OL KH2SOL DSEP

0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

Adsorption/Exchange option (N=no) = N

IBMIX ITMIX

0 0

LOG KT TO BE CHANGED AT TEMP = 25.00

0 0.0000E+00 0 0.0000E+00

LOG KT TO BE CHANGED AT TEMP = 0.00

0 0.0000E+00 0 0.0000E+00

ANS1 ANS2

0 0

Number of Additional Minerals = 0

FLAG FOR ACTIVITY COEFF OF NEUTRAL SPECIES: 1

FLAG FOR ACTIVITY COEFF BY PITZERS EQUATIONS: 0

FLAGS FOR CALCULATING REDOX SPECIES:

Fe Cu Hg Mn U V

1 1 1 1 0 0

PRINTING OPTIONS:

INFORM RATIO GEOTH IPRIN1 IPRIN2

0 1 1 1

TOLERANCE FACTORS: CONV1 = 0.5000E-04 CONV2 = 0.5000E-04

SOLMINEQ.87 (VERSION: USGS-ARC-88-8) - SOLUTION-MINERAL-EQUILIBRIUM COMPUTATIONS

SAMPLE IDENT:- Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C

ITERATIVE CONVERGENCE TEST AT TEMPERATURE = 25.00

ITER	CARBONATE	SULFATE	FLUORIDE	PHOSPHATE	CHLORIDE	ACETATE	SULFIDE	OXYLATE	SUCCINATE	USR-DEF #1	USR-DEF #2
1	3.442E-01	1.131E+00	6.964E-01	3.761E+00	3.108E-02	3.447E-01	0.000E+00	8.063E+00	4.936E-01	0.000E+00	0.000E+00
6	5.388E-06	1.801E-05	1.245E-05	2.843E-05	2.752E-07	5.398E-06	0.000E+00	3.134E-05	9.374E-06	0.000E+00	0.000E+00

Total number of iterations = 6 at pH = 8.20

SAMPLE IDENT:- Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C

PH	EH	TEMP	ANIONS		DIFFERENCE (NEQ/L)		H - OH BALANCE (MOLES)		DIFFERENCE
8.20	0.5000	25.00	ANAL=	619.6747	618.2648	1.4099	HTOT	OHTOT	
			CALC=	577.6364	569.7726	7.8638	0.2198E-02	0.1351E-02	0.8477E-03
-----PRESSURE-----									
DENSITY AT	TOTAL DISSOLVED	IONIC	ACTIVITY	P TOTAL	PH2O	PCO2	PH2S	PNH3	
INPUT T	SOLIDS (MG/L)	STRENGTH	OF WATER	(BARS)	(BARS)	(BARS)	(BARS)	(BARS)	
1.0230	35906.34	0.64945	0.9809	1.0000	0.3169E-01	0.4782E-03	0.0000E+00	0.5252E-02	0.1644E-08
Dissolved Inorganic Carbon									
Total Alkalinity as		as		HCO3-		H2CO3		Sum of	
HCO3- CO3=		TIC		Alkalinity		species		HCO3- CO3=	
(MG/L)=0.1423E+03		0.6999E+02		0.1167E+03		0.2485E+02		0.1373E+03	
(PPM)=0.1391E+03		0.6842E+02		0.1141E+03		0.2429E+02		0.1343E+03	
(MOLALITY)=0.2363E-02		0.1182E-02		0.1182E-02		0.2096E-02		0.2287E-02	
-----ANALYZED-----		-----CALCULATED-----		MG/L		MOLALITY		ACTIVITY	
SPECIES	PPM	MG/L	PPM	MG/L	PPM	MOLALITY	ACTIVITY	ACTIVITY	-LOG10
1 Ca ++	412.3000	421.7829	0.1066E-01	0.2844E+03	0.2909E+03	0.7353E-02	0.1807E-02	0.2458	2.7429
2 Mg ++	1292.0000	1321.7160	0.5508E-01	0.1121E+04	0.1147E+04	0.4779E-01	0.1261E-01	0.2640	1.8992
3 Na +	10770.0000	11017.7100	0.4855E+00	0.1024E+05	0.1048E+05	0.4618E+00	0.3099E+00	0.6710	0.5088
4 K +	399.1000	408.2793	0.1058E-01	0.3825E+03	0.3913E+03	0.1014E-01	0.6357E-02	0.6269	2.1968
5 Cl -	19350.0000	19795.0500	0.5656E+00	0.1874E+05	0.1917E+05	0.5478E+00	0.3434E+00	0.6269	0.4641
6 SO4 --	2712.0000	2774.3760	0.2926E-01	0.1203E+04	0.1231E+04	0.1298E-01	0.2189E-02	0.1687	2.6598
7 HCO3 -	123.4000	126.2382	0.2096E-02	0.8534E+02	0.8730E+02	0.1449E-02	0.1000E-02	0.6899	3.0000
8 H +				0.7638E-05	0.7814E-05	0.7853E-08	0.6310E-08	0.8034	8.2000
9 OH -				0.4016E-01	0.4108E-01	0.2447E-05	0.1591E-05	0.6501	5.7984
11 H4SiO4				0.6615E+01	0.6767E+01	0.7133E-04	0.7133E-04	1.0000	4.1467
12 SiO2	4.2800	4.3784	0.7382E-04	0.1039E-08	0.1063E-08	0.9982E-14	0.6000E-14	0.6011	14.2219
13 Ag +	0.0000	0.0000	0.3843E-09	0.4280E-11	0.4379E-11	0.1644E-15	0.1404E-16	0.0854	16.8525
14 Al +3	0.0020	0.0020	0.7682E-07	0.1815E-01	0.1857E-01	0.1370E-06	0.2849E-07	0.2080	7.5453
15 Ba ++	0.0200	0.0205	0.1509E-06	0.2395E-09	0.2450E-09	0.3906E-14	0.2348E-14	0.6011	14.6294
16 Cu +	0.0007	0.0007	0.1142E-07	0.3648E-03	0.3732E-03	0.5950E-08	0.1462E-08	0.2458	8.8349
17 Cu ++				0.1268E-08	0.1297E-08	0.2353E-13	0.5784E-14	0.2458	14.2378
18 Fe ++	0.0020	0.0020	0.3711E-07	0.1009E-12	0.1032E-12	0.1872E-17	0.1599E-18	0.0854	18.7962
19 Fe +3				0.7474E-18	0.7646E-18	0.3861E-23	0.8033E-24	0.2080	24.0951
21 Hg ++	0.0000	0.0000	0.1550E-09	0.1792E+00	0.1833E+00	0.2677E-04	0.1973E-04	0.7373	4.7048
22 Li +	0.1810	0.1852	0.2703E-04	0.5864E-06	0.5999E-06	0.1106E-10	0.2719E-11	0.2458	11.5656
23 Mn ++	0.0002	0.0002	0.3773E-08	0.8887E-23	0.9092E-23	0.1677E-27	0.1432E-28	0.0854	28.8440
24 Mn +3				0.9966E-06	0.1020E-05	0.4985E-11	0.9397E-12	0.1885	12.0270
25 Pb ++	0.0001	0.0001	0.2501E-09	0.7551E+01	0.7725E+01	0.8931E-04	0.1858E-04	0.2080	4.7310
26 Sr ++	8.1400	8.3272	0.9628E-04	0.2886E-02	0.2952E-02	0.4575E-07	0.1124E-07	0.2458	7.9490
27 Zn ++	0.0049	0.0050	0.7768E-07	0.7209E-03	0.7375E-03	0.5706E-08	0.3829E-08	0.6710	8.4169
28 H2AsO3-	0.0067	0.0068	0.5281E-07	0.5919E-05	0.6055E-05	0.6459E-10	0.1748E-11	0.0271	11.7573
29 PO4 -3	0.0600	0.0614	0.6548E-06	0.7672E+00	0.7848E+00	0.4185E-04	0.2721E-04	0.6501	4.5653
30 F -	1.3900	1.4220	0.7583E-04	0.2205E+02	0.2256E+02	0.3696E-03	0.3696E-03	1.0000	3.4323
31 B(OH)3	25.4540	26.0394	0.4266E-03	0.7083E-09	0.7246E-09	0.1597E-13	0.3566E-14	0.2234	14.4478
32 NH3	0.0300	0.0307	0.1826E-05	0.3364E-08	0.3442E-08	0.5366E-13	0.3863E-13	0.7198	13.4131
34 AlF ++				0.1024E-08	0.1047E-08	0.1263E-13	0.1263E-13	1.0000	13.8984
35 AlF2 +				0.1215E-10	0.1243E -9	0.1223E-15	0.8438E-16	0.6899	16.0737
36 AlF3									
37 AlF4 -									

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
38 Al(OH) ⁺⁺			0.4655E-08	0.4762E-08	0.2234	13.6109
39 Al(OH) ₂ ⁺			0.3336E-05	0.3413E-05	0.7198	10.3893
40 Al(OH) ₄ ⁻			0.7037E-02	0.7199E-02	0.6899	7.2761
41 AlSO ₄ ⁺			0.5289E-11	0.5411E-11	0.6899	16.5123
42 AlSO ₄ 2 ⁻			0.1600E-11	0.1637E-11	0.6899	17.2822
43 AgCl			0.5954E-06	0.6091E-06	1.0000	11.3660
44 AgCl ₂ ⁻			0.3801E-04	0.3889E-04	0.6710	9.8301
45 AgCl ₃ ⁻⁻			0.3041E-04	0.3111E-04	0.2080	10.5143
46 AgCl ₄ ⁻³			0.4054E-05	0.4148E-05	0.0394	12.1784
47 AgSO ₄ ⁻			0.7863E-10	0.8044E-10	0.6710	15.5717
48 CH ₃ COO ⁻	0.1000	0.1023	0.7225E-01	0.7391E-01	0.6899	6.0580
49 H ₃ AsO ₃			0.5724E-02	0.5856E-02	1.0000	7.3269
51 BaCO ₃			0.1272E-04	0.1301E-04	1.0000	10.1753
52 BaHCO ₃ ⁺			0.2238E-03	0.2290E-03	0.6710	9.1053
53 BaOH ⁺			0.3234E-07	0.3309E-07	0.7071	12.8137
54 BaSO ₄			0.2867E-02	0.2933E-02	1.0000	7.8951
55 CaCO ₃			0.2147E+01	0.2197E+01	1.0000	4.6529
56 CaHCO ₃ ⁺			0.3081E+01	0.3152E+01	0.7373	7.4013
57 CaOH ⁺			0.1688E-02	0.1727E-02	0.7198	8.0303
58 CaPO ₄ ⁻			0.2333E-02	0.2387E-02	1.0000	7.9203
59 CaH ₂ PO ₄ ⁺			0.2207E-04	0.2258E-04	1.0000	3.1028
61 CaSO ₄			0.1037E+03	0.1061E+03	1.0000	12.3935
62 CuCl			0.3860E-07	0.3949E-07	1.0000	10.6177
63 CuCl ₂ ⁻			0.4663E-05	0.4770E-05	0.2080	10.8818
64 CuCl ₃ ⁻⁻			0.1035E-04	0.1058E-04	0.6710	9.2790
65 CuCl ⁺			0.7487E-04	0.7659E-04	1.0000	10.4732
66 CuCl ₂			0.4364E-05	0.4464E-05	0.6710	12.5273
67 CuCl ₃ ⁻			0.7255E-07	0.7422E-07	0.2080	15.2915
68 CuCl ₄ ⁻⁻			0.4869E-09	0.4981E-09	0.6710	8.5733
69 CuOH ⁺			0.3094E-03	0.3165E-03	1.0000	9.2447
70 CuSO ₄			0.8766E-04	0.8967E-04	0.6710	15.2319
71 FeCl ⁺			0.7697E-10	0.7874E-10	1.0000	23.3761
72 FeCl ₂			0.5145E-18	0.5263E-18	1.0000	18.2551
73 FeHPO ₄			0.8141E-13	0.8329E-13	1.0000	14.6673
74 H ₃ PO ₄			0.2034E-09	0.2081E-09	0.7071	15.5362
75 FeOH ⁺			0.2892E-10	0.2959E-10	1.0000	18.4446
76 Fe(OH) ₂			0.3115E-13	0.3187E-13	1.0000	18.6546
77 FeOOH ⁻			0.2686E-13	0.2748E-13	1.0000	14.4676
78 FeSO ₄			0.4994E-09	0.5109E-09	0.2080	17.7903
79 FeCl ⁺⁺			0.683E-12	0.7021E-12	1.0000	19.0586
80 FeCl ₂ ⁺			0.4400E-12	0.4501E-12	0.6710	21.4427
81 FeCl ₃			0.1368E-13	0.1399E-13	0.7071	17.3160
82 FeCl ₄ ⁻			0.1026E-15	0.1049E-15	0.2080	29.5358
83 FeSO ₄ ⁻			0.1001E-11	0.1024E-11	0.6710	12.7346
84 FeSO ₄ 2 ⁻			0.1038E-23	0.1062E-23	0.7198	9.5130
85 FeOH ⁺⁺			0.6227E-07	0.6370E-07	1.0000	7.6913
86 Fe(OH) ₂ ⁺			0.3697E-04	0.3782E-04	0.7198	7.9297
87 Fe(OH) ₃			0.2099E-02	0.2147E-02	0.6065	4.4607
88 Fe(OH) ₄ ⁻			0.1952E-02	0.1997E-02	0.2234	9.2767
89 B(OH) ₄ ⁻			0.4342E+01	0.4442E+01	0.6710	5.7767
90 H ₂ SiO ₄ ⁻⁻			0.2150E-03	0.2199E-03		
91 H ₃ SiO ₄ ⁻			0.2287E+00	0.2340E+00		

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
92 HAsO3 --			0.1173E-07	0.1200E-07	0.2080	13.7107
96 HF			0.5016E-05	0.5131E-05	1.0000	9.5853
97 H2CO3			0.8454E+00	0.8648E+00	1.0000	4.8500
98 CO3 --			0.1922E+01	0.1966E+01	0.2234	5.1300
99 HPO4 --			0.1074E-01	0.1099E-01	0.2080	7.6173
100 H2PO4 --			0.3138E-03	0.3210E-03	0.7198	8.6173
103 HSO4 -			0.1671E-03	0.1709E-03	0.6899	8.9098
104 HNO3			0.4331E-10	0.4431E-10	1.0000	15.1473
105 HgCl +			0.1665E-12	0.1704E-12	0.6710	18.3093
106 HgCl2			0.4517E-06	0.4621E-06	1.0000	11.7634
107 HgCl3 -			0.3216E-04	0.3290E-04	0.6710	10.1376
108 HgCl4 --			0.1476E-04	0.1510E-04	0.2080	11.0317
109 HgSO4			0.1264E-19	0.1293E-19	1.0000	25.3550
113 KCl			0.2070E+02	0.2118E+02	1.0000	3.5409
114 KO3 -			0.7987E-01	0.8171E-01	0.6629	6.2568
115 KHSO4			0.7277E-05	0.7445E-05	1.0000	10.2566
116 KSO4 -			0.1957E+02	0.2002E+02	0.7198	3.9666
117 KPO4 -			0.5417E-04	0.5541E-04	0.7198	9.5241
118 LiOH			0.1098E-05	0.1123E-05	1.0000	10.3232
119 LiSO4 -			0.2650E-01	0.2711E-01	0.7071	6.7246
120 MgCO3 +			0.7265E+01	0.7432E+01	1.0000	4.0492
121 MgHCO3 +			0.1818E+02	0.1860E+02	0.6710	3.8292
122 MgF +			0.1373E+01	0.1403E+01	0.6899	4.6445
123 MgOH +			0.4244E+00	0.4341E+00	0.7505	5.0976
124 MgSO4			0.8054E+03	0.8240E+03	1.0000	2.1590
125 MgPO4 -			0.1041E-01	0.1065E-01	0.7198	7.1865
126 MgHPO4			0.4552E-01	0.4657E-01	1.0000	6.4065
127 MgH2PO4+			0.1363E-03	0.1395E-03	0.6710	18.5297
128 MnCl +			0.3839E-13	0.3927E-13	0.6710	15.5938
129 MnCl2			0.3094E-10	0.3165E-10	1.0000	14.6580
130 MnCl3 -			0.5098E-09	0.5215E-09	0.2080	14.2221
131 MnCl4 --			0.5472E-08	0.5598E-08	0.6710	13.2956
132 MnHCO3 +			0.8443E-08	0.8637E-08	1.0000	11.9654
133 MnSO4			0.1578E-06	0.1614E-06	1.0000	15.6029
134 MnHPO4			0.3633E-10	0.3717E-10	0.6710	13.9239
135 MnOH +			0.1233E-08	0.1261E-08	0.6269	5.5173
136 NO3 -	0.2900	0.2967	0.2900E+00	0.2967E+00	1.0000	1.8229
137 NaCl			0.8478E+03	0.8673E+03	1.0000	4.3688
138 NaCO3 -			0.4759E+01	0.4869E+01	0.7198	3.7588
139 NaHCO3			0.1521E-01	0.1556E-01	1.0000	6.8276
140 Na2CO3			0.1413E+02	0.1445E+02	1.0000	2.1674
141 Na2SO4			0.9321E+03	0.9536E+03	1.0000	2.9386
142 NaSO4 -			0.1838E+03	0.1880E+03	0.7198	7.8361
143 NaHPO4 -			0.2326E-02	0.2379E-02	1.0000	5.9541
144 NaF			0.4503E-01	0.4607E-01	0.6011	5.9824
146 NH4 +			0.3015E-01	0.3085E-01	1.0000	7.0308
147 NH4OH			0.3150E-02	0.3223E-02	1.0000	11.0812
148 PbCl +			0.2894E-05	0.2961E-05	0.6710	10.9853
149 PbCl2			0.2776E-05	0.2840E-05	1.0000	11.7594
150 PbCl3 -			0.7845E-06	0.8026E-06	0.6710	12.4236
151 PbCl4 --			0.6104E-06	0.6244E-06	0.2080	11.9368
152 PbSO4			0.3384E-06	0.3462E-06	1.0000	26.6981
153 MnCl ++			0.8401E-21	0.8595E-21	0.2080	

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
154 SrOH -			0.2067E-04	0.2114E-04	0.7071	9.8394
155 SrCO3			0.1296E-01	0.1326E-01	1.0000	7.0410
156 SrHCO3 +			0.6151E-01	0.6292E-01	0.2878E-06	6.5410
157 SrSO4			0.1142E+01	0.1169E+01	1.0000	5.1908
158 ZnCl +			0.1473E-02	0.1507E-02	0.1016E-07	7.9932
159 ZnCl2			0.7271E-03	0.7438E-03	1.0000	8.2573
160 ZnCl3 -			0.2461E-03	0.2518E-03	0.6710	9.0015
161 ZnCl4 --			0.2276E-03	0.2328E-03	0.2080	9.6256
162 ZnSO4			0.6217E-03	0.6360E-03	1.0000	8.3989
163 AlF5 --			0.2976E-13	0.3044E-13	0.2080	19.2791
164 AlF6 -3			0.1492E-16	0.1526E-16	0.0394	23.3644
165 HgOH +			0.1153E-13	0.1180E-13	0.6710	19.4335
166 Hg(OH)2			0.3411E-08	0.3490E-08	1.0000	13.8219
228 CH3COOH			0.1841E-04	0.1883E-04	1.0000	9.4980
229 AlAce ++			0.3920E-14	0.4010E-14	0.1885	20.0506
230 BaAce +			0.9235E-07	0.9447E-07	0.6899	12.4734
231 CaAce +			0.3723E-02	0.3809E-02	0.6899	7.5710
232 CuAce +			0.2733E-13	0.2796E-13	0.6899	18.7974
233 FeAce +			0.1622E-12	0.1660E-12	0.6899	17.9958
234 Fe(Ace)2			0.9354E-20	0.9569E-20	1.0000	25.2539
235 Kace			0.2146E-03	0.2195E-03	1.0000	8.6448
236 MgAce +			0.2288E-01	0.2340E-01	0.6899	6.7072
237 NaAce			0.1264E-01	0.1293E-01	1.0000	6.7968
238 PbAce +			0.5570E-10	0.5699E-10	0.6899	15.8251
239 Pb(Ace)2			0.9855E-15	0.1008E-14	1.0000	20.5031
240 Pb(Ace)3			0.1775E-20	0.1816E-20	0.6899	26.4811
241 SrAce +			0.4820E-04	0.4930E-04	0.6899	9.6290
244 ZnAce +			0.1391E-03	0.1423E-03	0.6899	9.0971
245 Zn(Ace)2			0.3411E-13	0.3490E-13	1.0000	18.7151
246 C2O4 --	0.1000	0.1177E-05	0.9439E-02	0.9656E-02	0.2234	7.6051
247 HC2O4 -			0.3468E-09	0.3548E-09	0.6899	14.5551
248 H2C2O4			0.3117E-13	0.3189E-13	1.0000	18.4451
249 AlOxy +			0.5607E-13	0.5736E-13	0.6899	18.4576
250 AlOxy)2-			0.2457E-15	0.2514E-15	0.6899	21.0628
251 BaOxy			0.5714E-08	0.5845E-08	1.0000	13.5804
252 CaOxy			0.5546E-02	0.5673E-02	1.0000	7.3481
253 FeOxy			0.5006E-12	0.5122E-12	1.0000	17.4429
254 FeOxy +			0.3028E-13	0.3097E-13	0.6899	18.8225
255 KOxy -			0.1406E-03	0.1438E-03	0.6899	9.1019
256 MgOxy			0.1002E+00	0.1025E+00	1.0000	6.0343
257 MnOxy			0.9311E-10	0.9525E-10	1.0000	15.1707
258 MnOxy)2			0.7180E-03	0.7345E-03	0.2234	9.0758
259 MnOxy)3			0.1550E-06	0.1585E-06	0.0021	14.8809
260 MnOxy			0.2764E-19	0.2828E-19	0.6899	24.8593
261 NaOxy -			0.9487E-02	0.9705E-02	0.6899	7.2139
262 PbOxy			0.3651E-09	0.3735E-09	1.0000	14.8922
263 SrOxy			0.2710E-04	0.2773E-04	1.0000	9.7961
264 ZnOxy			0.3282E-05	0.3357E-05	1.0000	10.6542
265 C4H4O4--	0.1000	0.1023	0.6405E-01	0.6553E-01	0.2234	6.8937
266 HC4H4O4-			0.2140E-05	0.2190E-05	0.6899	10.8837
267 H2C4H4O4			0.4102E-08	0.4197E-08	1.0000	13.4437
268 AlSuc +			0.7162E-13	0.7326E-13	0.6899	18.4462
269 AlSuc)2-			0.4585E-15	0.4690E-15	0.6899	20.6399

SPECIES	ANALYZED		CALCULATED		ACTIVITY	ACTIVITY	-LOG10
	PPM	MG/L	PPM	MG/L	COEFF.	ACTIVITY	
270 BaSUC			0.9318E-07	0.9532E-07		0.3811E-12	12.4190
271 CaSUC			0.3479E-02	0.3559E-02		0.2309E-07	7.6366
272 FeSUC			0.1942E-13	0.1987E-13		0.1171E-18	18.9315
273 FeSUC +			0.4911E-13	0.5024E-13		0.2042E-18	18.6898
274 KSUC -			0.3516E-03	0.3597E-03		0.1620E-08	8.7904
275 MgSUC			0.2449E-01	0.2505E-01		0.1808E-06	6.7428
276 MnSUC			0.8478E-11	0.8673E-11		0.5138E-16	16.2892
277 NaSUC -			0.1536E-01	0.1571E-01		0.7898E-07	7.1025
278 PbSUC			0.1184E-09	0.1211E-09		0.3796E-15	15.4207
279 SrSUC			0.4665E-04	0.4772E-04		0.2373E-09	9.6246
280 ZnSUC			0.7253E-07	0.7420E-07		0.4143E-12	12.3827
281 CaCl +			0.1773E+03	0.1814E+03		0.1633E-02	2.7871
282 CaCl2			0.3377E+01	0.3455E+01		0.3153E-04	4.5012
283 FeF ++			0.1510E-11	0.1543E-11		0.4350E-17	17.3615
284 SiF6 --			0.1180E-28	0.1207E-28		0.1791E-34	34.7469
285 CH4 Gas	0.1000	0.1023	0.1000E+00	0.1023E+00		0.0000E+00	0.0000
288 PbCO3			0.1796E-04	0.1837E-04		0.6966E-10	10.1570
289 PbOH +			0.3184E-04	0.3257E-04		0.9876E-10	10.0054
292 ZnHCO3 +			0.5376E-04	0.5499E-04		0.2958E-09	9.5290
293 ZnOH +			0.2323E-03	0.2377E-03		0.1961E-08	8.7074
294 Zn(OH)2			0.1037E-04	0.1061E-04		0.1082E-09	9.9658

SAMPLE IDENT - Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C TEMPERATURE = 25.00

MOLE RATIOS (USING ANALYTICAL MOLALITY)

CL/CA	CL/MG	CL/NA	CL/K	CL/AL	CL/FE	CL/SO4	CL/HCO3	CA/MG	SQRT(CA)/NA
0.5306E+02	0.1027E+02	0.1165E+01	0.5347E+02	0.7363E+07	0.1524E+08	0.1933E+02	0.2699E+03	0.1936E+00	0.2127E+00
NH3/NA	LI/NA	K/NA	MG/CA	SR/CA	BA/CA	SO4/CL	HCO3/CL	F/CL	B/CL
0.3760E-05	0.5568E-04	0.2179E-01	0.5166E+01	0.9031E-02	0.1416E-04	0.5173E-01	0.3705E-02	0.1341E-03	0.7542E-03

LOG OF ACTIVITY RATIOS

CA/H2	MG/H2	NA/H	K/H	AL/H3	FE/H2	CA/MG	NA/K
0.1366E+02	0.1450E+02	0.7691E+01	0.6003E+01	0.7747E+01	0.2162E+01	-0.8438E+00	0.1688E+01

$$\text{LOG}(\text{NA/K}) + 1/3(\text{LOG}(\text{SQRT}(\text{CA})/\text{NA})) = 0.144E+01$$

$$\text{LOG}(\text{NA/K}) + 4/3(\text{LOG}(\text{SQRT}(\text{CA})/\text{NA})) = 0.765E+00$$

CHEMICAL GEOTHERMOMETER TEMPERATURES (IN DEGREES CENTIGRADE)
 ("999.0" INDICATES THAT A VALUE GREATER THAN 0.0 WAS NOT CALCULATED)

TEMPERATURE	AND/OR ACTIVITY CORRECTION	TEMP. WITH PRESSURE
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14.0 : QUARTZ (CONDUCTIVE)	:	15.2	A. IF THE WATER IS BOILING OR STEAM IS LOST DURING THE SAMPLING OF GROUNDWATERS THEN USE THE QUARTZ ADIABATIC TEMPERATURE.
24.2 : QUARTZ (ADIABATIC)	:	25.3	B. IF THERE IS NO STEAM LOSS THEN USE THE QUARTZ CONDUCTIVE TEMPERATURE.
999.0 : CHALCEDONY WITH SiO2	:	999.0	C. The Amorphous Silica Temperature should be Considered when the Sample is Saturated with Amorphous Silica (THE DELTA G OF MINERAL NO. 275 IS POSITIVE).
999.0 : ALFA CRISTOBALITE WITH SiO2	:	999.0	D. IF THE IN SITU TEMPERATURE EXCEEDS 150 DEGREES THEN THE NA/K TEMPERATURE MAY BE USED.
999.0 : Amorphous Silica With SiO2	:	999.0	E. ALTHOUGH THE 4/3 LOG TEMPERATURE IS GENERALLY USED WHEN THE TEMPERATURE IS LESS THAN 100 DEGREES IT IS CONSIDERED LESS RELIABLE THAN THE 1/3 LOG TEMPERATURE.
144.5 : LOG (NA/K)			F. THE ACTIVITIES OF H4SiO4 AND WATER WILL BE COMPUTED AT THE SURFACE TEMPERATURE ONLY IF THE HITEMP OPTION IS SELECTED.
174.7 : LOG (NA/K) + 1/3 LOG(SQRT(CA)/NA)			G. THE ORDER OF RELIABILITY OF THE CATION GEOTHERMOMETERS: MG-LI>MG-CORRECTED NA-K>NA-LI>OTHERS
274.9 : LOG (NA/K) + 4/3 LOG(SQRT(CA)/NA)			H. DETAILS OF THE EQUATIONS AND PARAMETERS CAN BE FOUND IN KHARAKA AND MARINER, 1988).
194.0 : LOG (NA/K) + 4/3 LOG(SQRT(CA)/NA) + 1.36+0.253*LOG(PCO2)			
999.0 : MG CORRECTED 1/3 (NA-K-CA)			
10.2 : LOG (SQRT(MG)/LI)			
13.1 : LOG (NA/LI)			

SAMPLE IDENT - Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C

(TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
1 ADULARIA	1.344	1.260	0.084	0.115	82 NATRTRHM	-6.156	-0.010	-6.146	-8.385
2 AKERMANI	33.530	45.460	-11.930	-16.276	83 NATRON	-6.231	-0.880	-5.351	-7.301
3 ALBITE	3.032	2.500	0.532	0.726	84 NEPHALIN	11.292	13.520	-2.228	-3.040
4 ALBITE L	3.032	3.110	-0.078	-0.106	85 NESQUHON	-7.054	-5.350	-1.704	-2.325
5 ALBITE H	3.032	4.430	-1.398	-1.907	86 NONT, Na	1.506	-11.480	12.986	17.716
6 ALUNITE	-8.924	-2.790	-6.134	-8.369	87 NONT, K	0.949	-11.810	12.759	17.407
7 AMESITE	40.308	38.630	1.678	2.289	88 NONT, H	-1.032	-12.500	11.468	15.645
8 ANALCIME	7.154	6.050	1.104	1.506	89 NONT, Ca	1.222	-11.540	12.762	17.410
9 ANDALUSI	11.340	16.570	-5.230	-7.135	90 NONT, Mg	1.222	-11.560	12.782	17.437
10 ANDESITE	10.163	12.730	-2.567	-3.502	92 OLIGOCLA	6.597	8.730	-2.133	-2.909
11 ANHYDRIT	-5.403	-4.330	-1.073	-1.464	93 PARAGONI	18.493	14.390	4.103	5.598
12 ANNITE	7.797	29.140	-21.343	-29.117	94 PARAGASI	91.371	100.790	-9.419	-12.850
13 ANORTHIT	20.859	25.830	-4.971	-6.782	95 PERICLAS	14.492	21.510	-7.018	-9.574
14 APATCHLR	-49.451	-66.150	16.699	22.781	96 PHILLIPS	2.180	3.300	-1.120	-1.528
15 APATFLUR	-53.552	-68.340	14.788	20.174	97 PHLOGPIT	44.813	37.220	7.593	10.359
16 APATHYDX	-54.785	-60.390	5.605	7.646	98 PHLOGPTF	19.299	16.730	2.569	3.505
17 ARAGONIT	-7.873	-8.340	0.467	0.637	99 PORTLAN	-14.340	-5.420	-8.920	-12.169
18 AUGITE	24.989	32.560	-7.571	-10.329	100 POTASSI	11.998	84.120	-72.122	-98.391
19 AZURITE	-48.361	-39.460	-8.901	-12.144	101 PREHNITE	30.369	32.020	-1.651	-2.253
20 BARITE	-10.205	-9.960	-0.245	-0.334	102 PYROPHYL	-1.058	-0.100	-0.958	-1.308
21 BOEHMITE	7.731	6.950	0.781	1.065	103 QUARTZ	-4.130	-3.930	-0.200	-0.273
22 BRUCITE	-13.496	-11.470	-2.026	-2.764	104 SANIDINE	1.344	1.180	0.164	0.224
23 BYTOWNIT	17.293	18.600	-1.307	-1.783	105 SAPO, Na	33.401	26.880	6.521	8.897
24 CALCITE	-7.873	-8.480	0.607	0.828	106 SAPO, K	32.844	26.550	6.294	8.587
25 CELESTIT	-7.391	-6.430	-0.961	-1.311	107 SAPO, H	30.863	25.850	5.013	6.839
26 CHALCEDO	-4.130	-3.730	-0.400	-0.546	108 SAPO, Ca	33.117	26.820	6.297	8.590
27 CHAM, 7A	15.631	29.030	-13.399	-18.280	109 SAPO, Mg	33.256	26.800	6.456	8.807
28 CHLOR, 7	75.509	71.940	3.569	4.868	110 SEPIOLIT	33.131	31.520	1.611	2.198
29 CHLOR, 1	75.509	68.570	6.939	9.466	111 SILICAAM	-4.130	-2.700	-1.430	-1.951
30 CRYSOITIL	35.201	32.030	3.171	4.326	112 SILICGEL	-4.130	-2.710	-1.420	-1.937
31 C-ENSTAT	10.362	11.290	-0.928	-1.265	113 SILLIMAN	11.340	15.730	-4.390	-5.989
32 C-PTIL, N	-10.523	-7.900	-2.623	-3.578	114 SNEC Ca	5.104	6.140	-1.036	-1.414
33 C-PTIL, K	-13.899	-15.000	1.101	1.502	115 SNEC K	4.837	5.860	-1.023	-1.396
34 C-PTIL, C	-12.248	-9.300	-2.948	-4.022	116 SNEC Mg	5.244	6.040	-0.796	-1.085
35 C-PTIL, M	-11.404	-5.000	-6.404	-8.737	117 SNEC Na	5.394	6.120	-0.726	-0.991
36 CORUNDUM	15.470	21.400	-5.930	-8.090	118 Na2O	15.374	67.430	-52.056	-71.017
37 CRISTOBA	-4.130	-3.540	-0.590	-0.805	119 SPINEL	29.962	36.460	-6.498	-8.864
38 CRISTOBB	-4.130	-2.940	-1.190	-1.623	120 STILBITE	0.150	1.410	-1.260	-1.719
39 DICKITE	7.193	6.170	1.023	1.396	121 STRENGIT	-30.570	-27.200	-3.370	-4.598
40 DIOPSIDE	19.881	19.630	0.251	0.343	122 STC03	-9.861	-9.270	-0.591	-0.806
41 DOLOMITE	-14.902	-18.060	3.158	4.308	123 SYLVITE	-2.661	0.910	-3.571	-4.872
42 DSORD	-14.902	-16.520	1.618	2.207	124 TALC	26.949	21.130	5.819	7.939
43 ENSTATIT	10.362	11.470	-1.108	-1.511	125 THENARDI	-3.677	-0.290	-3.387	-4.621
44 EPIDOTE	36.164	31.990	4.174	5.695	126 TREMOLIT	66.711	60.890	5.821	7.942
45 FAYALITE	0.178	19.430	-19.252	-26.265	127 TRONA	-9.673	-0.630	-9.043	-12.337
46 FLUORITE	-11.874	-10.960	-0.914	-1.246	128 VIVIANIT	-66.295	-36.000	-30.295	-41.330
47 FORSTERI	24.855	29.070	-4.215	-5.750	129 WAIRAKIT	12.582	17.330	-4.748	-6.478
48 GIBBS AM	-34.248	-34.420	0.172	0.235	130 WITHERIT	-12.675	-8.630	-4.045	-5.519
49 GIBBSITE	-34.248	-34.920	0.672	0.917	131 WOLLASTO	9.519	12.600	-3.081	-4.204
50 GREENALI	-1.815	22.580	-24.395	-33.281	132 ZOISITE	38.108	42.100	-3.992	-5.446
51 GYPSUM	-5.420	-4.600	-0.820	-1.118	133 SILVER	-9.663	-0.500	-9.163	-12.501

SAMPLE IDENT - Test Sample #1 for SOLMINEQ.88 - Modified Seawater at 25 C (TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
52 HALITE	-0.973	1.590	-2.563	-3.496	134 AGCL	-14.686	-9.730	-4.956	-6.761
53 HALLOYSI	7.193	8.910	-1.717	-2.342	136 COPPER	-10.071	4.250	-14.321	-19.537
54 HEULANDI	0.158	1.410	-1.252	-1.707	137 MALLACHIT	-34.397	-33.580	-0.817	-1.114
55 HUNTITE	-28.960	-30.620	1.660	2.264	138 CUO	7.557	7.670	-0.113	-0.155
56 HYDRMAGN	-36.508	-38.530	2.022	2.759	139 CU2O	-12.867	-1.900	-10.967	-14.962
57 HYPRILIT	-3.671	11.800	-15.471	-21.106	144 FeCl2	-15.166	7.900	-23.066	-31.468
58 ILLITE	10.550	10.340	0.210	0.286	145 FeCl3	-20.189	12.340	-32.529	-44.377
59 KAOLINIT	7.193	6.230	0.963	1.314	146 FeCO3	-19.368	-10.540	-8.828	-12.043
60 KENYAITE	-37.785	-25.000	-12.785	-17.441	147 FeO	2.154	13.500	-11.346	-15.479
61 K-SPAR	1.344	-0.550	1.894	2.584	148 Fe2O3HEM	11.582	0.040	11.542	15.747
62 KYANITE	11.340	14.480	-3.140	-4.284	149 Fe2O3MGM	11.582	6.400	5.182	7.070
63 LABRADOR	15.368	16.250	-0.882	-1.203	150 Fe3O4	13.736	10.750	2.986	4.074
64 LARNITE	23.167	38.880	-15.713	-21.436	151 Fe(OH)3	-36.191	-37.200	1.009	1.376
65 LAUMONTI	12.565	14.170	-1.605	-2.189	152 GOETHITE	5.787	0.480	5.307	7.240
66 LEUCITE	5.474	6.520	-1.046	-1.427	157 Hg(L)	-14.978	-2.840	-12.138	-16.560
67 LIME	-19.151	32.660	-51.811	-70.683	158 HgCl2(C)	-25.023	-14.110	-10.913	-14.888
68 MAGADITE	-21.260	-14.340	-6.920	-9.441	160 HgO	-7.704	2.440	-10.144	-13.838
69 MgFe2O4	26.075	21.100	4.975	6.787	163 MnCl2	-12.494	8.790	-21.284	-29.036
70 MAGNESIT	-7.029	-8.050	1.021	1.393	164 MnCO3	-16.696	-10.540	-6.156	-8.398
71 MgCl2	-2.827	22.150	-24.977	-34.075	165 MnO	4.826	17.700	-12.874	-17.563
72 MARIALIT	8.123	1.710	6.413	8.749	166 MnO2	-13.339	-8.330	-5.009	-6.834
73 MERWINIT	47.179	68.170	-20.991	-28.637	168 PbCl2	-12.955	-4.820	-8.135	-11.098
74 MICROCLN	1.344	-0.550	1.894	2.584	169 PbCO3	-17.157	-12.890	-4.267	-5.821
75 MIEONITE	54.703	69.950	-15.247	-20.801	170 PbOLITHR	4.365	12.550	-8.185	-11.167
76 MIRABILIT	-3.761	-1.090	-2.671	-3.644	171 PbOMASIC	4.365	12.690	-8.325	-11.358
77 MONTICEL	24.011	30.150	-6.139	-8.375	173 PbSO4	-14.687	-7.800	-6.887	-9.395
78 MORD, Na	-5.253	-3.900	-1.353	-1.846	174 ZnCO3	-13.079	-9.870	-3.209	-4.378
79 MORD, K	-6.941	-7.600	0.659	0.899	175 ZnO	8.443	11.200	-2.757	-3.762
80 MUSCOVIT	16.805	12.880	3.925	5.355	177 ZnSO4	-10.609	3.540	-14.149	-19.302
81 NACHOLIT	-3.509	-0.430	-3.079	-4.200					

***** INPUT DATA ECHO *****

TITLE : Test Sample #2 - Mix caustic flood with formation water

TEMP	HITEMP	DENS	PRESS	Na	K	Li	Ca	Mg	Fe	Al
0.2500E+02	0.0000E+00	0.1000E+01	0.0000E+00	SiO2	Cl	SO4	H2S	HCO3	CO3	TIC
0.1092E+02	0.9000E+01	0.9000E+01	0.9000E+01	F	PO4	NO3	NH3	B	Sr	Ba
				Pb	Zn	Cu	Mn	Hg	Ag	
				As	U	V				
				Acetate	Oxalate	Succinate	CH4			
				ALK	ITIC					
				DCO2	DH2S	DNH3	DCH4			
				ICCSAT	IMCO3	FIXIT	FCCSAT			
				IC02M	TCH4M	TH2SM	WROIL	KCO2OL	KCH4OL	KH2SOL
				0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
				Adsorption/Exchange option (N=no) = N						
				ITMIX	ITMIX					
				2	0					
				Number of mixtures = 1	starting at fraction of solution one =	0.5000	using a step increment of:	0.0000		
				and reading the second water composition from						
				the data set following this one.						
				LOG KT TO BE CHANGED AT TEMP = 25.00						
				0 0.0000E+00	0 0.0000E+00					
				LOG KT TO BE CHANGED AT TEMP = 0.00						
				0 0.0000E+00	0 0.0000E+00					
				ANS1	ANS2					
				0	0					
				Number of Additional Minerals =	0					
				FLAG FOR ACTIVITY COEFF OF NEUTRAL SPECIES:	1					
				FLAG FOR ACTIVITY COEFF BY PITZERS EQUATIONS:	0					
				FLAGS FOR CALCULATING REDOX SPECIES:						
				Fe Cu Hg Mn U V						
				1 1 1 1 0 0						
				PRINTING OPTIONS:						
				INFORM	RATIO	GEOTH	IPRIN1	IPRIN2		
				0	0	0	0	0		
				TOLERANCE FACTORS:	CONV1 =	0.5000E-04	CONV2 =	0.5000E-04		

SAMPLE IDENT:- Test Sample #2 - Mix caustic flood with formation water

[illegible]

SAMPLE IDENT - Test Sample #2 - Mix caustic flood with formation water (TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
52 HALITE	-3.334	1.590	-4.924	-6.717	83 NATRON	-5.281	-0.880	-4.401	-6.004
81 NACHOLIT	-4.328	-0.430	-3.898	-5.318	118 Na2O	18.766	67.430	-48.664	-66.390
82 NATRHRM	-5.276	-0.010	-5.266	-7.184	127 TRONA	-9.605	-0.630	-8.975	-12.244

*****This solution is to be mixed with the next solution.....

***** INPUT DATA ECHO *****

```

TITLE : McMurray Formation Water
TEMP      HI TEMP      DENS      PRESS
0.2500E+02 0.0000E+00 0.1000E+01 0.0000E+00
PH         EHM         EHM         EMFZSC
0.7100E+01 0.9000E+01 0.9000E+01 0.9000E+01
CONCENTRATION UNITS : MG/L
Na K Li Ca Mg Fe Al
0.1572E+05 0.0000E+00 0.0000E+00 0.8010E+03 0.4430E+03 0.0000E+00 0.0000E+00
SiO2 Cl SO4 H2S HCO3 CO3 TIC
0.0000E+00 0.2670E+05 0.1200E+02 0.0000E+00 0.4000E+03 0.0000E+00 0.0000E+00
F PO4 NO3 NH3 B Sr Ba
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
Pb Zn Cu Mn Hg Ag
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
As U V
0.0000E+00 0.0000E+00 0.0000E+00
Acetate Oxalate Succinate CH4
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
ALK ITIC
2 0
DCO2 DH2S DNH3 DCH4
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
ICCSAT INCO3 FIXIT FCCSAT
0 0 0.0000E+00 0.0500
TCO2M TCH4M TH2SM WROIL
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
Adsorption/Exchange option (N=no) = N
IBMIX ITMIX
2 0
Because the Mixing option was chosen in the previous data set,
the MIXING information will not be read from this data set.
LOG KT TO BE CHANGED AT TEMP = 25.00
0 0.0000E+00 0 0.0000E+00 0 0.0000E+00 0 0.0000E+00
LOG KT TO BE CHANGED AT TEMP = 0.00
0 0.0000E+00 0 0.0000E+00 0 0.0000E+00 0 0.0000E+00
ANS1 ANS2
0 0
Number of Additional Minerals = 0
FLAG FOR ACTIVITY COEFF OF NEUTRAL SPECIES: 1
FLAG FOR ACTIVITY COEFF BY PITZERS EQUATIONS: 0
FLAGS FOR CALCULATING REDOX SPECIES:
Fe Cu Hg Mn U V
1 1 1 1 0 0
PRINTING OPTIONS:
INFORM RATIO GEOTH IPRIN1 IPRIN2
0 0 0 0
TOLERANCE FACTORS: CONV1 = 0.5000E-04 CONV2 = 0.5000E-04

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SAMPLE IDENT - McMurray Formation Water

(TEMPERATURE = 25.00)

	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
11	ANHYDRIT	-7.559	-4.330	-3.229	-4.405	70	MAGNESIT	-8.027	-8.050	0.032
17	ARAGONIT	-8.176	-8.340	0.164	0.224	71	MgCl2	-2.988	22.150	-34.295
22	BRUCITE	-16.124	-11.470	-4.654	-6.349	76	MIRABILIT	-5.886	-1.090	-6.542
24	CALCITE	-8.176	-8.480	0.304	0.415	81	NACHOLIT	-2.817	-0.430	-3.257
41	DOLOMITE	-16.203	-18.060	1.857	2.534	82	NATRTHRM	-6.400	-0.010	-8.718
42	DSORD	-16.203	-16.520	0.317	0.433	83	NATRON	-6.502	-0.880	-7.670
51	GYPSUM	-7.582	-4.600	-2.982	-4.068	85	NESQUHON	-8.061	-5.350	-3.698
52	HALITE	-0.675	1.590	-2.265	-3.090	95	PERICLAS	11.868	21.510	-13.154
55	HUNTITE	-32.256	-30.620	-1.636	-2.232	99	PORTLAN	-16.273	-5.420	-14.806
56	HYDRMAGN	-42.559	-38.530	-4.029	-5.496	118	Na2O	13.505	67.430	-73.566
57	HYPHILIT	-3.137	11.800	-14.937	-20.378	125	THENARDI	-5.772	-0.290	-7.479
67	LIME	-16.681	32.660	-49.341	-67.313	127	TRONA	-9.229	-0.630	-11.731

**** Mixing of the two previous solutions in the following proportions:
Initial fraction of solution 1 = 0.5000
Number of mixtures = 1
and the increment between solutions = 0.5000

SAMPLE IDENT:- MIXTURE OF Test Sample #2 - Mix caustic flo AND McMurray Formation Water
(PROPORTIONS: 1= 0.50 2= 0.50)

PH	EH	TEMP	CATIONS	ANIONS	DIFFERENCE (MEQ/L)	HTOT	OH BALANCE (MOLES)	DIFFERENCE
9.67	9.0000	25.00	ANAL= 407.6953 CALC= 386.6610	407.5557 395.5575	0.1396 -8.8965	0.4307E-02	0.1313E-03	0.4176E-02
DENSITY AT INPUT T	TOTAL DISSOLVED SOLIDS (MG/L)	IONIC STRENGTH	ACTIVITY OF WATER	P TOTAL (BARS)	PH2O (BARS)	PCO2 (BARS)	PH2S (BARS)	PNH3 (BARS)
1.0000	23897.61	0.41785	0.9865	1.0000	0.3169E-01	0.4037E-04	0.0000E+00	0.0000E+00
Dissolved Inorganic Carbon								
as								
TIC Alkalinity species HCO3- CO3=								
(MG/L)=0.1354E+04 0.6659E+03 0.1111E+04								
(PPM)=0.1354E+04 0.6659E+03 0.1111E+04								
(MOLALITY)=0.2274E-01 0.1137E-01 0.1137E-01								
ANALYZED								
SPECIES	PPM	MG/L	MOLALITY	PPM	MG/L	MOLALITY	ACTIVITY	-LOG10 ACTIVITY
1 Ca ++	408.9541	408.9541	0.1045E-01	0.2642E+03	0.2642E+03	0.6752E-02	0.1845E-02	0.2732
2 Mg ++	226.1756	226.1756	0.9531E-02	0.1913E+03	0.1913E+03	0.8060E-02	0.2337E-02	0.2900
3 Na +	8476.0056	8476.0056	0.3777E+00	0.8178E+04	0.8178E+04	0.3644E+00	0.2513E+00	0.6896
5 Cl -	13978.8458	13978.8458	0.4039E+00	0.1360E+05	0.1360E+05	0.3930E+00	0.2569E+00	0.6538
6 SO4 --	6.1267	6.1267	0.6534E-04	0.3562E+01	0.3562E+01	0.3799E-04	0.7633E-05	0.2009
7 HCO3 -	801.5070	801.5070	0.1346E-01	0.2229E+03	0.2229E+03	0.3742E-02	0.2639E-02	0.7052
8 H +				0.2598E-06	0.2598E-06	0.2640E-09	0.2115E-09	0.8012
9 OH -				0.1178E+01	0.1178E+01	0.7096E-04	0.4772E-04	0.6726
55 CaCO3				0.1745E+03	0.1745E+03	0.1787E-02	0.1787E-02	1.0000
56 CaHCO3 +				0.8310E+01	0.8310E+01	0.8422E-04	0.6271E-04	0.7447
57 CaOH +				0.9093E-01	0.9093E-01	0.1632E-05	0.1215E-05	0.7447
61 CaSO4				0.3733E+00	0.3733E+00	0.2809E-05	0.2809E-05	1.0000
97 H2CO3				0.7566E-01	0.7566E-01	0.1250E-05	0.1250E-05	1.0000
98 CO3 --				0.1355E+03	0.1355E+03	0.2313E-02	0.5836E-03	0.2523
103 HS04 -				0.1933E-07	0.1933E-07	0.2040E-12	0.1439E-12	0.7052
120 MgCO3				0.1072E+03	0.1072E+03	0.1303E-02	0.1303E-02	1.0000
121 MgHCO3 +				0.8752E+01	0.8752E+01	0.1051E-03	0.7246E-04	0.6896
123 MgOH +				0.2369E+01	0.2369E+01	0.5874E-04	0.4440E-04	0.7558
124 MgSO4				0.5265E+00	0.5265E+00	0.4481E-05	0.4481E-05	1.0000
137 NaCl				0.5203E+03	0.5203E+03	0.9121E-02	0.9121E-02	1.0000
138 NaCO3 -				0.3031E+03	0.3031E+03	0.3741E-02	0.2731E-02	0.7300
139 NaHCO3				0.3059E+02	0.3059E+02	0.3730E-03	0.3730E-03	1.0000
140 Na2CO3				0.7968E+00	0.7968E+00	0.7702E-05	0.7702E-05	1.0000
141 Na2SO4				0.2163E+01	0.2163E+01	0.1560E-04	0.1560E-04	1.0000
142 NaSO4 -				0.5186E+00	0.5186E+00	0.4462E-05	0.3258E-05	0.7300
281 CaCl +				0.1333E+03	0.1333E+03	0.1808E-02	0.1247E-02	0.6896
282 CaCl2				0.1951E+01	0.1951E+01	0.1801E-04	0.1801E-04	1.0000

SAMPLE IDENT - MIXTURE OF Test Sample #2 - Mix caustic flo AND McMurray Formation Water
(PROPORTIONS: 1= 0.50 2= 0.50) (TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
11 ANHYDRIT	-7.951	-4.330	-3.521	-4.804	70 MAGNESIT	-5.865	-8.050	2.185	2.981
17 ARAGONIT	-5.968	-8.340	2.372	3.236	71 MgCl2	-3.812	22.150	-25.962	-35.418
22 BRUCITE	-11.274	-11.470	0.196	0.268	76 MIRABILIT	-6.376	-1.090	-5.286	-7.211
24 CALCITE	-5.968	-8.480	2.512	3.427	81 NACHOLIT	-3.178	-0.430	-2.748	-3.749
41 DOLOMIT	-11.833	-18.060	6.227	8.495	82 NATRTHRM	-4.439	-0.010	-4.429	-6.043
42 DSORD	-11.833	-16.520	4.687	6.394	83 NATRON	-4.493	-0.880	-3.613	-4.928
51 GYPSUM	-7.863	-4.600	-3.263	-4.452	85 NESQUHON	-5.883	-5.350	-0.533	-0.727
52 HALITE	-1.190	1.590	-2.780	-3.793	95 PERICLAS	16.712	21.510	-4.798	-6.546
55 HUNTITE	-23.564	-30.620	7.056	9.627	99 PORTLAN	-11.377	-5.420	-5.957	-8.126
56 HYDRMAGN	-31.519	-38.530	7.011	9.565	118 Na2O	18.144	67.430	-49.286	-67.238
57 HYPHILIT	-3.914	11.800	-15.714	-21.438	125 THENARDI	-6.317	-0.290	-6.027	-8.222
67 LIME	-22.089	32.660	-54.749	-74.691	127 TRONA	-7.624	-0.630	-6.994	-9.541

***** INPUT DATA ECHO *****

TITLE : Test Sample #3 - Dissolve Anorthite to saturate with Gibbsite in seawater

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TEMP      HITEMP      DENS      PRESS
0.2500E+02 0.0000E+00 0.1023E+01 0.0000E+00
PH        EHM        EHM        EMFZSC
0.8200E+01 0.5000E+00 0.9000E+01 0.9000E+01
CONCENTRATION UNITS : PPM
Na        K        Li        Ca        Mg        Fe        Al
0.1077E+05 0.3991E+03 0.1810E+00 0.4123E+03 0.1292E+04 0.2000E-02 0.2000E-02
SiO2      Cl        SO4      H2S      HCO3      CO3      TIC
0.4280E+01 0.1935E+05 0.2712E+04 0.0000E+00 0.1234E+03 0.0000E+00 0.0000E+00
F         PO4      NO3      NH3      B         Sr        Ba
0.1390E+01 0.6000E-01 0.2900E+00 0.3000E-01 0.4450E+01 0.8140E+01 0.2000E-01
Pb        Zn        Cu        Mn        Hg        Ag
0.5000E-04 0.4900E-02 0.7000E-03 0.2000E-03 0.3000E-04 0.4000E-04
As        U        V
0.4000E-02 0.0000E+00 0.0000E+00
Acetate   Oxalate   Succinate   CH4
0.1000E+00 0.1000E+00 0.1000E+00 0.1000E+00
ALK        ITIC
2          0
DCO2      DH2S      DNH3      DCH4
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
ICCSAT    IMCO3      FIXIT    FCCSAT
0          0          0.0000E+00 0.0500
TCO2M     TCH4M     TH2SM     WROIL    KC02OL    KCH4OL    KH2SOL    DSEP
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
Adsorption/Exchange option (N=no) = N
IBMX      ITMIX
1          0
MINERAL TO BE DISSOLVED/PRECIPITATED TO SATURATION: GIBBSITE      Index number: 49
MINERAL TO BE DISSOLVED/PRECIPITATED: ANORTHIT      Index number: 13
LOG KT TO BE CHANGED AT TEMP = 25.00      0 0.0000E+00      0 0.0000E+00      0 0.0000E+00
0 0.0000E+00      0 0.0000E+00      0 0.0000E+00
LOG KT TO BE CHANGED AT TEMP = 0.00      0 0.0000E+00      0 0.0000E+00      0 0.0000E+00
0 0.0000E+00      0 0.0000E+00
ANS1      ANS2
0          0
Number of Additional Minerals = 0
FLAG FOR ACTIVITY COEFF OF NEUTRAL SPECIES: 1
FLAG FOR ACTIVITY COEFF BY PITZERS EQUATIONS: 0
FLAGS FOR CALCULATING REDOX SPECIES:
Fe Cu Hg Mn U V
1 1 1 1 0 0
PRINTING OPTIONS:
INFORM      RATIO      GEOTH      IPRIN1      IPRIN2
0          0          0          0          0
TOLERANCE FACTORS: CONV1 = 0.5000E-04 CONV2 = 0.5000E-04

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(See pages 2-10 of Test Sample #1)

Total moles of ANORTHIT PPT/DISS . . . to achieve saturation: -.3076E-07

SAMPLE IDENT:- Test Sample #3 - Dissolve Anorthite to saturate with Gibbsite in seawater
ANORTHIT PPT/DISS

PH	EH	TEMP	CATIONS	ANIONS	DIFFERENCE (MEQ/L)	HTOT	OH BALANCE (MOLES)	DIFFERENCE
8.20	9.0000	25.00	ANAL= 619.6745	618.2648	1.4097	0.2198E-02	0.1350E-02	0.8477E-03
			CALC= 577.6363	569.7726	7.8638			
-----PRESSURE-----								
DENSITY AT	TOTAL DISSOLVED	IONIC	ACTIVITY	P TOTAL	PH2O	PCO2	PH2S	PCH4
INPUT T	SOLIDS (MG/L)	STRENGTH	OF WATER	(BARS)	(BARS)	(BARS)	(BARS)	(BARS)
1.0230	35906.27	0.64945	0.9809	1.0000	0.3169E-01	0.4780E-03	0.0000E+00	0.5252E-02
-----CALCULATED-----								
Dissolved Inorganic Carbon								
as								
TIC								
0.2485E+02								
0.2429E+02								
0.2096E-02								
-----ANALYZED-----								
Total Alkalinity as								
CO3=								
(MG/L)=0.1423E+03								
(PPM)=0.1391E+03								
(MOLALITY)=0.2363E-02								
-----ANALYZED-----								
SPECIES	PPM	MG/L	MOLALITY	PPM	MG/L	MOLALITY	ACTIVITY	ACTIVITY
1 Ca ++	412.2988	421.7817	0.1066E-01	0.2844E+03	0.2909E+03	0.7353E-02	0.1807E-02	0.2458
2 Mg ++	1292.0001	1321.7160	0.5508E-01	0.1121E+04	0.1147E+04	0.4779E-01	0.1261E-01	0.2640
3 Na +	10770.0007	11017.7102	0.4855E+00	0.1024E+05	0.1048E+05	0.4618E+00	0.3099E+00	0.6710
4 K +	399.1000	408.2793	0.1058E-01	0.3825E+03	0.3913E+03	0.1014E-01	0.6357E-02	0.6269
5 Cl -	19350.0013	19795.0504	0.5656E+00	0.1874E+05	0.1917E+05	0.5478E+00	0.3434E+00	0.5269
6 SO4 --	2712.0002	2774.3761	0.2926E-01	0.1203E+04	0.1231E+04	0.1298E-01	0.2189E-02	0.1687
7 HCO3 -	123.4007	126.2389	0.2096E-02	0.8534E+02	0.8730E+02	0.1449E-02	0.1000E-02	0.3699
8 H +				0.7635E-05	0.7810E-05	0.7850E-08	0.6307E-08	0.8034
9 OH -				0.4017E-01	0.4110E-01	0.2448E-05	0.1592E-05	0.6501
11 H4SiO4				0.6610E+01	0.6762E+01	0.7127E-04	0.7127E-04	1.0000
12 SiO2	4.2764	4.3748	0.7376E-04	0.1039E-08	0.1063E-08	0.9982E-14	0.6000E-14	0.6011
13 Ag +	0.0000	0.0000	0.3843E-09	0.8504E-12	0.8699E-12	0.3266E-16	0.2790E-17	0.0854
14 Al +3	0.0004	0.0004	0.1529E-07	0.1815E-01	0.1857E-01	0.1370E-06	0.2849E-07	0.2080
15 Ba ++	0.0200	0.0205	0.1509E-06	0.2749E-07	0.2812E-07	0.4483E-12	0.2695E-12	0.6011
16 Cu +	0.0007	0.0007	0.1142E-07	0.1667E-02	0.1705E-02	0.3094E-07	0.7604E-08	0.2458
18 Fe ++	0.0020	0.0020	0.3711E-07	0.1667E-02	0.1705E-02	0.3094E-07	0.7604E-08	0.2458
21 Hg ++	0.0000	0.0000	0.1550E-09	0.7474E-18	0.7646E-18	0.3861E-23	0.8033E-24	0.2080
22 Li +	0.1810	0.1852	0.2703E-04	0.1792E+00	0.1833E+00	0.2677E-04	0.1973E-04	0.7373
23 Mn ++	0.0002	0.0002	0.3773E-08	0.5864E-06	0.5999E-06	0.1106E-10	0.2719E-11	0.2458
25 Pb ++	0.0001	0.0001	0.2501E-09	0.9962E-06	0.1019E-05	0.4983E-11	0.9393E-12	0.1885
26 Sr ++	8.1400	8.3272	0.9628E-04	0.7551E+01	0.7725E+01	0.8931E-04	0.1858E-04	0.2080
27 Zn ++	0.0049	0.0050	0.7768E-07	0.2885E-02	0.2952E-02	0.4575E-07	0.1124E-07	0.2458
28 H2AsO3-	0.0067	0.0068	0.5281E-07	0.7212E-03	0.7378E-03	0.5708E-08	0.3830E-08	0.6710
29 PO4 -3	0.0600	0.0614	0.6548E-06	0.5921E-05	0.6058E-05	0.6462E-10	0.1749E-11	0.0271
30 F -	1.3900	1.4220	0.7583E-04	0.7672E+00	0.7848E+00	0.4185E-04	0.2721E-04	0.6501
31 B(OH)3	25.4540	26.0394	0.4266E-03	0.2205E+02	0.2255E+02	0.3695E-03	0.3695E-03	1.0000
32 NH3	0.0300	0.0307	0.1826E-05					
34 AlF ++				0.1407E-09	0.1440E-09	0.3172E-14	0.7085E-15	0.2234
35 AlF2 +				0.6684E-09	0.6838E-09	0.1066E-13	0.7674E-14	0.7198
36 AlF3				0.2034E-09	0.2081E-09	0.2510E-14	0.2510E-14	1.0000
37 AlF4 -				0.2415E-11	0.2470E-11	0.2430E-16	0.1677E-16	0.6899
38 Al(OH)++				0.9253E-09	0.9466E-09	0.2180E-13	0.4869E-14	0.2234
39 Al(OH)2+				0.6635E-06	0.6787E-06	0.1127E-10	0.8115E-11	0.7198
40 Al(OH)4-				0.1401E-02	0.1433E-02	0.1528E-07	0.1054E-07	0.6899

SPECIES	ANALYZED		CALCULATED		ACTIVITY	ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L			
41 ALS04 +	0.1000	0.1023	0.1051E-11	0.1075E-11	0.6107E-17	0.6899	17.2142
42 ALS04)2-			0.3179E-12	0.3252E-12	0.1504E-17	0.6899	17.9840
43 AgCl			0.5954E-06	0.6091E-06	0.4305E-11	1.0000	11.3660
44 AgCl2 -			0.3801E-04	0.3889E-04	0.2204E-09	0.6710	9.8301
45 AgCl3 --			0.3041E-04	0.3111E-04	0.1471E-09	0.2080	10.5143
46 AgCl4 -3			0.4054E-05	0.4148E-05	0.1683E-10	0.0394	12.1784
47 AgSO4 -			0.7863E-10	0.8044E-10	0.3996E-15	0.6710	15.5717
48 CH3COO -	0.1000	0.1755E-05	0.7225E-01	0.7391E-01	0.1268E-05	0.6899	6.0580
49 H3AsO3			0.5724E-02	0.5856E-02	0.4710E-07	1.0000	7.3270
51 BaCO3			0.1272E-04	0.1302E-04	0.6681E-10	1.0000	10.1751
52 BaHCO3 +			0.2238E-03	0.2290E-03	0.1169E-08	0.6710	9.1053
53 BaOH +			0.2236E-07	0.3310E-07	0.2173E-12	0.7071	12.8135
54 BaSO4			0.2867E-02	0.2933E-02	0.1273E-07	1.0000	7.8951
55 CaCO3			0.2148E+01	0.2198E+01	0.2225E-04	1.0000	4.6528
56 CaHCO3 +			0.3081E+01	0.3152E+01	0.3158E-04	0.7373	4.6330
57 CaOH +			0.2967E-02	0.3035E-02	0.5386E-07	0.7373	7.4011
58 CaPO4 -			0.1689E-02	0.1728E-02	0.1296E-07	0.7198	8.0301
59 CaHPO4			0.2333E-02	0.2386E-02	0.1777E-07	1.0000	7.7503
60 CaH2PO4+			0.2206E-04	0.2257E-04	0.1668E-09	0.7198	9.9205
61 CaSO4			0.1037E+03	0.1061E+03	0.7893E-03	1.0000	3.1028
62 CuCl			0.4431E-05	0.4533E-05	0.4639E-10	1.0000	10.3336
63 CuCl2 -			0.5353E-03	0.5476E-03	0.4126E-08	0.6710	8.5577
64 CuCl3 --			0.1188E-02	0.1215E-02	0.7244E-08	0.2080	8.8219
71 FeCl +			0.1012E-03	0.1035E-03	0.1149E-08	0.6710	9.1131
72 FeCl2			0.6764E-12	0.6920E-12	0.5531E-17	1.0000	17.2572
73 FeHPO4			0.1070E-06	0.1095E-06	0.7306E-12	1.0000	12.1363
74 H3PO4			0.2032E-09	0.2079E-09	0.2149E-14	1.0000	14.6678
75 FeOH +			0.3805E-04	0.3892E-04	0.5412E-09	0.7071	9.4171
76 Fe(OH)2			0.4100E-07	0.4194E-07	0.4728E-12	1.0000	12.3253
77 FeOOH -			0.5336E-07	0.5617E-07	0.4125E-12	0.7071	12.5351
78 FeSO4			0.6566E-03	0.6717E-03	0.4480E-08	1.0000	8.3488
89 B(OH)4 -			0.4344E+01	0.4444E+01	0.5710E-04	0.6065	4.4605
90 H2SiO4--			0.2150E-03	0.2199E-03	0.2368E-08	0.2234	9.2767
91 H3SiO4 -			0.2286E+00	0.2339E+00	0.2491E-05	0.6710	5.7769
92 HAsO3 --			0.1174E-07	0.1201E-07	0.9366E-13	0.2080	13.7104
96 HF			0.5013E-05	0.5129E-05	0.2597E-09	1.0000	9.5855
97 H2CO3			0.8450E+00	0.8644E+00	0.1412E-04	1.0000	4.8502
98 CO3 --			0.1923E+01	0.1967E+01	0.3320E-04	0.2234	5.1298
99 HPO4 --			0.1074E-01	0.1099E-01	0.1160E-06	0.2080	7.6174
100 H2PO4 -			0.3136E-03	0.3208E-03	0.3351E-08	0.7198	8.6176
103 HSO4 -			0.1670E-03	0.1709E-03	0.1783E-08	0.6899	8.9100
104 HNO3			0.4329E-10	0.4429E-10	0.7120E-15	1.0000	15.1475
105 HgCl +			0.1665E-12	0.1704E-12	0.7311E-18	0.6710	18.3093
106 HgCl2			0.4517E-06	0.4621E-06	0.1724E-11	1.0000	11.7634
107 HgCl3 -			0.3216E-04	0.3290E-04	0.1086E-09	0.6710	10.1376
108 HgCl4 --			0.1476E-04	0.1510E-04	0.4469E-10	0.2080	11.0317
109 HgSO4			0.1264E-19	0.1293E-19	0.4416E-25	1.0000	25.3550
113 KCl			0.2070E+02	0.2118E+02	0.2878E-03	1.0000	3.5409
114 KCO3 -			0.7990E-01	0.8174E-01	0.8355E-06	0.6629	6.2566
115 KHSO4			0.7274E-05	0.7441E-05	0.5536E-10	1.0000	10.2568
116 KSO4 -			0.1957E+02	0.2002E+02	0.1500E-03	0.7198	3.9666
117 KHP04 -			0.5416E-04	0.5541E-04	0.4155E-09	0.7198	9.5242
118 LiOH			0.1098E-05	0.1124E-05	0.4754E-10	1.0000	10.3230

SPECIES	ANALYZED			CALCULATED			ACTIVITY	COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	MOLALITY	PPM	MG/L	MOLALITY			
119 LiSO4 -				0.2650E-01	0.2711E-01	0.2666E-06	0.1885E-06	0.7071	6.7246
120 MgCO3				0.7268E+01	0.7436E+01	0.8933E-04	0.8933E-04	1.0000	4.0490
121 MgHCO3 +				0.1818E+02	0.1860E+02	0.2209E-03	0.1482E-03	0.6710	3.8292
122 MgF +				0.1373E+01	0.1405E+01	0.3286E-04	0.2267E-04	0.6899	4.6445
123 MgOH +				0.4245E+00	0.4343E+00	0.1065E-04	0.7992E-05	0.7505	5.0974
124 MgSO4				0.8054E+03	0.8240E+03	0.6934E-02	0.6934E-02	1.0000	2.1590
125 MgPO4 -				0.1041E-01	0.1065E-01	0.9045E-07	0.6511E-07	0.7198	7.1864
126 MgHPO4				0.4552E-01	0.4656E-01	0.3922E-06	0.3922E-06	1.0000	6.4065
127 MgH2PO4+				0.1363E-03	0.1394E-03	0.1164E-08	0.8380E-09	0.7198	9.0767
128 MnCl +				0.3839E-13	0.3927E-13	0.4401E-18	0.2953E-18	0.6710	18.5297
129 MnCl2				0.3094E-10	0.3165E-10	0.2548E-15	0.2548E-15	1.0000	15.5938
130 MnCl3 -				0.5098E-09	0.5215E-09	0.3276E-14	0.2198E-14	0.6710	14.6580
131 MnCl4 -				0.5472E-08	0.5598E-08	0.2882E-13	0.5996E-14	0.2080	14.2221
132 MnHCO3 +				0.8443E-08	0.8637E-08	0.7546E-13	0.5063E-13	0.6710	13.2956
133 MnSO4				0.1578E-06	0.1614E-06	0.1083E-11	0.1083E-11	1.0000	11.9654
134 MnHPO4				0.3633E-10	0.3717E-10	0.2495E-15	0.2495E-15	1.0000	15.6029
135 MnOH +				0.1233E-08	0.1262E-08	0.1776E-13	0.1192E-13	0.6710	13.9237
136 NO3 -	0.2900	0.2967	0.4847E-05	0.2900E+00	0.2967E+00	0.4847E-05	0.3039E-05	0.6269	5.5173
137 NaCl				0.8478E+03	0.8673E+03	0.1503E-01	0.1503E-01	1.0000	1.8229
138 NaCO3 -				0.4761E+01	0.4871E+01	0.5945E-04	0.4279E-04	0.7198	4.3686
139 NaHCO3				0.1413E+02	0.1445E+02	0.1743E-03	0.1743E-03	1.0000	3.7588
140 Na2CO3				0.1522E-01	0.1557E-01	0.1488E-06	0.1488E-06	1.0000	6.8274
141 Na2SO4				0.9321E+03	0.9536E+03	0.6801E-02	0.6801E-02	1.0000	2.1674
142 NaSO4 -				0.1838E+03	0.1880E+03	0.1600E-02	0.1152E-02	0.7198	2.9386
143 NaHPO4 -				0.2326E-02	0.2379E-02	0.2026E-07	0.1458E-07	0.7198	7.8362
144 NaF				0.4503E-01	0.4607E-01	0.1111E-05	0.1111E-05	1.0000	5.9541
146 NH4 +				0.3015E-01	0.3085E-01	0.1732E-05	0.1041E-05	0.6011	5.9824
147 NH4OH				0.3151E-02	0.3224E-02	0.9319E-07	0.9319E-07	1.0000	7.0306
148 PbCl +				0.2893E-05	0.2960E-05	0.1236E-10	0.8292E-11	0.6710	11.0813
149 PbCl2				0.2775E-05	0.2838E-05	0.1034E-10	0.1034E-10	1.0000	10.9855
150 PbCl3 -				0.7843E-06	0.8023E-06	0.2592E-11	0.1739E-11	0.6710	11.7596
151 PbCl4 -				0.6102E-06	0.6242E-06	0.1812E-11	0.3769E-12	0.2080	12.4238
152 PbSO4				0.3383E-06	0.3461E-06	0.1156E-11	0.1156E-11	1.0000	11.9370
154 SiOH -				0.2068E-04	0.2115E-04	0.2048E-09	0.1448E-09	0.7071	9.8392
155 SrCO3				0.1297E-01	0.1327E-01	0.9104E-07	0.9104E-07	1.0000	7.0408
156 SrHCO3 +				0.6151E-01	0.6292E-01	0.4289E-06	0.2878E-06	0.6710	6.5410
157 SrSO4				0.1142E+01	0.1169E+01	0.6445E-05	0.6445E-05	1.0000	5.1908
158 ZnCl +				0.1473E-02	0.1507E-02	0.1514E-07	0.1016E-07	0.6710	7.9932
159 ZnCl2				0.7271E-03	0.7438E-03	0.5529E-08	0.5529E-08	1.0000	8.2573
160 ZnCl3 -				0.2461E-03	0.2518E-03	0.1485E-08	0.9964E-09	0.6710	9.0015
161 ZnCl4 -				0.2276E-03	0.2328E-03	0.1138E-08	0.2368E-09	0.2080	9.6256
162 ZnSO4				0.6217E-03	0.6360E-03	0.3991E-08	0.3991E-08	1.0000	8.3989
163 AlF5 -				0.5912E-14	0.6048E-14	0.5023E-19	0.1045E-19	0.2080	19.9809
164 AlF6 -3				0.2964E-17	0.3032E-17	0.2179E-22	0.8586E-24	0.0394	24.0662
165 HgOH +				0.1154E-13	0.1180E-13	0.5495E-19	0.3687E-19	0.6710	19.4333
166 Hg(OH)2				0.3414E-08	0.3493E-08	0.1508E-13	0.1508E-13	1.0000	13.8215
228 CH3COOH				0.1840E-04	0.1882E-04	0.3175E-09	0.3175E-09	1.0000	9.4982
229 AlAce ++				0.7788E-15	0.7967E-15	0.9382E-20	0.1769E-20	0.1885	20.7524
230 BaAce +				0.9235E-07	0.9447E-07	0.4874E-12	0.3362E-12	0.6899	12.4734
231 CaAce +				0.3723E-02	0.3809E-02	0.3892E-07	0.2685E-07	0.6899	7.5710
232 CuAce +				0.3138E-11	0.3210E-11	0.2653E-16	0.1830E-16	0.6899	16.7375
233 FeAce +				0.2133E-06	0.2182E-06	0.1924E-11	0.1327E-11	0.6899	11.8770
234 Fe(Ace)2				0.1230E-13	0.1258E-13	0.7328E-19	0.7328E-19	1.0000	19.1350

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
235 KAc			0.2146E-03	0.2195E-03	1.0000	8.6448
236 MgAc +			0.2288E-01	0.2340E-01	0.6899	6.7072
237 NaAc			0.1264E-01	0.1293E-01	1.0000	6.7968
238 PbAc +			0.5568E-10	0.5696E-10	0.6899	15.8252
239 Pb(Ac)2			0.9851E-15	0.1008E-14	1.0000	20.5033
240 Pb(Ac)3			0.1775E-20	0.1815E-20	0.6899	26.4813
241 SrAc +			0.4820E-04	0.4930E-04	0.6899	9.6290
244 ZnAc +			0.1391E-03	0.1423E-03	0.6899	9.0971
245 Zn(Ac)2			0.3411E-13	0.3490E-13	1.0000	18.7151
246 C2O4 --	0.1000	0.1023	0.9439E-02	0.9656E-02	0.2234	7.6051
247 H2C2O4			0.3466E-09	0.3546E-09	0.6899	14.5553
248 H2C2O4			0.3114E-13	0.3186E-13	1.0000	18.4455
249 AlOxy +			0.1114E-13	0.1140E-13	0.6899	19.1595
250 AlOxy)2-			0.4882E-16	0.4994E-16	0.6899	21.7646
251 BaOxy			0.5714E-08	0.5845E-08	1.0000	13.5804
252 CaOxy			0.5546E-02	0.5673E-02	1.0000	7.3481
253 FeOxy			0.6582E-06	0.6734E-06	1.0000	11.3241
255 KOxy -			0.1002E+00	0.1025E+00	0.6899	9.1019
256 MgOxy			0.9311E-10	0.9525E-10	1.0000	15.1707
257 MnOxy			0.7180E-03	0.7345E-03	0.2234	9.0758
258 MnOxy)2			0.1550E-06	0.1585E-06	0.0021	14.8809
259 MnOxy)3			0.9487E-02	0.9705E-02	0.6899	7.2139
261 NaOxy -			0.3650E-09	0.3734E-09	1.0000	14.8923
262 PbOxy			0.2710E-04	0.2773E-04	1.0000	9.7961
263 SrOxy			0.3282E-05	0.3357E-05	1.0000	10.6542
265 ZnOxy	0.1000	0.1023	0.6405E-01	0.6553E-01	0.2234	6.8937
265 CaH4O4 --			0.2139E-05	0.2189E-05	0.6899	10.8839
266 H4C4H4O4-			0.4099E-08	0.4193E-08	1.0000	13.4441
267 H2C4H4O4			0.1423E-13	0.1456E-13	0.6899	19.1480
268 AlSuc +			0.9109E-16	0.9319E-16	0.6899	21.3417
269 AlSuc)2-			0.9318E-07	0.9532E-07	1.0000	12.4190
270 BaSuc			0.3479E-02	0.3559E-02	1.0000	7.6366
271 CaSuc			0.2554E-07	0.2613E-07	1.0000	12.8126
272 FeSuc			0.3516E-03	0.3597E-03	0.6899	8.7904
274 KSuc -			0.2449E-01	0.2505E-01	1.0000	6.7428
275 MgSuc			0.8478E-11	0.8673E-11	1.0000	16.2892
276 MnSuc			0.1536E-01	0.1571E-01	0.6899	7.1025
277 NaSuc -			0.1184E-09	0.1211E-09	1.0000	15.4209
278 PbSuc			0.4665E-04	0.4772E-04	1.0000	9.6246
279 SrSuc			0.7253E-07	0.7419E-07	1.0000	12.3827
280 ZnSuc			0.1773E+03	0.1814E+03	0.6710	2.7871
281 CaCl +			0.3377E+01	0.3455E+01	1.0000	4.5012
282 CaCl2			0.1177E-28	0.1204E-28	0.2080	34.7481
284 SiF6 --	0.1000	0.1023	0.1000E+00	0.1023E+00	1.0000	0.0000
285 CH4 Gas			0.1796E-04	0.1837E-04	1.0000	10.1570
288 PbCO3			0.3184E-04	0.3258E-04	0.6710	10.0054
289 PbOH +			0.5375E-04	0.5499E-04	0.6710	9.5291
292 ZnHCO3 +			0.2324E-03	0.2378E-03	0.6710	8.7072
293 ZnOH +			0.1038E-04	0.1062E-04	1.0000	9.9654
294 Zn(OH)2						

SAMPLE IDENT - Test Sample #3 - Dissolve Anorthite to saturate with Gibbsite in seawater (TEMPERATURE = 25.00)
ANORTHIT PPT/DISS

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
1 ADULARIA	0.642	1.260	-0.618	-0.843	74 MICROCLIN	0.642	-0.550	1.192	1.626
2 AKERMANI	33.530	45.460	-11.930	-16.275	75 MIRONITE	50.494	69.950	-19.456	-26.542
3 ALBITE	2.330	2.500	-0.170	-0.232	76 MIRABILIT	-3.761	-1.090	-2.671	-3.644
4 ALBITE L	2.330	3.110	-0.780	-1.064	77 MONTICEL	24.012	30.150	-6.138	-8.374
5 ALBITE H	2.330	4.430	-2.100	-2.865	78 MORD, Na	-2.956	-3.900	-2.056	-2.805
6 ALUNITE	-11.029	-2.790	-8.239	-11.239	79 MORD, K	-7.644	-7.600	-0.044	-0.060
7 AMESITE	38.906	38.630	0.276	0.376	80 MUSCOVIT	14.701	12.880	1.821	2.484
8 ANALCIME	6.452	6.050	0.402	0.548	81 NACHOLIT	-3.509	-0.430	-3.079	-4.200
9 ANDALUSI	9.937	16.570	-6.633	-9.049	82 NATRTHRM	-6.156	-0.010	-6.146	-8.384
10 ANDESITE	9.180	12.730	-3.550	-4.843	83 NATRON	-6.231	-0.880	-5.351	-7.300
11 ANHYDRIT	-5.403	-4.330	-1.073	-1.464	84 NEPHALIN	10.591	13.520	-2.929	-3.996
12 ANNITE	25.453	29.140	-3.687	-5.030	85 NESQUEHON	-7.054	-5.350	-1.704	-2.325
13 ANORTHIT	19.456	25.830	-6.374	-8.696	92 OLIGOCLA	5.755	8.730	-2.975	-4.059
14 APATCHLR	-49.450	-66.150	-16.700	-22.782	93 PARAGONI	16.389	14.390	1.999	2.727
15 APATFLUR	-53.552	-68.340	-14.788	-20.175	94 PARAGASI	89.267	100.790	-11.523	-15.720
16 APATHYDX	-54.784	-60.390	-5.606	-7.647	95 PERICLAS	14.493	21.510	-7.017	-9.573
17 ARAGONIT	-7.873	-8.340	-0.467	-0.637	96 PHILLIPS	1.477	3.300	-1.823	-2.486
18 AUGITE	23.586	32.560	-8.974	-12.243	97 PHLOGPIT	44.112	37.220	6.892	9.402
20 BARITE	-10.205	-9.960	-0.245	-0.334	98 PHLOGPTF	18.598	16.730	1.868	2.548
21 BOEHMITE	7.029	6.950	0.079	0.108	99 PORTLAN	-14.339	-5.420	-8.919	-12.168
22 BRUCITE	-13.496	-11.470	-2.026	-2.763	100 POTASSI	11.998	84.120	-72.122	-98.391
23 BYTONIT	16.031	18.600	-2.569	-3.505	101 PREHNITE	28.966	32.020	-3.054	-4.166
24 CALCITE	-7.873	-8.480	-0.607	-0.828	102 PYROPHYL	-2.462	-0.100	-2.362	-3.223
25 CELESTIT	-7.391	-6.430	-0.961	-1.311	103 QUARTZ	-4.130	-3.930	-0.200	-0.273
26 CHALCEDO	-4.130	-3.730	-0.400	-0.546	104 SANIDINE	0.642	1.180	-0.538	-0.734
27 CHAM 7A	26.466	29.030	-2.564	-3.497	105 SAPO, Na	33.170	26.880	6.290	8.581
28 CHLOR, 7	74.107	71.940	2.167	2.956	106 SAPO, K	32.613	26.550	6.063	8.271
29 CHLOR, 1	74.107	68.570	5.537	7.554	107 SAPO, H	30.632	25.850	4.782	6.523
30 CRYSTOL	35.201	32.030	3.171	4.326	108 SAPO, Ca	32.885	26.820	6.065	8.274
31 C-ENSTAT	10.363	11.290	-0.927	-1.265	109 SAPO, Mg	33.024	26.800	6.224	8.491
32 C-PTIL,N	-11.929	-7.900	-4.029	-5.496	110 SEPIOLIT	33.131	31.520	1.611	2.197
33 C-PTIL,K	-15.305	-15.000	-0.305	-0.416	111 SILICAM	-4.130	-2.700	-1.430	-1.951
34 C-PTIL,C	-13.654	-9.300	-4.354	-5.940	112 SILICGEL	-4.130	-2.710	-1.420	-1.938
35 C-PTIL,M	-12.810	-5.000	-7.810	-10.655	113 SILLIMAN	9.937	15.730	-5.793	-7.903
36 CORUNDUM	14.067	21.400	-7.333	-10.004	114 SMEC Ca	3.468	6.140	-2.672	-3.645
37 CRISTOBA	-4.130	-3.540	-0.590	-0.805	115 SMEC K	3.201	5.860	-2.659	-3.627
38 CRISTOBB	-4.130	-2.940	-1.190	-1.624	116 SMEC Mg	3.609	6.040	-2.431	-3.316
39 DICKITE	5.790	6.170	-0.380	-0.519	117 SMEC Na	3.758	6.120	-2.362	-3.222
40 DIOPSIDE	19.881	19.630	0.251	0.343	118 Na2O	15.374	67.430	-52.056	-71.016
41 DOLOMITE	-14.902	-18.060	3.158	4.309	119 SPINEL	28.560	36.460	-7.900	-10.777
42 DSORD	-14.902	-16.520	1.618	2.208	120 STILBITE	-1.255	1.410	-2.665	-3.735
43 ENSTATIT	10.363	11.470	-1.107	-1.511	122 SrCO3	-9.861	-9.270	-0.591	-0.806
45 FAYALITE	12.416	19.430	-7.014	-9.569	123 SYLVITE	-2.661	0.910	-3.571	-4.872
46 FLUORITE	-11.874	-10.960	-0.914	-1.246	124 TALC	26.949	21.130	5.819	7.938
47 FORSTERI	24.855	29.070	-4.215	-5.750	125 THENARDI	-3.677	-0.290	-3.387	-4.621
48 GIBBS AM	-34.949	-34.420	-0.529	-0.722	126 TREMOLIT	66.711	60.890	5.821	7.942
49 GIBBSITE	-34.949	-34.920	-0.029	-0.039	127 TRONA	-9.673	-0.630	-9.043	-12.337
50 GREENALI	16.542	22.580	-6.038	-8.238	128 VIVIANIT	-47.938	-36.000	-11.938	-16.287
51 GYPSUM	-5.420	-4.600	-0.820	-1.118	129 WAIKAKIT	11.178	17.330	-6.152	-8.392
52 HALITE	-0.973	1.590	-2.563	-3.496	130 WITHERIT	-12.675	-8.630	-4.045	-5.519
53 HALLOYSI	5.790	8.910	-3.120	-4.257	131 WOLLASTO	9.519	12.600	-3.081	-4.204

SAMPLE IDENT - Test Sample #3 - Dissolve Anorthite to saturate with Gibbsite in seawater
ANORTHIT PPT/DISS (TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
54 HEULANDI	-1.246	1.410	-2.656	-3.624	132 ZOISITE	36.004	42.100	-6.096	-8.317
55 HUNTITE	-28.960	-30.620	1.660	2.265	134 AgCl	-14.686	-9.730	-4.956	-6.761
56 HYDRMAGN	-36.507	-38.530	2.023	2.760	139 Cu2O	-8.747	-1.900	-6.847	-9.341
57 HYPHILIT	-3.671	11.800	-15.471	-21.106	144 FeCl2	-9.047	7.900	-16.947	-23.120
58 ILLITE	8.936	10.340	-1.404	-1.916	146 FeCO3	-13.249	-10.540	-2.709	-3.695
59 KAOLINIT	5.790	6.230	-0.440	-0.600	147 FeO	8.273	13.500	-5.227	-7.131
60 KENYAITE	-37.788	-25.000	-12.788	-17.446	158 HgCl2(C)	-25.023	-14.110	-10.913	-14.888
61 K-SPAR	0.642	-0.550	1.192	1.626	160 HgO	-7.703	2.440	-10.143	-13.838
62 KYANITE	9.937	14.480	-4.543	-6.198	163 MnCl2	-12.494	8.790	-21.284	-29.036
63 LABRADOR	14.245	16.250	-2.005	-2.735	164 MnCO3	-16.695	-10.540	-6.155	-8.397
64 LARNITE	23.168	38.880	-15.712	-21.435	165 MnO	4.826	17.700	-12.874	-17.563
65 LAUMONTI	11.162	14.170	-3.008	-4.104	168 PbCl2	-12.955	-4.820	-8.135	-11.099
66 LEUCITE	4.772	6.520	-1.748	-2.384	169 PbCO3	-17.157	-12.890	-4.267	-5.821
67 LIME	-19.152	32.660	-51.812	-70.683	170 PbOLITHR	4.365	12.550	-8.185	-11.167
68 MAGADITE	-21.263	-14.340	-6.923	-9.444	171 PbOMASIC	4.365	12.690	-8.325	-11.358
70 MAGNESIT	-7.029	-8.050	1.021	1.393	173 PbSO4	-14.687	-7.800	-6.887	-9.396
71 MgCl2	-2.827	22.150	-24.977	-34.075	174 ZnCO3	-13.079	-9.870	-3.209	-4.378
72 MARIALIT	6.017	1.710	4.307	5.875	175 ZnO	8.443	11.200	-2.757	-3.761
73 MERWINIT	47.179	68.170	-20.991	-28.636	177 ZnSO4	-10.609	3.540	-14.149	-19.302

***** INPUT DATA ECHO *****

TITLE : Test Sample #4 - Ca/Mg exchange in seawater

TEMP HITEMP DENS PRESS

0.2500E+02 0.0000E+00 0.1023E+01 0.0000E+00

PH EHM EHW ENFZSC

0.8200E+01 0.5000E+00 0.9000E+01 0.9000E+01

CONCENTRATION UNITS : PPM

Na	K	Li	Ca	Mg	Fe	Al
0.1077E+05	0.3991E+03	0.1810E+00	0.4123E+03	0.1292E+04	0.2000E-02	0.0000E+00
SiO2	Cl	SO4	H2S	HCO3	CO3	TIC
0.4280E+01	0.1935E+05	0.2712E+04	0.1000E+02	0.1234E+03	0.0000E+00	0.0000E+00

F	PO4	NO3	NH3	B	Sr	Ba
0.1390E+01	0.6000E-01	0.2900E+00	0.0000E+00	0.4450E+01	0.8140E+01	0.2000E-01
Pb	Zn	Cu	Mn	Hg	Ag	
0.5000E-04	0.4900E-02	0.7000E-03	0.2000E-03	0.3000E-04	0.4000E-04	

As	U	V				
0.4000E-02	0.0000E+00	0.0000E+00				
Acetate	Oxalate	Succinate	CH4			
0.1000E+00	0.1000E+00	0.1000E+00	0.1000E+00			

ALK	ITIC					
2	0					
DCO2	DH2S	DNH3	DCH4			
0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00			

ICCSAT	IMCO3	FIXIT	FCCSAT			
0	0	0.0000E+00	0.0000			
TCO2M	TC4M	TH2SM	WROIL	KCO2OL	KCH4OL	KH2SOL
0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

DSEP						
0.0000E+00						

Adsorption/Exchange option (N=no) = E						
Surface Chemistry input for Ion Exchange:						

CEC	TAREA	SAREA	INSP			
0.1000E+03	0.0000E+00	0.0000E+00	2			
NAME	CHARGE	Fract. Surf. Sites				
CaX2	0	0.5000E+00				

MgX2	0	0.5000E+00				

K = 1. *	* Coef	* ID	+	----		
1.0000	CaX2	-0.1000E+01	1	-0.2000E+01	0	
1.0000	MgX2	-0.1000E+01	2	-0.2000E+01	0	

IBMX	ITMIX					
0	0					

LOG KT TO BE CHANGED AT TEMP = 25.00						
0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00

LOG KT TO BE CHANGED AT TEMP = 0.00						
0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00	0 0.0000E+00

ANS1	ANS2					
0	0					

Number of Additional Minerals =	0					
FLAG FOR ACTIVITY COEFF OF NEUTRAL SPECIES:	1					

FLAG FOR ACTIVITY COEFF BY PITZERS EQUATIONS:	0					
FLAGS FOR CALCULATING REDOX SPECIES:						

Fe	Cu	Hg	Mn	U	V	
1	1	1	1	0	0	

PRINTING OPTIONS:						
INFORM	RATIO	GEOH	IPRIN1	IPRIN2		
0	0	0	0	0		

TOLERANCE FACTORS:	CONV1 =	0.5000E-04	CONV2 =	0.5000E-04		
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SAMPLE IDENT:- Test Sample #4 - Ca/Mg exchange in seawater

PH	EH	TEMP	CATIONS	ANIONS	DIFFERENCE (MEQ/L)	HTOT	OH	OH BALANCE (MOLES)	DIFFERENCE
8.20	0.5000	25.00	ANAL= 619.6745	618.2648	1.4097	0.2514E-02	0.1350E-02	0.1163E-02	
			CALC= 577.6281	570.0555	7.5726				
-----PRESSURE-----									
DENSITY AT	TOTAL DISSOLVED	IONIC	ACTIVITY	P TOTAL	PH2O	PCO2	PH2S	PCN4	PNH3
INPUT T	SOLIDS (MG/L)	STRENGTH	OF WATER	(BARS)	(BARS)	(BARS)	(BARS)	(BARS)	(BARS)
1.0230	35916.54	0.64960	0.9809	1.0000	0.3169E-01	0.4782E-03	0.1449E-03	0.5252E-02	0.0000E+00
-----CALCULATED-----									
Dissolved Inorganic Carbon									
as HCO3- H2CO3 Sum of CO3=									
TIC Alkalinity species HCO3- CO3=									
(MG/L)=0.1594E+03 0.7840E+02 0.1308E+03									
(PPM)=0.1559E+03 0.7664E+02 0.1278E+03									
(MOLALITY)=0.2647E-02 0.1324E-02 0.1324E-02									
-----ANALYZED-----									
SPECIES	PPM	MG/L	MOLALITY	PPM	MG/L	MOLALITY	ACTIVITY	ACTIVITY	-LOG10
1 Ca ++	412.3000	421.7829	0.1066E-01	0.2844E+03	0.2909E+03	0.7533E-02	0.1807E-02	0.2458	2.7430
2 Mg ++	1292.0000	1321.7160	0.5508E-01	0.1121E+04	0.1147E+04	0.4779E-01	0.1261E-01	0.2639	1.8992
3 Na +	10770.0000	11017.7100	0.4855E+00	0.1024E+05	0.1048E+05	0.4618E+00	0.3099E+00	0.6710	0.5088
4 K +	399.1000	408.2793	0.1058E-01	0.3825E+03	0.3913E+03	0.1014E-01	0.6356E-02	0.6269	2.1968
5 Cl -	19350.0000	19795.0500	0.5657E+00	0.1874E+05	0.1917E+05	0.5478E+00	0.3434E+00	0.6269	0.4641
6 SO4 --	2712.0000	2774.3760	0.2926E-01	0.1203E+04	0.1231E+04	0.1298E-01	0.2189E-02	0.1886	2.6598
7 HCO3 -	123.4000	126.2382	0.2096E-02	0.8534E+02	0.8730E+02	0.1449E-02	0.1000E-02	0.6899	3.0000
8 H +				0.7638E-05	0.7814E-05	0.7853E-08	0.6310E-08	0.8034	8.2000
9 OH -				0.4016E-01	0.4108E-01	0.2447E-05	0.1591E-05	0.6501	5.7984
11 H4SiO4				0.6615E+01	0.6767E+01	0.7133E-04	0.7133E-04	1.0000	4.1467
12 SiO2	4.2800	4.3784	0.7382E-04						
13 Ag +	0.0000	0.0000	0.3843E-09	0.1039E-08	0.1063E-08	0.9982E-14	0.6000E-14	0.6011	14.2219
15 Ba ++	0.0200	0.0205	0.1509E-06	0.1815E-01	0.1857E-01	0.1370E-06	0.2849E-07	0.2080	7.5453
16 Cu +	0.0007	0.0007	0.1142E-07	0.2394E-09	0.2450E-09	0.3906E-14	0.2348E-14	0.6011	14.6294
17 Cu ++	0.0020	0.0020	0.3712E-07	0.3648E-03	0.3732E-03	0.5950E-08	0.1462E-08	0.2458	8.8349
18 Fe ++	0.0000	0.0000	0.1550E-09	0.1268E-08	0.1297E-08	0.2353E-13	0.5784E-14	0.2458	14.2378
19 Fe +3	0.0000	0.0000	0.1550E-09	0.1009E-12	0.1032E-12	0.1872E-17	0.1599E-18	0.0854	18.7962
21 Hg ++	0.0000	0.0000	0.1810	0.7470E-18	0.7642E-18	0.3860E-23	0.8029E-24	0.2080	24.0954
22 Li +	0.0002	0.0002	0.2703E-04	0.1792E+00	0.1833E+00	0.2677E-04	0.1973E-04	0.7373	4.7048
23 Mn ++	0.0002	0.0002	0.3773E-08	0.5864E-06	0.5998E-06	0.1106E-10	0.2719E-11	0.2458	11.5656
24 Mn +3	0.0001	0.0001	0.2501E-09	0.8886E-23	0.9091E-23	0.1676E-27	0.1432E-28	0.0854	28.8441
25 Pb ++	8.1400	8.3272	0.9628E-04	0.9758E-12	0.9983E-12	0.4881E-17	0.9200E-18	0.1885	18.0362
26 Sr ++	0.0049	0.0050	0.7769E-07	0.7551E+01	0.7725E+01	0.8932E-04	0.1858E-04	0.2080	4.7310
27 Zn ++	0.0067	0.0068	0.5281E-07	0.2691E-10	0.2753E-10	0.4267E-15	0.1049E-15	0.2458	15.9794
28 H2AsO3-	0.0600	0.0614	0.6548E-06	0.7209E-03	0.7375E-03	0.5706E-08	0.3829E-08	0.6710	8.4169
29 PO4 -3	1.3900	1.4220	0.7583E-04	0.5920E-05	0.6056E-05	0.6461E-10	0.1748E-11	0.0271	11.7573
30 F -	25.4540	26.0394	0.4266E-03	0.7672E+00	0.7848E+00	0.4185E-04	0.2721E-04	0.6501	4.5653
31 B(OH)3	10.0000	10.2300	0.3041E-03	0.2205E+02	0.2256E+02	0.3696E-03	0.3696E-03	1.0000	3.4323
33 H2S				0.3685E+00	0.3770E+00	0.1121E-04	0.1166E-04	1.0407	4.9332
43 AgCl				0.5954E-06	0.6091E-06	0.4305E-11	0.4305E-11	1.0000	11.3660
44 AgCl2 -				0.3801E-04	0.3889E-04	0.2204E-09	0.1479E-09	0.6710	9.8301
45 AgCl3 --				0.3041E-04	0.3111E-04	0.1471E-09	0.3060E-10	0.2080	10.5143
46 AgCl4 -3				0.4055E-05	0.4148E-05	0.1683E-10	0.6631E-12	0.0394	12.1784
47 AgSO4 -				0.7863E-10	0.8043E-10	0.3996E-15	0.2681E-15	0.6710	15.5717

SPECIES	ANALYZED			CALCULATED			ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	MOLALITY	PPM	MG/L	MOLALITY		
48 CH3COO -	0.1000	0.1023	0.1755E-05	0.7230E-01	0.7396E-01	0.1269E-05	0.6899	6.0577
49 H3ASO3				0.5724E-02	0.5856E-02	0.4710E-07	1.0000	7.3269
51 BaCO3				0.1272E-04	0.1301E-04	0.6678E-10	1.0000	10.1753
52 BaHCO3 +				0.2238E-03	0.2290E-03	0.1169E-08	0.6710	9.1053
53 BaOH +				0.3234E-07	0.3308E-07	0.2172E-12	0.7071	12.8137
54 BaSO4				0.2867E-02	0.2933E-02	0.1273E-07	1.0000	7.8952
55 CaCO3				0.2147E+01	0.2197E+01	0.2224E-04	1.0000	4.6529
56 CaHCO3 +				0.3081E+01	0.3152E+01	0.3158E-04	0.7373	4.6329
57 CaOH +				0.2965E-02	0.3033E-02	0.5383E-07	0.7373	7.4013
58 CaPO4 -				0.1688E-02	0.1727E-02	0.1296E-07	0.7198	8.0303
59 CaHPO4				0.2333E-02	0.2387E-02	0.1777E-07	1.0000	7.7503
60 CaH2PO4+				0.2207E-04	0.2258E-04	0.1669E-09	0.7198	9.9203
61 CaSO4				0.1037E+03	0.1061E+03	0.7892E-03	1.0000	3.1028
62 CuCl				0.3860E-07	0.3948E-07	0.4041E-12	1.0000	12.3935
63 CuCl2 -				0.4663E-05	0.4770E-05	0.3594E-10	0.6710	10.6177
64 CuCl3 --				0.1035E-04	0.1058E-04	0.6311E-10	0.2080	10.8818
65 CuCl +				0.7487E-04	0.7659E-04	0.7838E-09	0.6710	9.2791
66 CuCl2				0.4363E-05	0.4464E-05	0.3364E-10	1.0000	10.4732
67 CuCl3 -				0.7255E-07	0.7421E-07	0.4425E-12	0.6710	12.5273
68 CuCl4 --				0.4869E-09	0.4981E-09	0.2457E-14	0.2080	15.2915
69 CuOH +				0.3094E-03	0.3165E-03	0.3981E-08	0.6710	8.5733
70 CuSO4				0.8765E-04	0.8967E-04	0.5692E-09	1.0000	9.2447
71 FeCl +				0.7697E-10	0.7874E-10	0.8737E-15	0.6710	15.2319
72 FeCl2				0.5145E-18	0.5263E-18	0.4207E-23	1.0000	23.3761
73 FeHPO4				0.8142E-13	0.8329E-13	0.5558E-18	1.0000	18.2551
74 H3PO4				0.2034E-09	0.2081E-09	0.2151E-14	1.0000	14.6673
75 FeOH +				0.2893E-10	0.2959E-10	0.4115E-15	0.7071	15.5362
76 Fe(OH)2				0.3115E-13	0.3187E-13	0.3593E-18	1.0000	18.4446
77 FeOH -				0.2686E-13	0.2748E-13	0.3133E-18	0.7071	18.6546
78 FeSO4				0.4994E-09	0.5109E-09	0.3407E-14	1.0000	14.4676
79 FeCl ++				0.6864E-12	0.7022E-12	0.7791E-17	0.2080	17.7903
80 FeCl2 +				0.4400E-12	0.4502E-12	0.3598E-17	0.7071	17.5945
81 FeCl3				0.1368E-13	0.1399E-13	0.8738E-19	1.0000	19.0586
82 FeCl4 -				0.1025E-15	0.1049E-15	0.5377E-21	0.6710	21.4427
83 FeSO4 +				0.1001E-11	0.1024E-11	0.6831E-17	0.7071	17.3160
84 FeSO4)2-				0.1038E-23	0.1062E-23	0.4340E-29	0.6710	29.5358
85 FeOH ++				0.6227E-07	0.6370E-07	0.8859E-12	0.2080	12.7346
86 Fe(OH)2+				0.3697E-04	0.3782E-04	0.4264E-09	0.7198	9.5129
87 Fe(OH)3				0.2099E-02	0.2147E-02	0.2035E-07	1.0000	7.6913
88 Fe(OH)4-				0.1952E-02	0.1997E-02	0.1633E-07	0.7198	7.9297
89 B(OH)4 -				0.4342E+01	0.4442E+01	0.5708E-04	0.6065	4.4607
90 H2SiO4 --				0.2150E-03	0.2199E-03	0.2368E-08	0.2233	9.2767
91 H3SiO4 -				0.2287E+00	0.2340E+00	0.2492E-05	0.6710	5.7767
92 HAsO3 --				0.1173E-07	0.1200E-07	0.9357E-13	0.2080	13.7108
96 HF				0.5016E-05	0.5131E-05	0.2598E-09	1.0000	9.5853
97 H2CO3				0.8454E+00	0.8648E+00	0.1413E-04	1.0000	4.8500
98 CO3 --				0.1922E+01	0.1966E+01	0.7413E-05	0.2233	5.1300
99 HPO4 --				0.1075E-01	0.1099E-01	0.1160E-06	0.2080	7.6173
100 H2PO4 -				0.3138E-03	0.3210E-03	0.3353E-08	0.7198	8.6173
101 HS -				0.9074E+01	0.9282E+01	0.2843E-03	0.6501	3.7332
102 S --				0.4357E-07	0.4458E-07	0.1408E-11	0.2080	12.5332
103 HS04 -				0.1671E-03	0.1709E-03	0.1784E-08	0.6899	8.9098
104 HNO3				0.4331E-10	0.4431E-10	0.7124E-15	1.0000	15.1473

SPECIES	ANALYZED-----		CALCULATED-----		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
105 HgCl +			0.1664E-12	0.1703E-12	0.6710	18.3095
106 HgCl2			0.4514E-06	0.4618E-06	1.0000	11.7637
107 HgCl3 -			0.3214E-04	0.3288E-04	0.6710	10.1378
108 HgCl4 --			0.1476E-04	0.1510E-04	0.2080	11.0319
109 HgSO4			0.1263E-19	0.1292E-19	1.0000	25.3552
111 Hg(HS)3-			0.2343E-07	0.2397E-07	0.6710	13.2649
113 KCl			0.2070E+02	0.2118E+02	1.0000	3.5409
114 KCO3 -			0.7987E-01	0.8171E-01	0.6629	6.2568
115 KHSO4			0.7277E-05	0.7444E-05	1.0000	10.2566
116 KSO4 -			0.1957E+02	0.2002E+02	0.7198	3.9666
117 KHP04 -			0.5417E-04	0.5541E-04	0.7198	9.5241
118 LiOH			0.1098E-05	0.1123E-05	1.0000	10.3232
119 LiSO4 -			0.2650E-01	0.2711E-01	0.7071	6.7246
120 MgCO3			0.7265E+01	0.7432E+01	1.0000	4.0492
121 MgHCO3 +			0.1818E+02	0.1860E+02	0.6710	3.8292
122 MgF +			0.1373E+01	0.1405E+01	0.6899	4.6445
123 MgOH +			0.4243E+00	0.4341E+00	0.7505	5.0976
124 MgSO4			0.8054E+03	0.8239E+03	1.0000	2.1590
125 MgPO4 -			0.1041E-01	0.1065E-01	0.7198	7.1865
126 MgHPO4			0.4552E-01	0.4657E-01	1.0000	6.4065
127 MgH2PO4+			0.1363E-03	0.1395E-03	0.7198	9.0765
128 MnCl +			0.3838E-13	0.3926E-13	0.6710	18.5298
129 MnCl2			0.3093E-10	0.3164E-10	1.0000	15.5939
130 MnCl3 -			0.5097E-09	0.5215E-09	0.6710	14.6581
131 MnCl4 --			0.5472E-08	0.5597E-08	0.2080	14.2222
132 MnHCO3 +			0.8442E-08	0.8636E-08	0.6710	13.2956
133 MnSO4			0.1578E-06	0.1614E-06	1.0000	11.9654
134 MnHPO4			0.3633E-10	0.3716E-10	1.0000	15.6030
135 MnOH +			0.1232E-08	0.1261E-08	0.6710	13.9240
136 NO3 -	0.2900	0.2967	0.2900E+00	0.2967E+00	0.6269	5.5173
137 NaCl			0.8477E+03	0.8672E+03	1.0000	1.8229
138 NaCO3 -			0.4759E+01	0.4869E+01	0.7198	4.3688
139 NaHCO3			0.1413E+02	0.1445E+02	1.0000	3.7588
140 Na2CO3			0.1521E-01	0.1556E-01	1.0000	6.8276
141 Na2SO4			0.9321E+03	0.9535E+03	1.0000	2.1674
142 NaSO4 -			0.1838E+03	0.1880E+03	0.7198	2.9386
143 NaHP04 -			0.2326E-02	0.2379E-02	0.7198	7.8361
144 NaF			0.4503E-01	0.4607E-01	1.0000	5.9541
145 NaHS			0.4583E+00	0.4689E+00	1.0000	5.0720
148 PbCl +			0.2834E-11	0.2899E-11	0.6710	17.0904
149 PbCl2			0.2718E-11	0.2780E-11	1.0000	16.9945
150 PbCl3 -			0.7681E-12	0.7858E-12	0.6710	17.7886
151 PbCl4 --			0.5976E-12	0.6114E-12	0.2080	18.4328
152 PbSO4			0.3313E-12	0.3389E-12	1.0000	17.9460
153 MnCl ++			0.8400E-21	0.8594E-21	0.2080	26.6982
154 SrOH -			0.2067E-04	0.2114E-04	0.7071	9.8394
155 SrCO3			0.1296E-01	0.1326E-01	1.0000	7.0410
156 SrHCO3 +			0.6151E-01	0.6292E-01	0.6710	6.5410
157 SrSO4			0.1142E+01	0.1168E+01	1.0000	5.1908
158 ZnCl +			0.1374E-10	0.1405E-10	0.6710	16.0235
159 ZnCl2			0.6780E-11	0.6936E-11	1.0000	16.2876
160 ZnCl3 -			0.2295E-11	0.2348E-11	0.6710	17.0318
161 ZnCl4 --			0.2122E-11	0.2171E-11	0.2080	17.6559

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
162 ZnSO4			0.5798E-11	0.5931E-11	1.0000	16.4292
165 HgOH +			0.1153E-13	0.1179E-13	0.6710	19.4337
166 Hg(OH)2			0.3409E-08	0.3488E-08	1.0000	13.8221
228 CH3COOH			0.1842E-04	0.1884E-04	1.0000	9.4977
230 BaAce +			0.9241E-07	0.9453E-07	0.6899	12.4731
231 CaAce +			0.3725E-02	0.3811E-02	0.6899	7.5707
232 CuAce +			0.2735E-13	0.2798E-13	0.6899	18.7971
233 FeAce +			0.1624E-12	0.1661E-12	0.6899	17.9955
234 Fe(Ace)2			0.9367E-20	0.9582E-20	1.0000	25.2533
235 KAce			0.2147E-03	0.2196E-03	1.0000	8.6445
236 MgAce +			0.2289E-01	0.2342E-01	0.6899	6.7069
237 NaAce			0.1265E-01	0.1294E-01	1.0000	6.7965
238 PbAce +			0.5458E-16	0.5583E-16	0.6899	21.8340
239 Pb(Ace)2			0.9661E-21	0.9884E-21	1.0000	26.5117
240 Pb(Ace)3			0.1742E-26	0.1782E-26	0.6899	32.4894
241 SrAce +			0.4823E-04	0.4933E-04	0.6899	9.6287
244 ZnAce +			0.1299E-11	0.1328E-11	0.6899	17.1271
245 Zn(Ace)2			0.3185E-21	0.3259E-21	1.0000	26.7448
246 C2O4 --	0.1000	0.1023	0.9440E-02	0.9657E-02	0.2233	7.6051
247 HC2O4 -			0.3468E-09	0.3548E-09	0.6899	14.5551
248 H2C2O4			0.3117E-13	0.3189E-13	1.0000	18.4451
251 BaOxy			0.5714E-08	0.5845E-08	1.0000	13.5804
252 CaOxy			0.5546E-02	0.5673E-02	1.0000	7.3481
253 FeOxy			0.5007E-12	0.5122E-12	1.0000	17.4429
254 FeOxy +			0.3028E-13	0.3098E-13	0.6899	18.8225
255 KOxy -			0.1406E-03	0.1438E-03	0.6899	9.1019
256 MgOxy			0.1002E+00	0.1025E+00	1.0000	6.0343
257 MnOxy			0.9310E-10	0.9524E-10	1.0000	15.1707
258 MnOxy)2			0.7180E-03	0.7345E-03	0.2233	9.0758
259 MnOxy)3			0.1550E-06	0.1586E-06	0.0021	14.8809
260 MnOxy			0.2764E-19	0.2827E-19	0.6899	24.8594
261 NaOxy -			0.9487E-02	0.9705E-02	0.6899	7.2139
262 PbOxy			0.3575E-15	0.3657E-15	1.0000	20.9013
263 SrOxy			0.2710E-04	0.2773E-04	1.0000	9.7961
264 ZnOxy			0.3061E-13	0.3131E-13	1.0000	18.6845
265 C4H4O4 --			0.6406E-01	0.6553E-01	0.2233	6.8937
266 HC4H4O4-			0.2140E-05	0.2190E-05	0.6899	10.8837
267 H2C4H4O4			0.4102E-08	0.4196E-08	1.0000	13.4437
270 BaSuc			0.9317E-07	0.9532E-07	1.0000	12.4190
271 CaSuc			0.3478E-02	0.3558E-02	1.0000	7.6366
272 FeSuc			0.1942E-13	0.1987E-13	1.0000	18.9315
273 FeSuc +			0.4911E-13	0.5024E-13	0.6899	18.6898
274 KSuc -			0.3516E-03	0.3597E-03	0.6899	8.7905
275 MgSuc			0.2449E-01	0.2505E-01	1.0000	6.7429
276 MnSuc			0.8476E-11	0.8671E-11	1.0000	16.2893
277 NaSuc -			0.1536E-01	0.1571E-01	0.6899	7.1025
278 PbSuc			0.1159E-15	0.1186E-15	1.0000	21.4299
279 SrSuc			0.4664E-04	0.4772E-04	1.0000	9.6247
280 ZnSuc			0.6764E-15	0.6919E-15	1.0000	20.4130
281 CaCl +			0.1773E+03	0.1814E+03	0.6710	2.7871
282 CaCl2			0.3377E+01	0.3454E+01	1.0000	4.5012
283 FeF ++			0.1510E-11	0.1543E-11	0.2080	17.3615
284 SiF6 --			0.1180E-28	0.1207E-28	0.2080	34.7469

SPECIES	ANALYZED		CALCULATED		ACTIVITY	ACTIVITY	-LOG10
	PPM	MG/L	PPM	MG/L	COEFF.	ACTIVITY	
285 CH4 Gas	0.1000	0.1023	0.1000E+00	0.1023E+00	0.0000E+00	0.0000	0.0000
286 Pb(HS)2			0.6586E-04	0.6737E-04	0.2497E-09	1.0000	9.6026
287 Pb(HS)3-			0.1170E-06	0.1197E-06	0.3959E-12	0.6710	12.5757
288 PbCO3			0.1758E-10	0.1799E-10	0.6820E-16	1.0000	16.1662
289 PbOH +			0.3117E-10	0.3189E-10	0.1441E-15	0.6710	16.0146
290 Zn(HS)2			0.2740E-04	0.2803E-04	0.2159E-09	1.0000	9.6657
291 Zn(HS)3-			0.1397E-05	0.1429E-05	0.8798E-11	0.6710	11.2289
292 ZnHCO3 +			0.5013E-12	0.5129E-12	0.4111E-17	0.6710	17.5593
293 ZnOH +			0.2167E-11	0.2217E-11	0.2726E-16	0.6710	16.7377
294 Zn(OH)2			0.9675E-13	0.9898E-13	0.1009E-17	1.0000	17.9961
295 ZnHSOH			0.8629E-02	0.8827E-02	0.7746E-07	1.0000	7.1109

SAMPLE IDENT - Test Sample #4 - Ca/Mg exchange in seawater

(TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
2 AKERMANI	33.530	45.460	-11.930	-16.276	122 STCO3	-9.861	-9.270	-0.591	-0.806
11 ANHYDRIT	-5.403	-4.330	-1.073	-1.464	123 SYLVITE	-2.661	0.910	-3.571	-4.872
14 APATCHLR	-49.451	-66.150	16.699	22.781	124 TALC	26.949	21.130	5.819	7.939
15 APATFLUR	-53.552	-68.340	14.788	20.174	125 THENARDI	-3.677	-0.290	-3.387	-4.621
16 APATHYDX	-54.785	-60.390	5.605	7.646	126 TREMOLIT	66.711	60.890	5.821	7.942
17 ARAGONIT	-7.873	-8.340	0.467	0.637	127 TRONA	-9.673	-0.630	-9.043	-12.337
19 AZURITE	-48.361	-39.460	-8.901	-12.144	128 VIVIANIT	-66.295	-36.000	-30.295	-41.330
20 BARITE	-10.205	-9.960	-0.245	-0.334	130 WITHERIT	-12.675	-8.630	-4.045	-5.519
22 BRUCITE	-13.496	-11.470	-2.026	-2.764	131 MOLLASTO	9.519	12.600	-3.081	-4.204
24 CALCITE	-7.873	-8.480	0.607	0.828	133 SILVER	-9.663	-0.500	-9.163	-12.501
25 CELESTIT	-7.391	-6.430	-0.961	-1.311	134 AgCl	-14.686	-9.730	-4.956	-6.761
26 CHALCEDO	-4.130	-3.730	-0.400	-0.546	135 Ag2S	-23.977	-36.260	12.283	16.757
30 CRYSTOLIT	35.201	32.030	3.171	4.325	136 COPPER	-10.071	4.250	-14.321	-19.537
31 C-ENSTAT	10.362	11.290	-0.928	-1.265	137 MALACHIT	-34.397	-33.580	-0.817	-1.114
37 CRISTOBA	-4.130	-3.540	-0.590	-0.805	138 CUO	7.557	7.670	-0.113	-0.155
38 CRISTOBB	-4.130	-2.940	-1.190	-1.623	139 CU2O	-12.867	-1.900	-10.967	-14.962
40 DIOPSIDE	19.881	19.630	0.251	0.343	140 CUS	-4.368	-22.830	18.462	25.186
41 DOLOMITE	-14.902	-18.060	3.158	4.308	141 Cu2S	-24.792	-34.950	10.158	13.858
42 DSORD	-14.902	-16.520	1.618	2.207	142 CuFeS2	-14.139	-34.070	19.931	27.191
43 ENSTATIT	10.362	11.470	-1.108	-1.511	143 BORNITE	-63.723	-102.510	38.787	52.915
45 FAYALITE	0.178	19.430	-19.252	-26.265	144 FeCl2	-15.166	7.900	-23.066	-31.468
46 FLUORITE	-11.874	-10.960	-0.914	-1.246	145 FeCl3	-20.189	12.340	-32.529	-44.377
47 FORSTERI	24.855	29.070	-4.215	-5.750	146 FeCO3	-19.368	-10.540	-8.828	-12.043
50 GREENALI	-1.815	22.580	-24.395	-33.281	147 FeO	2.154	13.500	-11.346	-15.479
51 GYPSUM	-5.420	-4.600	-0.820	-1.118	148 Fe2O3HEM	11.583	0.040	11.543	15.747
52 HALITE	-0.973	1.590	-2.563	-3.496	149 Fe2O3MGH	11.583	6.400	5.183	7.070
55 HUNITE	-28.960	-30.620	1.660	2.264	150 Fe3O4	13.736	10.750	2.986	4.074
56 HYDRMAGN	-36.508	-38.530	2.022	2.759	151 Fe(OH)3	-36.191	-37.200	1.009	1.376
57 HYPHILIT	-3.671	11.800	-15.471	-21.106	152 GOETHITE	5.787	0.480	5.307	7.240
60 KENYAITE	-37.784	-25.000	-12.784	-17.441	153 FeSPYRHO	-9.771	3.760	-6.011	-8.200
64 LARNITE	23.167	38.880	-15.713	-21.436	154 FeSTROLT	-9.771	-3.870	-5.901	-8.050
67 LINE	-19.151	32.660	-51.811	-70.683	155 FeS2PYR	-23.477	-24.710	1.233	1.682
68 MAGADITE	-21.260	-14.340	-6.920	-9.441	156 GREIGITE	-33.963	-45.000	11.037	15.057
69 MgFe2O4	26.075	21.100	4.975	6.787	157 Hg(L)	-14.979	-2.840	-12.139	-16.560
70 MAGNESIT	-7.029	-8.050	1.021	1.393	158 HgCl2(C)	-25.024	-14.110	-10.914	-14.889
71 MgCl2	-2.827	22.150	-24.977	-34.075	160 HgO	-7.704	2.440	-10.144	-13.838
73 MERWINIT	47.178	68.170	-20.992	-28.637	161 CINNABAR	-19.629	-39.860	20.231	27.601
76 MIRABILIT	-3.761	-1.090	-2.671	-3.644	162 CINABMET	-19.629	-38.580	18.951	25.854
77 MONTICEL	24.011	30.150	-6.139	-8.375	163 MnCl2	-12.494	8.790	-21.284	-29.036
81 NACHOLIT	-3.509	-0.430	-3.079	-4.200	164 MnCO3	-16.696	-10.540	-6.156	-8.398
82 NATRTHRM	-6.156	-0.010	-6.146	-8.385	165 MnO	4.826	17.700	-12.874	-17.563
83 NATRON	-6.231	-0.880	-5.351	-7.301	166 MnO2	-13.339	-8.330	-5.009	-6.834
85 NESQUEHON	-7.054	-5.350	-1.704	-2.325	167 MnS	-7.099	-0.470	-6.629	-9.043
91 OLDHAMIT	1.724	11.900	-10.176	-13.883	168 PbCl2	-18.964	-4.820	-14.144	-19.296
95 PERICLAS	14.492	21.510	-7.018	-9.574	169 PbCO3	-23.166	-12.890	-10.276	-14.019
99 PORTLAN	-14.340	-5.420	-8.920	-12.169	170 PbOLITHR	-1.645	12.550	-14.195	-19.365
100 POTASSI	11.998	84.120	-72.122	-98.391	171 PbOMASIC	-1.645	12.690	-14.335	-19.556
103 QUARTZ	-4.130	-3.930	-0.200	-0.273	172 PbS GALN	-13.569	-14.780	1.211	1.652
110 SEPIOLIT	33.131	31.520	1.611	2.198	173 PbSO4	-20.696	-7.800	-12.896	-17.593
111 SILICAAM	-4.130	-2.700	-1.430	-1.951	174 ZnCO3	-21.109	-9.870	-11.239	-15.333
112 SILICGEL	-4.130	-2.710	-1.420	-1.937	175 ZnO	0.412	11.200	-10.788	-14.717

(TEMPERATURE = 25.00)

SAMPLE IDENT - Test Sample #4 - Ca/Mg exchange in seawater

118	121	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
		Na2O	15.374	67.430	-52.056	-71.017	ZnS	-11.513	-11.790	0.277	0.379
		STRENGIT	-30.570	-27.200	-3.370	-4.598	ZnSO4	-18.639	3.540	-22.179	-30.258

Initial Surface Conditions

Surface Complex	Moles on Surface	Moles of Surface Site	Fraction of Surface Sites
CaX2	0.25000E-01	0.50000E-01	0.5000
MgX2	0.25000E-01	0.50000E-01	0.5000

K Surface Comp. Species and Coef.

0.10000E+01 = CaX2 * (Ca ++ ** -1.00) * (X- ** -2.00)
 0.10000E+01 = MgX2 * (Mg ++ ** -1.00) * (X- ** -2.00)

Final Equilibrium Surface Conditions

Surface Complex	Moles on Surface	Moles of Surface Site	Fraction of Surface Sites
CaX2	0.14040E-01	0.28079E-01	0.2808
MgX2	0.35960E-01	0.71921E-01	0.7192

CEC = 0.10000E+03 milli-equivalents
 0.10000E+00 moles exchange capacity for monovalent cations and anions

SAMPLE IDENT:- Test Sample #4 - Ca/Mg exchange in seawater

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SPECIES	ANALYZED		CALCULATED		ACTIVITY	ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L			
48 CH3COO -	0.1000	0.1023	0.7300E-01	0.7468E-01	0.8842E-06	0.6901	6.0534
49 H3ASO3			0.5732E-02	0.5864E-02	0.4717E-07	1.0000	7.3263
51 BaCO3			0.1261E-04	0.1290E-04	0.6623E-10	1.0000	10.1790
52 BaHCO3 +			0.2247E-03	0.2299E-03	0.1174E-08	0.6712	9.1035
53 BaOH +			0.3192E-07	0.3265E-07	0.2143E-12	0.7072	12.8194
54 BaSO4			0.2927E-02	0.2994E-02	0.1300E-07	1.0000	7.8862
55 CaCO3			0.4322E+01	0.4421E+01	0.4475E-04	1.0000	4.3492
56 CaHCO3 +			0.6279E+01	0.6424E+01	0.6437E-04	0.7373	4.3237
57 CaOH +			0.5940E-02	0.6077E-02	0.1078E-06	0.7373	7.0996
58 CaPO4 -			0.3765E-02	0.3851E-02	0.2889E-07	0.7199	7.6820
59 CaHPO4			0.5269E-02	0.5390E-02	0.4013E-07	1.0000	7.3965
60 CaH2PO4+			0.5049E-04	0.5165E-04	0.3817E-09	0.7199	9.5610
61 CaSO4			0.2148E+03	0.2197E+03	0.1635E-02	1.0000	2.7864
62 CuCl			0.3863E-07	0.3952E-07	0.4045E-12	1.0000	12.3931
63 CuCl2 -			0.4647E-05	0.4754E-05	0.3582E-10	0.6712	10.6190
64 CuCl3 --			0.1026E-04	0.1049E-04	0.6256E-10	0.2084	10.8849
65 CuCl +			0.7488E-04	0.7661E-04	0.7840E-09	0.6712	9.2789
66 CuCl2			0.4348E-05	0.4448E-05	0.3351E-10	1.0000	10.4748
67 CuCl3 -			0.7197E-07	0.7363E-07	0.4390E-12	0.6712	12.5307
68 CuCl4 --			0.4804E-09	0.4914E-09	0.2425E-14	0.2084	15.2966
69 CuOH +			0.3068E-03	0.3139E-03	0.3948E-08	0.6712	8.5768
70 CuSO4			0.8991E-04	0.9198E-04	0.5838E-09	1.0000	9.2337
71 FeCl +			0.8003E-10	0.8187E-10	0.9085E-15	0.6712	15.2148
72 FeCl2			0.5330E-18	0.5452E-18	0.4358E-23	1.0000	23.3607
73 FeHPO4			0.9464E-13	0.9682E-13	0.6461E-18	1.0000	18.1897
74 H3PO4			0.2322E-09	0.2376E-09	0.2456E-14	1.0000	14.6098
75 FeOH +			0.2982E-10	0.3051E-10	0.4243E-15	0.7072	15.5228
76 Fe(OH)2			0.3172E-13	0.3245E-13	0.3659E-18	1.0000	18.4367
77 FeOH -			0.2700E-13	0.2762E-13	0.3149E-18	0.7072	18.6522
78 FeSO4			0.5326E-09	0.5448E-09	0.3633E-14	1.0000	14.4397
79 FeCl ++			0.7127E-12	0.7291E-12	0.8090E-17	0.2084	17.7732
80 FeCl2 +			0.4558E-12	0.4662E-12	0.3726E-17	0.7072	17.5791
81 FeCl3			0.1411E-13	0.1443E-13	0.9015E-19	1.0000	19.0450
82 FeCl4 -			0.1053E-15	0.1078E-15	0.5523E-21	0.6712	21.4309
83 FeSO4 +			0.1068E-11	0.1092E-11	0.7284E-17	0.7072	17.2881
84 FeSO4)2-			0.1130E-23	0.1156E-23	0.4724E-29	0.6712	29.4988
85 FeOH ++			0.6411E-07	0.6558E-07	0.9120E-12	0.2084	12.7212
86 Fe(OH)2+			0.3764E-04	0.3851E-04	0.4342E-09	0.7199	9.5051
87 Fe(OH)3			0.2110E-02	0.2159E-02	0.2047E-07	1.0000	7.6890
88 Fe(OH)4-			0.1938E-02	0.1983E-02	0.1621E-07	0.7199	7.9328
89 B(OH)4 -			0.4293E+01	0.4391E+01	0.5643E-04	0.6068	4.4654
90 H2SiO4 --			0.2094E-03	0.2142E-03	0.2306E-08	0.2237	9.2876
91 H3SiO4 -			0.2258E+00	0.2310E+00	0.2461E-05	0.6712	5.7820
92 HASO3 --			0.1147E-07	0.1174E-07	0.9151E-13	0.2084	13.7197
96 HF			0.5565E-05	0.5693E-05	0.2883E-09	1.0000	9.5402
97 H2CO3			0.8601E+00	0.8799E+00	0.1437E-04	1.0000	4.8425
98 CO3 --			0.1904E+01	0.1947E+01	0.3288E-04	0.2237	5.1335
99 HPO4 --			0.1194E-01	0.1222E-01	0.1289E-06	0.2084	7.5708
100 H2PO4 -			0.3537E-03	0.3618E-03	0.3780E-08	0.7199	8.5653
101 HS -			0.9069E+01	0.9278E+01	0.2842E-03	0.6503	3.7332
102 S --			0.4295E-07	0.4394E-07	0.1388E-11	0.2084	12.5387
103 HS04 -			0.1728E-03	0.1767E-03	0.1844E-08	0.6901	8.8952
104 HNO3			0.4389E-10	0.4490E-10	0.7218E-15	1.0000	15.1416

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
105 HgCl +			0.1680E-12	0.1719E-12	0.6712	18.3052
106 HgCl2			0.4541E-06	0.4645E-06	1.0000	11.7611
107 HgCl3 -			0.3219E-04	0.3293E-04	0.6712	10.1370
108 HgCl4 --			0.1470E-04	0.1504E-04	0.2084	11.0329
109 HgSO4			0.1308E-19	0.1338E-19	1.0000	25.3400
111 Hg(HS)3-			0.2374E-07	0.2429E-07	0.6712	13.2590
113 KCl			0.2062E+02	0.2110E+02	1.0000	3.5426
114 KCO3 -			0.7923E-01	0.8105E-01	0.6631	6.2601
115 KHSO4			0.7528E-05	0.7701E-05	1.0000	10.2419
116 KSO4 -			0.1998E+02	0.2044E+02	0.7199	3.9574
117 KHP04 -			0.6030E-04	0.6169E-04	0.7199	9.4775
118 LiOH			0.1084E-05	0.1109E-05	1.0000	10.3287
119 LiSO4 -			0.2705E-01	0.2767E-01	0.7072	6.7156
120 MgCO3			0.5762E+01	0.5895E+01	1.0000	4.1498
121 MgHCO3 +			0.1460E+02	0.1494E+02	0.6712	3.9243
122 MgF +			0.1203E+01	0.1230E+01	0.6901	4.7020
123 MgOH +			0.3350E+00	0.3427E+00	0.7505	5.2002
124 MgSO4			0.6576E+03	0.6727E+03	1.0000	2.2471
125 MgPO4 -			0.9144E-02	0.9355E-02	0.7199	7.2426
126 MgHP04			0.4051E-01	0.4144E-01	1.0000	6.4571
127 MgH2PO4+			0.1229E-03	0.1257E-03	0.7199	9.1216
128 MnCl +			0.2973E-13	0.3041E-13	0.6712	18.6406
129 MnCl2			0.2387E-10	0.2442E-10	1.0000	15.7065
130 MnCl3 -			0.3916E-09	0.4006E-09	0.6712	14.7724
131 MnCl4 --			0.4181E-08	0.4277E-08	0.2084	14.3383
132 MnHCO3 +			0.5596E-08	0.6747E-08	0.6712	13.4027
133 MnSO4			0.1253E-06	0.1282E-06	1.0000	12.0654
134 MnHP04			0.3146E-10	0.3218E-10	1.0000	15.6655
135 MnOH +			0.9464E-09	0.9682E-09	0.6712	14.0386
136 NO3 -	0.2900	0.2967	0.2900E+00	0.2967E+00	0.8272	5.5171
137 NaCl			0.8443E+03	0.8638E+03	1.0000	1.8247
138 NaCO3 -			0.4721E+01	0.4829E+01	0.7199	4.3723
139 NaHCO3			0.1419E+02	0.1452E+02	1.0000	3.7568
140 Na2CO3			0.1509E-01	0.1544E-01	1.0000	6.8311
141 Na2SO4			0.9519E+03	0.9737E+03	1.0000	2.1583
142 NaSO4 -			0.1877E+03	0.1920E+03	0.7199	2.9295
143 NaHP04 -			0.2589E-02	0.2648E-02	0.7199	7.7896
144 NaF			0.4933E-01	0.5046E-01	1.0000	5.9145
145 NaHS			0.4583E+00	0.4688E+00	1.0000	5.0720
148 PbCl +			0.2822E-11	0.2887E-11	0.6712	17.0920
149 PbCl2			0.2696E-11	0.2758E-11	1.0000	16.9979
150 PbCl3 -			0.7588E-12	0.7762E-12	0.6712	17.7738
151 PbCl4 --			0.5872E-12	0.6007E-12	0.2084	18.4397
152 PbSO4			0.3384E-12	0.3462E-12	1.0000	17.9369
153 MnCl ++			0.6501E-21	0.6650E-21	0.2084	26.8088
154 SrOH -			0.2041E-04	0.2087E-04	0.7072	9.8448
155 SrCO3			0.1286E-01	0.1316E-01	1.0000	7.0444
156 SrHCO3 +			0.6178E-01	0.6320E-01	0.6712	6.5389
157 SrSO4			0.1166E+01	0.1193E+01	1.0000	5.1817
158 ZnCl +			0.1385E-10	0.1417E-10	0.6712	16.0197
159 ZnCl2			0.6812E-11	0.6968E-11	1.0000	16.2856
160 ZnCl3 -			0.2296E-11	0.2349E-11	0.6712	17.0315
161 ZnCl4 --			0.2111E-11	0.2160E-11	0.2084	17.6574

SPECIES	ANALYZED		CALCULATED		ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	PPM	MG/L		
162 ZnSO4			0.5996E-11	0.6134E-11	1.0000	16.4146
165 HgOH +			0.1154E-13	0.1180E-13	0.6712	19.4332
166 Hg(OH)2			0.3371E-08	0.3449E-08	1.0000	13.8271
228 CH3COOH			0.1884E-04	0.1927E-04	1.0000	9.4879
230 BaAce +			0.9328E-07	0.9542E-07	0.6901	12.4689
231 CaAce +			0.7632E-02	0.7808E-02	0.6901	7.2591
232 CuAce +			0.2776E-13	0.2840E-13	0.6901	18.7906
233 FeAce +			0.1712E-12	0.1751E-12	0.6901	17.9724
234 Fe(Ace)2			0.9978E-20	0.1021E-19	1.0000	25.2258
235 KAce			0.2169E-03	0.2219E-03	1.0000	8.6401
236 MgAce +			0.1848E-01	0.1891E-01	0.6901	6.7998
237 NaAce			0.1277E-01	0.1307E-01	1.0000	6.7922
238 PbAce +			0.5512E-16	0.5639E-16	0.6901	21.8296
239 Pb(Ace)2			0.9857E-21	0.1008E-20	1.0000	26.5030
240 Pb(Ace)3			0.1794E-26	0.1835E-26	0.6901	32.4764
241 SrAce +			0.4870E-04	0.4982E-04	0.6901	9.6244
244 ZnAce +			0.1328E-11	0.1359E-11	0.6901	17.1173
245 Zn(Ace)2			0.3291E-21	0.3366E-21	1.0000	26.7307
246 C2O4 --	0.1000	0.1023	0.1070E-01	0.1094E-01	0.2237	7.5501
247 H2C2O4 -			0.3986E-09	0.4078E-09	0.6901	14.4946
248 H2C2O4			0.3629E-13	0.3713E-13	1.0000	18.3791
251 BaOxy			0.6483E-08	0.6632E-08	1.0000	13.5256
252 CaOxy			0.1277E-01	0.1307E-01	1.0000	6.9858
253 FeOxy			0.5935E-12	0.6071E-12	1.0000	17.3690
254 FeOxy +			0.3589E-13	0.3672E-13	0.6901	18.7485
255 KOxy -			0.1596E-03	0.1633E-03	0.6901	9.0468
256 MgOxy			0.9090E-01	0.9299E-01	1.0000	6.0764
257 MnOxy			0.8220E-10	0.8409E-10	1.0000	15.2248
258 MnOxy)2			0.7185E-03	0.7350E-03	0.2237	9.0729
259 MnOxy)3			0.1751E-06	0.1791E-06	0.0021	14.8250
260 MnOxy			0.2438E-19	0.2494E-19	0.6901	24.9138
261 NaOxy -			0.1077E-01	0.1101E-01	0.6901	7.1589
262 PbOxy			0.4059E-15	0.4152E-15	1.0000	20.8462
263 SrOxy			0.3077E-04	0.3147E-04	1.0000	9.7410
264 ZnOxy			0.3518E-13	0.3599E-13	1.0000	18.6239
265 C4H4O4--			0.2200E-05	0.2251E-05	0.2237	6.8871
266 HC4H4O4-			0.6493E-01	0.6642E-01	0.6901	10.8716
267 H2C4H4O4			0.4271E-08	0.4370E-08	1.0000	13.4261
270 BaSuc			0.9456E-07	0.9673E-07	1.0000	12.4126
271 CaSuc			0.7165E-02	0.7329E-02	1.0000	7.3228
272 FeSuc			0.2059E-13	0.2107E-13	1.0000	18.9061
273 FeSuc +			0.5205E-13	0.5325E-13	1.0000	18.6645
274 KSuc -			0.3570E-03	0.3652E-03	0.6901	8.7838
275 MgSuc			0.1988E-01	0.2033E-01	1.0000	6.8335
276 MnSuc			0.6694E-11	0.6848E-11	1.0000	16.3918
277 NaSuc -			0.1559E-01	0.1595E-01	0.6901	7.0959
278 PbSuc			0.1177E-15	0.1204E-15	1.0000	21.4232
279 SrSuc			0.4736E-04	0.4845E-04	1.0000	9.6181
280 ZnSuc			0.6954E-15	0.7114E-15	1.0000	20.4010
281 CaCl +			0.3582E+03	0.3665E+03	0.6712	2.4816
282 CaCl2			0.6796E+01	0.6952E+01	1.0000	4.1975
283 FeF ++			0.1725E-11	0.1765E-11	0.2084	17.3030
284 SiF6 --			0.2147E-28	0.2196E-28	0.2084	34.4865

SPECIES	ANALYZED			CALCULATED			ACTIVITY COEFF.	-LOG10 ACTIVITY
	PPM	MG/L	MOLALITY	PPM	MG/L	MOLALITY		
285 CH ₄ Gas	0.1000	0.1023	0.6460E-05	0.1000E+00	0.1023E+00	0.6460E-05	1.0000	0.0000
286 Pb(HS)2				0.6586E-04	0.6737E-04	0.2497E-09	1.0000	9.6026
287 Pb(HS)3-				0.1170E-06	0.1197E-06	0.3957E-12	0.6712	12.5758
288 PbCO3				0.1745E-10	0.1789E-10	0.6767E-16	1.0000	16.1696
289 PbOH +				0.3078E-10	0.3149E-10	0.1423E-15	0.6712	16.0200
290 Zn(HS)2				0.2774E-04	0.2838E-04	0.2186E-09	1.0000	9.6603
291 Zn(HS)3-				0.1414E-05	0.1447E-05	0.8905E-11	0.6712	11.2235
292 ZnHCO3 +				0.5100E-12	0.5217E-12	0.4182E-17	0.6712	17.5518
293 ZnOH +				0.2166E-11	0.2216E-11	0.2726E-16	0.6712	16.7377
294 Zn(OH)2				0.9555E-13	0.9774E-13	0.9964E-18	1.0000	18.0016
295 ZnHSOH				0.8628E-02	0.8827E-02	0.7746E-07	1.0000	7.1109

SAMPLE IDENT - Test Sample #4 - Ca/Mg exchange in seawater

(TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
2 AKERMANI	34.015	45.460	-11.445	-15.614	122 STCO3	-9.864	-9.270	-0.594	-0.811
11 ANHYDRIT	-5.086	-4.330	-0.756	-1.032	123 SYLVITE	-2.663	0.910	-3.573	-4.874
14 APATCHLR	-47.793	-66.150	18.357	25.043	124 TALC	26.625	21.130	5.495	7.497
15 APATFLUR	-51.853	-68.340	16.487	22.492	125 THENARDI	-3.668	-0.290	-3.378	-4.609
16 APATHYDX	-53.131	-60.390	7.259	9.903	126 TREMOLIT	66.764	60.890	5.874	8.014
17 ARAGONIT	-7.569	-8.340	0.771	1.052	127 TRONA	-9.675	-0.630	-9.045	-12.339
19 AZURITE	-48.374	-39.460	-8.914	-12.160	128 VIVIANIT	-66.156	-36.000	-30.156	-41.140
20 BARITE	-10.196	-9.960	-0.236	-0.322	130 WITHERIT	-12.679	-8.630	-4.049	-5.524
22 BRUCITE	-13.604	-11.470	-2.134	-2.911	131 WOLLASTO	9.815	12.600	-2.785	-3.799
24 CALCITE	-7.569	-8.480	0.911	1.243	133 SILVER	-9.659	-0.500	-9.159	-12.495
25 CELESTIT	-7.382	-6.430	-0.952	-1.298	134 AGCL	-14.683	-9.730	-4.953	-6.757
26 CHALCEDO	-4.130	-3.730	-0.400	-0.545	135 AG2S	-23.973	-36.260	12.287	16.762
30 CRYOTIL	34.877	32.030	2.847	3.883	136 COPPER	-10.069	4.250	-14.319	-19.534
31 C-ENSTAT	10.254	11.290	-1.036	-1.413	137 MALACHIT	-34.407	-33.580	-0.827	-1.128
37 CRISTOBA	-4.130	-3.540	-0.590	-0.805	138 CUO	7.548	7.670	-0.122	-0.167
38 CRISTOBB	-4.130	-2.940	-1.190	-1.623	139 CU2O	-12.874	-1.900	-10.974	-14.971
40 DIOPSIDE	20.070	19.630	0.440	0.600	140 CUS	-4.372	-22.830	18.458	25.182
41 DOLOMITE	-14.699	-18.060	3.361	4.585	141 CU2S	-24.793	-34.950	10.157	13.856
42 DSORD	-14.699	-16.520	1.821	2.484	142 CUFES2	-14.129	-34.070	19.941	27.204
43 ENSTATIT	10.254	11.470	-1.216	-1.658	143 BORNITE	-63.716	-102.510	38.794	52.925
45 FAYALITE	0.194	19.430	-19.236	-26.243	144 FeCl2	-15.151	7.900	-23.051	-31.447
46 FLUORITE	-11.487	-10.960	-0.527	-0.719	145 FeCl3	-20.175	12.340	-32.515	-44.358
47 FORSTERI	24.639	29.070	-4.431	-6.045	146 FeCO3	-19.352	-10.540	-8.812	-12.022
50 GREENALI	-1.791	22.580	-24.371	-33.248	147 FeO	2.162	13.500	-11.338	-15.468
51 GYPSUM	-5.103	-4.600	-0.503	-0.686	148 Fe2O3HEM	11.587	0.040	11.547	15.753
52 HALITE	-0.975	1.590	-2.565	-3.499	149 Fe2O3MCH	11.587	6.400	5.187	7.077
55 HUNTITE	-28.959	-30.620	1.661	2.266	150 Fe3O4	13.749	10.750	2.999	4.091
56 HYDRMAGN	-37.015	-38.530	1.515	2.067	151 Fe(OH)3	-36.189	-37.200	1.011	1.379
57 HYPHILIT	-3.367	11.800	-15.167	-20.692	152 GOETHITE	5.789	0.480	5.309	7.243
60 KENVAITE	-37.788	-25.000	-12.788	-17.446	153 FESPYRHO	-9.758	-3.760	-5.998	-8.182
64 LARNITE	23.760	38.880	-15.120	-20.627	154 FESTROLT	-9.758	-3.870	-5.888	-8.032
67 LIME	-18.833	32.660	-51.493	-70.249	155 FES2PYR	-23.455	-24.710	1.255	1.712
68 MAGADITE	-21.265	-14.340	-6.925	-9.447	156 GREIGITE	-33.929	-45.000	11.071	15.104
69 MgFe2O4	25.971	21.100	4.871	6.466	157 Hg(L)	-14.973	-2.840	-12.133	-16.552
70 MAGNESIT	-7.130	-8.050	0.920	1.255	158 HgCl2(C)	-25.021	-14.110	-10.911	-14.885
71 MgCl2	-2.928	22.150	-25.078	-34.213	160 HgO	-7.709	2.440	-10.149	-13.845
73 MERWINIT	47.959	68.170	-20.211	-27.572	161 CINNABAR	-19.628	-39.860	20.232	27.601
76 MIRABILT	-3.752	-1.090	-2.662	-3.632	162 CINABHET	-19.628	-38.580	18.952	25.855
77 MONTICEL	24.199	30.150	-5.951	-8.118	163 MnCl2	-12.607	8.790	-21.397	-29.190
81 NACHOLIT	-3.507	-0.430	-3.077	-4.197	164 MnCO3	-16.808	-10.540	-6.268	-8.551
82 NATRTHRM	-6.159	-0.010	-6.149	-8.389	165 MnO	4.706	17.700	-12.994	-17.727
83 NATRON	-6.235	-0.880	-5.355	-7.305	166 MnO2	-13.470	-8.330	-5.140	-7.012
85 NESQUEHON	-7.155	-5.350	-1.805	-2.462	167 MnS	-7.213	-0.470	-6.743	-9.200
91 OLDHAMIT	2.026	11.900	-9.874	-13.471	168 PbCl2	-18.968	-4.820	-14.148	-19.301
95 PERICLAS	14.384	21.510	-7.126	-9.721	169 PbCO3	-23.170	-12.890	-10.280	-14.024
99 PORTLAN	-14.043	-5.420	-8.623	-11.764	170 PbOLITHR	-1.655	12.550	-14.205	-19.380
100 POTASSI	11.987	84.120	-72.133	-98.406	171 PbOMASIC	-1.655	12.690	-14.345	-19.571
103 QUARTZ	-4.130	-3.930	-0.200	-0.273	172 PbS GALN	-13.575	-14.780	1.205	1.644
110 SEPIOLIT	32.700	31.520	1.180	1.609	173 PbSO4	-20.687	-7.800	-12.887	-17.581
111 SILICAAM	-4.130	-2.700	-1.430	-1.951	174 ZnCO3	-21.107	-9.870	-11.237	-15.330
112 SILICEL	-4.130	-2.710	-1.420	-1.937	175 ZnO	0.407	11.200	-10.793	-14.725

SAMPLE IDENT - Test Sample #4 - Ca/Mg exchange in seawater

(TEMPERATURE = 25.00)

PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG	PHASE	LOG (AP)	LOG (KT)	LOG (AP/KT)	DELG
118 Na2O	15.363	67.430	-52.067	-71.032	176 ZnS	-11.513	-11.790	0.277	0.378
121 STRENGIT	-30.510	-27.200	-3.310	-4.516	177 ZnSO4	-18.625	3.540	-22.165	-30.238

APPENDIX IV. Listing of SOLMINEQ.88

PROGRAM SOLMIN	SOL 0010
=====	SOL 0020
Program SOLMINEQ.88 : SOLution-MINeral EQUilibrium 1/11/89 JDD	SOL 0030
	SOL 0040
Written by: P.K. Aggarwal (now at Battelle)	SOL 0050
J.D. DeBraal (U.S. Geological Survey)	SOL 0060
W.D. Gunter (Alberta Research Council)	SOL 0070
R.W. Hull (U.S. Geological Survey)	SOL 0080
Y.K. Kharaka (U.S. Geological Survey)	SOL 0090
E.H. Perkins (Alberta Research Council)	SOL 0100
D.J. Specht (U.S. Geological Survey)	SOL 0110
	SOL 0120
SOLMINEQ.88 is based on SOLMNEQ (Kharaka and Barnes, 1973),	SOL 0130
SOLMNEQF (Aggarwal and others, 1986), and many other unpublished	SOL 0140
versions.	SOL 0150
	SOL 0160
This version has been extensively re-written and modified by	SOL 0170
E.H. Perkins. The input format was redesigned in conjunction	SOL 0180
with W.D. Gunter and Y.K. Kharaka; these changes were	SOL 0190
implemented by J.D. DeBraal.	SOL 0200
	SOL 0210
Financial support for designing SOLMINEQ.88 was provided by	SOL 0220
Brian Hitchon (Alberta Geological Survey) and by the Oil Sands	SOL 0230
and Hydrocarbon Recovery department, Alberta Research Council.	SOL 0240
	SOL 0250
Input/output units:	SOL 0260
5: Sample input file	SOL 0270
6: Output from solmineq.88	SOL 0280
7: Data file for Pitzer's equations	SOL 0290
10: Main data file for solmineq.88	SOL 0300
12: Data file for dissolution reactions of the minerals	SOL 0310
	SOL 0320
Routines and their purpose	SOL 0330
	SOL 0340
ACTIVE : Calculate and print activity products of minerals	SOL 0350
ADSORB : Routine for calculating surface adsorption	SOL 0360
and ion exchange	SOL 0370
AITLIM : Determines the maximum stepsize for convergence on the	SOL 0380
anions	SOL 0390
CALCUL : Calculate analyzed molality, cation-anion balance,	SOL 0400
stoichiometric ionic strength, activity coefficients	SOL 0410
of neutral species, temperature effects on debye-huckel	SOL 0420
constants, and bdot.	SOL 0430
CO2OPT : Routine for titrating co2 to a given criterion	SOL 0440
(pH, pco2, m(h2co3), or saturation with calcite,	SOL 0450
siderite, or dolomite)	SOL 0460
DISTRB : Calculate the distribution of species	SOL 0470
DPVT : Calculate the vapor pressure and vapor density	SOL 0480
GASES : Routine for partitioning of a gas phase (co2/ch4)	SOL 0490
Between liquid, oil, and vapor	SOL 0500
GUESS : Routine for calculating the root of a function which	SOL 0510
is known to change sign in a given interval	SOL 0520
INPUT : Read sample input file from unit 5	SOL 0530
INTIAL : Initialize several variable to 0.0 or default values	SOL 0540
LAGINT : Calculate logk values for aqueous complexes and	SOL 0550
minerals at the desired temperature (t)	SOL 0560

C	MIXER	:	Routine for precipitation/dissolution, mixing, boiling	SOL 0570
C	NACALC	:	Calculate the osmotic coefficient of NaCl (aq) and	SOL 0580
C			pure water	SOL 0590
C	PAGE	:	Keeps track of output paging	SOL 0600
C	PCLOGK	:	Calculate the effect of pressure on logk if pressure	SOL 0610
C			is greater than ph2o	SOL 0620
C	PHCALC	:	Routine for calculating pH at a higher temperature	SOL 0630
C	PHOPT	:	Routine for the pH option (adjust pH to saturation	SOL 0640
C			with calcite or siderite or dolomite)	SOL 0650
C	PITZER	:	Calculate the activity of aqueous species and the	SOL 0660
C			osmotic coefficient based up the pitzer ion pairing	SOL 0670
C			model	SOL 0680
C	POLY	:	Solves the cubic equation which describes the	SOL 0690
C			partitioning between gas, oil, and water.	SOL 0700
C	PRATIO	:	Print mole ratio, log of activity ratio, and	SOL 0710
C			calculated subsurface temperatures	SOL 0720
C	PRINTR	:	Print calculated distribution of species	SOL 0730
C	PRNTAB	:	Print the calculated values of aqueous log k	SOL 0740
C	PSAT	:	Calculate the vapor saturated pressure of water (ph2o)	SOL 0750
C			at temperature t	SOL 0760
C	PTZINT	:	Calculate the parameters for the pitzer equation as a	SOL 0770
C			function of temperature	SOL 0780
C	SORTA	:	Sorts arrays	SOL 0790
C	STORE	:	Creates the restart file	SOL 0800
C	TABLES	:	Read main data file from unit 10	SOL 0810
C	WAPVT	:	Calculate the properties of pure water	SOL 0820
C	WDBP	:	Calculate the dielectric properties of water	SOL 0830
C				SOL 0840
C	Functions			SOL 0850
C				SOL 0860
C	ATCPRD	:	Calculates the activity product of a mineral	SOL 0870
C	DEBYE	:	Determines the value of an unknown ion size parameter	SOL 0880
C	GETUNT	:	Return the unit number of a file	SOL 0890
C	KHCH4	:	Calculate the Henry's law constant for CH4	SOL 0900
C	KHCO2	:	Calculate the Henry's law constant for CO2	SOL 0910
C	KHH2S	:	Calculate the Henry's law constant for H2S	SOL 0920
C	KHNH3	:	Calculate the Henry's law constant for NH3	SOL 0930
C	LENGTH	:	Determines the length of a character string	SOL 0940
C	SEXP10	:	Substitute exponetial function	SOL 0950
C	SLOG10	:	Substitute common log function	SOL 0960
C				SOL 0970
C	Declare constants			SOL 0980
C				SOL 0990
C	CPUMAX	DBL	Largest positive real value program uses	SOL 1000
C	CPUMIN	DBL	Smallest positive real value program uses	SOL 1010
C	NMAX	INT	General array dimension to allow easy expansion	SOL 1020
C	UNI	INT	File unit assigned for input file	SOL 1030
C	UNO	INT	File unit assigned for output file	SOL 1040
C				SOL 1050
C	INTEGER NMAX, UNI, UNO			SOL 1060
C	DOUBLE PRECISION CPUMAX, CPUMIN			SOL 1070
C	PARAMETER (NMAX = 340, UNI = 5, UNO = 6)			SOL 1080
C	PARAMETER (CPUMAX = 1.0D+35, CPUMIN = 1.0D-35)			SOL 1090
C				SOL 1100
C				SOL 1110
C	Declare variables			SOL 1120
C				SOL 1130
C	A	DBL	Molal Debye-Huckel coefficient	SOL 1140

C	ALMIX	DBL	HTOT, OHTOT, and TIC for comp 1 of a mixture	SOL 1150
C	ADENS	DBL	Density of solution A	SOL 1160
C	ADEX	INT	Flag for surface chemistry option	SOL 1170
C	AHI	DBL	Pressure correction fit parameter	SOL 1180
C	ALFA	DBL	Activity of aqueous species i	SOL 1190
C	ALK	INT	Flag for distribution of carbonate species	SOL 1200
C	ALOW	DBL	Pressure correction fit parameter	SOL 1210
C	AMOL	DBL	Molality of aqueous/mineral species added	SOL 1220
C	ANALM	DBL	Analyzed molality of species i	SOL 1230
C	ANMMIX	DBL	Analyzed molality of species i in solution A	SOL 1240
C	ANMTIC	DBL	Analysed TIC	SOL 1250
C	ATEMP	DBL	Temperature of solution A	SOL 1260
C	B	DBL	Molal Debye-Huckel coefficient	SOL 1270
C	B2MIX	DBL	HTOT, OHTOT, and TIC for comp 1 of a mixture	SOL 1280
C	BDAT	DBL	B-dot as a function of temperature	SOL 1290
C	BDENS	DBL	Density of solution B	SOL 1300
C	BDOT	DBL	Activity coefficient deviation function	SOL 1310
C	BHI	DBL	Pressure correction fit parameter	SOL 1320
C	BLOW	DBL	Pressure correction fit parameter	SOL 1330
C	BNMMIX	DBL	Analyzed molality of species i in solution B	SOL 1340
C	BTEMP	DBL	Temperature of solution B	SOL 1350
C	BUFFER	CHA	Used for memory/memory writes	SOL 1360
C	CEC	DBL	Cation exchange capacity	SOL 1370
C	CHI	DBL	Pressure correction fit parameter	SOL 1380
C	CLOW	DBL	Pressure correction fit parameter	SOL 1390
C	CO2F	DBL	Sum of CO2 plus CO2 lost from solution	SOL 1400
C	COEF	DBL	Stoichiometric coefficient and Id number	SOL 1410
C	CONV1	DBL	Tolerance factor for convergence of anions	SOL 1420
C	CONV2	DBL	Tolerance factor for hydronium mass-balance	SOL 1430
C	CR	CHA	Inserts carriage returns in output	SOL 1440
C	CUNITS	DBL	Analytical input concentration	SOL 1450
C	DCH4	DBL	Used to add/remove CH4 from water	SOL 1460
C	DDCH4	DBL	Concentration of CH4 lost before pH measurement	SOL 1470
C	DCO2	DBL	Used to add/remove CO2 from water	SOL 1480
C	DDCO2	DBL	Concentration of CO2 lost before pH measurement	SOL 1490
C	DH2S	DBL	Used to add/remove H2S from Water	SOL 1500
C	DDH2S	DBL	Concentration of H2S lost before pH measurement	SOL 1510
C	DNH3	DBL	Used to add/remove NH3 from water	SOL 1520
C	DDNH3	DBL	Concentration of NH3 lost before pH measurement	SOL 1530
C	DELVR	DBL	Change in volume at 25 degrees	SOL 1540
C	DENS	DBL	Density	SOL 1550
C	DFRAC1	DBL	Smallest fraction of soln 1 mixed with soln 2	SOL 1560
C	DHA	DBL	Ion size parameter	SOL 1570
C	DINC	DBL	Increment of solution 1 to be added	SOL 1580
C	DNS	CHA	Determines if density should be calculated	SOL 1590
C	DP	DBL	Dissolution/precipitation switch	SOL 1600
C	DSEP	DBL	Density of oil at 15 degree C	SOL 1610
C	EHM	DBL	Measured Eh in volts	SOL 1620
C	EHMC	DBL	Measured Eh using the Calomel electrode	SOL 1630
C	EMFZSC	DBL	Measured Eh using the Zobell's solution	SOL 1640
C	EXELT	DBL	Total moles of component.	SOL 1650
C	FBOIL	DBL	Fraction of solution boiled-off as steam	SOL 1660
C	FCCSAT	DBL	Tolerance factor for pH and CO2 options	SOL 1670
C	FILEIN	CHA	Name of input file	SOL 1680
C	FILEOT	CHA	Name of output file	SOL 1690
C	FIXIT	DBL	Fixing value in the CO2 option	SOL 1700
C	FLAGS	INT	Selection flags for calculation of redox equil.	SOL 1710
C	FMIX	DBL	Stores fraction of mixing	SOL 1720

C	GAMMA	DBL	Activity coefficient	SOL 1730
C	GEOTH	INT	Flag to select geothermometer	SOL 1740
C	GFW	DBL	Gram formula weight of aqueous species	SOL 1750
C	HITEMP	DBL	In-situ temperature	SOL 1760
C	HTOT	DBL	Current sum of all H+ in solution	SOL 1770
C	HTOTI	DBL	Target sum of all H+ in solution	SOL 1780
C	I	INT	Loop variable/counter	SOL 1790
C	IACT	INT	Switch for printing activity ratios	SOL 1800
C	IADJ	INT	Has HITEMP been calculated or not	SOL 1810
C	IBMIX	INT	Switch for mixing option	SOL 1820
C	ICALL	INT	Loop variable	SOL 1830
C	ICCSAT	INT	Switch for pH option	SOL 1840
C	ICO2	INT	Switch for CO2 option	SOL 1850
C	IDDP	INT	Id number of the mineral to be dissolved/ppt	SOL 1860
C	IDMIX	INT	Id number of the aqueous species to be added	SOL 1870
C	IDN	INT	Id numbers of the ISCOMP components adsorption	SOL 1880
C	IDSAT	INT	Id number of the mineral to be equilibrated	SOL 1890
C	IEXCH	INT	Switch for adsorption/ion exchange	SOL 1900
C	IGAS	INT	Loop variable for gas option	SOL 1910
C	ILO	INT	Lower limit for index for low/high T log K's	SOL 1920
C	IMAX	INT	Max number of iterations for various options	SOL 1930
C	IMCO3	INT	Selects CO2 option	SOL 1940
C	IMIX	INT	Switch used in MIXER routines	SOL 1950
C	INFORM	INT	Flag to print all the log K values in data base	SOL 1960
C	INMIX	INT	Total number of mixtures of two solution mixed	SOL 1970
C	INSP	INT	Total number of surface sites for adsorption	SOL 1980
C	IOPT	INT	Switch for CO2 option	SOL 1990
C	IPAGE	INT	Current page number of output file	SOL 2000
C	IPGLN	INT	Current line number of the output file	SOL 2010
C	IPHASE	INT	Switch used for GAS options	SOL 2020
C	IPHNUM	INT	Counter used in PHCALC	SOL 2030
C	IPIT	INT	Flag to use pitzer activity coefficients	SOL 2040
C	IPRIN1	INT	Flag for printing iteration of anions	SOL 2050
C	IPRIN2	INT	Flag for printing hydronium balance	SOL 2060
C	IRUN	INT	Keeps track of the number of runs completed	SOL 2070
C	IRXDP	INT	Id number of the aqueous species to be added	SOL 2080
C	ISALT	INT	Switch used in mixer to indicate option	SOL 2090
C	ISAT	INT	Counter used in co2opt	SOL 2100
C	ISCHG	INT	Charge of each surface site for adsorption	SOL 2110
C	ISCOMP	INT	Total number of components in dissociation	SOL 2120
C	ITIC	INT	Hitemp distribution of carbonate species	SOL 2130
C	ITMIX	INT	Switch for the mineral saturation option	SOL 2140
C	ITWR	INT	Switch to control printing of some headings	SOL 2150
C	J	INT	Loop counter	SOL 2160
C	JCCST	INT	Switch indicating if phopt called 1st time	SOL 2170
C	JCO3	INT	Switch to control printing of some headings	SOL 2180
C	JMIXTR	INT	Counter for maximum number of mixtures	SOL 2190
C	KCH4OL	DBL	Henry's law coefficient for CH4 in oil	SOL 2200
C	KCO2OL	DBL	Henry's law coefficient for CO2 in oil	SOL 2210
C	KH2SOL	DBL	Henry's law coefficient for H2S in oil	SOL 2220
C	KRXN	DBL	K for dissociation reaction of surface species	SOL 2230
C	KT1	DBL	Equilibrium constant of the aqueous reactions	SOL 2240
C	LKT1	DBL	Log K for aqueous species with temperature	SOL 2250
C	LKT2	DBL	Log K for minerals with temperature	SOL 2260
C	LOGKT1	DBL	Log K for aqueous species at specified temp.	SOL 2270
C	LOGKT2	DBL	Log K for minerals at specified temperature	SOL 2280
C	M	DBL	Calculated molality of aqueous species	SOL 2290
C	MBASE	DBL	Equivalence Mole Fraction (initial) on surface	SOL 2300

C	MINCO	DBL	Stoichiometric coefficient for added minerals	SOL 2310
C	MININD	INT	Index number of the added mineral	SOL 2320
C	MINLOG	DBL	Log K values for added minerals	SOL 2330
C	MNACLD	DBL	Sum of Molality * charge / 2	SOL 2340
C	MU	DBL	Ionic strength of aqueous solution	SOL 2350
C	MXAQK	INT	Total number of aqueous log k values	SOL 2360
C	MXMNK	INT	Total number of mineral log k values	SOL 2370
C	MXPC	INT	Total number of mineral pressure constants	SOL 2380
C	MXSP	INT	Total number of aqueous species	SOL 2390
C	NDUM	INT	Id of mineral/aqueous complex with K(T) changed	SOL 2400
C	NH2O	DBL	Number of water ionization reactions	SOL 2410
C	NUFLAG	INT	Sets the activity coefficients of neutral species	SOL 2420
C	ODUM	CHA	Switch to indicate a mineral/aqueous complex	SOL 2430
C	OHTOT	DBL	Current sum of all OH- in solution	SOL 2440
C	OHTOTI	DBL	Target sum of all OH- in solution	SOL 2450
C	OK	INT	Error flag for Lagrange interpolation routine	SOL 2460
C	OUTIN	CHA	Name of restart file name	SOL 2470
C	PAGE1	CHA	Names of aqueous species	SOL 2480
C	PAGE2	CHA	Names of equilibrium constants	SOL 2490
C	PAGE3	CHA	Names of solubility constants	SOL 2500
C	PCO2	DBL	Partial pressure of CO2	SOL 2510
C	PH	DBL	Measured pH of the solution	SOL 2520
C	PH2O	DBL	Partial pressure of H2O	SOL 2530
C	PHHIT	INT	Hitemp switch, used to control phcalc	SOL 2540
C	PPHHIT	INT	Switch to control calling phcalc	SOL 2550
C	PRESS	DBL	Total pressure	SOL 2560
C	RATIO	INT	Flag for printing activity ratios of elements	SOL 2570
C	RXDP	DBL	Molal amount of the aqueous species added	SOL 2580
C	SAREA	DBL	Total surface area per kilogram of solvent	SOL 2590
C	SCO2	DBL	Sum of CO2 species	SOL 2600
C	SPN	CHA	Name of each surface species adsorption	SOL 2610
C	TAREA	DBL	Site density per unit area	SOL 2620
C	TCH4M	DBL	Moles CH4 distributed between oil, water, vapor	SOL 2630
C	TCO2	DBL	Activity coefficients of CO2 with temperature	SOL 2640
C	TCO2M	DBL	Moles CO2 distributed between oil, water, vapor	SOL 2650
C	TDS	DBL	Total Dissolved Solids (UNITS = KG/L)	SOL 2660
C	TEMP	DBL	Temperature of the solution when pH was measured	SOL 2670
C	TH2SM	DBL	Moles H2S distributed between oil, water, vapor	SOL 2680
C	TIC	DBL	Concentration of total inorganic carbon	SOL 2690
C	TIT1	CHA	Name of solution A	SOL 2700
C	TIT2	CHA	Name of solution B	SOL 2710
C	TITLE	CHA	Name of the sample	SOL 2720
C	TITMIX	CHA	Title for mixtures	SOL 2730
C	TITR	DBL	Iteration array in DISTRB, used for guesses	SOL 2740
C	TK	DBL	Temperature steps used by program	SOL 2750
C	TOF	CHA	Places a form feed in output file	SOL 2760
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	SOL 2770
C	UNITS	CHA	Units of concentration	SOL 2780
C	UNM	INT	File unit connected the external mixing file	SOL 2790
C	WROIL	DBL	Oil to water weight ratio	SOL 2800
C	XD	DBL	Holds Log K's for additional anions & cations	SOL 2810
C	XDUM	DBL	New log K(T) value	SOL 2820
C	Y28	INT	Set at hitemp to skip unneeded calculations	SOL 2830
C	Z	INT	Charge of aqueous species	SOL 2840
C	-----			SOL 2850
	INTEGER ALK, ANS1, ANS2, FLAGS(6), GEOTH			SOL 2860
	INTEGER I, IACT, IADJ, IBMIX, ICALL, ICCSAT, ICO2, IDDP			SOL 2870
	INTEGER IDMIX(50), IDN(10,10), IDONE, IDSAT			SOL 2880

INTEGER IEXCH, IGAS, ILO, IMAX, IMCO3, IMIX, INFORM, INMIX, INSP	SOL 2890
INTEGER IOPT, IPAGE, IPGLN, IPHASE, IPHNUM, IPIT, IPRIN1, IPRIN2	SOL 2900
INTEGER IRUN, IRXDP(10), ISALT, ISAT, ISCHG(10), ISCOMP(10)	SOL 2910
INTEGER ITIC, ITMIX, ITT, ITWR, J, JCCST, JCO3, JMIXTR, LEN	SOL 2920
INTEGER LENGTH, MININD(8,5), MIXFLG, MXAQK, MXMNK, MXPC, MXSP	SOL 2930
INTEGER NDUM(12), NUFLAG, NUM, NUMCOM, NUMINS, OK, PHHIT, PPHIT	SOL 2940
INTEGER RATIO, UNM, Y28, Z(NMAX)	SOL 2950
	SOL 2960
CHARACTER*1 ADEX, CR, DNS, ODUM(12), TOF	SOL 2970
CHARACTER*5 UNITS	SOL 2980
CHARACTER*8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)	SOL 2990
CHARACTER*10 SPN(10)	SOL 3000
CHARACTER*32 TIT1, TIT2	SOL 3010
CHARACTER*40 TITMIX	SOL 3020
CHARACTER*80 ANS, BUFFER, FILEIN, FILEOT, MIXFLE, OUTIN, TITLE	SOL 3030
	SOL 3040
DOUBLE PRECISION A, A1MIX(5), ADENS, AHI(200), ALFA(NMAX)	SOL 3050
DOUBLE PRECISION ALOW(200), AMOL(50), ANALM(NMAX), ANMMIX(NMAX)	SOL 3060
DOUBLE PRECISION ANMTIC, ATEMP, B, B2MIX(5), BDAT(10), BDENS, BDOTS	SOL 3070
DOUBLE PRECISION BHI(200), BLOW(200), BNMMIX(NMAX), BTEMP	SOL 3080
DOUBLE PRECISION CEC, CHI(200), CLOW(200), CO2F	SOL 3090
DOUBLE PRECISION COEF(10,10), CONV1, CONV2	SOL 3100
DOUBLE PRECISION CUNITS(NMAX), DCH4, DCO2, DDCH4, DDCO2, DDH2S	SOL 3110
DOUBLE PRECISION DDNH3, DELVR(NMAX), DENS, DFRAC1, DH2S	SOL 3120
DOUBLE PRECISION DHA(NMAX), DINC, DNH3, DP	SOL 3130
DOUBLE PRECISION EHM, EPMC, EMFZSC, EXELT(35)	SOL 3140
DOUBLE PRECISION FBOIL, FCCSAT, FIXIT, FMIX(10)	SOL 3150
DOUBLE PRECISION GAMMA(NMAX), GFW(NMAX), HITEMP, HTOT, HTOTI	SOL 3160
DOUBLE PRECISION KCH4OL, KCO2OL, KH2SOL, KRXX(10)	SOL 3170
DOUBLE PRECISION KT1(NMAX)	SOL 3180
DOUBLE PRECISION LKT1(NMAX,11), LKT2(NMAX,11)	SOL 3190
DOUBLE PRECISION LOGKT1(NMAX), LOGKT2(NMAX), M(NMAX)	SOL 3200
DOUBLE PRECISION MBASE(10), MINCO(9,5), MINLOG(2,5)	SOL 3210
DOUBLE PRECISION MNACLD, MU, NH2O(NMAX), OHTOT, OHTOTI	SOL 3220
DOUBLE PRECISION PCO2, PH, PH2O, PRESS, DSEP, RXDP(10)	SOL 3230
DOUBLE PRECISION SAREA, SCO2	SOL 3240
DOUBLE PRECISION TAREA, TCH4M, TCO2(10), TCO2M, TDS, TEMP	SOL 3250
DOUBLE PRECISION TH2SM, TIC, TITR(11), TK(11), TOTEL(5)	SOL 3260
DOUBLE PRECISION WROIL, XD(2,45), XDUM(12)	SOL 3270
	SOL 3280
EXTERNAL ACTIVE, ADSORB, CALCUL, CO2OPT, DISTRB, GASES, INPUT	SOL 3290
EXTERNAL INTIAL, LENGTH, MIXER, PHCALC, PHOPT, PRATIO, PRINTR	SOL 3300
EXTERNAL PRNTAB, PSAT, PCLOCK, STORE, TABLES, LAGINT, PAGE	SOL 3310
	SOL 3320
INTRINSIC DABS, DLOG10, INDEX	SOL 3330
	SOL 3340
COMMON /AL / NDUM, XDUM	SOL 3350
COMMON /ALOGK / LOGKT1, LOGKT2	SOL 3360
COMMON /AMM / IDMIX, AMOL, ITMIX, INMIX, DFRAC1, DINC, FBOIL	SOL 3370
COMMON /BASIC / DENS, PRESS, EHM, EPMC, EMFZSC, TIC, FCCSAT, XD,	SOL 3380
NUMCOM, NUMINS, MINLOG, MINCO, MININD, CONV1,	SOL 3390
CONV2	SOL 3400
COMMON /CH / ODUM	SOL 3410
COMMON /DIST / TCO2M, TCH4M, TH2SM, WROIL, KCH4OL, KCO2OL,	SOL 3420
KH2SOL, IPHASE, DSEP	SOL 3430
COMMON /EXCHAN/ COEF, MBASE, KRXX, CEC, TAREA,	SOL 3440
SAREA, IDN, ISCHG, ISCOMP, INSP	SOL 3450
COMMON /EXTOT / EXELT, TOTEL, TITR	SOL 3460

COMMON /FLAGCM/	ALK, ITIC, ICCSAT, IMCO3, ITT, ANS1, ANS2,	SOL 3470
	NUFLAG, IPIT, FLAGS, INFORM, RATIO, GEOTH,	SOL 3480
	IPRIN1, IPRIN2	SOL 3490
COMMON /FMFD /	TOF, CR, TITMIX	SOL 3500
COMMON /FORM /	IPAGE, IPGLN	SOL 3510
COMMON /GAS /	DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,	SOL 3520
	DCH4, DDCH4, IOPT, FIXIT	SOL 3530
COMMON /IMM /	IBMIX, IMIX	SOL 3540
COMMON /KK /	LKT1, LKT2	SOL 3550
COMMON /MM /	ANMMIX, ALMIX, B2MIX, FMIX, BNMMIX, ADENS, BDENS,	SOL 3560
	ATEMP, BTEMP	SOL 3570
COMMON /MOLS /	PH, ANALM, M, ALFA, CUNITS	SOL 3580
COMMON /NAMES1/	PAGE1, PAGE2, PAGE3	SOL 3590
COMMON /NAMES2/	SPN	SOL 3600
COMMON /NAMES3/	MIXFLE, OUTIN, TITLE, UNITS, ADEX	SOL 3610
COMMON /PTK /	DELVR, NH2O, ALOW, BLOW, CLOW, AHI, BHI, CHI	SOL 3620
COMMON /SAT/	IDDP, IDSAT, DP, RXDP, IRXDP	SOL 3630
COMMON /TABCOM/	MXSP, MXMNK, GFW, Z, DHA	SOL 3640
COMMON /TOTALS/	CO2F, HTOTI, OHTOTI	SOL 3650
COMMON /TTK /	KT1	SOL 3660
COMMON /ZPH /	PHHIT, PPHIT, JCO3, SCO2, HTOT, OHTOT	SOL 3670
C =====		SOL 3680
		SOL 3690
C -----		SOL 3700
C	The following open statements have been commented out by	SOL 3710
C	Ernie Perkins (ORSD, ARC) in order to allow a command	SOL 3720
C	proceedure under VMS 4.5 on DEC VAX's to assign the files	SOL 3730
C	external to the program.	SOL 3740
C		SOL 3750
	PRINT *, ' ENTER THE NAME OF THE SAMPLE INPUT FILE ?'	SOL 3760
	PRINT *, ' Default = [SOLMINEQ.IN]'	SOL 3770
	READ '(A)', FILEIN	SOL 3780
	IF (FILEIN .EQ. ' ') FILEIN = 'SOLMINEQ.IN'	SOL 3790
		SOL 3800
	NUM = INDEX (FILEIN, '.')	SOL 3810
		SOL 3820
	IF (NUM .EQ. 0) THEN	SOL 3830
	NUM = LENGTH(FILEIN)	SOL 3840
	FILEOT = FILEIN(1:NUM) // '.OUT'	SOL 3850
	ELSE	SOL 3860
	FILEOT = FILEIN(1:NUM) // 'OUT'	SOL 3870
	END IF	SOL 3880
		SOL 3890
	LEN = LENGTH(FILEOT)	SOL 3900
		SOL 3910
	PRINT *, ' ENTER THE NAME OF THE OUTPUT FILE ?'	SOL 3920
	PRINT '(1X, A, A, A)', ' Default = [', FILEOT(1:LEN), ']'	SOL 3930
	READ '(A)', ANS	SOL 3940
	IF (ANS .NE. ' ') FILEOT = ANS	SOL 3950
		SOL 3960
	OPEN (UNIT=UNI, FILE = FILEIN, STATUS = 'OLD')	SOL 3970
	OPEN (UNIT=UNO, FILE = FILEOT, STATUS = 'UNKNOWN')	SOL 3980
C -----		SOL 3990
		SOL 4000
	TOF = '1'	SOL 4010
	CR = '+'	SOL 4020
		SOL 4030
		SOL 4040

MIXFLG = 0	SOL 4050
IRUN = 0	SOL 4060
IPGLN = 0	SOL 4070
IPAGE = 0	SOL 4080
	SOL 4090
DO 10 I = 1, NMAX	SOL 4100
PAGE1(I) = ' '	SOL 4110
GFW(I) = 0.0	SOL 4120
DHA(I) = 0.0	SOL 4130
Z(I) = 0	SOL 4140
10 CONTINUE	SOL 4150
	SOL 4160
C -----	SOL 4170
C Read the data base on unit 10	SOL 4180
C -----	SOL 4190
CALL TABLES (MXAQK, BDAT, TK, TCO2, MXPC)	SOL 4200
	SOL 4210
	SOL 4220
C -----	SOL 4230
C Initialize values for each new sample input	SOL 4240
C -----	SOL 4250
	SOL 4260
20 CONTINUE	SOL 4270
ICALL = 0	SOL 4280
ISALT = 0	SOL 4290
IMIX = 0	SOL 4300
IBMIX = 0	SOL 4310
JMXTR = 0	SOL 4320
INMIX = 0	SOL 4330
TITMIX = ' '	SOL 4340
	SOL 4350
CALL INTIAL (OK, ALK, INFORM, RATIO, GAMMA, TEMP, HITEMP, PRESS,	SOL 4360
HTOTI, OHTOTI, ICO2, IMCO3, IBMIX, FCCSAT, IEXCH,	SOL 4370
ISAT, IPHNUM, JCCST)	SOL 4380
	SOL 4390
C -----	SOL 4400
C Read one data set from the input file on unit 5	SOL 4410
C -----	SOL 4420
CALL INPUT (UNI, TEMP, HITEMP, DNS, PHHIT, IEXCH, ICO2, MIXFLG)	SOL 4440
	SOL 4450
ILO = 1	SOL 4460
	SOL 4470
C -----	SOL 4480
C Compute aqueous LOGKT'S at the desired temperature	SOL 4490
C -----	SOL 4500
	SOL 4510
30 CONTINUE	SOL 4520
CALL LAGINT (TK, LKT1, TEMP, LOGKT1, MXAQK, NMAX, OK)	SOL 4530
	SOL 4540
C -----	SOL 4550
C If the sample "TEMP" is within the range from 0-350 degrees	SOL 4560
C then continue, otherwise get the next data set or stop.	SOL 4570
C -----	SOL 4580
	SOL 4590
IF (OK .NE. 1) THEN	SOL 4600
CALL STORE (TEMP, HITEMP)	SOL 4610
GO TO 20	SOL 4620

END IF	SOL 4630
	SOL 4640
C -----	SOL 4650
C Compute mineral LOGKT'S at the desired temperature.	SOL 4660
C -----	SOL 4670
CALL LAGINT (TK, LKT2, TEMP, LOGKT2, MXMNK, NMAX, OK)	SOL 4680
	SOL 4690
	SOL 4700
C -----	SOL 4710
C Calculate the saturation pressure of H2O	SOL 4720
C -----	SOL 4730
CALL PSAT (TEMP, PH2O)	SOL 4740
	SOL 4750
	SOL 4760
	SOL 4770
C -----	SOL 4780
C If input pressure is greater than PH2O, the logkt of	SOL 4790
C aqueous species are adjusted using the "density model" of mesmer.	SOL 4800
C If hitemp is > 0, adjustment of logkt is done only at hitemp.	SOL 4810
C -----	SOL 4820
IADJ = 0	SOL 4830
IF (PHHIT .EQ. 1) THEN	SOL 4840
IF (DABS(HITEMP - TEMP) .LT. CPUMIN) THEN	SOL 4850
ILO = 7	SOL 4860
ELSE	SOL 4870
IADJ = 1	SOL 4880
END IF	SOL 4890
END IF	SOL 4900
	SOL 4910
	SOL 4920
C -----	SOL 4930
C Replace some of the logkt's that were read in input	SOL 4940
C -----	SOL 4950
DO 40 I = ILO, (ILO + 5)	SOL 4960
IF (NDUM(I) .GT. 0) THEN	SOL 4970
IF (ODUM(I).EQ.'A') THEN	SOL 4980
LOGKT1(NDUM(I)) = XDUM(I)	SOL 4990
ELSE IF (ODUM(I).EQ.'M') THEN	SOL 5000
LOGKT2(NDUM(I)) = XDUM(I)	SOL 5010
END IF	SOL 5020
END IF	SOL 5030
40 CONTINUE	SOL 5040
	SOL 5050
	SOL 5060
DO 50 I = 2, 15	SOL 5070
IF (DABS(HITEMP - TEMP) .LT. CPUMIN) THEN	SOL 5080
LOGKT1(MXAQK+I- 1) = XD(2,I)	SOL 5090
LOGKT1(MXAQK+I+13) = XD(2,I+15)	SOL 5100
LOGKT1(MXAQK+I+27) = XD(2,I+30)	SOL 5110
ELSE	SOL 5120
LOGKT1(MXAQK+I- 1) = XD(1,I)	SOL 5130
LOGKT1(MXAQK+I+13) = XD(1,I+15)	SOL 5140
LOGKT1(MXAQK+I+27) = XD(1,I+30)	SOL 5150
END IF	SOL 5160
50 CONTINUE	SOL 5170
	SOL 5180
DO 60 I = 1, 5	SOL 5190
IF (DABS(HITEMP - TEMP) .LT. CPUMIN) THEN	SOL 5200

LOGKT2(MXMNK+I) = MINLOG(2,I)	SOL 5210
ELSE	SOL 5220
LOGKT2(MXMNK+I) = MINLOG(1,I)	SOL 5230
END IF	SOL 5240
60 CONTINUE	SOL 5250
	SOL 5260
C -----	SOL 5270
C Adjust aqueous logkts for the pressure difference (press - ph2o)	SOL 5280
C -----	SOL 5290
	SOL 5300
IF (IADJ .EQ. 0 .AND. PRESS .GT. PH2O .AND. PRESS .GT. 1.0D00)	SOL 5310
CALL PCLOGK (TEMP, PH2O, PRESS, MXAQK, MXPC)	SOL 5320
	SOL 5330
C -----	SOL 5340
C Reset aqueous logkt's so there will be no zero divide and	SOL 5350
C calculate kt from logkt	SOL 5360
C -----	SOL 5370
	SOL 5380
DO 70 I = 1, NMAX	SOL 5390
IF (LOGKT1(I) .LT. DLOG10(CPUMIN)) LOGKT1(I) = DLOG10(CPUMIN)	SOL 5400
IF (LOGKT1(I) .GT. DLOG10(CPUMAX)) LOGKT1(I) = DLOG10(CPUMAX)	SOL 5410
KT1(I) = 10.0** (LOGKT1(I))	SOL 5420
70 CONTINUE	SOL 5430
	SOL 5440
C -----	SOL 5450
C Print log k values	SOL 5460
C -----	SOL 5470
	SOL 5480
IF (INFORM .EQ. 1) CALL PRNTAB (TITLE, TEMP, MXAQK)	SOL 5490
Y28 = 1	SOL 5500
	SOL 5510
C -----	SOL 5520
C If "temp" is greater than 0 and equal to "hitemp" then go to	SOL 5530
C calculate.	SOL 5540
C -----	SOL 5550
	SOL 5560
IF (TEMP.GT.1.0D-10.AND.(DABS(HITEMP-TEMP)).LT.1.0D-10) GO TO 80	SOL 5570
ALFA(8) = 10.0D00**(-PH)	SOL 5580
	SOL 5590
C -----	SOL 5600
C Calculate the molality of total inorganic carbon from	SOL 5610
C the given value of tic and assign first-guess values	SOL 5620
C to the concentration of hco3 and co3	SOL 5630
C -----	SOL 5640
	SOL 5650
IF (TIC .GT. CPUMIN) THEN	SOL 5660
IF (UNITS .NE. 'MOL/L' .AND. UNITS .NE. 'MOL/K') THEN	SOL 5670
ANMTIC = TIC / 12011.0	SOL 5680
CUNITS(98) = (TIC / 12011.0) / (1.0D00 + (ALFA(8) / KT1(1))	SOL 5690
+ (ALFA(8)**2.0 / (KT1(1) * KT1(72))))	SOL 5700
CUNITS(7) = CUNITS(98) * ALFA(8) / KT1(1)	SOL 5710
CUNITS(98) = CUNITS(98) * 1.0D3 * GFW(98)	SOL 5720
CUNITS(7) = CUNITS(7) * 1.0D3 * GFW(7)	SOL 5730
ELSE	SOL 5740
ANMTIC = TIC	SOL 5750
CUNITS(98) = TIC / (1.0D00 + (ALFA(8) / KT1(1))	SOL 5760
+ (ALFA(8)**2.0 / (KT1(1) * KT1(72))))	SOL 5770
CUNITS(7) = (CUNITS(98) * ALFA(8) / KT1(1))	SOL 5780

END IF	SOL 5790
ALK = 2	SOL 5800
END IF	SOL 5810
	SOL 5820
Y28 = 0	SOL 5830
	SOL 5840
C -----	SOL 5850
C Calculation of eh, cation-anion balance, gamma of neutral species	SOL 5860
C temperature effects on debye-huckel constants and assignment	SOL 5870
C of mass-balance criteria for speciation calculations	SOL 5880
C -----	SOL 5890
	SOL 5900
80 CONTINUE	SOL 5910
CALL CALCUL (A, B, TDS, Y28, DNS, TEMP, HITEMP, PRESS, DENS, EHM,	SOL 5920
. EPMC, EMFZSC, GFW, Z, UNITS, MXSP, TIC, ANMTIC,	SOL 5930
. GAMMA, TCO2, BDAT, BDOT, MNACLD, NUFLAG)	SOL 5940
	SOL 5950
C -----	SOL 5960
C ITWR is set equal to 1 in distrb to avoid the printing of	SOL 5970
C headings during ph calculations	SOL 5980
C -----	SOL 5990
	SOL 6000
ITWR = 0	SOL 6010
	SOL 6020
90 CONTINUE	SOL 6030
IACI = 0	SOL 6040
	SOL 6050
C -----	SOL 6060
C Distribution of species calculations	SOL 6070
C -----	SOL 6080
	SOL 6090
CALL DISTRB (NUFLAG, FLAGS, GAMMA, Z, DHA, TEMP, HITEMP, EHM, ALK,	SOL 6100
. TITLE, A, B, MXSP, MXAQK, MU, IPRIN1, IPIT, TK,	SOL 6110
. CONVI, ANMTIC, ITIC, HTOT, OHTOT, SCO2, JCO3, ITWR,	SOL 6120
. BDOT)	SOL 6130
	SOL 6140
IF (PHHIT .EQ. 1 .AND. DABS(HITEMP-TEMP) .LT. 1.0D-10) GO TO 110	SOL 6150
IF (PHHIT .NE. 1 .AND. IOPT .GT. 0) GO TO 120	SOL 6160
	SOL 6170
IF (ICCSAT .EQ. 0) THEN	SOL 6180
IACI = 1	SOL 6190
GO TO 100	SOL 6200
END IF	SOL 6210
	SOL 6220
C -----	SOL 6230
C Do the ph option, if asked for	SOL 6240
C -----	SOL 6250
	SOL 6260
IF (ICCSAT .GT. 0) CALL PHOPT (ICCSAT, FCCSAT, ITWR, JCCST, *90)	SOL 6270
IF (PHHIT .EQ. 1) IACI = 1	SOL 6280
	SOL 6290
C -----	SOL 6300
C Print the distribution of species calculations.	SOL 6310
C -----	SOL 6320
	SOL 6330
100 CONTINUE	SOL 6340
CALL PRINTR (TITLE, EHM, UNITS, DENS, PRESS, GFW, TEMP, Z, GAMMA,	SOL 6350
. PH20, PCO2, TDS, MU, MNACLD, SCO2, HTOT, OHTOT, MXSP)	SOL 6360

	IF (IACT .EQ. 1) GO TO 210	SOL 6370
		SOL 6380
		SOL 6390
C	-----	SOL 6400
C	Iteration routine for the calculation of a new ph	SOL 6410
C	-----	SOL 6420
		SOL 6430
	110 CONTINUE	SOL 6440
	IF (PPHHIT .EQ. 0) CALL PHCALC (TEMP, HITEMP, CONV2, ITIC, ITWR,	SOL 6450
	ISALT, IPHNUM, IPRIN2, *30, *90,	SOL 6460
	*100, *220)	SOL 6470
		SOL 6480
C	-----	SOL 6490
C	Do the co2 option	SOL 6500
C	-----	SOL 6510
		SOL 6520
	120 CONTINUE	SOL 6530
	IF (IOPT .GT. 0) THEN	SOL 6540
	CALL CO2OPT (TEMP, HITEMP, GAMMA, ICO2, IMCO3, FCCSAT, MNACLD,	SOL 6550
	ITIC, ISAT, IPRIN2, *100)	SOL 6560
	GO TO 110	SOL 6570
	END IF	SOL 6580
		SOL 6590
C	-----	SOL 6600
C	Gas distribution option. Note a max. of twenty five tries	SOL 6610
C	-----	SOL 6620
		SOL 6630
	IF (IPHASE .GT. 0) THEN	SOL 6640
	IMAX = 25	SOL 6650
	DO 150 IGAS = 1, IMAX	SOL 6660
	I = IGAS	SOL 6670
	CALL GASES (TEMP, PRESS, MNACLD, PH2O, FCCSAT, I, IMAX,	SOL 6680
	IPRIN2)	SOL 6690
	IF (IPHASE .LE. 0) GO TO 160	SOL 6700
	JCO3 = 0	SOL 6710
	ITIC = 2	SOL 6720
	IOPT = 0	SOL 6730
	PPHHIT = 1	SOL 6740
	PPHHIT = 0	SOL 6750
	IPHNUM = 0	SOL 6760
	DO 140 J = 1, IMAX	SOL 6770
	CALL PHCALC (TEMP, HITEMP, CONV2, ITIC, ITWR, ISALT, IPHNUM,	SOL 6780
	IPRIN2, *150, *130, *150, *150)	SOL 6790
	GO TO 150	SOL 6800
130	CONTINUE	SOL 6810
	CALL DISTRB (NUFLAG, FLAGS, GAMMA, Z, DHA, TEMP, HITEMP,	SOL 6820
	EHM, ALK, TITLE, A, B, MXSP, MXAQK, MU, IPRIN1,	SOL 6830
	IPIT, TK, CONV1, ANMTIC, ITIC, HTOT, OHTOT,	SOL 6840
	SCO2, JCO3, ITWR, BDOT)	SOL 6850
140	CONTINUE	SOL 6860
150	CONTINUE	SOL 6870
160	CONTINUE	SOL 6880
	IACT = 0	SOL 6890
	CALL PRINTR (TITLE, EHM, UNITS, DENS, PRESS, GFW, TEMP, Z,	SOL 6900
	GAMMA, PH2O, PCO2, TDS, MU, MNACLD, SCO2, HTOT,	SOL 6910
	OHTOT, MXSP)	SOL 6920
	END IF	SOL 6930
		SOL 6940

C	-----	SOL 6950
C	Exchange and adsorption options	SOL 6960
C	-----	SOL 6970
	IF (IEXCH .GT. 0) THEN	SOL 6980
	UNITS = 'MOL/K'	SOL 6990
	IMAX = 100	SOL 7000
	HITEMP = TEMP	SOL 7010
	DO 190 ICALL = 1, IMAX	SOL 7020
	I = ICALL	SOL 7030
	CALL ADSORB (TEMP, Z, IDONE, I, IEXCH, MXSP, IPRIN2)	SOL 7040
	IF (IDONE .LE. 0) THEN	SOL 7050
	IEXCH = 0	SOL 7060
	GO TO 200	SOL 7070
	END IF	SOL 7080
	JCO3 = 0	SOL 7090
	ITIC = 2	SOL 7100
	IOPT = 0	SOL 7110
	PHHIT = 1	SOL 7120
	PPHHIT = 0	SOL 7130
	IPHNUM = 0	SOL 7140
	CALL DISTRB (NUFLAG, FLAGS, GAMMA, Z, DHA, TEMP, HITEMP, EHM,	SOL 7150
	ALK, TITLE, A, B, MXSP, MXAQK, MU, IPRIN1,	SOL 7160
	IPIT, TK, CONV1, ANMTIC, ITIC, HTOT, OHTOT,	SOL 7170
	SCO2, JCO3, ITWR, BDOT)	SOL 7180
	DO 180 J = 1, IMAX	SOL 7190
	CALL PHCALC (TEMP, HITEMP, CONV2, ITIC, ITWR, ISALT, IPHNUM,	SOL 7200
	IPRIN2, *190, *170, *190, *190)	SOL 7210
	GO TO 190	SOL 7220
170	CONTINUE	SOL 7230
	CALL DISTRB (NUFLAG, FLAGS, GAMMA, Z, DHA, TEMP, HITEMP,	SOL 7240
	EHM, ALK, TITLE, A, B, MXSP, MXAQK, MU,	SOL 7250
	IPRIN1, IPIT, TK, CONV1, ANMTIC, ITIC, HTOT,	SOL 7260
	OHTOT, SCO2, JCO3, ITWR, BDOT)	SOL 7270
180	CONTINUE	SOL 7280
190	CONTINUE	SOL 7290
	IPGLN = IPGLN + 6	SOL 7300
	IF (IPGLN .GT. 58) CALL PAGE	SOL 7310
	WRITE (UNO, 910)	SOL 7320
		SOL 7330
		SOL 7340
		SOL 7350
200	CONTINUE	SOL 7360
	IACT = 0	SOL 7370
	CALL PRINTR (TITLE, EHM, UNITS, DENS, PRESS, GFW, TEMP, Z,	SOL 7380
	GAMMA, PH2O, PCO2, TDS, MU, MNACLD, SCO2, HTOT,	SOL 7390
	OHTOT, MXSP)	SOL 7400
	END IF	SOL 7410
		SOL 7420
	IF (IACT .EQ. 1) GO TO 220	SOL 7430
		SOL 7440
C	-----	SOL 7450
C	Print mole ratios, log of activity ratios, and temperatures	SOL 7460
C	calculated by chemical geothermometers	SOL 7470
C	-----	SOL 7480
		SOL 7490
210	CONTINUE	SOL 7500
	CALL PRATIO (TITLE, PRESS, TEMP, DENS, UNITS, PCO2, GEOTH, RATIO)	SOL 7510
		SOL 7520

C	-----	SOL 7530
C	Calculate and print activity products of phases	SOL 7540
C	-----	SOL 7550
	CALL ACTIVE (TITLE, ALFA, TEMP, MXMKN, LOGKT2, PAGE3, MINCO,	SOL 7560
	MININD)	SOL 7570
		SOL 7580
	IF (IACT .EQ. 1) GO TO 110	SOL 7590
		SOL 7600
		SOL 7610
C	-----	SOL 7620
C	Process the mixing/boiling/mineral saturation option	SOL 7630
C	-----	SOL 7640
		SOL 7650
220	CONTINUE	SOL 7660
	IF (IBMIX .NE. 0) THEN	SOL 7670
	IF (IRUN .EQ. 0 .AND. ISALT .EQ. 0) THEN	SOL 7680
	TIT1 = TITLE	SOL 7690
	END IF	SOL 7700
	IF (IBMIX .EQ. 1) THEN	SOL 7710
	IF (ICALL .NE. 3) THEN	SOL 7720
	ICALL = 1	SOL 7730
	ISALT = 1	SOL 7740
	IMIX = 1	SOL 7750
	IF (ITMIX .EQ. 0) ISALT = 3	SOL 7760
	IF (ISALT .EQ. 1) TITLE = 'MIXTURE OF '// TIT1 //	SOL 7770
	' WITH A SALT OR MINERAL'	SOL 7780
	END IF	SOL 7790
	CALL MIXER (TEMP, MNACLD, PRESS, DENS, ICALL, ISALT, IRUN,	SOL 7800
	MXSP, FCCSAT, PH2O, IPRIN2, MXMKN)	SOL 7810
	IF (ICALL .EQ. 1) THEN	SOL 7820
	PHHIT = 0	SOL 7830
	PPHHIT = 1	SOL 7840
	IMIX = 0	SOL 7850
	IBMIX = 0	SOL 7860
	GO TO 100	SOL 7870
	ELSE	SOL 7880
	IF (ISALT .EQ. 1) IBMIX = 0	SOL 7890
	GO TO 230	SOL 7900
	END IF	SOL 7910
	ELSE IF (IBMIX .EQ. 2) THEN	SOL 7920
	ICALL = 1	SOL 7930
	IF (IRUN .NE. 0) THEN	SOL 7940
	ICALL = 2	SOL 7950
	IMIX = 1	SOL 7960
	TIT2 = TITLE	SOL 7970
	END IF	SOL 7980
	CALL MIXER (TEMP, MNACLD, PRESS, DENS, ICALL, ISALT, IRUN,	SOL 7990
	MXSP, FCCSAT, PH2O, IPRIN2, MXMKN)	SOL 8000
	IF (IMIX .EQ. 1) THEN	SOL 8010
	IBMIX = 0	SOL 8020
	TITLE = 'MIXTURE OF '//TIT1//' AND ' // TIT2	SOL 8030
	GO TO 250	SOL 8040
	END IF	SOL 8050
	ICALL = 0	SOL 8060
	ISALT = 0	SOL 8070
	IMIX = 0	SOL 8080
	JMIXTR = 0	SOL 8090
	TITMIX = '	SOL 8100

CALL INTIAL (OK, ALK, INFORM, RATIO, GAMMA, TEMP, HITEMP,	SOL 8110
PRESS, HTOTI, OHTOTI, ICO2, IMCO3, IBMIX,	SOL 8120
FCCSAT, IEXCH, ISAT, IPHNUM, JCCST)	SOL 8130
IF (MIXFLE .EQ. ' ') THEN	SOL 8140
CALL INPUT (UNI, TEMP, HITEMP, DNS, PHHIT, IEXCH, ICO2,	SOL 8150
MIXFLG)	SOL 8160
ELSE	SOL 8170
UNM = 39	SOL 8180
OPEN (UNM, FILE = MIXFLE, STATUS = 'OLD')	SOL 8190
CALL INPUT (UNM, TEMP, HITEMP, DNS, PHHIT, IEXCH, ICO2,	SOL 8200
MIXFLG)	SOL 8210
CLOSE (UNM)	SOL 8220
END IF	SOL 8230
IBMIX = 2	SOL 8240
ILO = 1	SOL 8250
GO TO 30	SOL 8260
ELSE	SOL 8270
IF (ISALT .NE. 2) THEN	SOL 8280
ICALL = 1	SOL 8290
IMIX = 1	SOL 8300
ISALT = 2	SOL 8310
TITLE = 'SOLUTION AFTER BOILING OF .. ' // TIT1	SOL 8320
END IF	SOL 8330
CALL MIXER (TEMP, MNACLD, PRESS, DENS, ICALL, ISALT, IRUN,	SOL 8340
MXSP, FCCSAT, PH2O, IPRIN2, MXMNK)	SOL 8350
IF (ICALL .EQ. 1) THEN	SOL 8360
PHHIT = 0	SOL 8370
PPHHIT = 1	SOL 8380
IMIX = 0	SOL 8390
IBMIX = 0	SOL 8400
GO TO 100	SOL 8410
ELSE	SOL 8420
GO TO 230	SOL 8430
END IF	SOL 8440
END IF	SOL 8450
END IF	SOL 8460
IMIX = 0	SOL 8470
IF (INMIX .EQ. 0) THEN	SOL 8480
CALL STORE (TEMP, HITEMP)	SOL 8490
GO TO 20	SOL 8500
END IF	SOL 8510
	SOL 8520
	SOL 8530
	SOL 8540
	SOL 8550
C -----	SOL 8560
C Change the solution parameters to those of the mixture	SOL 8570
C -----	SOL 8580
230 CONTINUE	SOL 8590
IF (IMIX .EQ. 1) THEN	SOL 8600
CALL INTIAL (OK, ALK, INFORM, RATIO, GAMMA, TEMP, HITEMP, PRESS,	SOL 8610
HTOTI, OHTOTI, ICO2, IMCO3, IMIX, FCCSAT, IEXCH,	SOL 8620
ISAT, IPHNUM, JCCST)	SOL 8630
	SOL 8640
	SOL 8650
UNITS = 'MOL/K'	SOL 8660
ALK = 2	SOL 8670
ITIC = 0	SOL 8680

HITEMP = TEMP	SOL 8690
EHM = 9.0D0	SOL 8700
EMFZSC = 9.0D0	SOL 8710
EHMC = 9.0D0	SOL 8720
Y28 = 0	SOL 8730
PHHIT = 1	SOL 8740
HTOTI = TOTEL(1)	SOL 8750
OHTOTI = TOTEL(2)	SOL 8760
ANMTIC = TOTEL(3)	SOL 8770
DO 240 I = 1, NMAX	SOL 8780
IF (I .EQ. 8) ANALM(I) = 0.0D00	SOL 8790
IF (I .EQ. 9) ANALM(I) = 0.0D00	SOL 8800
CUNITS(I) = ANALM(I)	SOL 8810
M(I) = ANALM(I)	SOL 8820
240 CONTINUE	SOL 8830
GO TO 80	SOL 8840
END IF	SOL 8850
	SOL 8860
C -----	SOL 8870
C Mix the two solution in a single or multiple mixtures case	SOL 8880
C -----	SOL 8890
	SOL 8900
250 CONTINUE	SOL 8910
JMIXTR = JMIXTR + 1	SOL 8920
CALL STORE (TEMP, HITEMP)	SOL 8930
IF (INMIX .LT. JMIXTR) GO TO 20	SOL 8940
	SOL 8950
WRITE (BUFFER, 900) FMIX(JMIXTR), (1.0D0 - FMIX(JMIXTR))	SOL 8960
READ (BUFFER, '(A)') TITMIX	SOL 8970
	SOL 8980
DO 260 I = 1, MXSP + 44	SOL 8990
ANALM(I) = (ANMMIX(I) * FMIX(JMIXTR))	SOL 9000
+ (BNMMIX(I) * (1.0D0 - FMIX(JMIXTR)))	SOL 9010
260 CONTINUE	SOL 9020
	SOL 9030
DO 270 I = 1, 5	SOL 9040
TOTEL(I) = (A1MIX(I) * FMIX(JMIXTR))	SOL 9050
+ (B2MIX(I) * (1.0D0 - FMIX(JMIXTR)))	SOL 9060
270 CONTINUE	SOL 9070
	SOL 9080
IMIX = 1	SOL 9090
DNS = 'Y'	SOL 9100
DENS = (ADENS * FMIX(JMIXTR)) + (BDENS * (1.0D0 - FMIX(JMIXTR)))	SOL 9110
TEMP = (ATEMP * FMIX(JMIXTR)) + (BTEMP * (1.0D0 - FMIX(JMIXTR)))	SOL 9120
HITEMP = 0.0D00	SOL 9130
GO TO 230	SOL 9140
	SOL 9150
900 FORMAT('(PROPORTIONS: 1= ',F4.2,' 2= ',F4.2,')')	SOL 9160
910 FORMAT(//, ' *****WARNING*****',	SOL 9170
/, ' Convergence not reached in ADSORBPTION',	SOL 9180
/, ' /ION EXCHANGE routine. Following results',	SOL 9190
/, ' may be in error . ',	SOL 9200
/)	SOL 9210
END	SOL 9220

	SUBROUTINE ACTIVE (TITLE, ALFA, TEMP, MXMNK, LOGKT2, PAGE3,			ACT 0010
	MINCO, MININD)			ACT 0020
C	=====			ACT 0030
C	This routine calculates and prints activity products of phases			ACT 0040
C	-----			ACT 0050
C	Declare constants			ACT 0060
C	-----			ACT 0070
C	CPUMIN	DBL	Smallest positive real value program uses	ACT 0080
C	NMAX	INT	General array dimension to allow easy expansion	ACT 0090
C	UNO	INT	File unit assigned for output file	ACT 0100
C	UNR	INT	File unit assigned for reaction file	ACT 0110
C	-----			ACT 0120
	INTEGER NMAX, UNO, UNR			ACT 0130
	DOUBLE PRECISION R, CPUMIN			ACT 0140
	PARAMETER (NMAX = 340, UNO = 6, UNR = 12)			ACT 0150
	PARAMETER (R = 1.98719D-3, CPUMIN=1.0D-35)			ACT 0160
				ACT 0170
C	-----			ACT 0180
C	ALFA	DBL	Activity of aqueous species i	ACT 0190
C	AP	DBL	Activity product of the reaction	ACT 0200
C	C2	DBL	Saturation index	ACT 0210
C	COEF	DBL	Coefficient of species in reaction	ACT 0220
C	CR	CHA	Inserts carriage returns in output	ACT 0230
C	DUMM	DBL	Delta gibbs free energy difference	ACT 0240
C	I	INT	Loop counting variable	ACT 0250
C	IC	INT	Number of components in reaction	ACT 0260
C	IFIN	INT	Formats the output	ACT 0270
C	INDEX	INT	Index values of the minerals to be printed out	ACT 0280
C	INDX	INT	Index of the species in the reaction	ACT 0290
C	IPAGE	INT	Current page number of output file	ACT 0300
C	IPGLN	INT	Current line number of the output file	ACT 0310
C	J	INT	Loop counting variable	ACT 0320
C	K	INT	Index number of the right side of the output	ACT 0330
C	L	INT	Index number of the left side of the output	ACT 0340
C	LOGKT2	DBL	Log K for minerals at specified temperature	ACT 0350
C	MCOEF	DBL	Coefficient of species read in from table	ACT 0360
C	MINCO	DBL	Stoichiometric coefficient for added minerals	ACT 0370
C	MINDX	DBL	Index number of the species read in from table	ACT 0380
C	MININD	INT	Index number of the added mineral	ACT 0390
C	MXMNK	INT	Total number of mineral log k values	ACT 0400
C	NUM	INT	Count of minerals to be printed out	ACT 0410
C	PAGE3	CHA	Names of solubility constants	ACT 0420
C	R	DBL	Gas constant	ACT 0430
C	T	DBL	Current temperature in degrees kelvin	ACT 0440
C	TEMP	DBL	Current temperature in degrees centigrade	ACT 0450
C	TITLE	CHA	Name of the sample	ACT 0460
C	TITMIX	CHA	Title used for mixing	ACT 0470
C	TOF	CHA	Places a form feed in output file	ACT 0480
C	-----			ACT 0490
				ACT 0500
	INTEGER I, IC, IFIN, INDEX(NMAX), INDX(10), IPGLN, IPAGE			ACT 0510
	INTEGER J, K, L, MINDX(10,NMAX), MININD(9,5), MXMNK, NUM			ACT 0520
				ACT 0530
	CHARACTER * 1 TOF, CR			ACT 0540
	CHARACTER * 8 PAGE3(NMAX)			ACT 0550
	CHARACTER * 40 TITMIX			ACT 0560
	CHARACTER * 80 TITLE			ACT 0570
				ACT 0580

DOUBLE PRECISION ATCPRD, ALFA(NMAX), AP(NMAX), C2(2)	ACT 0590
DOUBLE PRECISION COEF(10), DUMM(2), LOGKT2(NMAX), MCOEF(10,NMAX)	ACT 0600
DOUBLE PRECISION MINCO(9,5), T, TEMP	ACT 0610
	ACT 0620
INTRINSIC DABS	ACT 0630
	ACT 0640
EXTERNAL ATCPRD, PAGE	ACT 0650
	ACT 0660
COMMON /FMFD / TOF, CR, TITMIX	ACT 0670
COMMON /FORM / IPAGE, IPGLN	ACT 0680
	ACT 0690
C -----	ACT 0700
C -----	ACT 0710
C The following open statement have been changed out by	ACT 0720
C Ernie Perkins (ORSO, ARC) in order to allow an command	ACT 0730
C proceedure under VMS 4.5 on DEC VAX's to assign the files	ACT 0740
C external to the program.	ACT 0750
C -----	ACT 0760
C OPEN (UNR, STATUS = 'OLD', shared, readonly)	ACT 0770
C OPEN (UNR, FILE = 'RXN.TBL', STATUS = 'OLD')	ACT 0780
	ACT 0790
DO 10 L = 1, MXMKN	ACT 0800
READ (UNR, 900) I, (MCOEF(J,I), MINDX(J,I), J = 1, 10)	ACT 0810
10 CONTINUE	ACT 0820
	ACT 0830
CLOSE (UNR)	ACT 0840
	ACT 0850
DO 20 I = 1, MXMKN + 5	ACT 0860
AP(I) = 0.0D0	ACT 0870
20 CONTINUE	ACT 0880
	ACT 0890
T = TEMP + 273.15	ACT 0900
	ACT 0910
C -----	ACT 0920
C Activity products of phases	ACT 0930
C -----	ACT 0940
	ACT 0950
DO 40 I = 1, MXMKN	ACT 0960
IC = 0	ACT 0970
DO 30 J = 1, 10	ACT 0980
IF (DABS(MCOEF(J,I)) .GT. CPUMIN) THEN	ACT 0990
IC = IC + 1	ACT 1000
COEF(J) = MCOEF(J,I)	ACT 1010
INDX(J) = MINDX(J,I)	ACT 1020
ELSE	ACT 1030
COEF(J) = 0.0D0	ACT 1040
INDX(J) = MINDX(J,I)	ACT 1050
END IF	ACT 1060
30 CONTINUE	ACT 1070
AP(I) = ATCPRD (IC, INDX, COEF, ALFA)	ACT 1080
40 CONTINUE	ACT 1090
	ACT 1100
C -----	ACT 1110
C Calculate activity product for added minerals	ACT 1120
C -----	ACT 1130
	ACT 1140
DO 60 I = 1, 5	ACT 1150
DO 50 J = 1, 8	ACT 1160

IF (DABS(MINCO(J,I)) .GT. CPUMIN) AP(MXMNK+I) =	ACT 1170
AP(MXMNK+I) + MINCO(J,I)*ALFA(MININD(J,I))	ACT 1180
50 CONTINUE	ACT 1190
AP(MXMNK+I) = AP(MXMNK+I) + MINCO(9,I)	ACT 1200
60 CONTINUE	ACT 1210
	ACT 1220
C -----	ACT 1230
C Write out activity products	ACT 1240
C -----	ACT 1250
	ACT 1260
CALL PAGE	ACT 1270
WRITE (UNO, 910) TITLE, TEMP, TITMIX	ACT 1280
WRITE (UNO, 920)	ACT 1290
WRITE (UNO, 930) CR	ACT 1300
IPGLN = IPGLN + 4	ACT 1310
NUM = 0	ACT 1320
	ACT 1330
DO 70 I = 1, MXMNK + 5	ACT 1340
IF (DABS(AP(I)) .LE. 300.0 .AND.	ACT 1350
DABS(LOGKT2(I)) .LE. 300.0) THEN	ACT 1360
NUM = NUM + 1	ACT 1370
INDEX(NUM) = I	ACT 1380
END IF	ACT 1390
70 CONTINUE	ACT 1400
	ACT 1410
IFIN = (NUM + 1) / 2	ACT 1420
DO 80 I = 1, IFIN	ACT 1430
L = INDEX(I)	ACT 1440
C2(1) = AP(L) - LOGKT2(L)	ACT 1450
DUMM(1) = 2.302585D0 * R * T * C2(1)	ACT 1460
J = I + IFIN	ACT 1470
IF (J .LE. NUM) THEN	ACT 1480
K = INDEX(J)	ACT 1490
C2(2) = AP(K) - LOGKT2(K)	ACT 1500
DUMM(2) = 2.302585D0 * R * T * C2(2)	ACT 1510
END IF	ACT 1520
	ACT 1530
IF (IPGLN .GT. 58) THEN	ACT 1540
CALL PAGE	ACT 1550
WRITE (UNO, 910) TITLE, TEMP, TITMIX	ACT 1560
WRITE (UNO, 920)	ACT 1570
WRITE (UNO, 930) CR	ACT 1580
IPGLN = IPGLN + 4	ACT 1590
END IF	ACT 1600
	ACT 1610
IF (J .LE. NUM) THEN	ACT 1620
WRITE (UNO, 940)	ACT 1630
L, PAGE3(L), AP(L), LOGKT2(L), C2(1), DUMM(1),	ACT 1640
K, PAGE3(K), AP(K), LOGKT2(K), C2(2), DUMM(2)	ACT 1650
IPGLN = IPGLN + 1	ACT 1660
ELSE	ACT 1670
WRITE (UNO, 940)	ACT 1680
L, PAGE3(L), AP(L), LOGKT2(L), C2(1), DUMM(1)	ACT 1690
IPGLN = IPGLN + 1	ACT 1700
END IF	ACT 1710
80 CONTINUE	ACT 1720
	ACT 1730
RETURN	ACT 1740

900	FORMAT(I3,/,10(F10.4,I4))	ACT 1750
910	FORMAT(' SAMPLE IDENT - ',A80,4X,'(TEMPERATURE = ',F6.2,')',	ACT 1760
	/,20X,A40)	ACT 1770
920	FORMAT(/,6X,'PHASE',5X,'LOG (AP)',4X,'LOG (KT)',2X,	ACT 1780
	'LOG (AP/KT)',7X,'DELG', 10X,'PHASE',5X,	ACT 1790
	'LOG (AP)',4X,'LOG (KT)',2X,	ACT 1800
	'LOG (AP/KT)',7X,'DELG')	ACT 1810
930	FORMAT(A1,6X,'_____',5X,'_____',4X,'_____',2X,	ACT 1820
	'_____',7X,'_____', 10X,'_____',5X,	ACT 1830
	'_____',4X,'_____',2X,	ACT 1840
	'_____',7X,'_____')	ACT 1850
940	FORMAT (1X, I3, 2X, A8, F10.3, 3(2X,F10.3),	ACT 1860
	5X, I3, 2X, A8, F10.3, 3(2X,F10.3))	ACT 1870
		ACT 1880
		ACT 1890
	END	ACT 1900

	SUBROUTINE ADSORB (TC, Z, OK, ICALL, IEXCH, MXSP, IPRIN2)	ADS 0010
C	=====	ADS 0020
C	This is the adsorption routine	ADS 0030
C	-----	ADS 0040
C	Declare constants	ADS 0050
C	-----	ADS 0060
C	AVOG DBL Avogadro's number	ADS 0070
C	BOLTZ DBL Boltzman constant	ADS 0080
C	CPUMIN DBL Smallest positive real value program uses	ADS 0090
C	ECHG DBL Electron charge	ADS 0100
C	NMAX INT General array dimension to allow easy expansion	ADS 0110
C	UNO INT File unit assigned for output file	ADS 0120
C	PERMV DBL Perm. in a vacuum	ADS 0130
C	TEST DBL Value to test against.	ADS 0140
C	-----	ADS 0150
	INTEGER NMAX, UNO	ADS 0160
	DOUBLE PRECISION AVOG, BOLTZ, CPUMIN, DIE, ECHG, PERMV, TEST	ADS 0170
	PARAMETER (NMAX = 340, UNO = 6)	ADS 0180
	PARAMETER (AVOG = 6.022D+23, BOLTZ = 1.38D-23)	ADS 0190
	PARAMETER (CPUMIN = 1.0D-35, DIE = 78.27, ECHG = 1.6022D-19)	ADS 0200
	PARAMETER (PERMV = 8.854D-12, TEST = 1.0D-03)	ADS 0210
		ADS 0220
C	-----	ADS 0230
C	Declare variables	ADS 0240
C	-----	ADS 0250
C	ALMIX DBL HTOT, OHTOT, TIC for initial conditions	ADS 0260
C	ADD DBL Amount of component to add/remove from water	ADS 0270
C	ANALM DBL Analyzed molality of species i	ADS 0280
C	ANMIX DBL Number of moles of initial components	ADS 0290
C	ANSWER DBL Coefficient array used to calculate results	ADS 0300
C	B2MIX DBL HTOT, OHTOT, and TIC for comp 1 of a mixture	ADS 0310
C	BNMMIX DBL Analyzed molality of species i in solution B	ADS 0320
C	C3MIX DBL Temp storage for HTOT, OHTOT, TIC	ADS 0330
C	CEC DBL Cation Exchange Capacity	ADS 0340
C	CNMMIX DBL Temp Storage for total mass of each component	ADS 0350
C	COEF DBL Stoichiometric coefficient and Id number	ADS 0360
C	CROSS LOG Have we crossed the root for species adsorption?	ADS 0370

BNMMIX(7) = TOTEL(3)	ADS 1540
BNMMIX(98) = 0.0	ADS 1550
DO 40 I = 1, INSP	ADS 1560
NEUT = 0	ADS 1570
II = 0	ADS 1580
X = 0.0	ADS 1590
IBASE(I) = 0	ADS 1600
DO 25 K = 1, ISCOMP(I)	ADS 1610
J = IDN(I,K)	ADS 1620
IF (J .EQ. 0) THEN	ADS 1630
NEUT = K	ADS 1640
ELSE	ADS 1650
IF (II .EQ. 0 .OR. II .EQ. 8 .OR.	ADS 1660
II .EQ. 9 .OR. II .EQ. 10) THEN	ADS 1670
II = J	ADS 1680
X = 10.0	ADS 1690
ELSE	ADS 1700
IF (COEF(I,K) .LT. X) THEN	ADS 1710
X = COEF(I,K)	ADS 1720
II = J	ADS 1730
END IF	ADS 1740
END IF	ADS 1750
END IF	ADS 1760
25 CONTINUE	ADS 1770
IBASE(I) = II	ADS 1780
DO 30 K = 1, ISCOMP(I)	ADS 1790
J = IDN(I,K)	ADS 1800
IF (J .EQ. 0 .OR. DABS(COEF(I,K)) .LT. CPUMIN) GO TO 30	ADS 1810
X = CEC * 1.0D-03 * MBASE(I) / (DABS(COEF(I, NEUT)))	ADS 1820
X = X * (-1.0) * COEF(I,K)	ADS 1830
EQFAC = 0.0	ADS 1840
IF (J .EQ. 7) EQFAC = 1.0	ADS 1850
IF (J .EQ. 8) EQFAC = 1.0	ADS 1860
IF (J .EQ. 9) EQFAC = -1.0	ADS 1870
IF (J .EQ. 11) J = 12	ADS 1880
IF (J .EQ. 12) EQFAC = 4.0	ADS 1890
IF (J .EQ. 28) EQFAC = 2.0	ADS 1900
IF (J .EQ. 31) EQFAC = -3.0	ADS 1910
IF (J .EQ. 32) EQFAC = -1.0	ADS 1920
IF (J .EQ. 33) EQFAC = 2.0	ADS 1930
IF (J .EQ. 49) EQFAC = 1.0	ADS 1940
IF (J .EQ. 97) EQFAC = 2.0	ADS 1950
EQH = EQH + (X * EQFAC)	ADS 1960
	ADS 1970
IF (J .EQ. 7) EQC = (X) + EQC	ADS 1980
IF (J .EQ. 97) EQC = (X) + EQC	ADS 1990
IF (J .EQ. 98) EQC = (X) + EQC	ADS 2000
IF (J .EQ. 207) EQC = (X) + EQC	ADS 2010
IF (J .EQ. 208) EQC = (X * 2.0) + EQC	ADS 2020
IF (J .EQ. 209) EQC = (X * 3.0) + EQC	ADS 2030
IF (J .EQ. 7 .OR. J .EQ. 97 .OR. J .EQ. 98 .OR.	ADS 2040
J .EQ. 207 .OR. J .EQ. 208 .OR. J .EQ. 209) J = 7	ADS 2050
	ADS 2060
BNMMIX(J) = BNMMIX(J) + X	ADS 2070
30 CONTINUE	ADS 2080
40 CONTINUE	ADS 2090
	ADS 2100
B2MIX(1) = B2MIX(1) + EQH	ADS 2110

B2MIX(3) = B2MIX(3) + EQC	ADS 2120
IF (B2MIX(3) .GT. 0.0) THEN	ADS 2130
BNMMIX(7) = B2MIX(3)	ADS 2140
BNMMIX(98) = 0.0	ADS 2150
ELSE	ADS 2160
BNMMIX(7) = 0.0	ADS 2170
BNMMIX(98) = 0.0	ADS 2180
END IF	ADS 2190
	ADS 2200
DO 50 I = 1, 11	ADS 2210
ADD(I) = 0.0D00	ADS 2220
STEP(I) = 0.0D00	ADS 2230
50 CONTINUE	ADS 2240
	ADS 2250
YO = 0.0	ADS 2260
END IF	ADS 2270
	ADS 2280
C -----	ADS 2290
C Zero out local arrays	ADS 2300
C -----	ADS 2310
	ADS 2320
NEUT = 0	ADS 2330
DO 80 I = 1, 11	ADS 2340
DO 70 J = 1, 11	ADS 2350
ANSWER(J, I) = 0.0D00	ADS 2360
70 CONTINUE	ADS 2370
KNOWN(I) = 0.0D00	ADS 2380
80 CONTINUE	ADS 2390
	ADS 2400
C -----	ADS 2410
C Set Coefficient array and known column vector	ADS 2420
C -----	ADS 2430
	ADS 2440
100 DO 120 I = 1, INSP	ADS 2450
KNOWN(I) = DLOG10(KRXN(I))	ADS 2460
DO 110 J = 1, ISCOMP(I)	ADS 2470
IF (IDN(I, J) .EQ. 0) THEN	ADS 2480
ANSWER(I, 11) = COEF(I, J)	ADS 2490
ELSE	ADS 2500
IF (IEXCH .EQ. 1) THEN	ADS 2510
KNOWN(I) = KNOWN(I) - (COEF(I, J) * DLOG10((M(IDN(I, J)) * DEXP(((-1.0) * YO * DBLE(ISCHG(I)))))))	ADS 2520
	ADS 2530
ELSE	ADS 2540
KNOWN(I) = KNOWN(I) - (COEF(I, J) * DLOG10(M(IDN(I, J))))	ADS 2550
END IF	ADS 2560
END IF	ADS 2570
110 CONTINUE	ADS 2580
ANSWER(I, I) = 1.0D00	ADS 2590
IF (ISCOMP(I) .EQ. 1 .AND. IDN(I, 1) .EQ. 0) NEUT = I	ADS 2600
120 CONTINUE	ADS 2610
	ADS 2620
IF (NEUT .EQ. 0) NEUT = INSP + 1	ADS 2630
	ADS 2640
DO 130 I = 1, INSP	ADS 2650
ANSWER(NEUT, I) = 0.0	ADS 2660
ANSWER(I, NEUT) = ANSWER(I, 11)	ADS 2670
ANSWER(I, 11) = 0.0D00	ADS 2680
130 CONTINUE	ADS 2690

C	CROSSY	LOG	Have we crossed the root for epsilon?	ADS 0380
C	DIE	DBL	Dielectric constant	ADS 0390
C	DIFF	DBL	Difference from root	ADS 0400
C	DIFYO	DBL	Difference from Y0	ADS 0410
C	DONE	LOG	If we are finished, set to .TRUE.	ADS 0420
C	DUM	CHA	Dummy character array	ADS 0430
C	EQC	DBL	Equivalent carbon in material been added/removed	ADS 0440
C	EQFAC	DBL	Factor for adding/removing material	ADS 0450
C	EQH	DBL	Equivalent Hydrogen in material added/removed	ADS 0460
C	EXELT	DBL	Total amount of components	ADS 0470
C	HTOTI	DBL	Total hydronium	ADS 0480
C	I	INT	Loop Counter	ADS 0490
C	IBASE	INT	ID numbers of the surface for adsorption	ADS 0500
C	ICALL	INT	Number of calls to this routine	ADS 0510
C	IDN	INT	Id numbers of the ISCOMP components adsorption	ADS 0520
C	IEXCH	INT	Switch for adsorption/ion exchange	ADS 0530
C	II	INT	Local pointer used to check for H, OH or H2O	ADS 0540
C	INSP	INT	Total number of surface sites for adsorption	ADS 0550
C	IPRIN2	INT	Print switch to print out iterations	ADS 0560
C	ISCHG	INT	Charge of each surface site for adsorption	ADS 0570
C	ISCOMP	INT	Total number of components in dissociation	ADS 0580
C	IVAL	INT	Number of Iterations	ADS 0590
C	IY	INT	Pointer to last value calculated	ADS 0600
C	J	INT	Loop counter	ADS 0610
C	K	INT	Loop counter	ADS 0620
C	KNOWN	DBL	Final value of moles of complex on surface	ADS 0630
C	KRXN	DBL	K for dissociation reaction of surface species	ADS 0640
C	M	DBL	Calculated molality of aqueous species	ADS 0650
C	MAT	DBL	Matrix used for intermediate calculations	ADS 0660
C	MBASE	DBL	Equivalence Mole Fraction (initial) on surface	ADS 0670
C	MXSP	INT	Max number of species	ADS 0680
C	NEUT	INT	Index for the bare surface complex	ADS 0690
C	OHTOTI	DBL	Initial OH total	ADS 0700
C	OK	INT	Normal exit?	ADS 0710
C	PAGE1	CHA	Names of aqueous species	ADS 0720
C	SIGD	DBL	Charge density in the difuse layer	ADS 0730
C	SIGO	DBL	Charge density at the surface	ADS 0740
C	SINGLE	LOG	Switch if all surface comp. have same # of X's	ADS 0750
C	SPN	CHA	Name of each surface species adsorption	ADS 0760
C	STEP	DBL	Step size for amount added/sub	ADS 0770
C	SUM	DBL	Total of charged species on surface	ADS 0780
C	TC	DBL	Temperature in deg C	ADS 0790
C	TITR	DBL	Iteration array in DISTRB, used for guesses	ADS 0800
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	ADS 0810
C	TRYV	DBL	Working storage for mass on surface	ADS 0820
C	TRYO	DBL	Guess for Y0	ADS 0830
C	VAL	DBL	Intermediate storage	ADS 0840
C	VECT	DBL	Solution vector for surface complexes	ADS 0850
C	X	DBL	Temperary storage	ADS 0860
C	Y0	DBL	Y0	ADS 0870
C	Z	INT	Charge of aqueous species	ADS 0880
C	-----			ADS 0890
	LOGICAL DONE, CROSS, CROSSY, SINGLE			ADS 0900
				ADS 0910
				ADS 0920
	CHARACTER*8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)			ADS 0930
	CHARACTER*8 DUM(11)			ADS 0940
	CHARACTER*10 SPN(10)			ADS 0950

INTEGER I, IBASE(10), ICALL	ADS 0960
INTEGER IDN(10,10), IEXCH, II, IPRIN2, ISCHG(10), INSP	ADS 0970
INTEGER IPAGE, IPGLN, ISCOMP(10), IVAL, IY, J, K, MXSP	ADS 0980
INTEGER NEUT, OK, Z(NMAX)	ADS 0990
	ADS 1000
	ADS 1010
DOUBLE PRECISION ADD(11), ADENS, ALFA(NMAX), ANALM(NMAX)	ADS 1020
DOUBLE PRECISION ANMMIX(NMAX), ANSWER(11,11), ATEMP, AlMIX(5)	ADS 1030
DOUBLE PRECISION BDENS, BNMMIX(NMAX), BTEMP, B2MIX(5)	ADS 1040
DOUBLE PRECISION CEC, CNMMIX(NMAX), COEF(10,10)	ADS 1050
DOUBLE PRECISION CUNITS(NMAX), CO2F, C3MIX(5), DIFF(10)	ADS 1060
DOUBLE PRECISION DIFYO(10), EQC, EQFAC, EQH	ADS 1070
DOUBLE PRECISION EXELT(35), FMIX(10), HTOTI, KNOWN(11)	ADS 1080
DOUBLE PRECISION KRXN(10), M(NMAX), MAT(10,10), MBASE(10)	ADS 1090
DOUBLE PRECISION OHTOTI, PH, SAREA, SIGD, SIGO	ADS 1100
DOUBLE PRECISION STEP(11), SUM, TAREA, TC, TITR(11)	ADS 1110
DOUBLE PRECISION TOTEL(5), TRYV(10), TRYVO(10)	ADS 1120
DOUBLE PRECISION VAL, VECT(10), X, YO	ADS 1130
	ADS 1140
EXTERNAL GUESS, SORTA, PAGE	ADS 1150
	ADS 1160
INTRINSIC DABS, DBLE, DEXP, DLOG10, DSIGN, MAX0, DSQRT	ADS 1170
	ADS 1180
COMMON /EXCHAN/ COEF, MBASE, KRXN, CEC, TAREA, SAREA, IDN,	ADS 1190
ISCHG, ISCOMP, INSP	ADS 1200
COMMON /EXTOT / EXELT, TOTEL, TITR	ADS 1210
COMMON /FORM / IPAGE, IPGLN	ADS 1220
COMMON /MM / ANMMIX, AlMIX, B2MIX, FMIX, BNMMIX, ADENS, BDENS,	ADS 1230
ATEMP, BTEMP	ADS 1240
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	ADS 1250
COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	ADS 1260
COMMON /NAMES2/ SPN	ADS 1270
COMMON /TOTALS/ CO2F, HTOTI, OHTOTI	ADS 1280
	ADS 1290
SAVE ADD, IBASE, KNOWN, STEP, YO	ADS 1300
	ADS 1310
C =====	ADS 1320
	ADS 1330
IY = 0	ADS 1340
CROSSY = .FALSE.	ADS 1350
	ADS 1360
C -----	ADS 1370
C Store solution parameters if first call	ADS 1380
C totel: (1) = htot; (2) = ohtot; (3) = tic	ADS 1390
C -----	ADS 1400
IF (ICALL .EQ. 1) THEN	ADS 1410
DO 10 I = 1, 5	ADS 1420
AlMIX(I) = TOTEL(I)	ADS 1430
B2MIX(I) = TOTEL(I)	ADS 1440
10 CONTINUE	ADS 1450
	ADS 1460
DO 20 I = 1, MXSP + 44	ADS 1470
ANMMIX(I) = ANALM(I)	ADS 1480
BNMMIX(I) = ANALM(I)	ADS 1490
20 CONTINUE	ADS 1500
	ADS 1510
EQC = 0.0	ADS 1520
EQH = 0.0	ADS 1530

	SINGLE = .TRUE.	ADS 2700
		ADS 2710
	DO 132 I = 1, (INSP-1)	ADS 2720
	IF (DABS(ANSWER(I,NEUT) - ANSWER(INSP,NEUT)) .GT. 1.0E-05)	ADS 2730
	SINGLE = .FALSE.	ADS 2740
132	CONTINUE	ADS 2750
		ADS 2760
	KNOWN(NEUT) = 0.0	ADS 2770
	ANSWER(NEUT,NEUT) = 1.0	ADS 2780
		ADS 2790
		ADS 2800
C	-----	ADS 2810
C	Now normalize values and get current values	ADS 2820
C	-----	ADS 2830
		ADS 2840
	IF (SINGLE) THEN	ADS 2850
	SUM = 0.0	ADS 2860
	DO 150 I = 1, INSP	ADS 2870
	KNOWN(I) = 10.0**KNOWN(I)	ADS 2880
	SUM = SUM + (KNOWN(I) * DABS(ANSWER(I,NEUT)))	ADS 2890
150	CONTINUE	ADS 2900
		ADS 2910
	DO 160 I = 1, INSP	ADS 2920
	KNOWN(I) = KNOWN(I) * CEC / (1000.0 * SUM)	ADS 2930
160	CONTINUE	ADS 2940
		ADS 2950
	ELSE	ADS 2960
	CROSS = .FALSE.	ADS 2970
	IVAL = 0	ADS 2980
	VAL = 0.0D00	ADS 2990
200	DO 220 I = 1, MAX0(INSP, NEUT)	ADS 3000
	VECT(I) = KNOWN(I)	ADS 3010
	DO 210 K = 1, MAX0(INSP, NEUT)	ADS 3020
	MAT(K,I) = ANSWER(K,I)	ADS 3030
210	CONTINUE	ADS 3040
220	CONTINUE	ADS 3050
		ADS 3060
	VECT(NEUT) = VAL	ADS 3070
		ADS 3080
	DO 250 I = 1, MAX0(INSP, NEUT)	ADS 3090
	IF (I .NE. NEUT) THEN	ADS 3100
	X = MAT(I,NEUT) / MAT(NEUT,NEUT)	ADS 3110
	VECT(I) = VECT(I) - (X * VECT(NEUT))	ADS 3120
	END IF	ADS 3130
250	CONTINUE	ADS 3140
		ADS 3150
	SUM = 0.0	ADS 3160
	DO 260 I = 1, INSP	ADS 3170
	SUM = SUM + (10.0**VECT(I))	ADS 3180
260	CONTINUE	ADS 3190
		ADS 3200
	IVAL = IVAL + 1	ADS 3210
	TRYV(IVAL) = VAL	ADS 3220
	DIFF(IVAL) = SUM - 1.0D00	ADS 3230
	IF (DABS(DIFF(IVAL)) .GT. TEST) THEN	ADS 3240
	IF (IVAL .GT. 1 .AND. .NOT. CROSS) THEN	ADS 3250
	IF ((DIFF(IVAL) * DIFF(IVAL-1)) .LT. 0.0) CROSS = .TRUE.	ADS 3260
	END IF	ADS 3270

	IF (IVAL .GT. 1) THEN	ADS 3280
	I = 1	ADS 3290
	CALL SORTA(TRYV, DIFF, IVAL, I)	ADS 3300
	END IF	ADS 3310
	IF (CROSS) THEN	ADS 3320
	K = 0	ADS 3330
	DO 270 I = 1, (IVAL-1)	ADS 3340
	IF ((DIFF(I) * DIFF(I+1)) .LT. 0.0) K = I	ADS 3350
270	CONTINUE	ADS 3360
	IF (IVAL .GT. 5) THEN	ADS 3370
	IF (K .GT. (IVAL/2)) THEN	ADS 3380
	DO 280 I = 1, (IVAL-1)	ADS 3390
	DIFF(I) = DIFF(I+1)	ADS 3400
	TRYV(I) = TRYV(I+1)	ADS 3410
280	CONTINUE	ADS 3420
	K = K - 1	ADS 3430
	END IF	ADS 3440
	IVAL = IVAL - 1	ADS 3450
	END IF	ADS 3460
	CALL GUESS(TRYV, DIFF, VAL, IVAL)	ADS 3470
	X = DABS(TRYV(K) - TRYV(K+1)) / 10000.0D00	ADS 3480
	IF (DABS(TRYV(K) - VAL) .LT. X .OR.	ADS 3490
	DABS(TRYV(K+1) - VAL) .LT. X) THEN	ADS 3500
	VAL = (TRYV(K) + TRYV(K+1)) / 2.0	ADS 3510
	END IF	ADS 3520
	END IF	ADS 3530
	IF (.NOT. CROSS) THEN	ADS 3540
	IF (IVAL .GT. 2) THEN	ADS 3550
	DO 290 I = 1, (IVAL-1)	ADS 3560
	DIFF(I) = DIFF(I+1)	ADS 3570
	TRYV(I) = TRYV(I+1)	ADS 3580
290	CONTINUE	ADS 3590
	IVAL = IVAL - 1	ADS 3600
	END IF	ADS 3610
	IF (IVAL .EQ. 1) THEN	ADS 3620
	VAL = VAL - 1.0D00	ADS 3630
	ELSE IF (DABS(DIFF(IVAL)) .LT. DABS(DIFF(IVAL-1))) THEN	ADS 3640
	VAL = (2.0 * TRYV(IVAL)) - TRYV(IVAL-1)	ADS 3650
	ELSE	ADS 3660
	VAL = (2.0 * TRYV(IVAL-1)) - TRYV(IVAL)	ADS 3670
	END IF	ADS 3680
	END IF	ADS 3690
	GO TO 200	ADS 3700
	END IF	ADS 3710
		ADS 3720
	DO 300 I = 1, INSP	ADS 3730
	KNOWN(I) = (10.0**VECT(I)) * CEC * 1.0D-3 /	ADS 3740
	DABS(ANSWER(I,NEUT))	ADS 3750
300	CONTINUE	ADS 3760
	END IF	ADS 3770
		ADS 3780
	IF (IEXCH .EQ. 1) THEN	ADS 3790
	SIGO = 0.0D00	ADS 3800
	SUM = 0.0D00	ADS 3810
	DO 330 I = 1, INSP	ADS 3820
	IF (ISCHG(I) .NE. 0) SIGO = (DBLE(ISCHG(I)) * KNOWN(I)) + SIGO	ADS 3830
	J = 0	ADS 3840
	DO 320 K = 1, ISCOMP(I)	ADS 3850

	IF (IDN(I,K) .EQ. 0) J = K	ADS 3860
320	CONTINUE	ADS 3870
	SUM = SUM + (DABS(COEF(I,J)) * KNOWN(I))	ADS 3880
330	CONTINUE	ADS 3890
	SIGO = ECHG * CEC * AVOG * SIGO / (SUM * 1000.0)	ADS 3900
	SIGD = 0.0D00	ADS 3910
	DO 350 I = 1, MXSP + 44	ADS 3920
	SIGD = (M(I) * (DEXP(DBLE(Z(I)) * YO * (-1.0D0)) - 1.0D0)) +	ADS 3930
	SIGD	ADS 3940
350	CONTINUE	ADS 3950
	SIGD = SIGD * 1000.0D00 * AVOG	ADS 3960
	IF (SIGD .GT. CPUMIN) THEN	ADS 3970
	SIGD = DSQRT(SIGD)	ADS 3980
	ELSE	ADS 3990
	SIGD = 0.0D00	ADS 4000
	END IF	ADS 4010
	SIGD = SIGD * DSQRT(2.0D00 * PERMV * DIE)	ADS 4020
	SIGD = SIGD * DSQRT(BOLTZ * (TC + 273.15))	ADS 4030
	IY = IY + 1	ADS 4040
	TRYO(IY) = YO	ADS 4050
	DIFYO(IY) = SIGD + SIGO	ADS 4060
	IF (DABS(DIFYO(IY)) .GT. TEST) THEN	ADS 4070
	IF (IY .GT. 1 .AND. .NOT. CROSSY) THEN	ADS 4080
	IF ((DIFYO(IY) * DIFYO(IY-1)) .LT. 0.0) CROSSY = .TRUE.	ADS 4090
	END IF	ADS 4100
	IF (CROSSY) THEN	ADS 4110
	I = 1	ADS 4120
	CALL SORTA(TRYO, DIFYO, IY, I)	ADS 4130
	END IF	ADS 4140
	IF (IY .GT. 6) THEN	ADS 4150
	K = 0	ADS 4160
	IF (CROSSY) THEN	ADS 4170
	DO 370 I = 1, (IY-1)	ADS 4180
	IF ((DIFYO(I) * DIFYO(I+1)) .LT. 0.0) K = I	ADS 4190
370	CONTINUE	ADS 4200
	END IF	ADS 4210
	IF (K .GT. (IY/2) .OR. .NOT. CROSSY) THEN	ADS 4220
	DO 380 I = 1, (IY-1)	ADS 4230
	DIFYO(I) = DIFYO(I+1)	ADS 4240
	TRYO(I) = TRYO(I+1)	ADS 4250
380	CONTINUE	ADS 4260
	K = K - 1	ADS 4270
	END IF	ADS 4280
	IY = IY - 1	ADS 4290
	END IF	ADS 4300
	IF (CROSSY) THEN	ADS 4310
	CALL GUESS(TRYO, DIFYO, YO, IY)	ADS 4320
	X = DABS(TRYO(K) - TRYO(K+1)) / 10000.0D00	ADS 4330
	IF (DABS(TRYO(K) - YO) .LT. X .OR.	ADS 4340
	DABS(TRYO(K+1) - YO) .LT. X) THEN	ADS 4350
	VAL = (TRYO(K) + TRYO(K+1)) / 2.0	ADS 4360
	END IF	ADS 4370
	ELSE	ADS 4380
	IF (DIFYO(IY) .GT. 0.0) THEN	ADS 4390
	YO = YO + 0.1D00	ADS 4400
	ELSE	ADS 4410
	YO = YO - 1.0D00	ADS 4420
	END IF	ADS 4430

END IF	ADS 4440
GO TO 100	ADS 4450
END IF	ADS 4460
END IF	ADS 4470
	ADS 4480
C -----	ADS 4490
C Check totels, see if we are done, calculate step size.	ADS 4500
C Always iterate at least once.	ADS 4510
C -----	ADS 4520
500 DO 505 I = 1, MXSP + 44	ADS 4530
CNMMIX(I) = ANALM(I)	ADS 4540
505 CONTINUE	ADS 4550
	ADS 4560
EQC = 0.0	ADS 4570
EQH = 0.0	ADS 4580
CNMMIX(7) = TOTEL(3)	ADS 4590
CNMMIX(98) = 0.0	ADS 4600
DO 520 I = 1, INSP	ADS 4610
DO 510 K = 1, ISCOMP(I)	ADS 4620
J = IDN(I,K)	ADS 4630
IF (J .EQ. 0 .OR. DABS(COEF(I,K)) .LT. CPUMIN) GO TO 510	ADS 4640
X = KNOWN(I) * COEF(I,K) * (-1.0)	ADS 4650
EQFAC = 0.0	ADS 4660
IF (J .EQ. 7) EQFAC = 1.0	ADS 4670
IF (J .EQ. 8) EQFAC = 1.0	ADS 4680
IF (J .EQ. 9) EQFAC = -1.0	ADS 4690
IF (J .EQ. 11) J = 12	ADS 4700
IF (J .EQ. 12) EQFAC = 4.0	ADS 4710
IF (J .EQ. 28) EQFAC = 2.0	ADS 4720
IF (J .EQ. 31) EQFAC = -3.0	ADS 4730
IF (J .EQ. 32) EQFAC = -1.0	ADS 4740
IF (J .EQ. 33) EQFAC = 2.0	ADS 4750
IF (J .EQ. 49) EQFAC = 1.0	ADS 4760
IF (J .EQ. 97) EQFAC = 2.0	ADS 4770
EQH = EQH + (X * EQFAC)	ADS 4780
	ADS 4790
	ADS 4800
IF (J .EQ. 7) EQC = (X) + EQC	ADS 4810
IF (J .EQ. 97) EQC = (X) + EQC	ADS 4820
IF (J .EQ. 98) EQC = (X) + EQC	ADS 4830
IF (J .EQ. 207) EQC = (X) + EQC	ADS 4840
IF (J .EQ. 208) EQC = (X * 2.0) + EQC	ADS 4850
IF (J .EQ. 209) EQC = (X * 3.0) + EQC	ADS 4860
IF (J .EQ. 7 .OR. J .EQ. 97 .OR. J .EQ. 98 .OR.	ADS 4870
J .EQ. 207 .OR. J .EQ. 208 .OR. J .EQ. 209) J = 7	ADS 4880
	ADS 4890
CNMMIX(J) = CNMMIX(J) + X	ADS 4900
510 CONTINUE	ADS 4910
520 CONTINUE	ADS 4920
	ADS 4930
C3MIX(1) = TOTEL(1) + EQH	ADS 4940
C3MIX(2) = TOTEL(2)	ADS 4950
C3MIX(3) = TOTEL(3) + EQC	ADS 4960
IF (C3MIX(3) .GT. 0.0) THEN	ADS 4970
CNMMIX(7) = C3MIX(3)	ADS 4980
CNMMIX(98) = 0.0	ADS 4990
ELSE	ADS 5000
CNMMIX(7) = 0.0	ADS 5010

CNMMIX(98) = 0.0	ADS 5020
END IF	ADS 5030
IF (ICALL .EQ. 1) THEN	ADS 5040
DONE = .FALSE.	ADS 5050
DO 530 I = 1, INSP	ADS 5060
J = IBASE(I)	ADS 5070
IF (J .EQ. 11) J = 12	ADS 5080
IF (J .NE. 0 .AND. J .NE. 8 .AND. J .NE. 9 .AND. J .NE. 10)	ADS 5090
THEN	ADS 5100
STEP(I) = (BNMMIX(J) - CNMMIX(J)) * 0.25	ADS 5110
ELSE IF (J .EQ. 8 .OR. J .EQ. 9) THEN	ADS 5120
X = (B2MIX(1) - B2MIX(2)) - (C3MIX(1) - C3MIX(2))	ADS 5130
IF (DABS(X) .GT. 1.0E-06) STEP(I) = X * 0.1	ADS 5140
END IF	ADS 5150
IF (DABS(STEP(I)) .LT. CPUMIN) THEN	ADS 5160
STEP(I) = (CEC / 1000.0) / 100.0	ADS 5170
END IF	ADS 5180
530 CONTINUE	ADS 5190
IF (INSP .EQ. 2) THEN	ADS 5200
X = (DABS(STEP(1)) + DABS(STEP(2))) / 2.0	ADS 5210
STEP(1) = DSIGN(X, STEP(1))	ADS 5220
STEP(2) = DSIGN(X, STEP(2))	ADS 5230
END IF	ADS 5240
ELSE	ADS 5250
DONE = .TRUE.	ADS 5260
DO 550 I = 1, INSP	ADS 5270
J = IBASE(I)	ADS 5280
IF (J .NE. 0 .AND. J .NE. 8 .AND. J .NE. 9 .AND. J .NE. 10)	ADS 5290
THEN	ADS 5300
IF ((DABS(BNMMIX(J) - CNMMIX(J)) / BNMMIX(J)) .GT. TEST)	ADS 5310
DONE = .FALSE.	ADS 5320
IF ((BNMMIX(J) - CNMMIX(J)) .GT. 0.0) THEN	ADS 5330
IF (STEP(I) .LT. 0.0) STEP(I) = STEP(I) * (-0.4)	ADS 5340
ELSE	ADS 5350
IF (STEP(I) .GT. 0.0) STEP(I) = STEP(I) * (-0.4)	ADS 5360
END IF	ADS 5370
ELSE IF (J .EQ. 8 .OR. J .EQ. 9) THEN	ADS 5380
X = (B2MIX(1) - B2MIX(2)) - (C3MIX(1) - C3MIX(2))	ADS 5390
IF ((DABS(B2MIX(1) - B2MIX(2))) .GT. 1.0D-8)	ADS 5400
X = X / (B2MIX(1) - B2MIX(2))	ADS 5410
IF (DABS(X) .GT. TEST) DONE = .FALSE.	ADS 5420
IF (X .GT. 0.0) THEN	ADS 5430
IF (STEP(I) .LT. 0.0) STEP(I) = STEP(I) * (-0.4)	ADS 5440
ELSE	ADS 5450
IF (STEP(I) .GT. 0.0) STEP(I) = STEP(I) * (-0.4)	ADS 5460
END IF	ADS 5470
END IF	ADS 5480
550 CONTINUE	ADS 5490
END IF	ADS 5500
IF (DONE) THEN	ADS 5510
J = NEUT	ADS 5520
IF (NEUT .EQ. 0) J = INSP+1	ADS 5530
OK = 0	ADS 5540
CALL PAGE	ADS 5550
IPGLN = IPGLN + 26 + (INSP * 3)	ADS 5560
WRITE (UNO, 1005)	ADS 5570
	ADS 5580
	ADS 5590

WRITE (UNO, 1002)	ADS 5600
DO 600 I = 1, INSP	ADS 5610
WRITE (UNO, 1003) SPN(I),	ADS 5620
(MBASE(I) * CEC / (1000.0 * DABS(ANSWER(I,J)))),	ADS 5630
(MBASE(I) * CEC / 1000.0), MBASE(I)	ADS 5640
600 CONTINUE	ADS 5650
	ADS 5660
WRITE (UNO, 1007)	ADS 5670
DO 620 I = 1, INSP	ADS 5680
DO 610 K = 1, ISCOMP(I)	ADS 5690
IF (IDN(I,K) .EQ. 0) THEN	ADS 5700
DUM(K) = 'X-'	ADS 5710
ELSE	ADS 5720
DUM(K) = PAGE1(IDN(I,K))	ADS 5730
END IF	ADS 5740
610 CONTINUE	ADS 5750
WRITE (UNO, 1008) KRXXN(I), SPN(I), (DUM(K), COEF(I,K), K=1,	ADS 5760
ISCOMP(I))	ADS 5770
620 CONTINUE	ADS 5780
	ADS 5790
WRITE (UNO, 1001)	ADS 5800
WRITE (UNO, 1002)	ADS 5810
DO 650 I = 1, INSP	ADS 5820
WRITE (UNO, 1003) SPN(I), KNOWN(I),	ADS 5830
(KNOWN(I) * DABS(ANSWER(I,J))),	ADS 5840
(KNOWN(I) * 1000.0 * DABS(ANSWER(I,J)) / CEC)	ADS 5850
650 CONTINUE	ADS 5860
	ADS 5870
WRITE (UNO, 1006) CEC, (CEC / 1000.0)	ADS 5880
RETURN	ADS 5890
END IF	ADS 5900
	ADS 5910
C -----	ADS 5920
C Change the original solution parameters for the new step and	ADS 5930
C go back to calculate species distribution	ADS 5940
C -----	ADS 5950
	ADS 5960
700 EQC = 0.0	ADS 5970
EQH = 0.0	ADS 5980
ANALM(7) = ALMIX(3)	ADS 5990
ANALM(98) = 0.0	ADS 6000
DO 710 I = 1, INSP	ADS 6010
ADD(I) = ADD(I) + STEP(I)	ADS 6020
710 CONTINUE	ADS 6030
	ADS 6040
DO 730 I = 1, INSP	ADS 6050
DO 720 K = 1, ISCOMP(I)	ADS 6060
J = IDN(I,K)	ADS 6070
IF (J .EQ. 0 .OR. DABS(COEF(I,K)) .LT. CPUMIN) GO TO 720	ADS 6080
X = COEF(I,K) * ADD(I) * (-1.0)	ADS 6090
EQFAC = 0.0	ADS 6100
IF (J .EQ. 7) EQFAC = 1.0	ADS 6110
IF (J .EQ. 8) EQFAC = 1.0	ADS 6120
IF (J .EQ. 9) EQFAC = -1.0	ADS 6130
IF (J .EQ. 11) J = 12	ADS 6140
IF (J .EQ. 12) EQFAC = 4.0	ADS 6150
IF (J .EQ. 28) EQFAC = 2.0	ADS 6160
IF (J .EQ. 31) EQFAC = -3.0	ADS 6170

IF (J .EQ. 32) EQFAC = -1.0	ADS 6180
IF (J .EQ. 33) EQFAC = 2.0	ADS 6190
IF (J .EQ. 49) EQFAC = 1.0	ADS 6200
IF (J .EQ. 97) EQFAC = 2.0	ADS 6210
EQH = EQH + (X * EQFAC)	ADS 6220
	ADS 6230
IF (J .EQ. 7) EQC = (X) + EQC	ADS 6240
IF (J .EQ. 97) EQC = (X) + EQC	ADS 6250
IF (J .EQ. 98) EQC = (X) + EQC	ADS 6260
IF (J .EQ. 207) EQC = (X) + EQC	ADS 6270
IF (J .EQ. 208) EQC = (X * 2.0) + EQC	ADS 6280
IF (J .EQ. 209) EQC = (X * 3.0) + EQC	ADS 6290
IF (J .EQ. 7 .OR. J .EQ. 97 .OR. J .EQ. 98 .OR.	ADS 6300
J .EQ. 207 .OR. J .EQ. 208 .OR. J .EQ. 209) J = 7	ADS 6310
	ADS 6320
ANALM(J) = ANMMIX(J) + X	ADS 6330
IF (J .NE. 8 .AND. J .NE. 9 .AND. J .NE. 10	ADS 6340
.AND. ANALM(J) .LE. 0.0) THEN	ADS 6350
DO 715 J = 1, INSP	ADS 6360
ADD(J) = ADD(J) - STEP(J)	ADS 6370
STEP(J) = STEP(J) * (0.5D00)	ADS 6380
715 CONTINUE	ADS 6390
GO TO 700	ADS 6400
END IF	ADS 6410
720 CONTINUE	ADS 6420
730 CONTINUE	ADS 6430
	ADS 6440
TOTEL(1) = A1MIX(1) + EQH	ADS 6450
TOTEL(3) = A1MIX(3) + EQC	ADS 6460
IF (TOTEL(3) .GT. 0.0) THEN	ADS 6470
ANALM(7) = TOTEL(3)	ADS 6480
ANALM(98) = 0.0	ADS 6490
ELSE	ADS 6500
ANALM(7) = 0.0	ADS 6510
ANALM(98) = 0.0	ADS 6520
END IF	ADS 6530
	ADS 6540
J = 0	ADS 6550
DO 800 I = 1, 28	ADS 6560
J = J + 1	ADS 6570
IF (J .EQ. 8) J = 12	ADS 6580
IF (J .EQ. 17) J = 18	ADS 6590
IF (J .EQ. 19) J = 21	ADS 6600
IF (J .EQ. 24) J = 25	ADS 6610
IF (J .EQ. 34) J = 48	ADS 6620
IF (J .EQ. 49) J = 169	ADS 6630
IF (J .EQ. 170) J = 210	ADS 6640
EXELT(I) = ANALM(J)	ADS 6650
800 CONTINUE	ADS 6660
EXELT(29) = ANALM(7)	ADS 6670
EXELT(30) = ANALM(246)	ADS 6680
EXELT(31) = ANALM(265)	ADS 6690
EXELT(32) = ANALM(136)	ADS 6700
EXELT(33) = ANALM(MXSP+1)	ADS 6710
EXELT(34) = ANALM(MXSP+16)	ADS 6720
EXELT(35) = ANALM(MXSP+31)	ADS 6730
	ADS 6740
TITR(1) = EXELT(29)	ADS 6750

TITR(2) = EXELT(6)	ADS 6760
TITR(3) = EXELT(22)	ADS 6770
TITR(4) = EXELT(21)	ADS 6780
TITR(5) = EXELT(5)	ADS 6790
TITR(6) = EXELT(26)	ADS 6800
TITR(7) = EXELT(25)	ADS 6810
TITR(8) = EXELT(30)	ADS 6820
TITR(9) = EXELT(31)	ADS 6830
TITR(10) = EXELT(33)	ADS 6840
TITR(11) = EXELT(34)	ADS 6850
	ADS 6860
HTOTI = TOTEL(1)	ADS 6870
OHTOTI = TOTEL(2)	ADS 6880
	ADS 6890
J = NEUT	ADS 6900
IF (NEUT .EQ. 0) J = INSP+1	ADS 6910
OK = 1	ADS 6920
IF (IPRIN2 .NE. 0) THEN	ADS 6930
IF ((IPGLN + INSP + 9) .GT. 58) CALL PAGE	ADS 6940
IPGLN = IPGLN + INSP + 9	ADS 6950
WRITE (UNO, 1000)	ADS 6960
WRITE (UNO, 1002)	ADS 6970
DO 970 I = 1, INSP	ADS 6980
WRITE (UNO, 1003) SPN(I), KNOWN(I),	ADS 6990
(KNOWN(I) * DABS(ANSWER(I,J))),	ADS 7000
(KNOWN(I) * 1000.0 * DABS(ANSWER(I,J)) / CEC)	ADS 7010
970 CONTINUE	ADS 7020
	ADS 7030
WRITE (UNO, 1004)	ADS 7040
END IF	ADS 7050
	ADS 7060
RETURN	ADS 7070
	ADS 7080
1000 FORMAT(/, ' Surface Conditions calculated for the next',	ADS 7090
' step ')	ADS 7100
1001 FORMAT(/, ' Final Equilibrium Surface Conditions')	ADS 7110
1002 FORMAT(/,3X, 'Surface', 9X, 'Moles on', 11X, 'Moles of', 6X,	ADS 7120
' Fraction of',	ADS 7130
/,3X, 'Complex', 9X, 'Surface', 10X, 'Surface Site', 4X,	ADS 7140
'Surface Sites')	ADS 7150
1003 FORMAT(5X, A, 2X, E12.5, 7X, E12.5, 7X, F6.4)	ADS 7160
1004 FORMAT(/)	ADS 7170
1005 FORMAT(/, ' Initial Surface Conditions')	ADS 7180
1006 FORMAT(/, ' CEC = ',E12.5,' milli-equivalents ',	ADS 7190
/, ' ',E12.5,' moles exchange capacity for mono',	ADS 7200
'valent cations and anions')	ADS 7210
1007 FORMAT(/, ' K Surface Comp. Species and Coef. '	ADS 7220
/)	ADS 7230
1008 FORMAT(E12.5, ' = ',A, 10(' * (' ,A,'**',F6.2,')',:))	ADS 7240
END	ADS 7250

	SUBROUTINE AITLIM (X, Y, CROSS)	AIT 0010
C	=====	AIT 0020
C	Determines maximum stepsize for convergence on anions	AIT 0030

C	-----	AIT 0040
C	CROSS LOG Indicates root has been crossed	AIT 0050
C	RATIO DBL Test value based on Y	AIT 0060
C	X DBL Multiplication factor for stepsize	AIT 0070
C	Y DBL Currently calculated value over mass of	AIT 0080
C	component in solution	AIT 0090
C	-----	AIT 0100
	DOUBLE PRECISION X, Y, RATIO	AIT 0110
	LOGICAL CROSS	AIT 0120
	INTRINSIC DABS	AIT 0130
C	=====	AIT 0140
	RATIO = DABS(1.0D00 - Y)	AIT 0150
		AIT 0160
	IF (CROSS) THEN	AIT 0170
	X = X / 2.0	AIT 0180
	IF (X .LT. 1.0) X = 1.0	AIT 0190
	ELSE	AIT 0200
	X = X * 1.3	AIT 0210
	END IF	AIT 0220
		AIT 0230
	IF (X .GT. 20.0) X = 20.0	AIT 0240
		AIT 0250
	IF (RATIO .GT. 0.02 .AND. X .GT. 10.0) X = 10.0	AIT 0260
	IF (RATIO .GT. 0.05 .AND. X .GT. 5.0) X = 5.0	AIT 0270
	IF (RATIO .GT. 0.10 .AND. X .GT. 3.0) X = 3.0	AIT 0280
	IF (RATIO .GT. 0.20 .AND. X .GT. 2.0) X = 2.0	AIT 0290
	IF (RATIO .GT. 0.3) X = 1.0	AIT 0300
		AIT 0310
	RETURN	AIT 0320
	END	AIT 0330
		AIT 0340

	DOUBLE PRECISION FUNCTION ATCPRD (IC, INDEX, COEF, ALFA)	ATC 0010
C	=====	ATC 0020
C	This function calculates the activity products for reactions	ATC 0030
C	-----	ATC 0040
C	ALFA DBL Activity of aqueous species	ATC 0050
C	COEF DBL Stoichiometric coefficient for the species	ATC 0060
C	CPUMIN DBL Smallest positive real value program uses	ATC 0070
C	I INT Loop counting variable	ATC 0080
C	IC INT Number of components	ATC 0090
C	INDEX INT Index number of the components	ATC 0100
C	J INT Current index number of this component	ATC 0110
C	-----	ATC 0120
	DOUBLE PRECISION CPUMIN	ATC 0130
	PARAMETER (CPUMIN = 1.0D-35)	ATC 0140
		ATC 0150
	INTEGER I, IC, INDEX(*), J	ATC 0160
	DOUBLE PRECISION ALFA(*), COEF(*)	ATC 0170
	INTRINSIC DLOG10	ATC 0180
		ATC 0190
		ATC 0200
C	=====	ATC 0210
		ATC 0220

ATCPRD = 0.0D00	ATC 0230
DO 100 I=1, IC	ATC 0240
J = INDEX(I)	ATC 0250
IF (J .GT. 0) THEN	ATC 0260
IF (ALFA(J) .LT. CPUMIN) THEN	ATC 0270
ATCPRD = -999.99	ATC 0280
RETURN	ATC 0290
END IF	ATC 0300
ATCPRD = ATCPRD + (COEF(I) * DLOG10(ALFA(J)))	ATC 0310
END IF	ATC 0320
100 CONTINUE	ATC 0330
RETURN	ATC 0340
END	ATC 0350
	ATC 0360
	ATC 0370

SUBROUTINE CALCUL (A, B, TDS, Y28, DNS, TEMP, HITEMP, PRESS, DENS,			CAL 0010
EHM, EHMC, EMFZSC, GFW, Z, UNITS, MXSP, TIC,			CAL 0020
ANMTIC, GAMMA, TCO2, BDAT, BDOT, MNACLD,			CAL 0030
NUFLAG)			CAL 0040
C	=====		CAL 0050
C	This routine will do the following:		CAL 0060
C	1) Calculate eh from field data.		CAL 0070
C	2) Calculate analyzed molality.		CAL 0080
C	3) Calculate cation-anion balance.		CAL 0090
C	4) Calc. temp. effects on debye-huckel solvent constants.		CAL 0100
C	-----		CAL 0110
C	A	DBL Molal Debye-Huckel coefficient	CAL 0120
C	ANALM	DBL Analyzed molality of species i	CAL 0130
C	ANMTIC	DBL Analyzed TIC	CAL 0140
C	B	DBL Molal Debye-Huckel coefficient	CAL 0150
C	BDAT	DBL B-dot as a function of temperature	CAL 0160
C	BDOT	DBL Activity coefficient deviation function	CAL 0170
C	CADENS	DBL Calculated density	CAL 0180
C	CPUMIN	DBL Smallest positive real value program uses	CAL 0190
C	CUNITS	DBL Analytical input concentration	CAL 0200
C	CURDEN	DBL Current density	CAL 0210
C	DENOLD	DBL Previous density, used for iterations	CAL 0220
C	DENS	DBL Density	CAL 0230
C	DNS	CHA Determines if density should be calculated	CAL 0240
C	EHM	DBL Measured Eh in volts	CAL 0250
C	EHMC	DBL Measured Eh using the Calomel electrode	CAL 0260
C	EMFZSC	DBL Measured Eh using the Zobell's solution	CAL 0270
C	EXELT	DBL Total moles of component.	CAL 0280
C	GAMMA	DBL Activity coef. of species	CAL 0290
C	GFW	DBL Gram formula weight of aqueous species	CAL 0300
C	GFWC	DBL Gram Formula weight of carbon	CAL 0310
C	HITEMP	DBL In-situ temperature	CAL 0320
C	I	INT Loop variable	CAL 0330
C	IMIX	INT Switch used in MIXER routines	CAL 0340
C	J	INT Loop variable	CAL 0350
C	M	DBL Calculated molality of aqueous species	CAL 0360
C	MNACLD	DBL Sum of Molality * charge / 2	CAL 0370
C	MXSP	INT Total number of aqueous species	CAL 0380

C	NMAX	INT	General array dimension to allow easy expansion	CAL 0390
C	NUFLAG	INT	Sets the activity coefficients of neutral species	CAL 0400
C	PRESS	DBL	Total pressure	CAL 0410
C	S1	DBL	Temperary sum variable	CAL 0420
C	S2	DBL	Temperary sum variable	CAL 0430
C	S3	DBL	Temperary sum variable	CAL 0440
C	T	DBL	Temperature in deg. K	CAL 0450
C	TCO2	DBL	Activity coefficients of CO2 with temperature	CAL 0460
C	TDS	DBL	Total Dissolved Solids (UNITS = KG/L)	CAL 0470
C	TEMP	DBL	Temperature of the solution when pH was measured	CAL 0480
C	TIC	DBL	Concentration of total inorganic carbon	CAL 0490
C	TITR	DBL	Used for convergence in DISTRB	CAL 0500
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	CAL 0510
C	UNITS	CHA	Units of concentration	CAL 0520
C	Y28	INT	Set at hitemp to skip unneeded calculations	CAL 0530
C	Z	INT	Charge of aqueous species	CAL 0540
C	-----			CAL 0550
	INTEGER NMAX			CAL 0560
	DOUBLE PRECISION CPUMIN, GFWC			CAL 0570
				CAL 0580
				CAL 0590
	PARAMETER (NMAX = 340)			CAL 0600
	PARAMETER (CPUMIN=1.0D-35, GFWC = 12.011D0)			CAL 0610
				CAL 0620
	CHARACTER*1 DNS			CAL 0630
	CHARACTER*5 UNITS			CAL 0640
				CAL 0650
	INTEGER I, IBMIX, IDMIX(50), IMIX, INMIX, ITMIX			CAL 0660
	INTEGER J, MXSP, NUFLAG, Y28, Z(NMAX)			CAL 0670
				CAL 0680
	DOUBLE PRECISION A, ALFA(NMAX), AMOL(50), ANALM(NMAX), ANMTIC			CAL 0690
	DOUBLE PRECISION B, BDAT(10), BDOT, CADENS, CO2F, CUNITS(NMAX)			CAL 0700
	DOUBLE PRECISION CURDEN, DENOLD, DENS, DFRAC1, DINC, EHM, EHMC			CAL 0710
	DOUBLE PRECISION EMFZSC, EXELT(35), FBOIL, GAMMA(NMAX)			CAL 0720
	DOUBLE PRECISION GFW(NMAX), HITEMP, HTOTI, KHCO2, KHH2S			CAL 0730
	DOUBLE PRECISION M(NMAX), MNACLD, OHTOTI, PH, PRESS, S1, S2, S3			CAL 0740
	DOUBLE PRECISION T, TCO2(10), TDS, TEMP, TIC, TITR(11), TOTEL(5)			CAL 0750
				CAL 0760
	EXTERNAL KHCO2, KHH2S			CAL 0770
				CAL 0780
	INTRINSIC DABS, DSQRT, IABS			CAL 0790
				CAL 0800
	COMMON /AMM / IDMIX, AMOL, ITMIX, INMIX, DFRAC1, DINC, FBOIL			CAL 0810
	COMMON /EXTOT / EXELT, TOTEL, TITR			CAL 0820
	COMMON /IMM / IBMIX, IMIX			CAL 0830
	COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS			CAL 0840
	COMMON /TOTALS/ CO2F, HTOTI, OHTOTI			CAL 0850
				CAL 0860
	SAVE DENOLD			CAL 0870
				CAL 0880
C	=====			CAL 0890
				CAL 0900
	T = TEMP + 273.15D0			CAL 0910
	IF (Y28 .EQ. 1) GO TO 70			CAL 0920
				CAL 0930
C	-----			CAL 0940
C	Calculation of Eh from field data.			CAL 0950
C	-----			CAL 0960

IF ((DABS(EMFZSC - 9.0D0)) .LT. 1.0D-10) THEN	CAL 0970
S1 = 0.2145D0 - (7.6D-04 * (TEMP - 25.0D0))	CAL 0980
ELSE	CAL 0990
S1 = 4.28D-1 - (2.2D-03 * (TEMP - 25.0D0)) - EMFZSC	CAL 1000
END IF	CAL 1010
	CAL 1020
IF (EHMC .LT. 9.D0) EHM = EHMC + S1	CAL 1030
	CAL 1040
	CAL 1050
C -----	CAL 1060
C Calculation of analyzed molality.	CAL 1070
C If no value for density is entered then one will be computed	CAL 1080
C using the empirical equation:	CAL 1090
C DENSITY = 1.00 + 6.88 X 10 D-7 X TOTAL DISSOLVED SOLIDS	CAL 1100
C -----	CAL 1110
	CAL 1120
CURDEN = DENS	CAL 1130
TDS = 0.0D00	CAL 1140
	CAL 1150
10 CONTINUE	CAL 1160
S1 = 0.0D00	CAL 1170
DO 20 I = 1, MXSP + 44	CAL 1180
IF (UNITS .EQ. 'PPM ') THEN	CAL 1190
S1 = S1 + (1.0D-6 * CUNITS(I) * DENS)	CAL 1200
ELSE IF (UNITS .EQ. 'MG/L ') THEN	CAL 1210
S1 = S1 + (1.0D-6 * CUNITS(I))	CAL 1220
ELSE IF (UNITS .EQ. 'MOL/L' .OR. UNITS .EQ. 'MOL/K') THEN	CAL 1230
S1 = S1 + (1.0D-3 * CUNITS(I) * GFW(I) * (DENS - TDS))	CAL 1240
ELSE IF (UNITS .EQ. 'MEQ/L' .AND. Z(I) .NE. 0) THEN	CAL 1250
S1 = S1 + (1.0D-6 * CUNITS(I) * GFW(I) * (DENS - TDS) /	CAL 1260
IABS(Z(I)))	CAL 1270
END IF	CAL 1280
20 CONTINUE	CAL 1290
	CAL 1300
CADENS = 1.0D0 + (6.88D-7 * (1.0D6 * S1))	CAL 1310
IF (DNS .EQ. 'U') THEN	CAL 1320
DENS = CADENS	CAL 1330
DENOLD = CADENS	CAL 1340
END IF	CAL 1350
	CAL 1360
IF (S1 .GT. CPUMIN) THEN	CAL 1370
IF (DABS((TDS - S1) / S1) .LT. 0.0001) THEN	CAL 1380
TDS = S1	CAL 1390
ELSE	CAL 1400
TDS = S1	CAL 1410
GO TO 10	CAL 1420
END IF	CAL 1430
END IF	CAL 1440
	CAL 1450
IF (DNS .EQ. 'N') THEN	CAL 1460
CURDEN = CURDEN + CADENS - DENOLD	CAL 1470
ELSE IF (DNS .EQ. 'U') THEN	CAL 1480
CURDEN = DENS	CAL 1490
END IF	CAL 1500
	CAL 1510
DNS = 'N'	CAL 1520
DENOLD = CADENS	CAL 1530
DENS = CURDEN	CAL 1540

IF (IMIX .EQ. 1) GO TO 40	CAL 1550
	CAL 1560
	CAL 1570
DO 30 I = 1, MXSP + 44	CAL 1580
M(I) = 0.0D0	CAL 1590
IF (UNITS .EQ. 'PPM ' .AND. GFW(I) .GT. CPUMIN) THEN	CAL 1600
M(I) = 1.0D-3 * CUNITS(I) * DENS / (GFW(I) * (DENS - TDS))	CAL 1610
ELSE IF (UNITS .EQ. 'MG/L ' .AND. GFW(I) .GT. CPUMIN) THEN	CAL 1620
M(I) = 1.0D-3 * CUNITS(I) / (GFW(I) * (DENS - TDS))	CAL 1630
ELSE IF (UNITS .EQ. 'MOL/L') THEN	CAL 1640
M(I) = CUNITS(I) / (DENS - TDS)	CAL 1650
ELSE IF (UNITS .EQ. 'MOL/K') THEN	CAL 1660
M(I) = CUNITS(I)	CAL 1670
ELSE IF (UNITS .EQ. 'MEQ/L' .AND. Z(I) .NE. 0) THEN	CAL 1680
M(I) = 1.0D-3 * CUNITS(I) / (IABS(Z(I)) * (DENS - TDS))	CAL 1690
END IF	CAL 1700
ANALM(I) = M(I)	CAL 1710
30 CONTINUE	CAL 1720
	CAL 1730
IF (UNITS .EQ. 'PPM ') THEN	CAL 1740
ANMTIC = TIC * 1.0D-3 * DENS / (GFWC * (DENS - TDS))	CAL 1750
ELSE IF (UNITS .EQ. 'MG/L ') THEN	CAL 1760
ANMTIC = TIC * 1.0D-3 / (GFWC * (DENS - TDS))	CAL 1770
ELSE IF (UNITS .EQ. 'MOL/L') THEN	CAL 1780
ANMTIC = TIC / (DENS - TDS)	CAL 1790
ELSE IF (UNITS .EQ. 'MOL/K') THEN	CAL 1800
ANMTIC = TIC	CAL 1810
END IF	CAL 1820
	CAL 1830
40 CONTINUE	CAL 1840
	CAL 1850
C -----	CAL 1860
C Set the mass balance variables to be used in species distribution	CAL 1870
C -----	CAL 1880
	CAL 1890
J = 0	CAL 1900
DO 60 I = 1, 28	CAL 1910
J = J + 1	CAL 1920
IF (J .EQ. 8) J = 12	CAL 1930
IF (J .EQ. 17) J = 18	CAL 1940
IF (J .EQ. 19) J = 21	CAL 1950
IF (J .EQ. 24) J = 25	CAL 1960
IF (J .EQ. 34) J = 48	CAL 1970
IF (J .EQ. 49) J = 169	CAL 1980
IF (J .EQ. 170) J = 210	CAL 1990
EXELT(I) = M(J)	CAL 2000
60 CONTINUE	CAL 2010
	CAL 2020
EXELT(29) = M(7) + (2.0 * M(98))	CAL 2030
EXELT(30) = M(246)	CAL 2040
EXELT(31) = M(265)	CAL 2050
EXELT(32) = M(136)	CAL 2060
EXELT(33) = M(MXSP+1)	CAL 2070
EXELT(34) = M(MXSP+16)	CAL 2080
EXELT(35) = M(MXSP+31)	CAL 2090
	CAL 2100
	CAL 2110
TITR(1) = EXELT(29)	CAL 2120

TITR(2) = EXELT(6)	CAL 2130
TITR(3) = EXELT(22)	CAL 2140
TITR(4) = EXELT(21)	CAL 2150
TITR(5) = EXELT(5)	CAL 2160
TITR(6) = EXELT(26)	CAL 2170
TITR(7) = EXELT(25)	CAL 2180
TITR(8) = EXELT(30)	CAL 2190
TITR(9) = EXELT(31)	CAL 2200
TITR(10) = EXELT(33)	CAL 2210
TITR(11) = EXELT(34)	CAL 2220
70 CONTINUE	CAL 2230
	CAL 2240
	CAL 2250
	CAL 2260
MNACLD = 0.0D0	CAL 2270
DO 80 I = 1, MXSP + 44	CAL 2280
MNACLD = MNACLD + (ANALM(I) * IABS(Z(I)))	CAL 2290
80 CONTINUE	CAL 2300
MNACLD = 0.5*MNACLD + 1.D0	CAL 2310
	CAL 2320
C -----	CAL 2330
C Calculation of the activity coeffs (gamma) for neutral species.	CAL 2340
C Gamma = 1 if nuflag = 1. If nuflag = 0 then gamma for neutral	CAL 2350
C species are equal to gamma(co2) except for gamma(h2s) which is	CAL 2360
C calculated separately. Gamma for co2 is calculated by the method	CAL 2370
C of drummond (unpublished disert.,1981).	CAL 2380
C -----	CAL 2390
	CAL 2400
S1 = KHCO2(T, MNACLD) / KHCO2(T, 1.0D00)	CAL 2410
	CAL 2420
DO 90 I = 1, MXSP + 44	CAL 2430
IF (IABS(Z(I)) .LT. 1) THEN	CAL 2440
IF (NUFLAG .EQ. 1) THEN	CAL 2450
GAMMA(I) = 1.0D0	CAL 2460
ELSE	CAL 2470
GAMMA(I) = S1	CAL 2480
END IF	CAL 2490
END IF	CAL 2500
90 CONTINUE	CAL 2510
	CAL 2520
IF (ANALM(33) .GT. CPUMIN) THEN	CAL 2530
GAMMA(33) = KHH2S(T,MNACLD) / KHH2S(T, 1.0D00)	CAL 2540
ELSE	CAL 2550
GAMMA(33) = 1.0D00	CAL 2560
END IF	CAL 2570
	CAL 2580
IF (IMIX .EQ. 1) RETURN	CAL 2590
	CAL 2600
C -----	CAL 2610
C Temperature effects on debye-huckel solvent constants.	CAL 2620
C -----	CAL 2630
	CAL 2640
S1 = 374.11D0 - TEMP	CAL 2650
S2 = S1*0.333333D0	CAL 2660
S3 = DSQRT((1.0D0 + 0.1342489D0 * S2 - 3.946263D-3 * S1) /	CAL 2670
(3.1975D0 - 0.3151548D0 * S2 - 1.203374D-3 * S1 +	CAL 2680
7.48908D-13 * S1**4))	CAL 2690
	CAL 2700

C	DCH4	DBL	Concentration of CH4 lost up annulus	CO2 0140
C	DDCH4	DBL	Concentration of CH4 lost before pH measurement	CO2 0150
C	DCO2	DBL	Concentration of CO2 lost up annulus	CO2 0160
C	DDCO2	DBL	Concentration of CO2 lost before pH measurement	CO2 0170
C	DH2S	DBL	Concentration of H2S lost up annulus	CO2 0180
C	DDH2S	DBL	Concentration of H2S lost before pH measurement	CO2 0190
C	DNH3	DBL	Concentration of NH3 lost up annulus	CO2 0200
C	DDNH3	DBL	Concentration of NH3 lost before pH measurement	CO2 0210
C	DONE	LOG	Switch indicating DONE	CO2 0220
C	EXELT	DBL	Total amount of components	CO2 0230
C	FCCSAT	DBL	Zero test value	CO2 0240
C	FIXIT	DBL	Fixing value in the CO2 option	CO2 0250
C	GAMMA	DBL	Activity coef. of aqueous species	CO2 0260
C	HFAC	DBL	Amount of H to be added to hydronium balance	CO2 0270
C	HITEMP	DBL	In-situ temperature	CO2 0280
C	HTOT	DBL	Current total hydronium	CO2 0290
C	HTOTI	DBL	Initial hydronium	CO2 0300
C	I	INT	Loop variable	CO2 0310
C	ICO2	INT	Switch for CO2 option	CO2 0320
C	IIC	INT	Index pointer to select carbonate species	CO2 0330
C	IMCO3	INT	Selects CO2 option	CO2 0340
C	IOPT	INT	Switch for CO2 option	CO2 0350
C	IPAGE	INT	Current page number of output file	CO2 0360
C	IPGLN	INT	Current line number of the output file	CO2 0370
C	IPRIN2	INT	Switch for printing	CO2 0380
C	ISAT	INT	Counter for storing things in the position	CO2 0390
C	ITIC	INT	Hitemp distribution of carbonate species	CO2 0400
C	JCO3	INT	Switch to control printing of some headings	CO2 0410
C	KH	DBL	Henry's law constant for CO2 at T	CO2 0420
C	KHCO2	DBL	Function to Calculate the Henry's law K for CO2	CO2 0430
C	KT1	DBL	Equilibrium constant of the aqueous reactions	CO2 0440
C	KTFAC	DBL	Correction for number of CO2 groups	CO2 0450
C	LOGKT1	DBL	Log K for aqueous species at specified temp.	CO2 0460
C	LOGKT2	DBL	Log K for minerals at specified temperature	CO2 0470
C	LTCSAT	DBL	Value used for testing	CO2 0480
C	M	DBL	Calculated molality of aqueous species	CO2 0490
C	MAXCO2	DBL	Determines which carbonate species has the	CO2 0500
C			largest molality	CO2 0510
C	MNACLD	DBL	Sum of Molality * charge / 2	CO2 0520
C	NDIM	INT	Parameter for dimension	CO2 0530
C	NMAX	INT	General array dimension to allow easy expansion	CO2 0540
C	OHTOT	DBL	Total OH in solution	CO2 0550
C	OHTOTI	DBL	Total OH in solution .. initially	CO2 0560
C	PH	DBL	Measured pH of the solution	CO2 0570
C	PHHIT	INT	HITEMP switch, used to control PHCALC	CO2 0580
C	PPHHIT	INT	Switch to control calling PHCALC	CO2 0590
C	SATNAM	CHA	Name used for this option, Cal, Dol,	CO2 0600
C	TEMP	DBL	Temperature of the solution when pH was measured	CO2 0610
C	TIAP	DBL	Temporary activity product	CO2 0620
C	TITR	DBL	Used for convergence in DISTRB	CO2 0630
C	TK	DBL	Temperature in deg K	CO2 0640
C	TKT	DBL	Temporary thermodynamic log k	CO2 0650
C	TOTEL	DBL	Total amount of each element	CO2 0660
C	UNO	INT	File unit assigned for output file	CO2 0670
C	-----			CO2 0680
				CO2 0690
	INTEGER	NDIM, NMAX, UNO		CO2 0700
	DOUBLE	PRECISION	CPUMIN	CO2 0710

PARAMETER (CPUMIN = 1.0D-35, NDIM = 7, NMAX = 340, UNO = 6)	CO2 0720
	CO2 0730
INTEGER I, ICO2, IIC, IMCO3, IOPT, IPAGE, IPGLN, IPRIN2, ISAT	CO2 0740
INTEGER ITIC, JCO3, PHHIT, PPHIT	CO2 0750
	CO2 0760
LOGICAL CROSS, DONE	CO2 0770
	CO2 0780
CHARACTER * 1 TOF, CR	CO2 0790
CHARACTER * 8 SATNAM(6)	CO2 0800
CHARACTER * 40 TITMIX	CO2 0810
	CO2 0820
DOUBLE PRECISION ALFA(NMAX), ANALM(NMAX)	CO2 0830
DOUBLE PRECISION CO2F, CO2SAT(NDIM), CO2INC(NDIM), CUNITS(NMAX)	CO2 0840
DOUBLE PRECISION DCH4, DDCH4, DCO2, DDCO2, DH2S, DDH2S	CO2 0850
DOUBLE PRECISION DNH3, DDNH3, EXELT(35), FCCSAT, FIXIT	CO2 0860
DOUBLE PRECISION GAMMA(NMAX), HFAC, HITEMP, HTOT, HTOTI	CO2 0870
DOUBLE PRECISION KH, KHCO2, KT1(NMAX), KTFAC	CO2 0880
DOUBLE PRECISION LOGKT1(NMAX), LOGKT2(NMAX), LTCSAT	CO2 0890
DOUBLE PRECISION M(NMAX), MAXCO2, MNACLD, OHTOT, OHTOTI, PH	CO2 0900
DOUBLE PRECISION SCO2, TEMP, TIAP, TITR(11), TK, TKT, TOTEL(5)	CO2 0910
	CO2 0920
EXTERNAL GUESS, KHCO2, PAGE, SORTA	CO2 0930
	CO2 0940
INTRINSIC DABS, DLOG10	CO2 0950
	CO2 0960
COMMON /ALOGK / LOGKT1, LOGKT2	CO2 0970
COMMON /EXTOT / EXELT, TOTEL, TITR	CO2 0980
COMMON /FMFD / TOF, CR, TITMIX	CO2 0990
COMMON /FORM / IPAGE, IPGLN	CO2 1000
COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,	CO2 1010
DCH4, DDCH4, IOPT, FIXIT	CO2 1020
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	CO2 1030
COMMON /TOTALS/ CO2F, HTOTI, OHTOTI	CO2 1040
COMMON /TTK / KT1	CO2 1050
COMMON /ZPH / PHHIT, PPHIT, JCO3, SCO2, HTOT, OHTOT	CO2 1060
	CO2 1070
SAVE CO2SAT, CO2INC, CROSS, DONE	CO2 1080
	CO2 1090
DATA SATNAM/ 'CALCITE ', 'DOLOMITE', 'SIDERITE', ' AQ CO2',	CO2 1100
' PH', ' PCO2'/	CO2 1110
	CO2 1120
C =====	CO2 1130
	CO2 1140
C -----	CO2 1150
C If CO2, H2S, NH3 or CH4 are being added	CO2 1160
C -----	CO2 1170
	CO2 1180
IF (ICO2 .EQ. 0) THEN	CO2 1190
DCO2 = DDCO2	CO2 1200
DH2S = DDH2S	CO2 1210
DNH3 = DDNH3	CO2 1220
DCH4 = DDCH4	CO2 1230
CALL PAGE	CO2 1240
WRITE (UNO, 1001) DCO2, DH2S, DNH3, DCH4	CO2 1250
IPGLN = IPGLN + 6	CO2 1260
	CO2 1270
IF (DABS(HITEMP-TEMP) .GT. CPUMIN) HITEMP = TEMP	CO2 1280
	CO2 1290

JCO3 = 1	CO2 1300
ITIC = 2	CO2 1310
IOPT = 0	CO2 1320
PHHIT = 1	CO2 1330
PPHHIT = 0	CO2 1340
HTOTI = HTOT	CO2 1350
OHTOTI = OHTOT	CO2 1360
	CO2 1370
EXELT(25) = EXELT(25) + DDH2S	CO2 1380
TITR(7) = EXELT(25)	CO2 1390
EXELT(24) = EXELT(24) + DDNH3	CO2 1400
EXELT(29) = EXELT(29) + DDCO2	CO2 1410
TITR(1) = EXELT(29)	CO2 1420
M(285) = M(285) + DDCH4	CO2 1430
ANALM(285) = M(285) + DDCH4	CO2 1440
	CO2 1450
DDCO2 = 0.0	CO2 1460
DDH2S = 0.0	CO2 1470
DDNH3 = 0.0	CO2 1480
DDCH4 = 0.0	CO2 1490
	CO2 1500
RETURN	CO2 1510
END IF	CO2 1520
	CO2 1530
C -----	CO2 1540
C Add the amount of CO2	CO2 1550
C required for saturation with CALCITE (IMCO3=1)	CO2 1560
C required for saturation with DOLOMITE (IMCO3=2)	CO2 1570
C required for saturation with SIDERITE (IMCO3=3)	CO2 1580
C required to reach a specified m H2CO3 (IMCO3=4)	CO2 1590
C which is stored in FIXIT	CO2 1600
C required to reach a specified pH (IMCO3=5)	CO2 1610
C which is stored in FIXIT	CO2 1620
C required to reach a specified p CO2 (IMCO3=6)	CO2 1630
C which is stored in FIXIT	CO2 1640
C	CO2 1650
C IC02 must be greater than zero for this option to be used.	CO2 1660
C -----	CO2 1670
	CO2 1680
IF (ISAT .EQ. 0) THEN	CO2 1690
CROSS = .FALSE.	CO2 1700
DONE = .FALSE.	CO2 1710
	CO2 1720
IF (DABS(HITEMP-TEMP) .GT. 1.0D-10) HITEMP = TEMP	CO2 1730
	CO2 1740
PHHIT = 1	CO2 1750
PPHHIT = 0	CO2 1760
HTOTI = HTOT	CO2 1770
OHTOTI = OHTOT	CO2 1780
JCO3 = 1	CO2 1790
ITIC = 2	CO2 1800
END IF	CO2 1810
	CO2 1820
ISAT = ISAT + 1	CO2 1830
	CO2 1840
C -----	CO2 1850
C Scan for the most abundant species of CO2 and use it later to	CO2 1860
C minimize round-off errors in calculations.	CO2 1870

C	-----	CO2 1880
		CO2 1890
	MAXCO2 = M(7)	CO2 1900
	HFAC = ALFA(8)	CO2 1910
	IIC = 7	CO2 1920
		CO2 1930
	DO 10 I = 97, 98	CO2 1940
	IF (M(I) .GT. MAXCO2) THEN	CO2 1950
	MAXCO2 = M(I)	CO2 1960
	IIC = I	CO2 1970
	END IF	CO2 1980
	10 CONTINUE	CO2 1990
		CO2 2000
	IF (IIC .EQ. 97) HFAC = ALFA(8)**2	CO2 2010
	IF (IIC .EQ. 98) HFAC = 1.0	CO2 2020
		CO2 2030
C	-----	CO2 2040
C	Set up TEST for each of the options	CO2 2050
C	-----	CO2 2060
		CO2 2070
	IF (IMCO3 .EQ. 1) THEN	CO2 2080
	TKT = LOGKT2(24)	CO2 2090
	KTFAC = 1.0	CO2 2100
	TIAP = ALFA(1) * ALFA(IIC) / HFAC	CO2 2110
	ELSE IF (IMCO3 .EQ. 2) THEN	CO2 2120
	TKT = LOGKT2(41)	CO2 2130
	KTFAC = 2.0	CO2 2140
	TIAP = ALFA(1) * ALFA(2) * ALFA(IIC)**2 / HFAC**2	CO2 2150
	ELSE IF (IMCO3 .EQ. 3) THEN	CO2 2160
	TKT = LOGKT2(146)	CO2 2170
	KTFAC = 1.0	CO2 2180
	TIAP = ALFA(18) * ALFA(IIC) / HFAC	CO2 2190
	ELSE IF (IMCO3 .EQ. 4) THEN	CO2 2200
	LTCSAT = DLOG10(FIXIT) - DLOG10(M(97))	CO2 2210
	ELSE IF (IMCO3 .EQ. 5) THEN	CO2 2220
	LTCSAT = PH - FIXIT	CO2 2230
	ELSE IF (IMCO3 .EQ. 6) THEN	CO2 2240
	TK = TEMP + 273.15	CO2 2250
	KH = KHCO2 (TK, MNACLD)	CO2 2260
	LTCSAT = DLOG10((FIXIT/KH)) - DLOG10(M(97))	CO2 2270
	END IF	CO2 2280
		CO2 2290
	IF (IMCO3 .EQ. 1 .OR. IMCO3 .EQ. 2 .OR. IMCO3 .EQ. 3) THEN	CO2 2300
	IF (IIC .EQ. 7) THEN	CO2 2310
	TKT = TKT - KTFAC * LOGKT1(1)	CO2 2320
	ELSE IF (IIC .EQ. 97) THEN	CO2 2330
	TKT = TKT - KTFAC * (LOGKT1(1) + LOGKT1(72))	CO2 2340
	END IF	CO2 2350
	LTCSAT = DLOG10(TIAP) - TKT	CO2 2360
	END IF	CO2 2370
		CO2 2380
	IF (DABS(LTCSAT) .LT. FCCSAT) DONE = .TRUE.	CO2 2390
		CO2 2400
	IF (DONE) THEN	CO2 2410
	IOPT = 0	CO2 2420
	PHHIT = 0	CO2 2430
	PPHHIT = 1	CO2 2440
	ISAT = 0	CO2 2450

JCO3	= 0	CO2	2460
HTOTI	= HTOTI + (2.DO * DCO2)	CO2	2470
TOTEL(1)	= HTOTI	CO2	2480
TOTEL(3)	= TOTEL(3) + DCO2	CO2	2490
CO2F	= CO2F + DCO2	CO2	2500
		CO2	2510
IF (IPGLN .GT. 55 .OR. IPRIN2 .EQ. 0)	CALL PAGE	CO2	2520
IF (IMCO3 .LE. 3)	THEN	CO2	2530
WRITE (UNO,1007)	SATNAM(IMCO3), DCO2	CO2	2540
ELSE IF (IMCO3 .EQ. 4)	THEN	CO2	2550
WRITE (UNO,1008)	SATNAM(IMCO3), FIXIT, DCO2	CO2	2560
ELSE IF (IMCO3 .EQ. 5)	THEN	CO2	2570
WRITE (UNO,1009)	FIXIT, DCO2	CO2	2580
ELSE IF (IMCO3 .EQ. 6)	THEN	CO2	2590
WRITE (UNO,1008)	SATNAM(IMCO3), FIXIT, DCO2	CO2	2600
END IF		CO2	2610
IPGLN	= IPGLN + 5	CO2	2620
DCO2	= 0.DO	CO2	2630
RETURN	1	CO2	2640
END IF		CO2	2650
		CO2	2660
IF (ISAT .EQ. 1)	THEN	CO2	2670
CO2SAT(1)	= LTCSAT	CO2	2680
CO2INC(1)	= 0.0	CO2	2690
IF (IMCO3 .EQ. 1)	THEN	CO2	2700
DCO2	= M(IIC) * ((1.0/(10.0**LTCSAT)) - 1.0)	CO2	2710
IF (DCO2 .LT. 0.0)	DCO2 = 0.01	CO2	2720
IF (DCO2 .GT. 0.05)	DCO2 = 0.01	CO2	2730
ELSE IF (IMCO3 .EQ. 2)	THEN	CO2	2740
DCO2	= M(IIC) * ((1.0/(10.0**LTCSAT)) - 1.0)	CO2	2750
DCO2	= DCO2 / 2.0	CO2	2760
IF (DCO2 .LT. 0.0)	DCO2 = 0.01	CO2	2770
IF (DCO2 .GT. 0.05)	DCO2 = 0.01	CO2	2780
ELSE IF (IMCO3 .EQ. 3)	THEN	CO2	2790
DCO2	= M(IIC) * ((1.0/(10.0**LTCSAT)) - 1.0)	CO2	2800
IF (DCO2 .LT. 0.0)	DCO2 = 0.01	CO2	2810
IF (DCO2 .GT. 0.05)	DCO2 = 0.01	CO2	2820
ELSE IF (IMCO3 .EQ. 4)	THEN	CO2	2830
IF (IIC .EQ. 7)	THEN	CO2	2840
DCO2	= FIXIT * KT1(72) * GAMMA(97) / ALFA(8)	CO2	2850
DCO2	= DCO2 / GAMMA(7)	CO2	2860
DCO2	= (DCO2 - M(7)) / 3.0	CO2	2870
ELSE IF (IIC .EQ. 97)	THEN	CO2	2880
DCO2	= FIXIT - M(97)	CO2	2890
ELSE IF (IIC .EQ. 98)	THEN	CO2	2900
DCO2	= FIXIT * KT1(72) * GAMMA(97) / ALFA(8)	CO2	2910
DCO2	= DCO2 * KT1(1) / (GAMMA(98) * ALFA(8))	CO2	2920
DCO2	= (DCO2 - M(98)) / 3.0	CO2	2930
END IF		CO2	2940
ELSE IF (IMCO3 .EQ. 5)	THEN	CO2	2950
DCO2	= 10.0**(-FIXIT) - 10.0**(-PH)	CO2	2960
DCO2	= DCO2 / 2.0	CO2	2970
ELSE IF (IMCO3 .EQ. 6)	THEN	CO2	2980
IF (IIC .EQ. 7)	THEN	CO2	2990
DCO2	= (FIXIT/KH) * KT1(72) * GAMMA(97) / ALFA(8)	CO2	3000
DCO2	= DCO2 / GAMMA(7)	CO2	3010
DCO2	= (DCO2 - M(7)) / 3.0	CO2	3020
ELSE IF (IIC .EQ. 97)	THEN	CO2	3030

DCO2 = (FIXIT/KH) - M(97)	CO2 3040
ELSE IF (IIC .EQ. 98) THEN	CO2 3050
DCO2 = (FIXIT/KH) * KT1(72) * GAMMA(97) / ALFA(8)	CO2 3060
DCO2 = DCO2 * KT1(1) / (GAMMA(98) * ALFA(8))	CO2 3070
DCO2 = (DCO2 - M(98)) / 3.0	CO2 3080
END IF	CO2 3090
END IF	CO2 3100
ELSE IF (ISAT .GE. 2) THEN	CO2 3110
CO2SAT(ISAT) = LTCSAT	CO2 3120
CO2INC(ISAT) = DCO2	CO2 3130
IF ((LTCSAT * CO2SAT(1)) .LT. 0.0) CROSS = .TRUE.	CO2 3140
	CO2 3150
C -----	CO2 3160
C Sort if Root has been crossed	CO2 3170
C -----	CO2 3180
	CO2 3190
I = 1	CO2 3200
IF (CROSS) CALL SORTA (CO2INC, CO2SAT, ISAT, I)	CO2 3210
	CO2 3220
C -----	CO2 3230
C Due to size of guess routine, keep only last NDIM-1 pts	CO2 3240
C -----	CO2 3250
	CO2 3260
IF (ISAT .EQ. NDIM) THEN	CO2 3270
IF (.NOT. CROSS) THEN	CO2 3280
DO 20 I = 1, (NDIM-1)	CO2 3290
CO2INC(I) = CO2INC(I+1)	CO2 3300
CO2SAT(I) = CO2SAT(I+1)	CO2 3310
20 CONTINUE	CO2 3320
END IF	CO2 3330
IF (CROSS) THEN	CO2 3340
IF (CO2SAT(1) * CO2SAT(2) .LT. 0.0) THEN	CO2 3350
ISAT = NDIM-1	CO2 3360
ELSE IF (CO2SAT(NDIM-1)*CO2SAT(NDIM) .LT. 0.0) THEN	CO2 3370
DO 30 I = 1, (NDIM-1)	CO2 3380
CO2INC(I) = CO2INC(I+1)	CO2 3390
CO2SAT(I) = CO2SAT(I+1)	CO2 3400
30 CONTINUE	CO2 3410
ELSE IF (DABS(CO2SAT(1)) .GT. DABS(CO2SAT(NDIM))) THEN	CO2 3420
DO 40 I = 1, (NDIM-1)	CO2 3430
CO2INC(I) = CO2INC(I+1)	CO2 3440
CO2SAT(I) = CO2SAT(I+1)	CO2 3450
40 CONTINUE	CO2 3460
END IF	CO2 3470
END IF	CO2 3480
ISAT = NDIM - 1	CO2 3490
END IF	CO2 3500
	CO2 3510
C -----	CO2 3520
C If root not yet crossed, keep on trucking	CO2 3530
C -----	CO2 3540
	CO2 3550
IF (.NOT. CROSS) THEN	CO2 3560
DCO2 = DCO2 * 2.0	CO2 3570
IF ((CO2F + DCO2) .LT. CPUMIN) DCO2 = 1.0D-10 - CO2F	CO2 3580
END IF	CO2 3590
	CO2 3600
C -----	CO2 3610

C	If ROOT crossed, go and get it	CO2 3620
C	-----	CO2 3630
		CO2 3640
	IF (CROSS) THEN	CO2 3650
	CALL GUESS (CO2INC, CO2SAT, DCO2, ISAT)	CO2 3660
	END IF	CO2 3670
	END IF	CO2 3680
		CO2 3690
	IF (IPRIN2 .GT. 0) THEN	CO2 3700
	IF (IMCO3 .LE. 3) THEN	CO2 3710
	WRITE (UNO,1004) SATNAM(IMCO3), LTCSAT	CO2 3720
	ELSE	CO2 3730
	WRITE (UNO,1002) SATNAM(IMCO3), LTCSAT	CO2 3740
	END IF	CO2 3750
	IPGLN = IPGLN + 2	CO2 3760
	IF (IPGLN .GT. 57) CALL PAGE	CO2 3770
	WRITE (UNO,1003) DCO2	CO2 3780
	IPGLN = IPGLN + 2	CO2 3790
	END IF	CO2 3800
		CO2 3810
		CO2 3820
	IF (ISAT .EQ. 1) THEN	CO2 3830
	EXELT(29) = DCO2 + EXELT(29)	CO2 3840
	TITR(1) = EXELT(29)	CO2 3850
	END IF	CO2 3860
		CO2 3870
	RETURN	CO2 3880
		CO2 3890
1001	FORMAT(/,' Adding gases to the analyses using the DCO2/DH2S/DNH3',	CO2 3900
	./DCH4 ',	CO2 3910
	./, ' option. Moles of CO2 added = ', E14.6,	CO2 3920
	./, ' of H2S added = ', E14.6,	CO2 3930
	./, ' of NH3 added = ', E14.6,	CO2 3940
	./, ' of CH4 added = ', E14.6,	CO2 3950
	./)	CO2 3960
1002	FORMAT(/,5X,'LOG (CALCULATED-DESIRED) ',A8,' = ',E10.4)	CO2 3970
1003	FORMAT(/,5X,'VALUE OF DCO2 FOR THIS ITERATION = ',E10.4)	CO2 3980
1004	FORMAT(/,5X,'LOG SI (' ,A8,') = ', E10.4)	CO2 3990
1005	FORMAT(/,' *** DESIRED EQUILIBRIUM DOES NOT SEEM TO ',	CO2 4000
	' CONVERGE WITHIN THE LIMITS OF',	CO2 4010
	' .5 AND 1.0E5 PPM AQ CO2 ***',	CO2 4020
	./, ' SI = ', D16.8, ' TIC = ', D16.8,	CO2 4030
	' MOLS/KG WATER')	CO2 4040
1006	FORMAT(/,' *** DESIRED EQUILIBRIUM DOES NOT SEEM TO ',	CO2 4050
	' CONVERGE ***', /)	CO2 4060
1007	FORMAT(/,5X,'CO2 added to achieve equilibrium with ', A8, ' = ',	CO2 4070
	E10.4, 'Moles/Kg Water',/)	CO2 4080
1008	FORMAT(/,5X,'CO2 added to achieve saturation with ',A8,' of ',	CO2 4090
	E10.4,' = ', E10.4, ' Moles/Kg water',/)	CO2 4100
1009	FORMAT(/,5X,'CO2 added to achieve pH of ', F10.4, ' = ',	CO2 4110
	E13.4, ' Moles/Kg water',/)	CO2 4120
		CO2 4130
		CO2 4140

	DOUBLE PRECISION FUNCTION DEBYE (CHARGE, DNA)	DEB 0010
C	=====	DEB 0020
C	This function returns the value of the ion size parameter based	DEB 0030
C	upon the charge of the species	DEB 0040
C	-----	DEB 0050
C	CHARGE INT Charge of the aqueous species	DEB 0060
C	CPUMIN DBL Smallest positive real value program uses	DEB 0070
C	DNA DBL Read-in value of the ion size parameter	DEB 0080
C	-----	DEB 0090
		DEB 0100
	DOUBLE PRECISION CPUMIN	DEB 0110
	PARAMETER (CPUMIN = 1.0D-35)	DEB 0120
		DEB 0130
	INTEGER CHARGE	DEB 0140
	DOUBLE PRECISION DNA	DEB 0150
		DEB 0160
	INTRINSIC IABS	DEB 0170
		DEB 0180
C	=====	DEB 0190
		DEB 0200
	IF (DNA .GT. CPUMIN) THEN	DEB 0210
	DEBYE = DNA	DEB 0220
	ELSE IF (IABS(CHARGE) .EQ. 0) THEN	DEB 0230
	DEBYE = 0.0D00	DEB 0240
	ELSE IF (IABS(CHARGE) .EQ. 1) THEN	DEB 0250
	DEBYE = 4.0D00	DEB 0260
	ELSE IF (IABS(CHARGE) .EQ. 2) THEN	DEB 0270
	DEBYE = 6.0D00	DEB 0280
	ELSE IF (IABS(CHARGE) .EQ. 3) THEN	DEB 0290
	DEBYE = 9.0D00	DEB 0300
	ELSE IF (IABS(CHARGE) .GE. 4) THEN	DEB 0310
	DEBYE = 12.0D00	DEB 0320
	END IF	DEB 0330
		DEB 0340
	RETURN	DEB 0350
	END	DEB 0360
	SUBROUTINE DISTRB (NUFLAG, FLAGS, GAMMA, Z, DHA, TEMP, HITEMP,	DIS 0010
	. EHM, ALK, TITLE, A, B, MXSP, MXAQK, MU,	DIS 0020
	. IPRIN1, IPIT, TK, CONV1, ANMTIC, ITIC, HTOT,	DIS 0030
	. OHTOT, SCO2, JCO3, ITWR, BDOT)	DIS 0040
C	=====	DIS 0050
C	This routine iterates and distributes the species	DIS 0060
C	-----	DIS 0070
C	A DBL Molal Debye-Huckel coefficient	DIS 0080
C	ALFA DBL Activity of aqueous species i	DIS 0090
C	ALK INT Flag for distribution of carbonate species	DIS 0100
C	ANALCO DBL Inorganic Carbon ... initially alk or tic	DIS 0110
C	ANALM DBL Analyzed molality of species i	DIS 0120
C	ANMTIC DBL Analyzed total inorganic carbon	DIS 0130
C	B DBL Molal Debye-Huckel coefficient	DIS 0140
C	BDOT DBL Activity coefficient deviation function	DIS 0150
C	C1 DBL TDS * 1000.0	DIS 0160
C	CO2F DBL Sum of CO2 plus CO2 lost from solution	DIS 0170

C	CONV1	DBL	Tolerance factor for convergence of anions	DIS 0180
C	CPUMIN	DBL	Smallest positive real value program uses	DIS 0190
C	CR	CHA	Inserts carriage returns in output	DIS 0200
C	CROSS	LOG	Local logical variable for crossing root	DIS 0210
C	CUNITS	DBL	Analytical input concentration	DIS 0220
C	DHA	DBL	Ion size parameter	DIS 0230
C	DIFF	DBL	Difference used in convergence	DIS 0240
C	DONE	LOG	Have we crossed root	DIS 0250
C	EHM	DBL	Measured Eh in volts	DIS 0260
C	EXELT	DBL	Total amount of each component	DIS 0270
C	F	DBL	Faraday constant	DIS 0280
C	FACTOR	DBL	Factor used in convergence	DIS 0290
C	FIXIT	DBL	Fixing value in the CO2 option	DIS 0300
C	FLAGS	INT	Selection flags for calculation of redox equil.	DIS 0310
C	GAMMA	DBL	Activity coefficient of species i	DIS 0320
C	HITEMP	DBL	In-situ temperature	DIS 0330
C	HTOT	DBL	Total hydronium (current)	DIS 0340
C	HTOTI	DBL	Total hydronium (initial)	DIS 0350
C	I	INT	Loop counter	DIS 0360
C	IFL1	INT	Switch sets activity coeffs of non-pitzer species	DIS 0370
C	IOPT	INT	H+ option	DIS 0380
C	IPAGE	INT	Current page number of output file	DIS 0390
C	IPGLN	INT	Current line number of the output file	DIS 0400
C	IPIT	INT	Flag to use pitzer activity coefficients	DIS 0410
C	IPRIN1	INT	Flag for printing iteration of anions	DIS 0420
C	ITER	INT	Iteration count	DIS 0430
C	ITIC	INT	Hitemp distribution of carbonate species	DIS 0440
C	ITWR	INT	Printing Flag	DIS 0450
C	JCO3	INT	Switch to control printing of some headings	DIS 0460
C	KT1	DBL	Equilibrium constant of the aqueous reactions	DIS 0470
C	LOGKT1	DBL	Log K for aqueous species at specified temp.	DIS 0480
C	LOGKT2	DBL	Log K for minerals at specified temperature	DIS 0490
C	M	DBL	Calculated molality of aqueous species	DIS 0500
C	MU	DBL	Ionic strength of aqueous solution	DIS 0510
C	MXAQK	INT	Total number of aqueous log k values	DIS 0520
C	MXSP	INT	Total number of aqueous species	DIS 0530
C	NMAX	INT	General array dimension to allow easy expansion	DIS 0540
C	NUFLAG	INT	Sets the activity coefficients of neutral species	DIS 0550
C	OHTOT	DBL	OH total	DIS 0560
C	OHTOTI	DBL	Initial OH total	DIS 0570
C	PAGE1	CHA	Names of aqueous species	DIS 0580
C	PAGE2	CHA	Names of equilibrium constants	DIS 0590
C	PAGE3	CHA	Names of solubility constants	DIS 0600
C	PALFA	DBL	Pitzer alpha's	DIS 0610
C	PG	DBL	Pitzer gamma's	DIS 0620
C	PGDCA	DBL	Pitzer gamma for Ca	DIS 0630
C	PGDNA	DBL	Pitzer gamma for Na	DIS 0640
C	PH	DBL	Measured pH of the solution	DIS 0650
C	R	DBL	Gas constant	DIS 0660
C	S	DBL	Sum of anions complexes	DIS 0670
C	SCO2	DBL	Sum of carbonate in solution	DIS 0680
C	T	DBL	Temperature	DIS 0690
C	TEMP	DBL	Temperature of the solution when pH was measured	DIS 0700
C	TITLE	CHA	Name of the sample	DIS 0710
C	TITMIX	CHA	Title for Mixtures	DIS 0720
C	TITR	DBL	Convergence (vector) for each component	DIS 0730
C	TK	DBL	Temperature steps used by program	DIS 0740
C	TOTEL	DBL	Total amount of each component	DIS 0750

C	UNO	INT	File unit assigned for output file	DIS 0760
C	VERSN	CHA	Version Number	DIS 0770
C	X	DBL	Temperary variable	DIS 0780
C	Z	INT	Charge of aqueous species	DIS 0790
C	-----			DIS 0800
				DIS 0810
	INTEGER NMAX, UNO			DIS 0820
	DOUBLE PRECISION CPUMIN, F, R			DIS 0830
				DIS 0840
	PARAMETER (NMAX = 340, UNO = 6)			DIS 0850
	PARAMETER (CPUMIN = 1.0D-35, F = 2.30603D+1, R = 1.98719D-3)			DIS 0860
				DIS 0870
	INTEGER ALK, FLAGS(6), I, IFL1, IOPT, IPAGE, IPGLN			DIS 0880
	INTEGER IPIT, IPRIN1, ITER, ITIC, ITWR			DIS 0890
	INTEGER JCO3, MXAQK, MXSP, NUFLAG, Z(NMAX)			DIS 0900
				DIS 0910
	LOGICAL DONE, CROSS			DIS 0920
				DIS 0930
	CHARACTER * 1 TOF, CR			DIS 0940
	CHARACTER * 8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)			DIS 0950
	CHARACTER * 14 VERSN			DIS 0960
	CHARACTER * 40 TITMIX			DIS 0970
	CHARACTER * 80 TITLE			DIS 0980
				DIS 0990
	DOUBLE PRECISION A, ALFA(NMAX), ANALCO, ANALM(NMAX), ANMTIC			DIS 1000
	DOUBLE PRECISION B, BDOT, C1, CO2F, CONV1, CUNITS(NMAX)			DIS 1010
	DOUBLE PRECISION DCH4, DCO2, DDCH4, DDCO2, DDH2S, DDNH3			DIS 1020
	DOUBLE PRECISION DH2S, DHA(NMAX), DIFF(11), DNH3			DIS 1030
	DOUBLE PRECISION EHM, EXELT(35), FACTOR(11), FIXIT, GAMMA(NMAX)			DIS 1040
	DOUBLE PRECISION HITEMP, HTOT, HTOTI, INC, KT1(NMAX)			DIS 1050
	DOUBLE PRECISION LALFA(NMAX), LOGKT1(NMAX), LOGKT2(NMAX)			DIS 1060
	DOUBLE PRECISION M(NMAX), MU, OHTOT, OHTOTI			DIS 1070
	DOUBLE PRECISION PALFA(NMAX), PG(NMAX), PGDCA, PGDNA, PH			DIS 1080
	DOUBLE PRECISION S(11), SCO2, SEXP10, SLOG10, T, TEMP, TITR(11)			DIS 1090
	DOUBLE PRECISION TK(11), TOTEL(5), X			DIS 1100
				DIS 1110
	EXTERNAL AITLIM, PAGE, PITZER, SEXP10, SLOG10			DIS 1120
				DIS 1130
	INTRINSIC DABS, DLOG10, DSQRT, IABS, MOD			DIS 1140
				DIS 1150
	COMMON /ALOGK / LOGKT1, LOGKT2			DIS 1160
	COMMON /EXTOT / EXELT, TOTEL, TITR			DIS 1170
	COMMON /FMFD / TOF, CR, TITMIX			DIS 1180
	COMMON /FORM / IPAGE, IPGLN			DIS 1190
	COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,			DIS 1200
	DCH4, DDCH4, IOPT, FIXIT			DIS 1210
	COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS			DIS 1220
	COMMON /NAMES1/ PAGE1, PAGE2, PAGE3			DIS 1230
	COMMON /TOTALS/ CO2F, HTOTI, OHTOTI			DIS 1240
	COMMON /TTK / KT1			DIS 1250
				DIS 1260
	SAVE DIFF, PGDCA, PGDNA			DIS 1270
				DIS 1280
C	=====			DIS 1290
				DIS 1300
	VERSN = 'USGS-ARC-88-8'			DIS 1310
				DIS 1320
	T = TEMP + 273.15			DIS 1330

	DIS 1340
C -----	DIS 1350
C Initialize activities to 0	DIS 1360
C -----	DIS 1370
DO 10 I = 1, NMAX	DIS 1380
ALFA(I) = 0.0D0	DIS 1390
PG(I) = 0.0D0	DIS 1400
10 CONTINUE	DIS 1410
	DIS 1420
ALFA(8) = 10.0**(-PH)	DIS 1430
	DIS 1440
IFL1 = 0	DIS 1450
	DIS 1460
DO 20 I = 1, 11	DIS 1470
DIFF(I) = 0.0	DIS 1480
FACTOR(I) = 1.0	DIS 1490
20 CONTINUE	DIS 1500
	DIS 1510
	DIS 1520
C -----	DIS 1530
C Write titles etc.	DIS 1540
C -----	DIS 1550
IF (JCO3 .EQ. 0 .AND. ITWR .EQ. 0) THEN	DIS 1560
IF (IPRIN1 .NE. 0) THEN	DIS 1570
IF (IPGLN .GE. 45) CALL PAGE	DIS 1580
WRITE (UNO, 1000) VERSN, CR	DIS 1590
WRITE (UNO, 1001) TITLE, TITMIX	DIS 1600
WRITE (UNO, 1002) TEMP	DIS 1610
WRITE (UNO, 1003)	DIS 1620
WRITE (UNO, 1004) CR	DIS 1630
IPGLN = IPGLN + 14	DIS 1640
END IF	DIS 1650
END IF	DIS 1660
	DIS 1670
	DIS 1680
C -----	DIS 1690
C Iterative loop	DIS 1700
C iter2 counts ph loop; iter counts species distribution	DIS 1710
C -----	DIS 1720
ITER = 0	DIS 1730
	DIS 1740
	DIS 1750
30 CONTINUE	DIS 1760
ITER = ITER + 1	DIS 1770
	DIS 1780
C -----	DIS 1790
C Calculation of total molality & ah2o.	DIS 1800
C -----	DIS 1810
C1 = 0.0D0	DIS 1820
DO 40 I = 1, MXSP + 44	DIS 1830
IF (I .NE. 10 .AND. I .NE. 12 .AND. I .NE. 32) C1 = C1 + M(I)	DIS 1840
40 CONTINUE	DIS 1850
	DIS 1860
	DIS 1870
IF (C1 .GT. 10.0) C1 = 10.0	DIS 1880
ALFA(10) = 1.0D0 - (1.7D-2 * C1)	DIS 1890
	DIS 1900
C -----	DIS 1910

C	Calculation of the ionic strength (i), equivalent mnacle=i.	DIS 1920
C	-----	DIS 1930
	MU = 0.0D0	DIS 1940
	DO 50 I = 1, MXSP + 44	DIS 1950
	IF (M(I) .LT. CPUMIN) THEN	DIS 1960
	M(I) = 0.0D0	DIS 1970
	ELSE IF (I .EQ. 163 .AND. M(I) .GT. 2.0) THEN	DIS 1980
	MU = MU + (1.0 * Z(I)**2)	DIS 1990
	ELSE	DIS 2000
	MU = MU + (M(I) * Z(I)**2)	DIS 2010
	END IF	DIS 2020
	50 CONTINUE	DIS 2030
		DIS 2040
	MU = 0.5D0 * MU	DIS 2050
	IF (MU .GT. 10.0) MU = 10.0	DIS 2060
		DIS 2070
		DIS 2080
C	-----	DIS 2090
C	Only call pitzer the first time each temperature is done	DIS 2100
C	-----	DIS 2110
		DIS 2120
	IF (IPIT .EQ. 1 .AND. ITER .EQ. 1) THEN	DIS 2130
	CALL PITZER (A, MU, MXSP, TEMP, PGDCA, PGDNA, PG, TK, PALFA,	DIS 2140
	EXELT(29), Z, IFL1)	DIS 2150
	END IF	DIS 2160
		DIS 2170
	IFL1 = 1	DIS 2180
		DIS 2190
	60 CONTINUE	DIS 2200
	IF (IPIT .EQ. 1) THEN	DIS 2210
	IF (IFL1 .EQ. 1) I = 3	DIS 2220
	IF (IFL1 .EQ. 2) I = 1	DIS 2230
	IF (IFL1 .EQ. 1) GAMMA(I) = PGDNA	DIS 2240
	IF (IFL1 .EQ. 2) GAMMA(I) = PGDCA	DIS 2250
		DIS 2260
C	-----	DIS 2270
C	The following statement when enabled may give improved results	DIS 2280
C	at lower temperatures and salinities. When high temperatures or	DIS 2290
C	salinities are involved this statement should be disabled since	DIS 2300
C	it will cause the program to return activity coefficients which	DIS 2310
C	are too high.	DIS 2320
C	IF (M(I) .GT. CPUMIN) GAMMA(I) = GAMMA(I) * EXELT(I) / M(I)	DIS 2330
C	-----	DIS 2340
		DIS 2350
	BDOT = DLOG10(GAMMA(I)) + ((A * Z(I)**2 * DSQRT(MU)) /	DIS 2360
	(1.0 + DHA(I) * B * DSQRT(MU)))	DIS 2370
	BDOT = BDOT / MU	DIS 2380
	END IF	DIS 2390
		DIS 2400
C	-----	DIS 2410
C	Calculation of the activity coefficients (gamma) for charged	DIS 2420
C	species by the bdot method (helgeson,1969). If pitzer equations	DIS 2430
C	are being used, bdot is not the same as in helgeson.	DIS 2440
C	-----	DIS 2450
		DIS 2460
	DO 70 I = 1, MXSP + 44	DIS 2470
	IF (Z(I).EQ.0) GO TO 70	DIS 2480
	IF (IFL1.EQ.1 .AND. (IABS(Z(I))).NE.1) GO TO 70	DIS 2490

IF (IFL1.EQ.2 .AND. (IABS(Z(I))).LT.2) GO TO 70	DIS 2500
GAMMA(I) = A * DSQRT(MU) * Z(I)**2	DIS 2510
GAMMA(I) = GAMMA(I) / (1.0 + (DHA(I) * B * DSQRT(MU)))	DIS 2520
GAMMA(I) = (BDOT * MU) - GAMMA(I)	DIS 2530
GAMMA(I) = 10.0**GAMMA(I)	DIS 2540
70 CONTINUE	DIS 2550
	DIS 2560
C -----	DIS 2570
C Calculation of a number of anion activities.	DIS 2580
C -----	DIS 2590
	DIS 2600
IF (NUFLAG .EQ. 0) THEN	DIS 2610
GAMMA(11) = 10.0**(0.00978 * 10.0**(280.0 / T) * (MU + 1.0D0))	DIS 2620
GAMMA(12) = GAMMA(11)	DIS 2630
END IF	DIS 2640
	DIS 2650
IF (IFL1 .EQ. 1) THEN	DIS 2660
IFL1 = 2	DIS 2670
GO TO 60	DIS 2680
END IF	DIS 2690
	DIS 2700
IFL1 = 3	DIS 2710
	DIS 2720
DO 80 I = 1, MXSP + 44	DIS 2730
IF (ALFA(I) .LT. CPUMIN) THEN	DIS 2740
ALFA(I) = 0.0D0	DIS 2750
LALFA(I) = -999.9	DIS 2760
ELSE	DIS 2770
LALFA(I) = DLOG10(ALFA(I))	DIS 2780
END IF	DIS 2790
IF (I .NE. 6 .AND. PG(I) .GT. CPUMIN) GAMMA(I) = PG(I)	DIS 2800
80 CONTINUE	DIS 2810
	DIS 2820
C -----	DIS 2830
C Activity of H+ and OH-	DIS 2840
C -----	DIS 2850
	DIS 2860
ALFA(8) = 10.0**(-PH)	DIS 2870
LALFA(8) = -PH	DIS 2880
M(8) = ALFA(8) / GAMMA(8)	DIS 2890
	DIS 2900
ALFA(9) = ALFA(10) * KT1(2) / ALFA(8)	DIS 2910
LALFA(9) = DLOG10(ALFA(9))	DIS 2920
M(9) = ALFA(9) / GAMMA(9)	DIS 2930
	DIS 2940
C -----	DIS 2950
C Chloride species	DIS 2960
C -----	DIS 2970
	DIS 2980
IF (EXELT(5) .GT. CPUMIN) THEN	DIS 2990
90 CONTINUE	DIS 3000
M(5) = TITR(5)	DIS 3010
ALFA(5) = M(5) * GAMMA(5)	DIS 3020
LALFA(5) = SLOG10(ALFA(5))	DIS 3030
	DIS 3040
IF (IPIT .EQ. 1 .AND. PG(5) .GT. CPUMIN	DIS 3050
.AND. GAMMA(5) .LE. 10) THEN	DIS 3060
IF (DABS(PALFA(5) - ALFA(5)) .GT. 1.0D-2 * PALFA(5)) THEN	DIS 3070

IF (PALFA(5) .GT. ALFA(5)) THEN	DIS 3080
INC=0.1	DIS 3090
ELSE	DIS 3100
INC=-0.01	DIS 3110
END IF	DIS 3120
GAMMA(5)=GAMMA(5)*(1.0+INC)	DIS 3130
GO TO 90	DIS 3140
END IF	DIS 3150
END IF	DIS 3160
IF (IPIT .EQ. 1 .AND. GAMMA(5) .GT. 10.0) GAMMA(5) = 10.0	DIS 3170
IF (IPIT .EQ. 1 .AND. GAMMA(5) .LT. PG(5)) GAMMA(5) = PG(5)	DIS 3180
END IF	DIS 3190
	DIS 3200
C -----	DIS 3210
C Acetate species	DIS 3220
C -----	DIS 3230
	DIS 3240
IF (EXELT(26) .GT. CPUMIN) THEN	DIS 3250
M(228) = TITR(6) / (1.0D0 + ((GAMMA(228) * KT1(25)) /	DIS 3260
(ALFA(8) * GAMMA(48))))	DIS 3270
ALFA(228) = M(228) * GAMMA(228)	DIS 3280
LALFA(228) = SLOG10(ALFA(228))	DIS 3290
	DIS 3300
M(48) = LOGKT1(25) + LALFA(228) - DLOG10(GAMMA(48)) - LALFA(8)	DIS 3310
M(48) = SEXP10(M(48))	DIS 3320
ALFA(48) = M(48) * GAMMA(48)	DIS 3330
LALFA(48) = SLOG10(ALFA(48))	DIS 3340
END IF	DIS 3350
	DIS 3360
C -----	DIS 3370
C Oxalate species	DIS 3380
C -----	DIS 3390
	DIS 3400
IF (EXELT(30) .GT. CPUMIN) THEN	DIS 3410
M(247) = TITR(8) / (1.0D0 + ((GAMMA(247) * ALFA(8) /	DIS 3420
KT1(224) * GAMMA(248)) + ((KT1(223) * GAMMA(247)) /	DIS 3430
(GAMMA(246) * ALFA(8))))	DIS 3440
	DIS 3450
ALFA(247) = M(247) * GAMMA(247)	DIS 3460
LALFA(247) = SLOG10(ALFA(247))	DIS 3470
	DIS 3480
M(248) = LALFA(247) + LALFA(8) - LOGKT1(224)	DIS 3490
- DLOG10(GAMMA(248))	DIS 3500
M(248) = SEXP10(M(248))	DIS 3510
	DIS 3520
ALFA(248) = M(248) * GAMMA(248)	DIS 3530
LALFA(248) = SLOG10(ALFA(248))	DIS 3540
	DIS 3550
M(246) = LOGKT1(223) + LALFA(247) - DLOG10(GAMMA(246))	DIS 3560
- LALFA(8)	DIS 3570
M(246) = SEXP10(M(246))	DIS 3580
ALFA(246) = M(246) * GAMMA(246)	DIS 3590
LALFA(246) = SLOG10(ALFA(246))	DIS 3600
END IF	DIS 3610
	DIS 3620
C -----	DIS 3630
C Succinate species	DIS 3640
C -----	DIS 3650

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IF (EXELT(31) .GT. CPUMIN) THEN
  M(266) = TITR(9) / (1.0D0 + ((GAMMA(266) * ALFA(8) /
    KT1(242) * GAMMA(267)) + ((KT1(241) * GAMMA(266)) /
    (GAMMA(265) * ALFA(8)))))
  ALFA(266) = M(266) * GAMMA(266)
  LALFA(266) = SLOG10(ALFA(266))
  M(267) = LALFA(266) + LALFA(8) - LOGKT1(242)
  M(267) = SEXP10(M(267))
  M(267) = M(267) / GAMMA(267)
  ALFA(267) = M(267) * GAMMA(267)
  LALFA(267) = SLOG10(ALFA(267))
  M(265) = LOGKT1(241) + LALFA(266) - LALFA(8)
  M(265) = SEXP10(M(265))
  M(265) = M(265) / GAMMA(265)
  ALFA(265) = M(265) * GAMMA(265)
  LALFA(265) = SLOG10(ALFA(265))
END IF

C -----
C User defined anion #1
C -----

IF (EXELT(33) .GT. CPUMIN) THEN
  M(MXSP+2) = TITR(10) / (1.0D0 + ((GAMMA(MXSP+2) * ALFA(8)) /
    (KT1(MXAQK+2) * GAMMA(MXSP+3)) +
    ((KT1(MXAQK+1) * GAMMA(MXSP+2)) /
    (GAMMA(MXSP+1) * ALFA(8)))))
  ALFA(MXSP+2) = M(MXSP+2) * GAMMA(MXSP+2)
  M(MXSP+3) = (ALFA(MXSP+2) * ALFA(8)) / (KT1(MXAQK+2) *
    GAMMA(MXSP+3))
  ALFA(MXSP+3) = M(MXSP+3) * GAMMA(MXSP+3)
  M(MXSP+1) = (KT1(MXAQK+1) * ALFA(MXSP+2)) /
    (GAMMA(MXSP+1) * ALFA(8))
  ALFA(MXSP+1) = M(MXSP+1) * GAMMA(MXSP+1)
END IF

C -----
C User defined anion #2
C -----

IF (EXELT(34) .GT. CPUMIN) THEN
  M(MXSP+17) = TITR(11) / (1.0D0 + ((GAMMA(MXSP+17) *
    ALFA(8)) / (KT1(MXAQK+16) * GAMMA(MXSP+18)) +
    ((KT1(MXAQK+15) * GAMMA(MXSP+17)) /
    (GAMMA(MXSP+16) * ALFA(8)))))
  ALFA(MXSP+17) = M(MXSP+17) * GAMMA(MXSP+17)
  M(MXSP+18) = (ALFA(MXSP+17) * ALFA(8)) / (KT1(MXAQK+16) *
    GAMMA(MXSP+18))

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ALFA(MXSP+18) = M(MXSP+18) * GAMMA(MXSP+18)	DIS 4240
	DIS 4250
M(MXSP+16) = (KT1(MXAQK+15) * ALFA(MXSP+17)) /	DIS 4260
(GAMMA(MXSP+16) * ALFA(8))	DIS 4270
ALFA(MXSP+16) = M(MXSP+16) * GAMMA(MXSP+16)	DIS 4280
END IF	DIS 4290
	DIS 4300
C -----	DIS 4310
C Fluoride species	DIS 4320
C -----	DIS 4330
	DIS 4340
IF (EXELT(22) .GT. CPUMIN) THEN	DIS 4350
M(30) = TITR(3) / (1.0D0 + ((GAMMA(30) * ALFA(8)) /	DIS 4360
(KT1(71) * GAMMA(96))))	DIS 4370
ALFA(30) = M(30) * GAMMA(30)	DIS 4380
LALFA(30) = SLOG10(ALFA(30))	DIS 4390
	DIS 4400
M(96) = (ALFA(30) * ALFA(8)) / (KT1(71) * GAMMA(96))	DIS 4410
ALFA(96) = M(96) * GAMMA(96)	DIS 4420
LALFA(96) = SLOG10(ALFA(96))	DIS 4430
END IF	DIS 4440
	DIS 4450
C -----	DIS 4460
C CO2 species	DIS 4470
C -----	DIS 4480
	DIS 4490
IF (EXELT(29) .GT. CPUMIN) THEN	DIS 4500
M(7) = TITR(1) / (1.0D0 + ((GAMMA(7) * KT1(1) * 2) /	DIS 4510
(GAMMA(98) * ALFA(8))))	DIS 4520
ALFA(7) = M(7) * GAMMA(7)	DIS 4530
LALFA(7) = SLOG10(ALFA(7))	DIS 4540
	DIS 4550
M(98) = (KT1(1) * ALFA(7)) / (GAMMA(98) * ALFA(8))	DIS 4560
ALFA(98) = M(98) * GAMMA(98)	DIS 4570
LALFA(98) = SLOG10(ALFA(98))	DIS 4580
	DIS 4590
M(97) = (ALFA(7) * ALFA(8)) / (KT1(72) * GAMMA(97))	DIS 4600
ALFA(97) = M(97) * GAMMA(97)	DIS 4610
LALFA(97) = SLOG10(ALFA(97))	DIS 4620
END IF	DIS 4630
	DIS 4640
C -----	DIS 4650
C Sulfur species	DIS 4660
C -----	DIS 4670
	DIS 4680
IF (EXELT(25) .GT. CPUMIN) THEN	DIS 4690
M(101) = TITR(7) / (1.0D0 + ((GAMMA(101) * ALFA(8)) /	DIS 4700
(KT1(10) * GAMMA(33)) + ((KT1(75) * GAMMA(101)) /	DIS 4710
(GAMMA(102) * ALFA(8))))	DIS 4720
ALFA(101) = GAMMA(101) * M(101)	DIS 4730
LALFA(101) = SLOG10(ALFA(101))	DIS 4740
	DIS 4750
M(33) = (ALFA(101) * ALFA(8)) / (KT1(10) * GAMMA(33))	DIS 4760
ALFA(33) = M(33) * GAMMA(33)	DIS 4770
LALFA(33) = SLOG10(ALFA(33))	DIS 4780
	DIS 4790
M(102) = (KT1(75) * ALFA(101)) / (GAMMA(102) * ALFA(8))	DIS 4800
ALFA(102) = M(102) * GAMMA(102)	DIS 4810

LALFA(102) = SLOG10(ALFA(102))	DIS 4820
END IF	DIS 4830
100 CONTINUE	DIS 4840
IF (EXELT(6) .GE. CPUMIN) THEN	DIS 4850
M(103) = TITR(2) / (1.0D0 + (((KT1(76) * GAMMA(103)) /	DIS 4860
(GAMMA(6) * ALFA(8))))	DIS 4870
ALFA(103) = M(103) * GAMMA(103)	DIS 4880
LALFA(103) = SLOG10(ALFA(103))	DIS 4890
	DIS 4900
	DIS 4910
M(6) = (KT1(76) * ALFA(103)) / (GAMMA(6) * ALFA(8))	DIS 4920
ALFA(6) = M(6) * GAMMA(6)	DIS 4930
LALFA(6) = SLOG10(ALFA(6))	DIS 4940
	DIS 4950
IF (IPIT .EQ. 1 .AND. PG(6) .GT. CPUMIN	DIS 4960
AND. GAMMA(6) .LE. 10.0) THEN	DIS 4970
IF (DABS(PALFA(6)-ALFA(6)) .GT. 1.0D-2*PALFA(6)) THEN	DIS 4980
IF (PALFA(6) .GT. ALFA(6)) THEN	DIS 4990
INC=0.1	DIS 5000
ELSE	DIS 5010
INC=-0.01	DIS 5020
END IF	DIS 5030
GAMMA(6)=GAMMA(6)*(1.0+INC)	DIS 5040
GO TO 100	DIS 5050
END IF	DIS 5060
END IF	DIS 5070
IF (IPIT.EQ.1 .AND. GAMMA(6) .GT. 10.0) GAMMA(6) = 10.0	DIS 5080
IF (IPIT.EQ.1 .AND. GAMMA(6) .LT. PG(6)) GAMMA(6) = PG(6)	DIS 5090
END IF	DIS 5100
	DIS 5110
C -----	DIS 5120
C Silica species	DIS 5130
C -----	DIS 5140
	DIS 5150
IF (EXELT(8) .GT. CPUMIN) THEN	DIS 5160
M(91) = EXELT(8) / (1.0D0 + ((GAMMA(91) * ALFA(8)) /	DIS 5170
(KT1(3) * GAMMA(11)) + ((KT1(66) * GAMMA(91)) /	DIS 5180
(GAMMA(90) * ALFA(8))))	DIS 5190
ALFA(91) = GAMMA(91) * M(91)	DIS 5200
LALFA(91) = SLOG10(ALFA(91))	DIS 5210
	DIS 5220
M(11) = (ALFA(91) * ALFA(8)) / (KT1(3) * GAMMA(11))	DIS 5230
ALFA(11) = M(11) * GAMMA(11)	DIS 5240
LALFA(11) = SLOG10(ALFA(11))	DIS 5250
	DIS 5260
M(90) = (KT1(66) * ALFA(91)) / (GAMMA(90) * ALFA(8))	DIS 5270
ALFA(90) = M(90) * GAMMA(90)	DIS 5280
LALFA(90) = SLOG10(ALFA(90))	DIS 5290
	DIS 5300
M(12) = M(11)	DIS 5310
ALFA(12) = M(12) * GAMMA(12)	DIS 5320
LALFA(12) = SLOG10(ALFA(12))	DIS 5330
	DIS 5340
M(284) = (ALFA(11) * ALFA(30)**2 * (ALFA(30) / ALFA(9))	DIS 5350
* (ALFA(30) / ALFA(9)) * (ALFA(30) / ALFA(9))	DIS 5360
* (ALFA(30) / ALFA(9))) / KT1(257)	DIS 5370
	DIS 5380
ALFA(284) = M(284) * GAMMA(284)	DIS 5390

LALFA(284) = SLOG10(ALFA(284))	DIS 5400
END IF	DIS 5410
C -----	DIS 5420
C Boron Species	DIS 5430
C -----	DIS 5440
IF (EXELT(23) .GT. CPUMIN) THEN	DIS 5450
M(31) = EXELT(23) / (1.0D0 + ((GAMMA(31) * ALFA(9)) /	DIS 5460
(KT1(64) * GAMMA(89))))	DIS 5470
ALFA(31) = M(31) * GAMMA(31)	DIS 5480
LALFA(31) = SLOG10(ALFA(31))	DIS 5490
	DIS 5500
M(89) = (ALFA(31) * ALFA(9)) / (KT1(64) * GAMMA(89))	DIS 5510
ALFA(89) = M(89) * GAMMA(89)	DIS 5520
LALFA(89) = SLOG10(ALFA(89))	DIS 5530
END IF	DIS 5540
C -----	DIS 5550
C Phosphate species	DIS 5560
C -----	DIS 5570
IF (EXELT(21) .GT. CPUMIN) THEN	DIS 5580
M(29) = TITR(4) / (1.0D0 + GAMMA(29) * ((ALFA(8) /	DIS 5590
(KT1(73) * GAMMA(99))) + (ALFA(8)**2 / (KT1(74) *	DIS 5600
GAMMA(100))) + (ALFA(8)**3 / (KT1(49) *	DIS 5610
GAMMA(74))))	DIS 5620
ALFA(29) = M(29) * GAMMA(29)	DIS 5630
LALFA(29) = SLOG10(ALFA(29))	DIS 5640
	DIS 5650
M(74) = (ALFA(29) * ALFA(8)**3) / (KT1(49) * GAMMA(74))	DIS 5660
ALFA(74) = M(74) * GAMMA(74)	DIS 5670
LALFA(74) = SLOG10(ALFA(74))	DIS 5680
	DIS 5690
M(99) = (ALFA(29) * ALFA(8)) / (KT1(73) * GAMMA(99))	DIS 5700
ALFA(99) = M(99) * GAMMA(99)	DIS 5710
LALFA(99) = SLOG10(ALFA(99))	DIS 5720
	DIS 5730
M(100) = (ALFA(29) * ALFA(8)**2) / (KT1(74) * GAMMA(100))	DIS 5740
ALFA(100) = M(100) * GAMMA(100)	DIS 5750
LALFA(100) = SLOG10(ALFA(100))	DIS 5760
END IF	DIS 5770
C -----	DIS 5780
C Nitrogen species	DIS 5790
C -----	DIS 5800
IF (EXELT(24) .GT. CPUMIN) THEN	DIS 5810
M(147) = ALFA(9) / (KT1(118) * GAMMA(147))	DIS 5820
	DIS 5830
M(146) = EXELT(24) / (1.0D0 + GAMMA(146) * M(147))	DIS 5840
ALFA(146) = M(146) * GAMMA(146)	DIS 5850
LALFA(146) = SLOG10(ALFA(146))	DIS 5860
	DIS 5870
M(147) = M(147) * ALFA(146)	DIS 5880
ALFA(147) = M(147) * GAMMA(147)	DIS 5890
LALFA(147) = SLOG10(ALFA(147))	DIS 5900
	DIS 5910
	DIS 5920
	DIS 5930
	DIS 5940
	DIS 5950
	DIS 5960
	DIS 5970

M(32)	= M(147)	DIS 5980
ALFA(32)	= M(32) * GAMMA(32)	DIS 5990
LALFA(32)	= SLOG10(ALFA(32))	DIS 6000
END IF		DIS 6010
IF (EXELT(32) .GT. CPUMIN) THEN		DIS 6020
M(136)	= EXELT(32) / (1.0D0 + ((GAMMA(136) * ALFA(8)) /	DIS 6030
	(KT1(77) * GAMMA(104))))	DIS 6040
ALFA(136)	= M(136) * GAMMA(136)	DIS 6050
LALFA(136)	= SLOG10(ALFA(136))	DIS 6060
		DIS 6070
		DIS 6080
M(104)	= (ALFA(8) * ALFA(136)) / (KT1(77) * GAMMA(104))	DIS 6090
ALFA(104)	= M(104) * GAMMA(104)	DIS 6100
LALFA(104)	= SLOG10(ALFA(104))	DIS 6110
END IF		DIS 6120
		DIS 6130
C -----		DIS 6140
C User defined cation		DIS 6150
C -----		DIS 6160
		DIS 6170
IF (EXELT(35) .GT. CPUMIN) THEN		DIS 6180
M(MXSP+32)	= ALFA(5) / (KT1(MXAQK+29) * GAMMA(MXSP+32))	DIS 6190
M(MXSP+33)	= ALFA(6) / (KT1(MXAQK+30) * GAMMA(MXSP+33))	DIS 6200
M(MXSP+34)	= ALFA(7) / (KT1(MXAQK+31) * GAMMA(MXSP+34))	DIS 6210
M(MXSP+35)	= ALFA(9) / (KT1(MXAQK+32) * GAMMA(MXSP+35))	DIS 6220
M(MXSP+36)	= ALFA(29) / (KT1(MXAQK+33) * GAMMA(MXSP+36))	DIS 6230
M(MXSP+37)	= ALFA(30) / (KT1(MXAQK+34) * GAMMA(MXSP+37))	DIS 6240
M(MXSP+38)	= ALFA(48) / (KT1(MXAQK+35) * GAMMA(MXSP+38))	DIS 6250
M(MXSP+39)	= ALFA(98) / (KT1(MXAQK+36) * GAMMA(MXSP+39))	DIS 6260
M(MXSP+40)	= ALFA(101) / (KT1(MXAQK+37) * GAMMA(MXSP+40))	DIS 6270
M(MXSP+41)	= ALFA(246) / (KT1(MXAQK+38) * GAMMA(MXSP+41))	DIS 6280
M(MXSP+42)	= ALFA(265) / (KT1(MXAQK+39) * GAMMA(MXSP+42))	DIS 6290
M(MXSP+43)	= ALFA(MXSP+ 1) / (KT1(MXAQK+40) * GAMMA(MXSP+43))	DIS 6300
M(MXSP+44)	= ALFA(MXSP+16) / (KT1(MXAQK+41) * GAMMA(MXSP+44))	DIS 6310
		DIS 6320
M(MXSP+31)	= EXELT(35) / (1.0D0 + GAMMA(MXSP+31) *	DIS 6330
	(M(MXSP+32) + M(MXSP+33) + M(MXSP+34) +	DIS 6340
	M(MXSP+35) + M(MXSP+36) + M(MXSP+37) +	DIS 6350
	M(MXSP+38) + M(MXSP+39) + M(MXSP+40) +	DIS 6360
	M(MXSP+41) + M(MXSP+42) + M(MXSP+43) +	DIS 6370
	M(MXSP+44)))	DIS 6380
ALFA(MXSP+31)	= M(MXSP+31) * GAMMA(MXSP+31)	DIS 6390
LALFA(MXSP+31)	= SLOG10(ALFA(MXSP+31))	DIS 6400
		DIS 6410
DO 110 I = 32, 44		DIS 6420
M(MXSP+I)	= M(MXSP+I) * ALFA(MXSP+31)	DIS 6430
ALFA(MXSP+I)	= M(MXSP+I) * GAMMA(MXSP+I)	DIS 6440
LALFA(MXSP+I)	= SLOG10(ALFA(MXSP+I))	DIS 6450
110 CONTINUE		DIS 6460
END IF		DIS 6470
		DIS 6480
C -----		DIS 6490
C Calcium species		DIS 6500
C -----		DIS 6510
		DIS 6520
120 CONTINUE		DIS 6530
IF (EXELT(1) .GT. CPUMIN) THEN		DIS 6540
M(55)	= ALFA(98) / (KT1(30) * GAMMA(55))	DIS 6550

M(56) = ALFA(7) / (KT1(31) * GAMMA(56))	DIS 6560
M(57) = ALFA(9) / (KT1(32) * GAMMA(57))	DIS 6570
M(58) = ALFA(29) / (KT1(33) * GAMMA(58))	DIS 6580
M(59) = ALFA(99) / (KT1(34) * GAMMA(59))	DIS 6590
M(60) = ALFA(100) / (KT1(35) * GAMMA(60))	DIS 6600
M(61) = ALFA(6) / (KT1(36) * GAMMA(61))	DIS 6610
M(231) = ALFA(48) / (KT1(211) * GAMMA(231))	DIS 6620
M(252) = ALFA(246) / (KT1(228) * GAMMA(252))	DIS 6630
M(271) = ALFA(265) / (KT1(246) * GAMMA(271))	DIS 6640
M(281) = ALFA(5) / (KT1(146) * GAMMA(281))	DIS 6650
M(282) = ALFA(5)**2 / (KT1(147) * GAMMA(282))	DIS 6660
M(MXSP+ 6) = ALFA(MXSP+ 1) / (KT1(MXAQK+ 5) * GAMMA(MXSP+ 6))	DIS 6670
M(MXSP+21) = ALFA(MXSP+16) / (KT1(MXAQK+19) * GAMMA(MXSP+21))	DIS 6680
	DIS 6690
M(1) = EXELT(1) / (1.0D0 + GAMMA(1) * (M(55) + M(56) + M(57) +	DIS 6700
M(58) + M(59) + M(60) + M(61) + M(231) + M(252) +	DIS 6710
M(271) + M(281) + M(282) + M(MXSP+6) + M(MXSP+21)))	DIS 6720
ALFA(1) = M(1) * GAMMA(1)	DIS 6730
LALFA(1) = SLOG10(ALFA(1))	DIS 6740
	DIS 6750
DO 130 I = 55, 61	DIS 6760
M(I) = M(I) * ALFA(1)	DIS 6770
ALFA(I) = M(I) * GAMMA(I)	DIS 6780
LALFA(I) = SLOG10(ALFA(I))	DIS 6790
130 CONTINUE	DIS 6800
	DIS 6810
M(231) = M(231) * ALFA(1)	DIS 6820
ALFA(231) = M(231) * GAMMA(231)	DIS 6830
LALFA(231) = SLOG10(ALFA(231))	DIS 6840
	DIS 6850
M(252) = M(252) * ALFA(1)	DIS 6860
ALFA(252) = M(252) * GAMMA(252)	DIS 6870
LALFA(252) = SLOG10(ALFA(252))	DIS 6880
	DIS 6890
M(271) = M(271) * ALFA(1)	DIS 6900
ALFA(271) = M(271) * GAMMA(271)	DIS 6910
LALFA(271) = SLOG10(ALFA(271))	DIS 6920
	DIS 6930
M(281) = M(281) * ALFA(1)	DIS 6940
ALFA(281) = M(281) * GAMMA(281)	DIS 6950
LALFA(281) = SLOG10(ALFA(281))	DIS 6960
	DIS 6970
M(282) = M(282) * ALFA(1)	DIS 6980
ALFA(282) = M(282) * GAMMA(282)	DIS 6990
LALFA(282) = SLOG10(ALFA(282))	DIS 7000
	DIS 7010
M(MXSP+6) = M(MXSP+6) * ALFA(1)	DIS 7020
ALFA(MXSP+6) = M(MXSP+6) * GAMMA(MXSP+6)	DIS 7030
LALFA(MXSP+6) = SLOG10(ALFA(MXSP+6))	DIS 7040
	DIS 7050
M(MXSP+21) = M(MXSP+21) * ALFA(1)	DIS 7060
ALFA(MXSP+21) = M(MXSP+21) * GAMMA(MXSP+21)	DIS 7070
LALFA(MXSP+21) = SLOG10(ALFA(MXSP+21))	DIS 7080
	DIS 7090
IF (IPIT.EQ.1 .AND. PG(1).GT.CPUMIN	DIS 7100
.AND. GAMMA(1).LE.10.0) THEN	DIS 7110
IF (DABS(PALFA(1) - ALFA(1)) .GT. 1.0D-2*PALFA(1)) THEN	DIS 7120
IF (PALFA(1) .GT. ALFA(1)) THEN	DIS 7130

INC = 0.1	DIS 7140
ELSE	DIS 7150
INC = -0.01	DIS 7160
END IF	DIS 7170
GAMMA(1) = GAMMA(1) * (1 + INC)	DIS 7180
GO TO 120	DIS 7190
END IF	DIS 7200
END IF	DIS 7210
IF (IPIT.EQ.1 .AND. GAMMA(1).GT.10.0)	DIS 7220
IF (IPIT.EQ.1 .AND. GAMMA(1).LT.PG(1))	DIS 7230
END IF	DIS 7240
	DIS 7250
C -----	DIS 7260
C Magnesium species	DIS 7270
C -----	DIS 7280
	DIS 7290
140 CONTINUE	DIS 7300
IF (EXELT(2) .GT. CPUMIN) THEN	DIS 7310
M(120) = ALFA(98) / (KT1(93) * GAMMA(120))	DIS 7320
M(121) = ALFA(7) / (KT1(94) * GAMMA(121))	DIS 7330
M(122) = ALFA(30) / (KT1(95) * GAMMA(122))	DIS 7340
M(123) = ALFA(9) / (KT1(96) * GAMMA(123))	DIS 7350
M(124) = ALFA(6) / (KT1(97) * GAMMA(124))	DIS 7360
M(125) = ALFA(29) / (KT1(98) * GAMMA(125))	DIS 7370
M(126) = ALFA(99) / (KT1(99) * GAMMA(126))	DIS 7380
M(127) = ALFA(100) / (KT1(100) * GAMMA(127))	DIS 7390
M(236) = ALFA(48) / (KT1(216) * GAMMA(236))	DIS 7400
M(256) = ALFA(246) / (KT1(232) * GAMMA(256))	DIS 7410
M(275) = ALFA(265) / (KT1(250) * GAMMA(275))	DIS 7420
M(MXSP+10) = ALFA(MXSP+ 1) / (KT1(MXAQK+ 9) * GAMMA(MXSP+10))	DIS 7430
M(MXSP+25) = ALFA(MXSP+16) / (KT1(MXAQK+23) * GAMMA(MXSP+25))	DIS 7440
	DIS 7450
	DIS 7460
	DIS 7470
M(2) = EXELT(2) / (1.0DO + GAMMA(2) * (M(120) + M(121) + M(122) + M(123) + M(124) + M(125) + M(126) + M(127) + M(236) + M(256) + M(275) + M(MXSP+10) + M(MXSP+25)))	DIS 7480
ALFA(2) = M(2) * GAMMA(2)	DIS 7490
LALFA(2) = SLOG10(ALFA(2))	DIS 7500
	DIS 7510
DO 150 I = 120, 127	DIS 7520
M(I) = M(I) * ALFA(2)	DIS 7530
ALFA(I) = M(I) * GAMMA(I)	DIS 7540
LALFA(I) = SLOG10(ALFA(I))	DIS 7550
150 CONTINUE	DIS 7560
	DIS 7570
	DIS 7580
	DIS 7590
M(236) = M(236) * ALFA(2)	DIS 7600
ALFA(236) = M(236) * GAMMA(236)	DIS 7610
LALFA(236) = SLOG10(ALFA(236))	DIS 7620
	DIS 7630
	DIS 7640
M(256) = M(256) * ALFA(2)	DIS 7650
ALFA(256) = M(256) * GAMMA(256)	DIS 7660
LALFA(256) = SLOG10(ALFA(256))	DIS 7670
	DIS 7680
M(275) = M(275) * ALFA(2)	DIS 7690
ALFA(275) = M(275) * GAMMA(275)	DIS 7700
LALFA(275) = SLOG10(ALFA(275))	DIS 7710

M(MXSP+10)	= M(MXSP+10) * ALFA(2)	DIS 7720
ALFA(MXSP+10)	= M(MXSP+10) * GAMMA(MXSP+10)	DIS 7730
LALFA(MXSP+10)	= SLOG10(ALFA(MXSP+10))	DIS 7740
		DIS 7750
		DIS 7760
M(MXSP+25)	= M(MXSP+25) * ALFA(2)	DIS 7770
ALFA(MXSP+25)	= M(MXSP+25) * GAMMA(MXSP+25)	DIS 7780
LALFA(MXSP+25)	= SLOG10(ALFA(MXSP+25))	DIS 7790
		DIS 7800
IF (IPIT.EQ.1 .AND. PG(2).GT.CPUMIN		DIS 7810
.AND. GAMMA(2).LE.50.0) THEN		DIS 7820
IF (DABS(PALFA(2)-ALFA(2)) .GT. 1.0D-2*PALFA(2)) THEN		DIS 7830
IF (PALFA(2) .GT. ALFA(2)) THEN		DIS 7840
INC=0.1		DIS 7850
ELSE		DIS 7860
INC=-0.01		DIS 7870
END IF		DIS 7880
GAMMA(2)=GAMMA(2)*(1.0+INC)		DIS 7890
GO TO 140		DIS 7900
END IF		DIS 7910
END IF		DIS 7920
		DIS 7930
IF (IPIT.EQ.1 .AND. GAMMA(2) .GT. 10.0) GAMMA(2) = 10.0		DIS 7940
IF (IPIT.EQ.1 .AND. GAMMA(2) .LT. PG(2)) GAMMA(2) = PG(2)		DIS 7950
END IF		DIS 7960
		DIS 7970
C -----		DIS 7980
C Sodium species		DIS 7990
C -----		DIS 8000
		DIS 8010
160 CONTINUE		DIS 8020
IF (EXELT(3) .GT. CPUMIN) THEN		DIS 8030
M(137) = ALFA(5) / (KT1(110) * GAMMA(137))		DIS 8040
M(138) = ALFA(98) / (KT1(111) * GAMMA(138))		DIS 8050
M(139) = ALFA(7) / (KT1(112) * GAMMA(139))		DIS 8060
M(140) = (M(3) * GAMMA(3) * ALFA(98)) / (KT1(113) * GAMMA(140))		DIS 8070
M(141) = (M(3) * GAMMA(3) * ALFA(6)) / (KT1(114) * GAMMA(141))		DIS 8080
M(142) = ALFA(6) / (KT1(115) * GAMMA(142))		DIS 8090
M(143) = ALFA(99) / (KT1(116) * GAMMA(143))		DIS 8100
M(144) = ALFA(30) / (KT1(120) * GAMMA(144))		DIS 8110
M(145) = ALFA(101) / (KT1(119) * GAMMA(145))		DIS 8120
M(237) = ALFA(48) / (KT1(217) * GAMMA(237))		DIS 8130
M(261) = ALFA(246) / (KT1(237) * GAMMA(261))		DIS 8140
M(277) = ALFA(265) / (KT1(252) * GAMMA(277))		DIS 8150
M(MXSP+12) = ALFA(MXSP+ 1) / (KT1(MXAQK+11) * GAMMA(MXSP+12))		DIS 8160
M(MXSP+27) = ALFA(MXSP+16) / (KT1(MXAQK+25) * GAMMA(MXSP+27))		DIS 8170
		DIS 8180
M(3) = EXELT(3) / (1.0D0 + GAMMA(3) * (M(137) + M(138) +		DIS 8190
M(139) + M(140) + M(141) + M(142) + M(143) + M(144) +		DIS 8200
M(145) + M(237) + M(261) + M(277) + M(MXSP+12)		DIS 8210
M(MXSP+27)))		DIS 8220
ALFA(3) = M(3) * GAMMA(3)		DIS 8230
LALFA(3) = SLOG10(ALFA(3))		DIS 8240
		DIS 8250
DO 170 I = 137, 145		DIS 8260
M(I) = M(I) * ALFA(3)		DIS 8270
ALFA(I) = M(I) * GAMMA(I)		DIS 8280
LALFA(I) = SLOG10(ALFA(I))		DIS 8290

170	CONTINUE	DIS 8300
		DIS 8310
	M(237) = M(237) * ALFA(3)	DIS 8320
	ALFA(237) = M(237) * GAMMA(237)	DIS 8330
	LALFA(237) = SLOG10(ALFA(237))	DIS 8340
		DIS 8350
	M(261) = M(261) * ALFA(3)	DIS 8360
	ALFA(261) = M(261) * GAMMA(261)	DIS 8370
	LALFA(261) = SLOG10(ALFA(261))	DIS 8380
		DIS 8390
	M(277) = M(277) * ALFA(3)	DIS 8400
	ALFA(277) = M(277) * GAMMA(277)	DIS 8410
	LALFA(277) = SLOG10(ALFA(277))	DIS 8420
		DIS 8430
	M(MXSP+12) = M(MXSP+12) * ALFA(3)	DIS 8440
	ALFA(MXSP+12) = M(MXSP+12) * GAMMA(MXSP+12)	DIS 8450
	LALFA(MXSP+12) = SLOG10(ALFA(MXSP+12))	DIS 8460
		DIS 8470
	M(MXSP+27) = M(MXSP+27) * ALFA(3)	DIS 8480
	ALFA(MXSP+27) = M(MXSP+27) * GAMMA(MXSP+27)	DIS 8490
	LALFA(MXSP+27) = SLOG10(ALFA(MXSP+27))	DIS 8500
		DIS 8510
	IF (IPIT.EQ.1 .AND. PG(3).GT.CPUMIN	DIS 8520
	.AND. GAMMA(3).LE.10.0) THEN	DIS 8530
	IF (DABS(PALFA(3)-ALFA(3)) .GT. 1.0D-2*PALFA(3)) THEN	DIS 8540
	IF (PALFA(3) .GT. ALFA(3)) THEN	DIS 8550
	INC = 0.1	DIS 8560
	ELSE	DIS 8570
	INC = -0.01	DIS 8580
	END IF	DIS 8590
	GAMMA(3)=GAMMA(3)*(1+INC)	DIS 8600
	GO TO 160	DIS 8610
	END IF	DIS 8620
	END IF	DIS 8630
		DIS 8640
	IF (IPIT .EQ. 1 .AND. GAMMA(3) .GT. 10.0) GAMMA(3) = 10.0	DIS 8650
	IF (IPIT .EQ. 1 .AND. GAMMA(3) .LT. PG(3)) GAMMA(3) = PG(3)	DIS 8660
	END IF	DIS 8670
		DIS 8680
C	-----	DIS 8690
C	Potassium species	DIS 8700
C	-----	DIS 8710
		DIS 8720
180	CONTINUE	DIS 8730
	IF (EXELT(4) .GT. CPUMIN) THEN	DIS 8740
	M(113) = ALFA(5) / (KT1(86) * GAMMA(113))	DIS 8750
	M(114) = ALFA(98) / (KT1(87) * GAMMA(114))	DIS 8760
	M(115) = ALFA(103) / (KT1(88) * GAMMA(115))	DIS 8770
	M(116) = ALFA(6) / (KT1(89) * GAMMA(116))	DIS 8780
	M(117) = ALFA(99) / (KT1(90) * GAMMA(117))	DIS 8790
	M(235) = ALFA(48) / (KT1(215) * GAMMA(235))	DIS 8800
	M(255) = ALFA(246) / (KT1(231) * GAMMA(255))	DIS 8810
	M(274) = ALFA(265) / (KT1(249) * GAMMA(274))	DIS 8820
		DIS 8830
	M(MXSP+ 9) = ALFA(MXSP+ 1) / (KT1(MXAQK+8) * GAMMA(MXSP+ 9))	DIS 8840
	M(MXSP+24) = ALFA(MXSP+16) / (KT1(MXAQK+22) * GAMMA(MXSP+24))	DIS 8850
		DIS 8860
	M(4) = EXELT(4) / (1.0D0 + GAMMA(4) * (M(113) + M(114) +	DIS 8870

.	M(115) + M(116) + M(117) + M(235) + M(255) +	DIS 8880
.	M(274) + M(MXSP+9) + M(MXSP+24)))	DIS 8890
	ALFA(4) = M(4) * GAMMA(4)	DIS 8900
		DIS 8910
	DO 190 I = 113, 117	DIS 8920
	M(I) = M(I) * ALFA(4)	DIS 8930
	ALFA(I) = M(I) * GAMMA(I)	DIS 8940
190	CONTINUE	DIS 8950
		DIS 8960
	M(235) = M(235) * ALFA(4)	DIS 8970
	ALFA(235) = M(235) * GAMMA(235)	DIS 8980
		DIS 8990
	M(255) = M(255) * ALFA(4)	DIS 9000
	ALFA(255) = M(255) * GAMMA(255)	DIS 9010
		DIS 9020
	M(274) = M(274) * ALFA(4)	DIS 9030
	ALFA(274) = M(274) * GAMMA(274)	DIS 9040
		DIS 9050
	M(MXSP+ 9) = M(MXSP+ 9) * ALFA(4)	DIS 9060
	ALFA(MXSP+ 9) = M(MXSP+ 9) * GAMMA(MXSP+ 9)	DIS 9070
		DIS 9080
	M(MXSP+24) = M(MXSP+24) * ALFA(4)	DIS 9090
	ALFA(MXSP+24) = M(MXSP+24) * GAMMA(MXSP+24)	DIS 9100
		DIS 9110
	IF (IPIT.EQ.1 .AND. PG(4).GT.CPUMIN	DIS 9120
	.AND. GAMMA(4).LE.10.0) THEN	DIS 9130
	IF (DABS(PALFA(4)-ALFA(4)) .GT. 1.0D-2*PALFA(4)) THEN	DIS 9140
	IF (PALFA(4) .GT. ALFA(4)) THEN	DIS 9150
	INC =0.1	DIS 9160
	ELSE	DIS 9170
	INC =-0.01	DIS 9180
	END IF	DIS 9190
	GAMMA(4)=GAMMA(4)*(1.0+INC)	DIS 9200
	GO TO 180	DIS 9210
	END IF	DIS 9220
	END IF	DIS 9230
		DIS 9240
	IF (IPIT .EQ. 1 .AND. GAMMA(4) .GT. 10.0) GAMMA(4) = 10.0	DIS 9250
	IF (IPIT .GT. 1 .AND. GAMMA(4) .LT. PG(4)) GAMMA(4) = PG(4)	DIS 9260
	END IF	DIS 9270
		DIS 9280
C	-----	DIS 9290
C	Silver species	DIS 9300
C	-----	DIS 9310
		DIS 9320
	IF (EXELT(9) .GT. CPUMIN) THEN	DIS 9330
	M(43) = 0.0D00	DIS 9340
	M(44) = 0.0D00	DIS 9350
	M(45) = 0.0D00	DIS 9360
	M(46) = 0.0D00	DIS 9370
	M(47) = 0.0D00	DIS 9380
	IF (DABS(KT1(20)) .GT. 1.0D-30)	DIS 9390
.	M(43) = ALFA(5) / (KT1(20) * GAMMA(43))	DIS 9400
.	IF (DABS(KT1(21)) .GT. 1.0D-30)	DIS 9410
.	M(44) = ALFA(5)**2 / (KT1(21) * GAMMA(44))	DIS 9420
.	IF (DABS(KT1(22)) .GT. 1.0D-30)	DIS 9430
.	M(45) = ALFA(5)**3 / (KT1(22) * GAMMA(45))	DIS 9440
.	IF (DABS(KT1(23)) .GT. 1.0D-30)	DIS 9450

M(46) = ALFA(5)**4 / (KT1(23) * GAMMA(46))	DIS 9460
IF (DABS(KT1(24)) .GT. 1.0D-30)	DIS 9470
M(47) = ALFA(6) / (KT1(24) * GAMMA(47))	DIS 9480
	DIS 9490
M(13) = EXELT(9) / (1.0D0 + GAMMA(13) * (M(42) + M(44) +	DIS 9500
M(45) + M(46) + M(47)))	DIS 9510
ALFA(13) = M(13) * GAMMA(13)	DIS 9520
	DIS 9530
DO 200 I = 43, 47	DIS 9540
M(I) = M(I) * ALFA(13)	DIS 9550
ALFA(I) = M(I) * GAMMA(I)	DIS 9560
200 CONTINUE	DIS 9570
END IF	DIS 9580
	DIS 9590
C -----	DIS 9600
C Aluminum species	DIS 9610
C -----	DIS 9620
	DIS 9630
IF (EXELT(10) .GT. CPUMIN) THEN	DIS 9640
M(34) = ALFA(30) / (KT1(11) * GAMMA(34))	DIS 9650
M(35) = ALFA(30)**2 / (KT1(12) * GAMMA(35))	DIS 9660
M(36) = ALFA(30)**3 / (KT1(13) * GAMMA(36))	DIS 9670
M(37) = 0.0	DIS 9680
IF (DABS(KT1(15)) .GT. 1.0D-30)	DIS 9690
M(37) = ALFA(30)**4 / (KT1(14) * GAMMA(37))	DIS 9700
	DIS 9710
M(38) = LALFA(9) - LOGKT1(15) - DLOG10(GAMMA(38))	DIS 9720
M(38) = SEXP10(M(38))	DIS 9730
M(39) = (2.0*LALFA(9)) - LOGKT1(16) - DLOG10(GAMMA(39))	DIS 9740
M(39) = SEXP10(M(39))	DIS 9750
M(40) = (4.0*LALFA(9)) - LOGKT1(17) - DLOG10(GAMMA(40))	DIS 9760
M(40) = SEXP10(M(40))	DIS 9770
	DIS 9780
M(41) = ALFA(6) / (KT1(18) * GAMMA(41))	DIS 9790
M(42) = ALFA(6)**2 / (KT1(19) * GAMMA(42))	DIS 9800
M(163) = 0.0D00	DIS 9810
IF (DABS(KT1(9)) .GT. 1.0D-30) M(163) = ALFA(30)**5	DIS 9820
/ (KT1(9) * GAMMA(163))	DIS 9830
M(164) = 0.0D00	DIS 9840
IF (DABS(KT1(65)) .GT. 1.0D-30) M(164) = ALFA(30)**6	DIS 9850
/ (KT1(65) * GAMMA(164))	DIS 9860
M(229) = ALFA(48) / (KT1(209) * GAMMA(229))	DIS 9870
M(249) = ALFA(246) / (KT1(225) * GAMMA(249))	DIS 9880
M(250) = ALFA(246)**2 / (KT1(226) * GAMMA(250))	DIS 9890
M(268) = ALFA(265) / (KT1(243) * GAMMA(268))	DIS 9900
M(269) = ALFA(265)**2 / (KT1(244) * GAMMA(269))	DIS 9910
M(MXSP+ 4) = ALFA(MXSP+ 1) / (KT1(MXAQK+3) * GAMMA(MXSP+ 4))	DIS 9920
M(MXSP+19) = ALFA(MXSP+16) / (KT1(MXAQK+17) * GAMMA(MXSP+19))	DIS 9930
	DIS 9940
M(14) = EXELT(10) / (1.0D0 + GAMMA(14) * (M(34) + M(35) +	DIS 9950
M(36) + M(37) + M(38) + M(39) + M(40) + M(41) +	DIS 9960
M(42) + M(163) + M(164) + M(229) + M(249) +	DIS 9970
M(250) + M(268) + M(269) + M(MXSP+4) + M(MXSP+19)))	DIS 9980
ALFA(14) = M(14) * GAMMA(14)	DIS 9990
	DIS10000
IF (M(163) .GT. 3.0) M(163) = 3.0	DIS10010
	DIS10020
DO 210 I = 34, 42	DIS10030

	M(I) = M(I) * ALFA(14)	DIS10040
	ALFA(I) = M(I) * GAMMA(I)	DIS10050
210	CONTINUE	DIS10060
	DO 220 I = 163, 164	DIS10070
	M(I) = M(I) * ALFA(14)	DIS10080
	ALFA(I) = M(I) * GAMMA(I)	DIS10090
220	CONTINUE	DIS10100
		DIS10110
		DIS10120
	M(229) = M(229) * ALFA(14)	DIS10130
	ALFA(229) = M(229) * GAMMA(229)	DIS10140
		DIS10150
	M(249) = M(249) * ALFA(14)	DIS10160
	ALFA(249) = M(249) * GAMMA(249)	DIS10170
		DIS10180
	M(250) = M(250) * ALFA(14)	DIS10190
	ALFA(250) = M(250) * GAMMA(250)	DIS10200
		DIS10210
	M(268) = M(268) * ALFA(14)	DIS10220
	ALFA(268) = M(268) * GAMMA(268)	DIS10230
		DIS10240
	M(269) = M(269) * ALFA(14)	DIS10250
	ALFA(269) = M(269) * GAMMA(269)	DIS10260
		DIS10270
	M(MXSP+ 4) = M(MXSP+ 4) * ALFA(14)	DIS10280
	ALFA(MXSP+4) = M(MXSP+ 4) * GAMMA(MXSP+ 4)	DIS10290
		DIS10300
	M(MXSP+19) = M(MXSP+19) * ALFA(14)	DIS10310
	ALFA(MXSP+19) = M(MXSP+19) * GAMMA(MXSP+19)	DIS10320
	END IF	DIS10330
		DIS10340
C	-----	DIS10350
C	Iron species	DIS10360
C	-----	DIS10370
	IF (EXELT(13) .GT. CPUMIN) THEN	DIS10380
		DIS10390
	M(71) = ALFA(5) / (KT1(46) * GAMMA(71))	DIS10400
	M(72) = ALFA(5)**2 / (KT1(47) * GAMMA(72))	DIS10410
	M(73) = ALFA(99) / (KT1(48) * GAMMA(73))	DIS10420
	M(75) = ALFA(9) / (KT1(50) * GAMMA(75))	DIS10430
	M(76) = ALFA(9)**2 / (KT1(51) * GAMMA(76))	DIS10440
	M(77) = ALFA(10)**2 / (KT1(52) * GAMMA(77) * ALFA(8)**3)	DIS10450
	M(78) = ALFA(6) / (KT1(53) * GAMMA(78))	DIS10460
	M(233) = ALFA(48) / (KT1(213) * GAMMA(233))	DIS10470
	M(234) = ALFA(48)**2 / (KT1(214) * GAMMA(234))	DIS10480
	M(253) = ALFA(246) / (KT1(229) * GAMMA(253))	DIS10490
	M(272) = ALFA(265) / (KT1(247) * GAMMA(272))	DIS10500
	M(MXSP+ 8) = ALFA(MXSP+ 1) / (KT1(MXAQK+ 7) * GAMMA(MXSP+ 8))	DIS10510
	M(MXSP+23) = ALFA(MXSP+16) / (KT1(MXAQK+21) * GAMMA(MXSP+23))	DIS10520
		DIS10530
C	-----	DIS10540
C	If fe+3 is to be calculated from eh measurements then put	DIS10550
C	flags(1) = 1. If from the reaction:	DIS10560
C	fe+3 + 1/2h2o + 1/8hs- = fe++ + 1/8so4 + 9/8h+	DIS10570
C	then flags(1) = 0.	DIS10580
C	-----	DIS10590
		DIS10600
	IF (EHM .LT. 9.0D0 .AND. FLAGS(1) .EQ. 1) THEN	DIS10610

C1	= 10.0**((EHM * F - LOGKT1(138)) / (2.303 * R * T))	DIS10620
M(19)	= C1 / GAMMA(19)	DIS10630
ELSE IF (EXELT(25) .LT. CPUMIN) THEN		DIS10640
M(19)	= 0.0	DIS10650
ELSE IF (FLAGS(1) .EQ. 0) THEN		DIS10660
M(19)	= (ALFA(6)**0.125 * ALFA(8)**1.125) / (KT1(5) * DSQRT(ALFA(10)) * ALFA(101)**0.125 * GAMMA(19))	DIS10670
END IF		DIS10680
		DIS10690
		DIS10700
M(79) = ALFA(5) / (KT1(54) * GAMMA(79))		DIS10710
M(80) = ALFA(5)**2 / (KT1(55) * GAMMA(80))		DIS10720
M(81) = 0.0D00		DIS10730
IF (DABS(KT1(56)) .GT. 1.0D-30)		DIS10740
M(81) = ALFA(5)**3 / (KT1(56) * GAMMA(81))		DIS10750
M(82) = 0.0D00		DIS10760
IF (DABS(KT1(57)) .GT. 1.0D-30)		DIS10770
M(82) = ALFA(5)**4 / (KT1(57) * GAMMA(82))		DIS10780
M(83) = ALFA(6) / (KT1(58) * GAMMA(83))		DIS10790
M(84) = ALFA(6)**2 / (KT1(59) * GAMMA(84))		DIS10800
M(85) = ALFA(9) / (KT1(60) * GAMMA(85))		DIS10810
M(86) = ALFA(9)**2 / (KT1(61) * GAMMA(86))		DIS10820
M(87) = 0.0D00		DIS10830
IF (DABS(KT1(62)) .GT. 1.0D-30)		DIS10840
M(87) = ALFA(9)**3 / (KT1(62) * GAMMA(87))		DIS10850
M(88) = 0.0D00		DIS10860
IF (DABS(KT1(53)) .GT. 1.0D-30)		DIS10870
M(88) = ALFA(9)**4 / (KT1(63) * GAMMA(88))		DIS10880
M(254) = ALFA(246) / (KT1(230) * GAMMA(253))		DIS10890
M(273) = ALFA(265) / (KT1(248) * GAMMA(273))		DIS10900
M(283) = ALFA(30) / (KT1(256) * GAMMA(283))		DIS10910
		DIS10920
DO 230 I = 79, 88		DIS10930
M(I) = M(I) * M(19) * GAMMA(19)		DIS10940
230 CONTINUE		DIS10950
		DIS10960
M(254) = M(254) * M(19) * GAMMA(19)		DIS10970
M(273) = M(273) * M(19) * GAMMA(19)		DIS10980
M(283) = M(283) * M(19) * GAMMA(19)		DIS10990
		DIS11000
M(18) = EXELT(13) / (1.0D0 + GAMMA(18) * (M(19) + M(71) +		DIS11010
M(72) + M(73) + M(75) + M(76) + M(77) + M(78) +		DIS11020
M(79) + M(80) + M(81) + M(82) + M(83) + M(84) +		DIS11030
M(85) + M(86) + M(87) + M(88) + M(233) + M(234) +		DIS11040
M(253) + M(254) + M(272) + M(273) + M(283) +		DIS11050
M(MXSP+8) + M(MXSP+23)))		DIS11060
ALFA(18) = M(18) * GAMMA(18)		DIS11070
		DIS11080
M(19) = M(19) * ALFA(18)		DIS11090
ALFA(19) = M(19) * GAMMA(19)		DIS11100
		DIS11110
DO 240 I = 71, 88		DIS11120
IF (I .EQ. 74) GO TO 240		DIS11130
M(I) = M(I) * ALFA(18)		DIS11140
ALFA(I) = M(I) * GAMMA(I)		DIS11150
240 CONTINUE		DIS11160
		DIS11170
M(233) = M(233) * ALFA(18)		DIS11180
ALFA(233) = M(233) * GAMMA(233)		DIS11190

M(234)	= M(234)	* ALFA(18)	DIS11200
ALFA(234)	= M(234)	* GAMMA(234)	DIS11210
			DIS11220
			DIS11230
M(253)	= M(253)	* ALFA(18)	DIS11240
ALFA(253)	= M(253)	* GAMMA(253)	DIS11250
			DIS11260
M(254)	= M(254)	* ALFA(18)	DIS11270
ALFA(254)	= M(254)	* GAMMA(254)	DIS11280
			DIS11290
M(272)	= M(272)	* ALFA(18)	DIS11300
ALFA(272)	= M(272)	* GAMMA(272)	DIS11310
			DIS11320
M(273)	= M(273)	* ALFA(18)	DIS11330
ALFA(273)	= M(273)	* GAMMA(273)	DIS11340
			DIS11350
M(283)	= M(283)	* ALFA(18)	DIS11360
ALFA(283)	= M(283)	* GAMMA(283)	DIS11370
			DIS11380
M(MXSP+ 8)	= M(MXSP+ 8)	* ALFA(18)	DIS11390
ALFA(MXSP+ 8)	= M(MXSP+ 8)	* GAMMA(MXSP+ 8)	DIS11400
			DIS11410
M(MXSP+23)	= M(MXSP+23)	* ALFA(18)	DIS11420
ALFA(MXSP+23)	= M(MXSP+23)	* GAMMA(MXSP+23)	DIS11430
END IF			DIS11440
			DIS11450
C -----			DIS11460
C Barium species			DIS11470
C -----			DIS11480
			DIS11490
IF (EXELT(11) .GT. CPUMIN) THEN			DIS11500
M(51) = ALFA(98) / (KT1(26) * GAMMA(51))			DIS11510
M(52) = ALFA(7) / (KT1(27) * GAMMA(52))			DIS11520
M(53) = ALFA(9) / (KT1(28) * GAMMA(53))			DIS11530
M(54) = ALFA(6) / (KT1(29) * GAMMA(54))			DIS11540
M(230) = ALFA(48) / (KT1(210) * GAMMA(230))			DIS11550
M(251) = ALFA(246) / (KT1(227) * GAMMA(251))			DIS11560
M(270) = ALFA(265) / (KT1(245) * GAMMA(270))			DIS11570
M(MXSP+ 5) = ALFA(MXSP+ 1) / (KT1(MXAQK+ 4) * GAMMA(MXSP+ 5))			DIS11580
M(MXSP+20) = ALFA(MXSP+16) / (KT1(MXAQK+18) * GAMMA(MXSP+20))			DIS11590
			DIS11600
M(15) = EXELT(11) / (1.0D0 + GAMMA(15) * (M(51) + M(52) +			DIS11610
M(53) + M(54) + M(230) + M(251) + M(270) +			DIS11620
M(MXSP+5) + M(MXSP+20)))			DIS11630
ALFA(15) = M(15) * GAMMA(15)			DIS11640
			DIS11650
DO 250 I = 51, 54			DIS11660
M(I) = M(I) * ALFA(15)			DIS11670
ALFA(I) = M(I) * GAMMA(I)			DIS11680
250 CONTINUE			DIS11690
			DIS11700
M(230) = M(230)	* ALFA(15)		DIS11710
ALFA(230) = M(230)	* GAMMA(230)		DIS11720
			DIS11730
M(251) = M(251)	* ALFA(15)		DIS11740
ALFA(251) = M(251)	* GAMMA(251)		DIS11750
			DIS11760
M(270) = M(270)	* ALFA(15)		DIS11770

ALFA(270)	= M(270)	* GAMMA(270)	DIS11780
			DIS11790
M(MXSP+5)	= M(MXSP+5)	* ALFA(15)	DIS11800
ALFA(MXSP+5)	= M(MXSP+5)	* GAMMA(MXSP+5)	DIS11810
			DIS11820
M(MXSP+20)	= M(MXSP+20)	* ALFA(15)	DIS11830
ALFA(MXSP+20)	= M(MXSP+20)	* GAMMA(MXSP+20)	DIS11840
END IF			DIS11850
			DIS11860
C -----			DIS11870
C Copper species			DIS11880
C -----			DIS11890
			DIS11900
IF (EXELT(12) .GE. CPUMIN) THEN			DIS11910
M(62) = ALFA(5)	/ (KT1(37) * GAMMA(62))		DIS11920
M(63) = ALFA(5)**2	/ (KT1(38) * GAMMA(63))		DIS11930
M(64) = ALFA(5)**3	/ (KT1(39) * GAMMA(64))		DIS11940
M(232) = ALFA(48)	/ (KT1(212) * GAMMA(232))		DIS11950
M(MXSP+ 7) = ALFA(MXSP+ 1)	/ (KT1(MXAQK+ 6) * GAMMA(MXSP+ 7))		DIS11960
M(MXSP+22) = ALFA(MXSP+16)	/ (KT1(MXAQK+20) * GAMMA(MXSP+22))		DIS11970
			DIS11980
C -----			DIS11990
C If cu++ is to be calculated from eh measurements then			DIS12000
C flags(2) = 1. If from cu++ + fe++ = cu+ + fe+3, then			DIS12010
C flags(2) = 0.			DIS12020
C -----			DIS12030
			DIS12040
IF (EHM .LT. 9.0 .AND. FLAGS(2) .EQ. 1) THEN			DIS12050
C1 = 1.0D1**((EHM * F - LOGKT1(139)) / (2.303 * R * T))			DIS12060
M(17) = C1 / GAMMA(19)			DIS12070
ELSE IF (EXELT(25) .LT. CPUMIN) THEN			DIS12080
M(17) = 0.0D0			DIS12090
ELSE IF (FLAGS(2) .EQ. 0) THEN			DIS12100
M(17) = ALFA(19) / (KT1(4) * ALFA(18) * GAMMA(17))			DIS12110
END IF			DIS12120
			DIS12130
M(65) = ALFA(5)	/ (KT1(40) * GAMMA(65))		DIS12140
M(66) = ALFA(5)**2	/ (KT1(41) * GAMMA(66))		DIS12150
M(67) = 0.0D00			DIS12160
IF (DABS(KT1(42)) .GT. 1.0D-30)			DIS12170
M(67) = ALFA(5)**3 / (KT1(42) * GAMMA(67))			DIS12180
M(68) = 0.0D00			DIS12190
IF (DABS(KT1(43)) .GT. 1.0D-30)			DIS12200
M(68) = ALFA(5)**4 / (KT1(43) * GAMMA(68))			DIS12210
M(69) = ALFA(9) / (KT1(44) * GAMMA(69))			DIS12220
M(70) = ALFA(6) / (KT1(45) * GAMMA(70))			DIS12230
			DIS12240
DO 260 I = 65, 70			DIS12250
M(I) = M(I) * M(17) * GAMMA(17)			DIS12260
260 CONTINUE			DIS12270
			DIS12280
M(16) = EXELT(12) / (1.0D0 + GAMMA(16) * (M(17) + M(62) +			DIS12290
M(63) + M(64) + M(65) + M(66) + M(67) + M(68) +			DIS12300
M(69) + M(70) + M(232) + M(MXSP+7) + M(MXSP+22)))			DIS12310
ALFA(16) = M(16) * GAMMA(16)			DIS12320
			DIS12330
M(17) = M(17) * ALFA(16)			DIS12340
ALFA(17) = M(17) * GAMMA(17)			DIS12350

		DIS12360
	DO 270 I = 62, 70	DIS12370
	M(I) = M(I) * ALFA(16)	DIS12380
	ALFA(I) = M(I) * GAMMA(I)	DIS12390
270	CONTINUE	DIS12400
		DIS12410
	M(232) = M(232) * ALFA(16)	DIS12420
	ALFA(232) = M(232) * GAMMA(232)	DIS12430
		DIS12440
	M(MXSP+7) = M(MXSP+7) * ALFA(16)	DIS12450
	ALFA(MXSP+7) = M(MXSP+7) * GAMMA(MXSP+7)	DIS12460
		DIS12470
	M(MXSP+22) = M(MXSP+22) * ALFA(16)	DIS12480
	ALFA(MXSP+22) = M(MXSP+22) * GAMMA(MXSP+22)	DIS12490
	END IF	DIS12500
		DIS12510
C	-----	DIS12520
C	Mercury species	DIS12530
C	-----	DIS12540
		DIS12550
	IF (EXELT(14) .GT. CPUMIN) THEN	DIS12560
	M(105) = ALFA(5) / (KT1(78) * GAMMA(105))	DIS12570
	M(106) = ALFA(5)**2 / (KT1(79) * GAMMA(106))	DIS12580
	M(107) = ALFA(5)**3 / (KT1(80) * GAMMA(107))	DIS12590
	M(108) = ALFA(5)**4 / (KT1(81) * GAMMA(108))	DIS12600
	M(109) = ALFA(6) / (KT1(82) * GAMMA(109))	DIS12610
		DIS12620
C	-----	DIS12630
C	The k values for hgsh2s)2 are so small a divide by zero error	DIS12640
C	will occur is the reason for the following statement.	DIS12650
C	-----	DIS12660
	M(110) = 0.0	DIS12670
	IF (DABS(KT1(83)) .GT. 1.0D-30) M(110) = ALFA(33)**2	DIS12680
	* ALFA(101) / (KT1(83) * GAMMA(110) * ALFA(8))	DIS12690
	M(111) = ALFA(101)**3 / (KT1(84) * GAMMA(111))	DIS12700
	M(165) = ALFA(9) / (KT1(117) * GAMMA(165))	DIS12710
	M(166) = ALFA(9)**2 / (KT1(137) * GAMMA(166))	DIS12720
		DIS12730
C	-----	DIS12740
C	If hg++ is to be calculated from eh then flags(3) = 1.	DIS12750
C	If from 2hg++ + 2fe++ = hg++ + 2fe+3 then flags(3) = 0.	DIS12760
C	-----	DIS12770
		DIS12780
	IF (EHM .LT. 9.0 .AND. FLAGS(3) .EQ. 1) THEN	DIS12790
	C1 = 10.0**(((EHM*F - LOGKT1(140))*2) / (2.303*R*T))	DIS12800
	M(20) = C1 * M(21) * GAMMA(21) / GAMMA(20)	DIS12810
	ELSE IF (EXELT(25) .LT. CPUMIN .OR. EXELT(13) .LT. CPUMIN	DIS12820
	.OR. ALFA(18) .LT. 1.0D-30 .OR. ALFA(19) .LT. 1.0D-30)	DIS12830
	THEN	DIS12840
	M(20) = 0.0	DIS12850
	M(112) = 0.0	DIS12860
	ELSE IF (FLAGS(3) .EQ. 0) THEN	DIS12870
	M(20) = 2.0 * DLOG10(ALFA(18)) - 2.0 * DLOG10(ALFA(19))	DIS12880
	+ DLOG10(M(21)) + DLOG10(GAMMA(21)) + DLOG10(KT1(6))	DIS12890
	- DLOG10(GAMMA(20))	DIS12900
	IF (M(20) .GT. -30.0 .AND. M(20) .LT. +30.0) THEN	DIS12910
	M(20) = 10.0**M(20)	DIS12920
	ELSE	DIS12930

M(20) = 0.0D00	DIS12940
END IF	DIS12950
M(112) = 2.0 * DLOG10(ALFA(18)) - 2.0 * DLOG10(ALFA(19))	DIS12960
+ DLOG10(KT1(85)) - DLOG10(GAMMA(112))	DIS12970
IF (M(112) .GT. -30.0 .AND. M(112) .LT. +30.0) THEN	DIS12980
M(112) = 10.0**M(112)	DIS12990
ELSE	DIS13000
M(112) = 0.0	DIS13010
END IF	DIS13020
END IF	DIS13030
	DIS13040
	DIS13050
M(21) = EXELT(14) / (1.0D0 + GAMMA(21) * (M(20) + M(105) +	DIS13060
M(106) + M(107) + M(108) + M(109) + M(110) +	DIS13070
M(111) + M(112) + M(165) + M(166)))	DIS13080
ALFA(21) = M(21) * GAMMA(21)	DIS13090
	DIS13100
M(20) = M(20) * ALFA(21)	DIS13110
ALFA(20) = M(20) * GAMMA(20)	DIS13120
	DIS13130
DO 280 I = 105, 112	DIS13140
M(I) = M(I) * ALFA(21)	DIS13150
ALFA(I) = M(I) * GAMMA(I)	DIS13160
280 CONTINUE	DIS13170
	DIS13180
DO 290 I = 165, 166	DIS13190
M(I) = M(I) * ALFA(21)	DIS13200
ALFA(I) = M(I) * GAMMA(I)	DIS13210
290 CONTINUE	DIS13220
END IF	DIS13230
	DIS13240
C -----	DIS13250
C Lithium species	DIS13260
C -----	DIS13270
	DIS13280
IF (EXELT(15) .GT. CPUMIN) THEN	DIS13290
M(118) = ALFA(9) / (KT1(91) * GAMMA(118))	DIS13300
M(119) = ALFA(6) / (KT1(92) * GAMMA(119))	DIS13310
	DIS13320
M(22) = EXELT(15) / (1.0D0 + GAMMA(22) * (M(118) + M(119)))	DIS13330
ALFA(22) = M(22) * GAMMA(22)	DIS13340
	DIS13350
DO 300 I = 118, 119	DIS13360
M(I) = M(I) * ALFA(22)	DIS13370
ALFA(I) = M(I) * GAMMA(I)	DIS13380
300 CONTINUE	DIS13390
END IF	DIS13400
	DIS13410
C -----	DIS13420
C Manganese species	DIS13430
C -----	DIS13440
	DIS13450
IF (EXELT(16) .GT. CPUMIN) THEN	DIS13460
M(128) = ALFA(5) / (KT1(101) * GAMMA(128))	DIS13470
M(129) = ALFA(5)**2 / (KT1(102) * GAMMA(129))	DIS13480
M(130) = ALFA(5)**3 / (KT1(103) * GAMMA(130))	DIS13490
M(131) = 0.0D00	DIS13500
IF (DABS(KT1(104)) .GT. 1.0D-30)	DIS13510

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      M(131) = ALFA( 5)**4 / (KT1(104) * GAMMA(131))      DIS13520
      M(132) = ALFA( 7) / (KT1(105) * GAMMA(132))          DIS13530
      M(133) = ALFA( 6) / (KT1(106) * GAMMA(133))          DIS13540
      M(134) = ALFA( 99) / (KT1(108) * GAMMA(134))         DIS13550
      M(135) = ALFA( 9) / (KT1(109) * GAMMA(135))         DIS13560
      M(257) = ALFA(246) / (KT1(233) * GAMMA(257))         DIS13570
      M(258) = ALFA(246)**2 / (KT1(234) * GAMMA(258))      DIS13580
      M(259) = ALFA(246)**3 / (KT1(235) * GAMMA(259))      DIS13590
      M(276) = ALFA(265) / (KT1(251) * GAMMA(276))         DIS13600
      M(MXSP+11) = ALFA(MXSP+ 1) / (KT1(MXAQK+10) * GAMMA(MXSP+11)) DIS13610
      M(MXSP+26) = ALFA(MXSP+16) / (KT1(MXAQK+24) * GAMMA(MXSP+26)) DIS13620
C ----- DIS13630
C If mn+++ is to be calculated from eh then flags(4) = 1. DIS13640
C If from mn+3 + fe++ = mn++ + fe+3 then flags(4) = 0. DIS13650
C ----- DIS13660
      IF (EHM.LT.9.0D0 .AND. FLAGS(4) .EQ. 1) THEN DIS13670
      C1 = 1.0D1**((EHM * F - LOGKT1(141)) / (2.303 * R * T)) DIS13680
      M(24) = C1 / GAMMA(23) DIS13690
      ELSE IF (EXELT(25) .LT. CPUMIN) THEN DIS13700
      M(24) = 0.0D0 DIS13710
      ELSE IF (EXELT(13) .LT. CPUMIN) THEN DIS13720
      M(24) = 0.0D0 DIS13730
      ELSE IF (FLAGS(4) .EQ. 0) THEN DIS13740
      M(24) = ALFA(19) / (KT1(7) * ALFA(18) * GAMMA(24)) DIS13750
      END IF DIS13760
      M(24) = ALFA(19) / (KT1(7) * ALFA(18) * GAMMA(24)) DIS13770
      DIS13780
      DIS13790
      M(153) = ALFA( 5) / (KT1(107) * GAMMA(153)) DIS13800
      M(153) = M(153) * M(24) * GAMMA(24) DIS13810
      DIS13820
      M(260) = ALFA(246) / (KT1(236) * GAMMA(258)) DIS13830
      M(260) = M(260) * M(24) * GAMMA(24) DIS13840
      DIS13850
      M(23) = EXELT(16) / (1.0D0 + GAMMA(23) * (M(24) + M(128) + DIS13860
      M(129) + M(130) + M(131) + M(132) + M(133) + DIS13870
      M(134) + M(135) + M(153) + M(257) + M(258) + DIS13880
      M(259) + M(260) + M(276) + M(MXSP+11) + M(MXSP+26))) DIS13890
      ALFA(23) = M(23) * GAMMA(23) DIS13900
      DIS13910
      M(24) = M(24) * ALFA(23) DIS13920
      ALFA(24) = M(24) * GAMMA(24) DIS13930
      DIS13940
      DO 310 I = 128, 135 DIS13950
      M(I) = M(I) * ALFA(23) DIS13960
      ALFA(I) = M(I) * GAMMA(I) DIS13970
310 CONTINUE DIS13980
      DIS13990
      M(153) = M(153) * ALFA(23) DIS14000
      ALFA(153) = M(153) * GAMMA(153) DIS14010
      DIS14020
      DO 320 I = 257, 260 DIS14030
      M(I) = M(I) * ALFA(23) DIS14040
      ALFA(I) = M(I) * GAMMA(I) DIS14050
320 CONTINUE DIS14060
      DIS14070
      M(276) = M(276) * ALFA(23) DIS14080
      ALFA(276) = M(276) * GAMMA(276) DIS14090

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M(MXSP+11)	= M(MXSP+11) * ALFA(23)	DIS14100
ALFA(MXSP+11)	= M(MXSP+11) * GAMMA(MXSP+11)	DIS14110
		DIS14120
		DIS14130
M(MXSP+26)	= M(MXSP+26) * ALFA(23)	DIS14140
ALFA(MXSP+26)	= M(MXSP+26) * GAMMA(MXSP+26)	DIS14150
END IF		DIS14160
		DIS14170
C -----		DIS14180
C Lead species		DIS14190
C -----		DIS14200
		DIS14210
IF (EXELT(17) .GT. CPUMIN) THEN		DIS14220
M(148) = ALFA(5) / (KT1(121) * GAMMA(148))		DIS14230
M(149) = ALFA(5)**2 / (KT1(122) * GAMMA(149))		DIS14240
M(150) = ALFA(5)**3 / (KT1(123) * GAMMA(150))		DIS14250
M(151) = 0.0D00		DIS14260
IF (DABS(KT1(124)) .GT. 1.0D-30)		DIS14270
M(151) = ALFA(5)**4 / (KT1(124) * GAMMA(151))		DIS14280
M(152) = ALFA(6) / (KT1(125) * GAMMA(152))		DIS14290
M(238) = ALFA(48) / (KT1(218) * GAMMA(238))		DIS14300
M(239) = ALFA(48)**2 / (KT1(219) * GAMMA(239))		DIS14310
M(240) = ALFA(48)**3 / (KT1(220) * GAMMA(240))		DIS14320
M(262) = ALFA(246) / (KT1(238) * GAMMA(262))		DIS14330
M(278) = ALFA(265) / (KT1(253) * GAMMA(278))		DIS14340
M(286) = ALFA(101)**2 / (KT1(258) * GAMMA(286))		DIS14350
M(287) = ALFA(101)**3 / (KT1(259) * GAMMA(287))		DIS14360
M(288) = ALFA(98) / (KT1(260) * GAMMA(288))		DIS14370
M(289) = ALFA(9) / (KT1(261) * GAMMA(289))		DIS14380
M(MXSP+13) = ALFA(MXSP+ 1) / (KT1(MXAQK+12) * GAMMA(MXSP+13))		DIS14390
M(MXSP+28) = ALFA(MXSP+16) / (KT1(MXAQK+26) * GAMMA(MXSP+28))		DIS14400
		DIS14410
M(25) = EXELT(17) / (1.0D0 + GAMMA(25) * (M(148) + M(149) +		DIS14420
M(150) + M(151) + M(152) + M(238) + M(239) + M(240) +		DIS14430
M(262) + M(278) + M(286) + M(287) + M(288) + M(289) +		DIS14440
M(MXSP+13) + M(MXSP+28)))		DIS14450
ALFA(25) = M(25) * GAMMA(25)		DIS14460
		DIS14470
		DIS14480
DO 330 I = 148, 152		DIS14490
M(I) = M(I) * ALFA(25)		DIS14500
ALFA(I) = M(I) * GAMMA(I)		DIS14510
330 CONTINUE		DIS14520
		DIS14530
DO 340 I = 238, 240		DIS14540
M(I) = M(I) * ALFA(25)		DIS14550
ALFA(I) = M(I) * GAMMA(I)		DIS14560
340 CONTINUE		DIS14570
		DIS14580
M(262) = M(262) * ALFA(25)		DIS14590
ALFA(262) = M(262) * GAMMA(262)		DIS14600
		DIS14610
M(278) = M(278) * ALFA(25)		DIS14620
ALFA(278) = M(278) * GAMMA(278)		DIS14630
		DIS14640
DO 350 I = 286, 289		DIS14650
M(I) = M(I) * ALFA(25)		DIS14660
ALFA(I) = M(I) * GAMMA(I)		DIS14670


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350  CONTINUE
M(MXSP+13)  = M(MXSP+13) * ALFA(25)
ALFA(MXSP+13) = M(MXSP+13) * GAMMA(MXSP+13)
M(MXSP+28)  = M(MXSP+28) * ALFA(25)
ALFA(MXSP+28) = M(MXSP+28) * GAMMA(MXSP+28)
END IF

C -----
C   Strontium species
C -----

360  CONTINUE
IF (EXELT(18) .GT. CPUMIN) THEN
  M(154) = ALFA( 9) / (KT1(127) * GAMMA(154))
  M(155) = ALFA( 98) / (KT1(128) * GAMMA(155))
  M(156) = ALFA( 7) / (KT1(129) * GAMMA(156))
  M(157) = ALFA( 6) / (KT1(130) * GAMMA(157))
  M(241) = ALFA( 48) / (KT1(221) * GAMMA(241))
  M(263) = ALFA(246) / (KT1(239) * GAMMA(263))
  M(279) = ALFA(265) / (KT1(254) * GAMMA(279))
  M(MXSP+14) = ALFA(MXSP+ 1) / (KT1(MXAQK+13) * GAMMA(MXSP+14))
  M(MXSP+29) = ALFA(MXSP+16) / (KT1(MXAQK+27) * GAMMA(MXSP+29))

  M(26) = EXELT(18) / (1.0D0 + GAMMA(26) * (M(154) + M(155) +
    M(156) + M(157) + M(241) + M(263) + M(279) +
    M(MXSP+14) + M(MXSP+29)))
  ALFA(26) = M(26) * GAMMA(26)

  DO 370 I = 154, 157
    M(I) = M(I) * ALFA(26)
    ALFA(I) = M(I) * GAMMA(I)
370  CONTINUE

  M(241) = M(241) * ALFA(26)
  ALFA(241) = M(241) * GAMMA(241)

  M(263) = M(263) * ALFA(26)
  ALFA(263) = M(263) * GAMMA(263)

  M(279) = M(279) * ALFA(26)
  ALFA(279) = M(279) * GAMMA(279)

  M(MXSP+14) = M(MXSP+14) * ALFA(26)
  ALFA(MXSP+14) = M(MXSP+14) * GAMMA(MXSP+14)

  M(MXSP+29) = M(MXSP+29) * ALFA(26)
  ALFA(MXSP+29) = M(MXSP+29) * GAMMA(MXSP+29)

  IF (IPIT.EQ.1 .AND. PG(26).GT.CPUMIN
    .AND. GAMMA(26).LE.10.0) THEN
    IF (DABS(PALFA(26)-ALFA(26)) .GT. 1.0D-2*PALFA(26)) THEN
      IF (PALFA(26) .GT. ALFA(26)) THEN
        INC=0.1
      ELSE
        INC=-0.01
      END IF
    END IF

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GAMMA(26)=GAMMA(26)*(1.0+INC)	DIS15260
GO TO 360	DIS15270
END IF	DIS15280
END IF	DIS15290
	DIS15300
IF (IPIT.EQ.1 .AND. GAMMA(26).GT. 10.0) GAMMA(26) = 10.0	DIS15310
IF (IPIT.GT.1 .AND. GAMMA(26).LT.PG(26)) GAMMA(26) = PG(26)	DIS15320
END IF	DIS15330
	DIS15340
C -----	DIS15350
C Zinc species	DIS15360
C -----	DIS15370
	DIS15380
IF (EXELT(19) .GT. CPUMIN) THEN	DIS15390
M(158) = ALFA(5) / (KT1(131) * GAMMA(158))	DIS15400
M(159) = ALFA(5)**2 / (KT1(132) * GAMMA(159))	DIS15410
M(160) = ALFA(5)**3 / (KT1(133) * GAMMA(160))	DIS15420
M(161) = 0.0D00	DIS15430
IF (DABS(KT1(134)) .GT. 1.0D-30)	DIS15440
M(161) = ALFA(5)**4 / (KT1(134) * GAMMA(161))	DIS15450
M(162) = ALFA(6) / (KT1(135) * GAMMA(162))	DIS15460
M(244) = ALFA(48) / (KT1(222) * GAMMA(244))	DIS15470
M(245) = ALFA(48)**2 / (KT1(126) * GAMMA(245))	DIS15480
M(264) = ALFA(246) / (KT1(240) * GAMMA(264))	DIS15490
M(280) = ALFA(265) / (KT1(255) * GAMMA(280))	DIS15500
M(290) = ALFA(101)**2 / (KT1(262) * GAMMA(290))	DIS15510
M(291) = ALFA(101)**3 / (KT1(263) * GAMMA(291))	DIS15520
M(292) = ALFA(7) / (KT1(264) * GAMMA(292))	DIS15530
M(293) = ALFA(9) / (KT1(265) * GAMMA(293))	DIS15540
M(294) = ALFA(9)**2 / (KT1(266) * GAMMA(294))	DIS15550
M(295) = ALFA(101) * ALFA(9) / (KT1(267) * GAMMA(295))	DIS15560
M(MXSP+15) = ALFA(MXSP+ 1) / (KT1(MXAQK+14) * GAMMA(MXSP+15))	DIS15570
M(MXSP+30) = ALFA(MXSP+16) / (KT1(MXAQK+28) * GAMMA(MXSP+30))	DIS15580
	DIS15590
M(27) = EXELT(19) / (1.0D0 + GAMMA(27) * (M(158) + M(159) +	DIS15600
M(160) + M(161) + M(162) + M(244) + M(245) + M(264) +	DIS15610
M(280) + M(290) + M(291) + M(292) + M(293) + M(294) +	DIS15620
M(295) + M(MXSP+15) + M(MXSP+30)))	DIS15630
ALFA(27) = M(27) * GAMMA(27)	DIS15640
	DIS15650
DO 380 I = 158, 162	DIS15660
M(I) = M(I) * ALFA(27)	DIS15670
ALFA(I) = M(I) * GAMMA(I)	DIS15680
380 CONTINUE	DIS15690
	DIS15700
M(244) = M(244) * ALFA(27)	DIS15710
ALFA(244) = M(244) * GAMMA(244)	DIS15720
	DIS15730
M(245) = M(245) * ALFA(27)	DIS15740
ALFA(245) = M(245) * GAMMA(245)	DIS15750
	DIS15760
M(264) = M(264) * ALFA(27)	DIS15770
ALFA(264) = M(264) * GAMMA(264)	DIS15780
	DIS15790
M(280) = M(280) * ALFA(27)	DIS15800
ALFA(280) = M(280) * GAMMA(280)	DIS15810
	DIS15820
DO 390 I = 290, 295	DIS15830

	M(I) = M(I) * ALFA(27)	DIS15840
	ALFA(I) = M(I) * GAMMA(I)	DIS15850
390	CONTINUE	DIS15860
		DIS15870
	M(MXSP+15) = M(MXSP+15) * ALFA(27)	DIS15880
	ALFA(MXSP+15) = M(MXSP+15) * GAMMA(MXSP+15)	DIS15890
		DIS15900
	M(MXSP+30) = M(MXSP+30) * ALFA(27)	DIS15910
	ALFA(MXSP+30) = M(MXSP+30) * GAMMA(MXSP+30)	DIS15920
	END IF	DIS15930
		DIS15940
C	-----	DIS15950
C	Arsenic species	DIS15960
C	-----	DIS15970
		DIS15980
	IF (EXELT(20) .GT. CPUMIN) THEN	DIS15990
	M(49) = ALFA(8) / KT1(67) * GAMMA(49)	DIS16000
		DIS16010
C	-----	DIS16020
C	The following statement prevents a divide by zero error if the	DIS16030
C	concentration or fe+2 is zero	DIS16040
C	-----	DIS16050
	IF (DABS(ALFA(18)) .GT. 1.0D-30) M(50) = (ALFA(19) /	DIS16060
	ALFA(18))**2 * ALFA(10) / KT1(136) * ALFA(8)**4 * GAMMA(50)	DIS16070
		DIS16080
	M(92) = KT1(8) / ALFA(8) * GAMMA(92)	DIS16090
	M(93) = ALFA(8) / (KT1(68) * GAMMA(93))	DIS16100
	M(94) = ALFA(8)**2 / (KT1(69) * GAMMA(94))	DIS16110
	M(95) = ALFA(8)**3 / (KT1(70) * GAMMA(95))	DIS16120
		DIS16130
		DIS16140
	DO 400 I = 93, 95	DIS16150
	M(I) = M(I) * M(50) * GAMMA(50)	DIS16160
400	CONTINUE	DIS16170
		DIS16180
	M(28) = EXELT(20) / (1.0D0 + GAMMA(28) * (M(49) + M(50) +	DIS16190
	M(92) + M(93) + M(94) + M(95)))	DIS16200
	ALFA(28) = M(28) * GAMMA(28)	DIS16210
		DIS16220
	DO 410 I = 49, 50	DIS16230
	M(I) = M(I) * ALFA(28)	DIS16240
	ALFA(I) = M(I) * GAMMA(I)	DIS16250
410	CONTINUE	DIS16260
		DIS16270
	DO 420 I = 92, 95	DIS16280
	M(I) = M(I) * ALFA(28)	DIS16290
	ALFA(I) = M(I) * GAMMA(I)	DIS16300
420	CONTINUE	DIS16310
	END IF	DIS16320
		DIS16330
C	-----	DIS16340
C	Uranium species	DIS16350
C	-----	DIS16360
		DIS16370
	IF (EXELT(27) .GT. CPUMIN) THEN	DIS16380
	M(189) = ALFA(9) / (KT1(167) * GAMMA(189))	DIS16390
	M(190) = ALFA(9)**2 / (KT1(168) * GAMMA(190))	DIS16400
	M(191) = M(169) * GAMMA(169) * ALFA(9)**2 /	DIS16410

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      (KT1(169) * GAMMA(191))
M(192) = 0.0D00
IF (DABS(KT1(170)) .GT. CPUMIN)
      M(192) = M(169)**2 * GAMMA(169)**2 * ALFA(10)**5 /
      (ALFA(8)**5 * GAMMA(192) * KT1(170))
M(193) = 0.0D00
IF (DABS(KT1(171)) .GT. CPUMIN)
      M(193) = M(169)**2 * GAMMA(169)**2 * ALFA(10)**7 /
      (ALFA(8)**7 * GAMMA(193) * KT1(171))
M(194) = ALFA(6) / (KT1(172) * GAMMA(194))
M(195) = ALFA(6)**2 / (KT1(173) * GAMMA(195))
M(196) = ALFA(30) / (KT1(174) * GAMMA(196))
M(197) = ALFA(30)**2 / (KT1(175) * GAMMA(197))
M(198) = ALFA(30)**3 / (KT1(176) * GAMMA(198))
M(199) = 0.0
IF (DABS(KT1(177)) .GT. 1.0D-30)
      M(199) = ALFA(30)**4 / (KT1(177) * GAMMA(199))
M(200) = ALFA(5) / (KT1(178) * GAMMA(200))
M(201) = ALFA(11) / (KT1(179) * GAMMA(201) * ALFA(8))
M(202) = ALFA(99) / (KT1(180) * GAMMA(202))
M(203) = ALFA(99)**2 / (KT1(181) * GAMMA(203))
M(204) = ALFA(99) * ALFA(8) / (KT1(182) * GAMMA(204))
M(205) = ALFA(99)**2 * ALFA(8)**2 / (KT1(183) * GAMMA(205))
M(206) = ALFA(99)**3 * ALFA(8)**3 / (KT1(184) * GAMMA(206))
M(207) = ALFA(98) / (KT1(185) * GAMMA(207))
M(208) = ALFA(98)**2 / (KT1(186) * GAMMA(208))
M(209) = ALFA(98)**3 / (KT1(187) * GAMMA(209))
M(242) = ALFA(48) / (KT1(203) * GAMMA(242))
M(243) = ALFA(48)**2 / (KT1(204) * GAMMA(243))

C -----
C If uo2 is to be calculated from eh then flags(5) = 1, if from
C uo+2 + fe+2 = uo+ + fe+3 then flags(5) = 0.
C -----

      IF (EHM .LT. 9.0 .AND. FLAGS(5) .EQ. 1) THEN
            C1 = 10.0**((-EHM * F - LOGKT1(143)) / (2.303 * R * T))
            M(168) = C1 / (GAMMA(169))
      ELSE IF (EXELT(25) .LT. CPUMIN) THEN
            M(168) = 0.0
      ELSE IF (EXELT(13) .LT. CPUMIN) THEN
            M(168) = 0.0
      ELSE IF (FLAGS(5) .EQ. 0) THEN
            M(168) = ALFA(18) / (KT1(205) * ALFA(19) * GAMMA(168))
      END IF

C -----
C If u+4 is to be calculated from eh then flag(5) = 1, if from
C uo+2 + fe+2 + 4h+ = u+4 + fe+3 +2 h2o then flag(5) = 0.
C -----

      IF (EHM .LT. 9D0 .AND. FLAGS(5) .EQ. 1) THEN
            C1 = 1.0D1**((-EHM * F - (LOGKT1(142))) /
            (2.303 * R * T)) + DLOG10(ALFA(10)**2 / ALFA(8)**4)
            M(167) = C1 / GAMMA(168)
      ELSE IF (EXELT(25) .LT. CPUMIN .OR. EXELT(13) .LT. CPUMIN) THEN
            M(167) = 0.0D0
      ELSE IF (FLAGS(5) .EQ. 0) THEN

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      M(167) =          ALFA(18) * ALFA(8)**4 /          DIS17000
                    (KT1(206) * ALFA(19) * GAMMA(167) * ALFA(10)**2) DIS17010
END IF                                                    DIS17020
                                                        DIS17030
M(167) = M(167) * M(168) * GAMMA(168)                  DIS17040
M(170) = ALFA(9) / (KT1(148) * GAMMA(170))              DIS17050
M(171) = ALFA(9)**2 / (KT1(149) * GAMMA(171))           DIS17060
M(172) = ALFA(10)**3 / (KT1(150) * GAMMA(172) * ALFA(8)**3) DIS17070
M(173) = 0.0D00                                          DIS17080
IF (DABS(KT1(151)) .GT. 1.0D-30)                        DIS17090
      M(173) = ALFA(10)**4 / (KT1(151) * GAMMA(173) * ALFA(8)**4) DIS17100
M(174) = 0.0D00                                          DIS17110
IF (DABS(KT1(152)) .GT. 1.0D-30)                        DIS17120
      M(174) = ALFA(10)**5 / (KT1(152) * GAMMA(174) * ALFA(8)**5) DIS17130
M(175) = ALFA(30) / (KT1(153) * GAMMA(175))             DIS17140
M(176) = ALFA(30)**2 / (KT1(154) * GAMMA(176))          DIS17150
M(177) = 0.0D00                                          DIS17160
IF (DABS(KT1(155)) .GT. 1.0D-30)                        DIS17170
      M(177) = ALFA(30)**3 / (KT1(155) * GAMMA(177))     DIS17180
M(178) = 0.0D00                                          DIS17190
IF (DABS(KT1(156)) .GT. 1.0D-30)                        DIS17200
      M(178) = ALFA(30)**4 / (KT1(156) * GAMMA(178))     DIS17210
M(179) = 0.0D00                                          DIS17220
IF (DABS(KT1(157)) .GT. 1.0D-30)                        DIS17230
      M(179) = ALFA(30)**5 / (KT1(157) * GAMMA(179))     DIS17240
M(180) = 0.0D00                                          DIS17250
IF (DABS(KT1(158)) .GT. 1.0D-30)                        DIS17260
      M(180) = ALFA(30)**6 / (KT1(158) * GAMMA(180))     DIS17270
M(181) = ALFA(5) / (KT1(159) * GAMMA(181))              DIS17280
M(182) = ALFA(99) / (KT1(160) * GAMMA(182))             DIS17290
M(183) = ALFA(99)**2 / (KT1(161) * GAMMA(183))          DIS17300
M(184) = ALFA(100)**3 / (KT1(162) * GAMMA(184) * ALFA(8)**3) DIS17310
M(185) = 0.0D00                                          DIS17320
IF (DABS(KT1(185)) .GT. 1.0D-30)                        DIS17330
      M(185) = ALFA(100)**4 / (KT1(163) * GAMMA(185) * ALFA(8)**4) DIS17340
M(186) = ALFA(6) / (KT1(164) * GAMMA(186))              DIS17350
M(187) = ALFA(6)**2 / (KT1(165) * GAMMA(187))           DIS17360
                                                        DIS17370
IF (ALFA(167) .GT. 0.0D0) THEN                          DIS17380
      M(188) = ALFA(10)**12 * ALFA(9)**3 *              DIS17390
      1.0D1** (DLOG10(ALFA(167)) * 5) / (KT1(166) * GAMMA(188) * DIS17400
      1.0D1** (DLOG10(ALFA(8)) * 12))                  DIS17410
END IF                                                    DIS17420
                                                        DIS17430
DO 430 I = 170, 188                                     DIS17440
      M(I) = M(I) * M(167) * GAMMA(167)                 DIS17450
430 CONTINUE                                              DIS17460
                                                        DIS17470
M(169) = M(167) + M(168) +      M(170) +      M(171) +      M(172) DIS17480
      + M(173) +      M(174) +      M(175) +      M(176) DIS17490
      + M(177) +      M(178) +      M(179) +      M(180) DIS17500
      + M(181) +      M(182) +      M(183) +      M(184) DIS17510
      + M(185) +      M(186) +      M(187) + 6.0*M(188) DIS17520
      + M(189)                                              DIS17530
M(169) = M(169) + M(190) + 2.0*M(191) + 3.0*M(192) + 3.0*M(193) DIS17540
      + M(194) +      M(195) +      M(196) +      M(197) DIS17550
      + M(198) +      M(199) +      M(200) +      M(201) DIS17560
      + M(202) +      M(203) +      M(204) +      M(205) DIS17570

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      + M(206) +      M(207) +      M(208) +      M(209) DIS17580
      + M(242) +      M(243) DIS17590
M(169) = EXELT(27) / (1.0D0 + GAMMA(169) * M(169)) DIS17600
ALFA(169) = M(169) * GAMMA(169) DIS17610
DIS17620
M(167) = M(167) * ALFA(169) DIS17630
ALFA(167) = M(167) * GAMMA(167) DIS17640
M(168) = M(168) * ALFA(169) DIS17650
ALFA(168) = M(168) * GAMMA(168) DIS17660
DIS17670
DO 440 I = 170, 209 DIS17680
  M(I) = M(I) * ALFA(169) DIS17690
  ALFA(I) = M(I) * GAMMA(I) DIS17700
440 CONTINUE DIS17710
DIS17720
M(242) = M(242) * ALFA(169) DIS17730
ALFA(242) = M(242) * GAMMA(242) DIS17740
M(243) = M(243) * ALFA(169) DIS17750
ALFA(243) = M(243) * GAMMA(243) DIS17760
END IF DIS17770
DIS17780
C ----- DIS17790
C Vanadium species DIS17800
C ----- DIS17810
DIS17820
IF (EXELT(28) .GT. CPUMIN) THEN DIS17830
  M(213) = ALFA(8) / (KT1(188) * GAMMA(213)) DIS17840
  M(214) = ALFA(8)**2 / (KT1(189) * GAMMA(214)) DIS17850
  M(215) = ALFA(8)**3 / (KT1(190) * GAMMA(215)) DIS17860
  M(216) = ((ALFA(8)**2 / KT1(191)) / GAMMA(216)) * ALFA(8)**2 DIS17870
  M(217) = ALFA(3) * ALFA(8) / (KT1(192) * GAMMA(217)) DIS17880
  M(218) = ALFA(30) / (KT1(193) * GAMMA(218)) DIS17890
  M(219) = ALFA(30)**2 / (KT1(194) * GAMMA(218)) DIS17900
DIS17910
C ----- DIS17920
C If vo+2 is to be calculated from eh then flags(6) = 1, if DIS17930
C from vo4 -3 + 6h+ + fe+2 = vo+2 + 3h2o + fe+3 then flags(6) = 0. DIS17940
C ----- DIS17950
DIS17960
IF (EHM .LT. 9.0 .AND. FLAGS(6) .EQ. 1) THEN DIS17970
  C1 = 10.0**((EHM * F - LOGKT1(145) + DLOG10(ALFA(10)**3) - DIS17980
    6.0 * DLOG10(ALFA(8)))) / (2.303 * R * T)) DIS17990
  M(211) = C1 / GAMMA(210) DIS18000
ELSE IF (EXELT(25) .LT. CPUMIN .OR. EXELT(13) .LT. CPUMIN) THEN DIS18010
  M(211) = 0.0D0 DIS18020
ELSE IF (FLAGS(6) .EQ. 0 .AND. ALFA(18) .GT. CPUMIN) THEN DIS18030
  M(211) = 10.0**((DLOG10(ALFA(8)) * 6.0 + DLOG10(ALFA(18) / DIS18040
    ALFA(19)))) / (KT1(208) * GAMMA(167) * ALFA(10)**3)) DIS18050
ELSE DIS18060
  M(211) = 0.0 DIS18070
END IF DIS18080
DIS18090
M(223) = ALFA(9) / (KT1(198) * GAMMA(223)) DIS18100
M(224) = ALFA(6) / (KT1(199) * GAMMA(224)) DIS18110
M(225) = ALFA(5) / (KT1(200) * GAMMA(225)) DIS18120
M(226) = ALFA(30) / (KT1(201) * GAMMA(226)) DIS18130
M(227) = ALFA(30)**2 / (KT1(202) * GAMMA(227)) DIS18140
DIS18150

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DO 450 I = 223, 227	DIS18160
M(I) = M(I) * GAMMA(211) * M(211)	DIS18170
450 CONTINUE	DIS18180
	DIS18190
C -----	DIS18200
C If v+3 is to be calculated from eh then flag(6) = 1, if from	DIS18210
C vo+2 + 2h+ + fe+2 = v+3 + h2o + fe+3 then flag(6) = 0.	DIS18220
C -----	DIS18230
IF (EHM .LT. 9.0 .AND. FLAGS(6) .EQ. 1) THEN	DIS18240
C1 = 10.0**((EHM * F * LOGKT1(144) + DLOG10(ALFA(10)) -	DIS18250
2.0 * DLOG10(ALFA(8))) / (2.303 * R * T))	DIS18260
M(212) = C1 / GAMMA(211)	DIS18270
ELSE IF (EXELT(25) .LT. CPUMIN) THEN	DIS18280
M(211) = 0.0	DIS18290
ELSE IF (EXELT(13) .LT. CPUMIN) THEN	DIS18300
M(220) = 0.0	DIS18310
ELSE IF (FLAGS(6) .EQ. 0) THEN	DIS18320
M(212) = ALFA(18) * ALFA(8)**2 / (KT1(207) * ALFA(19) *	DIS18330
GAMMA(167) * ALFA(10))	DIS18340
END IF	DIS18350
	DIS18360
M(220) = ALFA(9) / (KT1(195) * GAMMA(220))	DIS18370
M(221) = ALFA(9)**2 / (KT1(196) * GAMMA(221))	DIS18380
M(222) = ALFA(9)**2 / (KT1(197) * GAMMA(222))	DIS18390
	DIS18400
	DIS18410
DO 460 I = 220, 222	DIS18420
M(I) = M(I) * M(212) * GAMMA(212)	DIS18430
460 CONTINUE	DIS18440
	DIS18450
C1 = 0.0D0	DIS18460
	DIS18470
DO 470 I = 211, 227	DIS18480
C1 = C1 + M(I)	DIS18490
470 CONTINUE	DIS18500
	DIS18510
M(210) = EXELT(28) / (1.0 + GAMMA(210) * C1)	DIS18520
ALFA(210) = M(210) * GAMMA(210)	DIS18530
	DIS18540
DO 480 I = 211, 227	DIS18550
M(I) = M(I) * ALFA(210)	DIS18560
ALFA(I) = M(I) * GAMMA(I)	DIS18570
480 CONTINUE	DIS18580
END IF	DIS18590
	DIS18600
C -----	DIS18610
C Summation of anion species	DIS18620
C -----	DIS18630
S(1) = M(7) + 2.0*M(98) + 2.0*M(51) + M(52) +	DIS18640
2.0*M(55) + M(56) + 2.0*M(114) + 2.0*M(120) +	DIS18650
M(121) + M(132) + 2.0*M(138) + M(139) +	DIS18660
2.0*M(140) + 2.0*M(155) + M(156) + 2.0*M(207) +	DIS18670
4.0*M(208) + 6.0*M(209) + 2.0*M(288) + M(292) +	DIS18680
M(MXSP+34) + 2.0*M(MXSP+39)	DIS18690
	DIS18700
S(2) = M(6) + M(41) + 2.0*M(42) + M(47) +	DIS18710
M(54) + M(61) + M(70) + M(78) +	DIS18720
	DIS18730

.	M(83) + 2.0*M(84) +	M(103) +	M(109) +	DIS18740
.	M(115) + M(116) +	M(119) +	M(124) +	DIS18750
.	M(133) + M(141) +	M(142) +	M(152) +	DIS18760
.	M(157) + M(162) +	M(186) + 2.0*M(187) +		DIS18770
.	M(194) + 2.0*M(195) +	M(224) +	M(MXSP+33)	DIS18780
				DIS18790
S(3) =	M(30) + M(34) + 2.0*M(35) + 3.0*M(36) +			DIS18800
.	4.0*M(37) + M(96) +	M(122) +	M(144) +	DIS18810
.	5.0*M(163) + 6.0*M(164) +	M(175) + 2.0*M(176) +		DIS18820
.	3.0*M(177) + 4.0*M(178) + 5.0*M(179) + 6.0*M(180) +			DIS18830
.	M(196) + 2.0*M(197) + 3.0*M(198) + 4.0*M(199) +			DIS18840
.	M(218) + 2.0*M(219) +	M(226) + 2.0*M(227) +		DIS18850
.	M(283) + 6.0*M(284) +	M(MXSP+37)		DIS18860
				DIS18870
S(4) =	M(29) + M(58) +	M(59) +	M(60) +	DIS18880
.	M(73) + M(74) +	M(99) +	M(100) +	DIS18890
.	M(117) + M(125) +	M(126) +	M(127) +	DIS18900
.	M(134) + M(143) +	M(182) + 2.0*M(183) +		DIS18910
.	3.0*M(184) + 4.0*M(185) +	M(202) + 2.0*M(203) +		DIS18920
.	M(204) + 2.0*M(205) + 3.0*M(206) +	M(MXSP+36)		DIS18930
				DIS18940
S(5) =	M(5) + M(43) + 2.0*M(44) + 3.0*M(45) +			DIS18950
.	4.0*M(46) + M(62) + 2.0*M(63) + 3.0*M(64) +			DIS18960
.	M(65) + 2.0*M(66) + 3.0*M(67) + 4.0*M(68) +			DIS18970
.	M(71) + 2.0*M(72) +	M(79) + 2.0*M(80) +		DIS18980
.	3.0*M(81) + 4.0*M(82) +	M(105) + 2.0*M(106) +		DIS18990
.	3.0*M(107) + 4.0*M(108) +	M(113) +	M(128)	DIS19000
S(5) = S(5)	+			DIS19010
.	2.0*M(129) + 3.0*M(130) + 4.0*M(131) +	M(137) +		DIS19020
.	M(148) + 2.0*M(149) + 3.0*M(150) + 4.0*M(151) +			DIS19030
.	M(153) + M(158) + 2.0*M(159) + 3.0*M(160) +			DIS19040
.	4.0*M(161) + M(181) +	M(200) +	M(225) +	DIS19050
.	M(281) + 2.0*M(282) +	M(MXSP+32)		DIS19060
				DIS19070
S(6) =	M(48) + M(228) +	M(229) +	M(230) +	DIS19080
.	M(231) + M(232) +	M(233) + 2.0*M(234) +		DIS19090
.	M(235) + M(236) +	M(237) +	M(238) +	DIS19100
.	2.0*M(239) + 3.0*M(240) +	M(241) +	M(242) +	DIS19110
.	2.0*M(243) +	M(244) + 2.0*M(245) +	M(MXSP+38)	DIS19120
				DIS19130
S(7) =	M(33) + M(101) +	M(102) + 4.0*M(110) +		DIS19140
.	3.0*M(111) + M(145) + 2.0*M(286) + 3.0*M(287) +			DIS19150
.	2.0*M(290) + 3.0*M(291) +	M(295)		DIS19160
				DIS19170
S(8) =	M(246) + M(247) +	M(248) +	M(249) +	DIS19180
.	2.0*M(250) + M(251) +	M(252) +	M(253) +	DIS19190
.	M(254) + M(255) +	M(256) +	M(257) +	DIS19200
.	2.0*M(258) + 3.0*M(259) +	M(260) +	M(261) +	DIS19210
.	M(262) + M(263) +	M(264) +	M(MXSP+41)	DIS19220
				DIS19230
S(9) =	M(265) + M(266) +	M(267) +	M(268) +	DIS19240
.	2.0*M(269) + M(270) +	M(271) +	M(272) +	DIS19250
.	M(273) + M(274) +	M(275) +	M(276) +	DIS19260
.	M(277) + M(278) +	M(279) +	M(280) +	DIS19270
.	M(MXSP+42)			DIS19280
				DIS19290
S(10) =	M(MXSP+ 1) + M(MXSP+ 2) + M(MXSP+ 3) + M(MXSP+ 4) +			DIS19300
.	M(MXSP+ 5) + M(MXSP+ 6) + M(MXSP+ 7) + M(MXSP+ 8) +			DIS19310


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      M(MXSP+ 9) + M(MXSP+10) + M(MXSP+11) + M(MXSP+12) +      DIS19320
      M(MXSP+13) + M(MXSP+14) + M(MXSP+15) + M(MXSP+43)      DIS19330
                                                                DIS19340
      S(11) = M(MXSP+16) + M(MXSP+17) + M(MXSP+18) + M(MXSP+19) +      DIS19350
      M(MXSP+20) + M(MXSP+21) + M(MXSP+22) + M(MXSP+23) +      DIS19360
      M(MXSP+24) + M(MXSP+25) + M(MXSP+26) + M(MXSP+27) +      DIS19370
      M(MXSP+28) + M(MXSP+29) + M(MXSP+30) + M(MXSP+44)      DIS19380
                                                                DIS19390
      SCO2 =      M(7)  +      M(51) +      M(52) +      M(55) +      DIS19400
      M(56) +      M(97) +      M(98) +      M(114) +      DIS19410
      M(120) +      M(121) +      M(132) +      M(138) +      DIS19420
      M(139) +      M(140) +      M(155) +      M(156) +      DIS19430
      M(207) + 2.0*M(208) + 3.0*M(209) +      M(288) +      DIS19440
      M(292) +      M(MXSP+34) +      M(MXSP+39)      DIS19450
                                                                DIS19460
      IF (ALK .EQ. 1) THEN      DIS19470
      ANALCO = EXELT(29)      DIS19480
      ELSE IF (ALK .EQ. 0) THEN      DIS19490
      ANALCO = EXELT(29) -      M(9) -      M(28) - 3.0*M(29) -      DIS19500
      M(38) - 2.0*M(39) - 4.0*M(40) -      M(48) -      DIS19510
      3.0*M(50) -      M(53) -      M(57) -      M(69) -      DIS19520
      M(75) - 2.0*M(76) -      M(77) -      M(85) -      DIS19530
      2.0*M(86) - 3.0*M(87) - 4.0*M(88) -      M(89) -      DIS19540
      2.0*M(90) -      M(91) - 2.0*M(92) - 2.0*M(93) -      DIS19550
      M(94) - 2.0*M(99) -      M(100) -      M(101)      DIS19560
      ANALCO = ANALCO -      DIS19570
      2.0*M(102) -      M(103) -      M(118) -      M(123) -      DIS19580
      M(135) -      M(147) -      M(154) -      M(165) -      DIS19590
      2.0*M(166) -      M(170) - 2.0*M(171) - 3.0*M(172) -      DIS19600
      4.0*M(173) - 5.0*M(174) - 2.0*M(182) - 4.0*M(183) -      DIS19610
      6.0*M(184) - 8.0*M(185) -15.0*M(188) -      M(189) -      DIS19620
      2.0*M(190) - 2.0*M(191) - 5.0*M(192) - 7.0*M(193)      DIS19630
      ANALCO = ANALCO -      DIS19640
      M(201) - 2.0*M(202) - 4.0*M(203) -      M(204) -      DIS19650
      2.0*M(205) - 3.0*M(206) - 4.0*M(212) - 3.0*M(213) -      DIS19660
      2.0*M(214) -      M(215) - 3.0*M(217) -      M(220) -      DIS19670
      2.0*M(221) - 3.0*M(222) -      M(223) -      M(234) -      DIS19680
      M(239) - 2.0*M(240) -      M(243) -      M(245) -      DIS19690
      M(246) -      M(250) -      M(258) - 2.0*M(259)      DIS19700
      ANALCO = ANALCO -      DIS19710
      2.0*M(265) -      M(266) -      M(269) -      M(289) -      DIS19720
      M(293) - 2.0*M(294) -      M(295)      DIS19730
      ANALCO = ANALCO -      M(MXSP+34) -      M(MXSP+35) -      DIS19740
      3.0*M(MXSP+36) - M(MXSP+38) - 2.0*M(MXSP+39) -      DIS19750
      2.0*M(MXSP+41) - M(MXSP+40) - 2.0*M(MXSP+42)      DIS19760
      DO 490 I = 229, 245      DIS19770
      ANALCO = ANALCO - M(I)      DIS19780
490    CONTINUE      DIS19790
                                                                DIS19800
      DO 500 I = 249, 264      DIS19810
      ANALCO = ANALCO - M(I)      DIS19820
500    CONTINUE      DIS19830
                                                                DIS19840
      DO 510 I = 268, 280      DIS19850
      ANALCO = ANALCO - M(I)      DIS19860
510    CONTINUE      DIS19870
      ELSE      DIS19880
      S(1) = SCO2      DIS19890

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IF (ANMTIC .GT. 0.0D0) THEN	DIS19900
ANALCO = ANMTIC	DIS19910
ELSE	DIS19920
ANALCO = ANALM(7) + ANALM(98)	DIS19930
END IF	DIS19940
END IF	DIS19950
IF ((DABS(HITEMP-TEMP)) .GT. 1.0D-10) CO2F = SCO2	DIS19960
	DIS19970
IF (ITIC .EQ. 2) THEN	DIS19980
S(1) = SCO2	DIS19990
ANALCO = CO2F + DCO2	DIS20000
END IF	DIS20010
	DIS20020
	DIS20030
C -----	DIS20040
C Iteration test	DIS20050
C -----	DIS20060
DONE = .TRUE.	DIS20070
	DIS20080
	DIS20090
IF (ANALCO .GT. CPUMIN) THEN	DIS20100
X = (S(1) - ANALCO) / ANALCO	DIS20110
CROSS = .FALSE.	DIS20120
IF ((X * DIFF(1)) .LT. 0.0) CROSS = .TRUE.	DIS20130
DIFF(1) = X	DIS20140
IF (DABS(DIFF(1)) .GE. CONV1) DONE = .FALSE.	DIS20150
	DIS20160
IF (DONE) THEN	DIS20170
FACTOR(1) = 1.0	DIS20180
ELSE IF (ITER .GT. 7) THEN	DIS20190
X = ANALCO / S(1)	DIS20200
CALL AITLIM (FACTOR(1), X, CROSS)	DIS20210
END IF	DIS20220
X = FACTOR(1)	DIS20230
	DIS20240
IF (S(1) .GT. CPUMIN) THEN	DIS20250
TITR(1) = TITR(1) - (X * (1.0 - (ANALCO / S(1)))) * TITR(1)	DIS20260
ELSE	DIS20270
TITR(1) = ANALCO	DIS20280
END IF	DIS20290
END IF	DIS20300
	DIS20310
IF (EXELT(6) .GE. CPUMIN) THEN	DIS20320
X = (S(2) - EXELT(6)) / EXELT(6)	DIS20330
CROSS = .FALSE.	DIS20340
IF ((X * DIFF(2)) .LT. 0.0) CROSS = .TRUE.	DIS20350
DIFF(2) = X	DIS20360
IF (DABS(DIFF(2)) .GE. CONV1) DONE = .FALSE.	DIS20370
	DIS20380
IF (DONE) THEN	DIS20390
FACTOR(2) = 1.0	DIS20400
ELSE IF (ITER .GT. 7) THEN	DIS20410
X = EXELT(6) / S(2)	DIS20420
CALL AITLIM (FACTOR(2), X, CROSS)	DIS20430
END IF	DIS20440
X = FACTOR(2)	DIS20450
IF (S(2) .GT. CPUMIN) THEN	DIS20460
TITR(2) = TITR(2) - (X * (1.0 - (EXELT(6) / S(2)))) * TITR(2)	DIS20470

ELSE	DIS20480
TITR(2) = EXELT(6)	DIS20490
END IF	DIS20500
END IF	DIS20510
	DIS20520
IF (EXELT(22) .GE. CPUMIN) THEN	DIS20530
X = (S(3) - EXELT(22)) / EXELT(22)	DIS20540
CROSS = .FALSE.	DIS20550
IF ((X * DIFF(3)) .LT. 0.0) CROSS = .TRUE.	DIS20560
DIFF(3) = X	DIS20570
IF (DABS(DIFF(3)) .GE. CONV1) DONE = .FALSE.	DIS20580
IF (DONE) THEN	DIS20590
FACTOR(3) = 1.0	DIS20600
ELSE IF (ITER .GT. 7) THEN	DIS20610
X = EXELT(22) / S(3)	DIS20620
CALL AITLIM (FACTOR(3), X, CROSS)	DIS20630
END IF	DIS20640
X = FACTOR(3)	DIS20650
IF (S(3) .GT. CPUMIN) THEN	DIS20660
TITR(3) = TITR(3) - (X * (1.0 - (EXELT(22) / S(3)))) * TITR(3)	DIS20670
ELSE	DIS20680
TITR(3) = EXELT(22)	DIS20690
END IF	DIS20700
END IF	DIS20710
	DIS20720
IF (EXELT(21) .GE. CPUMIN) THEN	DIS20730
X = (S(4) - EXELT(21)) / EXELT(21)	DIS20740
CROSS = .FALSE.	DIS20750
IF ((X * DIFF(4)) .LT. 0.0) CROSS = .TRUE.	DIS20760
DIFF(4) = X	DIS20770
IF (DABS(DIFF(4)) .GE. CONV1) DONE = .FALSE.	DIS20780
IF (DONE) THEN	DIS20790
FACTOR(4) = 1.0	DIS20800
ELSE IF (ITER .GT. 7) THEN	DIS20810
X = EXELT(21) / S(4)	DIS20820
CALL AITLIM (FACTOR(4), X, CROSS)	DIS20830
END IF	DIS20840
X = FACTOR(4)	DIS20850
IF (S(4) .GT. CPUMIN) THEN	DIS20860
TITR(4) = TITR(4) - (X * (1.0 - (EXELT(21) / S(4)))) * TITR(4)	DIS20870
ELSE	DIS20880
TITR(4) = EXELT(21)	DIS20890
END IF	DIS20900
END IF	DIS20910
	DIS20920
IF (EXELT(5) .GE. CPUMIN) THEN	DIS20930
X = (S(5) - EXELT(5)) / EXELT(5)	DIS20940
CROSS = .FALSE.	DIS20950
IF ((X * DIFF(5)) .LT. 0.0) CROSS = .TRUE.	DIS20960
DIFF(5) = X	DIS20970
IF (DABS(DIFF(5)) .GE. CONV1) DONE = .FALSE.	DIS20980
IF (DONE) THEN	DIS20990
FACTOR(5) = 1.0	DIS21000
ELSE IF (ITER .GT. 7) THEN	DIS21010
X = EXELT(5) / S(5)	DIS21020
CALL AITLIM (FACTOR(5), X, CROSS)	DIS21030
END IF	DIS21040
X = FACTOR(5)	DIS21050

```

IF (S(5) .GT. CPUMIN) THEN
    TITR(5) = TITR(5) - (X * (1.0 - (EXELT(5) / S(5))) * TITR(5))
ELSE
    TITR(5) = EXELT(5)
END IF
END IF

IF (EXELT(26) .GE. CPUMIN) THEN
    X = (S(6) - EXELT(26)) / EXELT(26)
    CROSS = .FALSE.
    IF ((X * DIFF(6)) .LT. 0.0) CROSS = .TRUE.
    DIFF(6) = X
    IF (DABS(DIFF(6)) .GE. CONV1) DONE = .FALSE.
    IF (DONE) THEN
        FACTOR(6) = 1.0
    ELSE IF (ITER .GT. 7) THEN
        X = EXELT(26) / S(6)
        CALL AITLIM (FACTOR(6), X, CROSS)
    END IF
    X = FACTOR(6)
    IF (S(6) .GT. CPUMIN) THEN
        TITR(6) = TITR(6) - (X * (1.0 - (EXELT(26) / S(6))) * TITR(6))
    ELSE
        TITR(6) = EXELT(26)
    END IF
END IF

IF (EXELT(25) .GT. CPUMIN) THEN
    X = (S(7) - EXELT(25)) / EXELT(25)
    CROSS = .FALSE.
    IF ((X * DIFF(7)) .LT. 0.0) CROSS = .TRUE.
    DIFF(7) = X
    IF (DABS(DIFF(7)) .GE. CONV1) DONE = .FALSE.
    IF (DONE) THEN
        FACTOR(7) = 1.0
    ELSE IF (ITER .GT. 7) THEN
        X = EXELT(25) / S(7)
        CALL AITLIM (FACTOR(7), X, CROSS)
    END IF
    X = FACTOR(7)
    IF (S(7) .GT. CPUMIN) THEN
        TITR(7) = TITR(7) - (X * (1.0 - (EXELT(25) / S(7))) * TITR(7))
    ELSE
        TITR(7) = EXELT(25)
    END IF
END IF

IF (EXELT(30) .GT. CPUMIN) THEN
    X = (S(8) - EXELT(30)) / EXELT(30)
    CROSS = .FALSE.
    IF ((X * DIFF(8)) .LT. 0.0) CROSS = .TRUE.
    DIFF(8) = X
    IF (DABS(DIFF(8)) .GE. CONV1) DONE = .FALSE.
    IF (DONE) THEN
        FACTOR(8) = 1.0
    ELSE IF (ITER .GT. 7) THEN
        X = EXELT(30) / S(8)
        CALL AITLIM (FACTOR(8), X, CROSS)

```

END IF	DIS21640
X = FACTOR(8)	DIS21650
IF (S(8) .GT. CPUMIN) THEN	DIS21660
TITR(8) = TITR(8) - (X * (1.0 - (EXELT(30) / S(8))) * TITR(8))	DIS21670
ELSE	DIS21680
TITR(8) = EXELT(30)	DIS21690
END IF	DIS21700
END IF	DIS21710
	DIS21720
IF (EXELT(31) .GT. CPUMIN) THEN	DIS21730
DIFF(9) = (S(9) - EXELT(31)) / EXELT(31)	DIS21740
X = (S(9) - EXELT(31)) / EXELT(31)	DIS21750
CROSS = .FALSE.	DIS21760
IF ((X * DIFF(9)) .LT. 0.0) CROSS = .TRUE.	DIS21770
DIFF(9) = X	DIS21780
IF (DABS(DIFF(9)) .GE. CONV1) DONE = .FALSE.	DIS21790
IF (DONE) THEN	DIS21800
FACTOR(9) = 1.0	DIS21810
ELSE IF (ITER .GT. 7) THEN	DIS21820
X = EXELT(31) / S(9)	DIS21830
CALL AITLIM (FACTOR(9), X, CROSS)	DIS21840
END IF	DIS21850
X = FACTOR(9)	DIS21860
IF (S(9) .GT. CPUMIN) THEN	DIS21870
TITR(9) = TITR(9) - (X * (1.0 - (EXELT(31) / S(9))) * TITR(9))	DIS21880
ELSE	DIS21890
TITR(9) = EXELT(31)	DIS21900
END IF	DIS21910
END IF	DIS21920
	DIS21930
IF (EXELT(33) .GT. CPUMIN) THEN	DIS21940
X = (S(10) - EXELT(33)) / EXELT(33)	DIS21950
CROSS = .FALSE.	DIS21960
IF ((X * DIFF(10)) .LT. 0.0) CROSS = .TRUE.	DIS21970
DIFF(10) = X	DIS21980
IF (DABS(DIFF(10)) .GE. CONV1) DONE = .FALSE.	DIS21990
IF (DONE) THEN	DIS22000
FACTOR(10) = 1.0	DIS22010
ELSE IF (ITER .GT. 7) THEN	DIS22020
X = EXELT(33) / S(10)	DIS22030
CALL AITLIM (FACTOR(10), X, CROSS)	DIS22040
END IF	DIS22050
X = FACTOR(10)	DIS22060
IF (S(10) .GT. CPUMIN) THEN	DIS22070
TITR(10) = TITR(10) - (X * (1.0 - (EXELT(33) / S(10))) * TITR(10))	DIS22080
ELSE	DIS22090
TITR(10) = EXELT(33)	DIS22100
END IF	DIS22110
END IF	DIS22120
	DIS22130
	DIS22140
IF (EXELT(34) .GT. CPUMIN) THEN	DIS22150
X = (S(11) - EXELT(34)) / EXELT(34)	DIS22160
CROSS = .FALSE.	DIS22170
IF ((X * DIFF(11)) .LT. 0.0) CROSS = .TRUE.	DIS22180
DIFF(11) = X	DIS22190
IF (DABS(DIFF(11)) .GE. CONV1) DONE = .FALSE.	DIS22200
IF (DONE) THEN	DIS22210

FACTOR(11) = 1.0	DIS22220
ELSE IF (ITER .GT. 7) THEN	DIS22230
X = EXELT(34) / S(11)	DIS22240
CALL AITLIM (FACTOR(11), X, CROSS)	DIS22250
END IF	DIS22260
X = FACTOR(11)	DIS22270
IF (S(11) .GT. CPUMIN) THEN	DIS22280
TITR(11) = TITR(11) - (X * (1.0 - (EXELT(34) / S(11)))) * TITR(11))	DIS22290
ELSE	DIS22300
TITR(11) = EXELT(34)	DIS22310
END IF	DIS22320
END IF	DIS22330
	DIS22340
	DIS22350
IF (ITER .GE. 100) DONE = .TRUE.	DIS22360
	DIS22370
IF (IPRIN1 .NE. 0) THEN	DIS22380
IF (ITER .EQ. 1 .OR. DONE .OR. MOD(ITER,10) .EQ. 0) THEN	DIS22390
IF (IPGLN .GT. 57) THEN	DIS22400
CALL PAGE	DIS22410
WRITE (UNO, 1001) TITLE, TITMIX	DIS22420
WRITE (UNO, 1002) TEMP	DIS22430
WRITE (UNO, 1003)	DIS22440
WRITE (UNO, 1004) CR	DIS22450
IPGLN = IPGLN + 9	DIS22460
END IF	DIS22470
WRITE (UNO,1005) ITER, (DIFF(I),I=1,11)	DIS22480
IPGLN = IPGLN + 1	DIS22490
END IF	DIS22500
END IF	DIS22510
	DIS22520
C -----	DIS22530
C GO BACK OR QUIT	DIS22540
C -----	DIS22550
	DIS22560
IF (.NOT. DONE) GO TO 30	DIS22570
	DIS22580
IF (ITER .GE. 100) THEN	DIS22590
IF (IPGLN .GT. 59) THEN	DIS22600
CALL PAGE	DIS22610
WRITE (UNO, 1001) TITLE, TITMIX	DIS22620
WRITE (UNO, 1002) TEMP	DIS22630
IPGLN = IPGLN + 5	DIS22640
END IF	DIS22650
WRITE (UNO,1006)	DIS22660
IPGLN = IPGLN + 2	DIS22670
END IF	DIS22680
	DIS22690
IF (IPRIN1 .NE. 0) THEN	DIS22700
IF (IPGLN .GT. 57) THEN	DIS22710
CALL PAGE	DIS22720
WRITE (UNO, 1001) TITLE, TITMIX	DIS22730
WRITE (UNO, 1002) TEMP	DIS22740
IPGLN = IPGLN + 5	DIS22750
END IF	DIS22760
WRITE (UNO,1007) ITER, PH	DIS22770
IPGLN = IPGLN + 2	DIS22780
END IF	DIS22790

HTOT = M(7) + M(8) + 4.0*M(11) + 2.0*M(28) +	DIS22800
. 2.0*M(33) + 3.0*M(49) + M(52) + M(56) +	DIS22810
. M(59) + 2.0*M(60) + M(73) + 3.0*M(74) +	DIS22820
. 2.0*M(90) + 3.0*M(91) + M(92) + M(93) +	DIS22830
. 2.0*M(94) + 3.0*M(95) + M(96) + 2.0*M(97) +	DIS22840
. M(99) + 2.0*M(100) + M(101) + M(103) +	DIS22850
. M(104) + 4.0*M(110) + 3.0*M(111) + M(115) +	DIS22860
. M(117) + M(121) + M(126) + 2.0*M(127) +	DIS22870
. M(132) + M(134) + M(139) + M(143)	DIS22880
HTOT = HTOT +	DIS22890
. M(145) + M(156) + M(182) +	DIS22900
. 2.0*M(183) + 3.0*M(184) + 4.0*M(185) + M(202) +	DIS22910
. 2.0*M(203) + 2.0*M(204) + 4.0*M(205) + 6.0*M(206) +	DIS22920
. M(213) + 2.0*M(214) + 3.0*M(215) + 4.0*M(216) +	DIS22930
. M(217) + M(228) + M(247) + 2.0*M(248) +	DIS22940
. M(266) + 2.0*M(267) + 2.0*M(286) + 3.0*M(287) +	DIS22950
. 2.0*M(290) + 3.0*M(291) + M(292) + M(295) +	DIS22960
. M(MXSP+34) + M(MXSP+40)	DIS22970
	DIS22980
OHTOT = M(9) + 3.0*M(31) + M(38) + 2.0*M(39) +	DIS22990
. 4.0*M(40) + M(53) + M(57) + M(69) +	DIS23000
. M(75) + 2.0*M(76) + M(77) + M(85) +	DIS23010
. 2.0*M(86) + 3.0*M(87) + 4.0*M(88) + 4.0*M(89) +	DIS23020
. M(118) + M(123) + M(135) + M(147) +	DIS23030
. M(154) + M(165) + 2.0*M(166) + M(170)	DIS23040
OHTOT = OHTOT +	DIS23050
. 2.0*M(171) + 3.0*M(172) + 4.0*M(173) + 5.0*M(174) +	DIS23060
. 15.0*M(188) + M(189) + 2.0*M(190) + 2.0*M(191) +	DIS23070
. 5.0*M(192) + 7.0*M(193) + M(220) + 2.0*M(221) +	DIS23080
. 3.0*M(222) + M(223) + M(289) + M(293) +	DIS23090
. 2.0*M(294) + M(295) + M(MXSP+35)	DIS23100
	DIS23110
IF (PALFA(6) .GT. CPUMIN .AND. DABS(PALFA(6)-ALFA(6))	DIS23120
. .GT. 1.0D-2*PALFA(6) .AND. IPIT .EQ. 1) THEN	DIS23130
ALFA(6) = PALFA(6)	DIS23140
END IF	DIS23150
IF (PALFA(1) .GT. CPUMIN .AND. DABS(PALFA(1)-ALFA(1))	DIS23160
. .GT. 1.0D-2*PALFA(1) .AND. IPIT .EQ. 1) THEN	DIS23170
ALFA(1) = PALFA(1)	DIS23180
END IF	DIS23190
	DIS23200
RETURN	DIS23210
	DIS23220
1000 FORMAT (/ , 2X, 'SOLMINEQ.87 (VERSION: ', A14,	DIS23230
. ') - SOLUTION-MINERAL-EQUILIBRIUM COMPUTATIONS',	DIS23240
. / , A1, 2X, 77(' '), ///)	DIS23250
1001 FORMAT (' SAMPLE IDENT:- ', A80, / , 20X, A40)	DIS23260
1002 FORMAT (///, 6X, 'ITERATIVE CONVERGENCE TEST AT TEMPERATURE =', F8.2)	DIS23270
1003 FORMAT (///, 1X, 'ITER', 1X, 'CARBONATE', 3X, 'SULFATE', 4X,	DIS23280
. 'FLUORIDE', 2X, 'PHOSPHATE', 3X, 'CHLORIDE', 3X,	DIS23290
. 'ACETATE', 4X, 'SULFIDE', 4X, 'OXYLATE', 3X,	DIS23300
. 'SUCCINATE', 2X, 'USR-DEF #1', 1X, 'USR-DEF #2')	DIS23310
1004 FORMAT (A1, ' ', 1X, 11(' '), 1X))	DIS23320
1005 FORMAT (1X, I3, 2X, 1P, 11(E10.3, 1X))	DIS23330
1006 FORMAT (' *** NO CONVERGENCE IN 100 ITERATIONS DURING SPECIES',	DIS23340
. ' DISTRIBUTION ***', / , 13X, 'RESULTS MAY BE IN ERROR')	DIS23350
1007 FORMAT (/ , 6X, 'Total number of iterations = ', I3,	DIS23360
	DIS23370

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      ' at pH = ',F5.2)
1008 FORMAT (/ ,6X, ' *** ACT. OF SO4 FROM PITZER ***',E12.5)
1009 FORMAT (/ ,6X, ' *** ACT. OF Ca FROM PITZER ***',E12.5)

```

END

DIS23380
DIS23390
DIS23400
DIS23410
DIS23420

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      SUBROUTINE DPVT (TC, TISA, PBAR, VDEN)
C -----
C Routine dpvt calculates the vapor pressure and vapor density
C given tc and the ionic strength of the solution.
C -----
C ALPHA      DBL      Coefficient of thermal expansion
C AW          DBL      Activity of water
C BETAG       DBL      Coefficient of compressibility
C GG          DBL      Intermediate storage variable
C GLO         DBL      Initial gibbs free energy per mole
C GX          DBL      Gibbs free energy per mole
C I           INT      Loop variable
C PO          DBL      Saturation pressure
C PBAR        DBL      Pressure in bars
C PHI         DBL      Osmotic coefficient
C R           DBL      Gas constant
C RQ          DBL      Gas constant in cubic centimeters
C T           DBL      Temperature in kelvin
C TC          DBL      Temperature in celcius
C TISA        DBL      Sum of Molality * charge / 2
C VDEN        DBL      Vapor density
C XG          DBL      Density
C XS          DBL      Intermediate storage variable
C YP          DBL      Low temperature fit constants
C ZP          DBL      High temperature fit constants
C -----
      INTEGER I
      DOUBLE PRECISION ALPHA, AW, BETAG, GG, GLO, GX
      DOUBLE PRECISION PO, PBAR, PHI, R, RQ
      DOUBLE PRECISION T, TC, TISA, VDEN
      DOUBLE PRECISION XG, XS, YP(57), ZP(57)
      EXTERNAL NACALC, PSAT, WAPVT
      INTRINSIC DABS, DEXP, DLOG
      DATA YP /-71659.702,      2.3483335,      -8.3668484D-5,
      .      2.4018168D-9,      624.88205,      -5.3697119D-4,
      .      3.5126966D-7,      0.,      -110.74702,
      .      0.038900801,      2.6973456D-6,      -6.2746876D-10,
      .      -1.5267612D-5,      0.,      516.99706,
      .      -5.9960300D6,      -656.81518,      24.879183,
      .      -2.1552731D-5,      5.0166855D-8,      0.,
      .      -4.4640952,      0.011087099,      -6.4479761D-8,
      .      -2.3234032D-10,      0.,      -5.2194871D-6,
      .      2.4445210D-10,      2.8527066D-13,      -1.5696231,

```

DPV 0010
DPV 0020
DPV 0030
DPV 0040
DPV 0050
DPV 0060
DPV 0070
DPV 0080
DPV 0090
DPV 0100
DPV 0110
DPV 0120
DPV 0130
DPV 0140
DPV 0150
DPV 0160
DPV 0170
DPV 0180
DPV 0190
DPV 0200
DPV 0210
DPV 0220
DPV 0230
DPV 0240
DPV 0250
DPV 0260
DPV 0270
DPV 0280
DPV 0290
DPV 0300
DPV 0310
DPV 0320
DPV 0330
DPV 0340
DPV 0350
DPV 0360
DPV 0370
DPV 0380
DPV 0390
DPV 0400
DPV 0410
DPV 0420
DPV 0430
DPV 0440
DPV 0450
DPV 0460
DPV 0470
DPV 0480

.	2.2337864D-3,	-6.3933891D-7,	4.5270573D-11,	DPV 0490
.	5.4151933,	0.,	0.,	DPV 0500
.	0.,	119.31966,	-0.48309327,	DPV 0510
.	1.4068095D-3,	-4.2345814,	-6.1084589,	DPV 0520
.	0.40743803,	-6.8152430D-6,	-0.075354649,	DPV 0530
.	1.2609014D-4,	6.2480692D-8,	1.8994373D-8,	DPV 0540
.	-1.0731284D-10,	0.32136572,	-2.5382945D-4,	DPV 0550
.	0.,	0.,	1.,	DPV 0560
.	1.,	1.,	1./	DPV 0570
.	DATA ZP /-71637.375,	2.2209012,	-7.7991396D-5,	DPV 0580
.	-4.8099272D-9,	624.68121,	6.0159787D-4,	DPV 0590
.	3.4069074D-7,	2.1962044D-11,	-110.74702,	DPV 0600
.	0.039494473,	-6.5313475D-7,	-6.4781894D-10,	DPV 0610
.	-1.5842012D-5,	3.2452006D-9,	516.99706,	DPV 0620
.	-5.9960301D6,	-656.81518,	24.86913,	DPV 0630
.	5.3812753D-5,	-5.5887470D-8,	6.5893263D-12,	DPV 0640
.	-4.4640952,	0.011109914,	-2.6573399D-7,	DPV 0650
.	1.7460070D-10,	1.0462619D-14,	-5.3070129D-6,	DPV 0660
.	8.6340233D-10,	-4.1785962D-13,	-1.579366,	DPV 0670
.	2.2022821D-3,	-1.3105503D-7,	-6.3813683D-11,	DPV 0680
.	9.706578,	-2.6860396D-2,	1.5344744D-5,	DPV 0690
.	-3.2153983D-9,	119.31966,	-0.48309327,	DPV 0700
.	1.4068095D-3,	-4.2345814,	-6.1084589,	DPV 0710
.	0.40217793,	2.2902837D-5,	-0.075354649,	DPV 0720
.	1.5317673D-4,	-9.0550901D-8,	-1.5386008D-8,	DPV 0730
.	8.6926600D-11,	0.35310414,	-4.3314252D-4,	DPV 0740
.	-0.091871455,	5.1904777D-4,	1.,	DPV 0750
.	1.,	1.,	1./	DPV 0760
.				DPV 0770
C	=====			DPV 0780
C	-----			DPV 0790
C	-----			DPV 0800
C	Nacalc calculates the osmotic coefficients of the nacl solution			DPV 0810
C	and the free energy of pure water at the saturation pressure of			DPV 0820
C	pure water and temperature.			DPV 0830
C	-----			DPV 0840
				DPV 0850
	IF (TC .LT. 65.1) THEN			DPV 0860
	CALL NACALC (TC, TISA, PBAR, PHI, YP, GLO)			DPV 0870
	ELSE			DPV 0880
	CALL NACALC (TC, TISA, PBAR, PHI, ZP, GLO)			DPV 0890
	END IF			DPV 0900
				DPV 0910
C	-----			DPV 0920
C	Calculate water activity from phi.			DPV 0930
C	-----			DPV 0940
				DPV 0950
	AW = DEXP(-3.60304D-2 * PHI * TISA)			DPV 0960
				DPV 0970
	CALL PSAT (TC, P0)			DPV 0980
				DPV 0990
	R = 8.31424			DPV 1000
	RQ = 83.14699			DPV 1010
	T = TC + 273.15			DPV 1020
				DPV 1030
C	-----			DPV 1040
C	Calculate an initial guess for the density of the vapor from the			DPV 1050
C	ideal gas law.			DPV 1060

C	-----	DPV 1070
		DPV 1080
	XG = 18.0153 * P0 / (RQ * T)	DPV 1090
		DPV 1100
C	-----	DPV 1110
C	Calculate the free energy of the salt solution from the free	DPV 1120
C	energy of pure liquid water and the activity of water in	DPV 1130
C	solution.	DPV 1140
C	-----	DPV 1150
		DPV 1160
	GG = GLO + (R * T) * DLOG(AW)	DPV 1170
		DPV 1180
C	-----	DPV 1190
C	Use wapvt to calculate the vapor pressure and vapor density at	DPV 1200
C	tc. wapvt is used iteratively along with a free energy	DPV 1210
C	adjustment of the vapor density until the vapor density	DPV 1220
C	converges. this requires that the free energy of the liquid and	DPV 1230
C	vapor are the same and that the equilibrium vapor pressure and	DPV 1240
C	density have been determined.	DPV 1250
C	-----	DPV 1260
		DPV 1270
	DO 10 I = 1, 100	DPV 1280
	CALL WAPVT (TC, XG, PBAR, BETAG, GX, ALPHA)	DPV 1290
	XS = XG	DPV 1300
	XG = XG * DEXP((GG - GX) / (R * T))	DPV 1310
	IF (DABS((XG-XS)/XS) .LT. 1.0D-8) GO TO 20	DPV 1320
10	CONTINUE	DPV 1330
		DPV 1340
20	CONTINUE	DPV 1350
	VLEN = XG	DPV 1360
		DPV 1370
	RETURN	DPV 1380
	END	DPV 1390

	SUBROUTINE GASES (TC, PTOTAL, MNACLD, PH2O, FCCSAT, IGAS, IMAX,	GAS 0010
	IPRIN2)	GAS 0020
C	-----	GAS 0030
C	Partitions gases between the oil, water, and gas phases	GAS 0040
C	-----	GAS 0050
C	A DBL Temporary working variable	GAS 0060
C	ANALM DBL Analyzed molality of species i	GAS 0070
C	B DBL Temporary working variable	GAS 0080
C	C DBL Temporary working variable	GAS 0090
C	CH4DIF DBL Difference in total CH4 ... zero is root	GAS 0100
C	CH4TRY DBL Next value of CH4 to try	GAS 0110
C	CO2DIF DBL Difference in total CO2 ... zero is root	GAS 0120
C	CO2TRY DBL Next value of CO2 to try	GAS 0130
C	CPUMIN DBL Smallest positive real value program uses	GAS 0140
C	D DBL Temporary working variable	GAS 0150
C	DCH4 DBL Concentration of CH4 lost before pH measurement	GAS 0160
C	DCO2 DBL Concentration of CO2 lost before pH measurement	GAS 0170
C	DH2S DBL Concentration of H2S lost before pH measurement	GAS 0180
C	DONE LOG Done?	GAS 0190
C	E DBL Temporary working variable	GAS 0200

C	EXELT	DBL	Total amount of components	GAS 0210
C	FCCSAT	DBL	Zero Test value	GAS 0220
C	G	DBL	Temporary working variable	GAS 0230
C	H2SDIF	DBL	Difference in total H2S ... zero is root	GAS 0240
C	H2STRY	DBL	Next value of H2S to try	GAS 0250
C	HTOT	DBL	Current sum of all H+ in solution	GAS 0260
C	HTOTI	DBL	Target sum of all H+ in solution	GAS 0270
C	I	INT	Loop counter	GAS 0280
C	IGAS	INT	Loop variable for gas option	GAS 0290
C	IMAX	INT	Max number of iterations for various options	GAS 0300
C	IPAGE	INT	Current page number of output file	GAS 0310
C	IPGLN	INT	Current line number of the output file	GAS 0320
C	IPHASE	INT	Switch used for GAS options	GAS 0330
C	IPRIN2	INT	Print switch	GAS 0340
C	J	DBL	Temporary working variable	GAS 0350
C	JCO3	INT	Switch to control printing of some headings	GAS 0360
C	KCH4OL	DBL	Henry's law coefficient for CH4 in oil	GAS 0370
C	KCH4W	DBL	Henry's law coefficient for CH4 in water	GAS 0380
C	KCO2OL	DBL	Henry's law coefficient for CO2 in oil	GAS 0390
C	KCO2W	DBL	Henry's law coefficient for CO2 in water	GAS 0400
C	KH2SOL	DBL	Henry's law coefficient for H2S in oil	GAS 0410
C	KH2SW	DBL	Henry's law coefficient for H2S in water	GAS 0420
C	KHCH4	DBL	Function to Calculate the Henry's law K for CH4	GAS 0430
C	KHCO2	DBL	Function to Calculate the Henry's law K for CO2	GAS 0440
C	KHH2S	DBL	Function to Calculate the Henry's law K for H2S	GAS 0450
C	M	DBL	Calculated molality of aqueous species	GAS 0460
C	MNACLD	DBL	Sum of Molality * charge / 2	GAS 0470
C	NMAX	INT	General array dimension to allow easy expansion	GAS 0480
C	OHTOT	DBL	Total OH in system	GAS 0490
C	OHTOTI	DBL	initial total OH in system	GAS 0500
C	ORGCH4	DBL	Initial amount of CH4 in system	GAS 0510
C	ORGC02	DBL	Initial amount of CO2 in system	GAS 0520
C	ORGH2S	DBL	Initial amount of H2S in system	GAS 0530
C	ORGT1	DBL	Original TOTEL(1)	GAS 0540
C	PCH4W	DBL	Partial Pressure of Methane	GAS 0550
C	PCO2W	DBL	Partial Pressure of Carbon Dioxide	GAS 0560
C	PH2O	DBL	Partial Pressure of Water	GAS 0570
C	PH2SW	DBL	Partial Pressure of Hydrogen Sulphide	GAS 0580
C	PTOTAL	DBL	Total pressure on the system	GAS 0590
C	ROOT	DBL	Root of the equation	GAS 0600
C	SCO2	DBL	Sum of CO2 species	GAS 0610
C	STEP	DBL	Step adjustment for the moles of each gas	GAS 0620
C	TC	DBL	Temperature in deg C	GAS 0630
C	TCH4M	DBL	Moles CH4 distributed between oil, water, vapor	GAS 0640
C	TCH4O	DBL	Moles CH4 in oil	GAS 0650
C	TCH4V	DBL	Moles CH4 in vapor	GAS 0660
C	TCH4W	DBL	Moles CH4 in water	GAS 0670
C	TCO2M	DBL	Moles CO2 distributed between oil, water, vapor	GAS 0680
C	TCO2O	DBL	Moles CO2 in oil	GAS 0690
C	TCO2V	DBL	Moles CO2 in vapor	GAS 0700
C	TCO2W	DBL	Moles CO2 in water	GAS 0710
C	TEST	DBL	Insure sum of partitioned moles equal total moles	GAS 0720
C	TH2SM	DBL	Moles H2S distributed between oil, water, vapor	GAS 0730
C	TH2SO	DBL	Moles H2S in oil	GAS 0740
C	TH2SV	DBL	Moles H2S in vapor	GAS 0750
C	TH2SW	DBL	Moles H2S in water	GAS 0760
C	TITR	DBL	Iteration array in DISTRB, used for guesses	GAS 0770
C	TK	DBL	Temperature in deg K	GAS 0780

C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	GAS 0790
C	UNO	INT	File unit assigned for output file	GAS 0800
C	WROIL	DBL	Oil to water weight ratio	GAS 0810
C	-----			GAS 0820
	INTEGER NMAX, UNO			GAS 0830
	DOUBLE PRECISION CPUMIN			GAS 0840
	PARAMETER (NMAX = 340, UNO = 6, CPUMIN = 1.0D-35)			GAS 0850
				GAS 0860
	INTEGER I, IGAS, IMAX, IOPT, IPAGE, IPGLN, IPHASE, IPRIN2			GAS 0870
	INTEGER PHHIT, PPHHIT, JCO3			GAS 0880
				GAS 0890
	LOGICAL DONE			GAS 0900
				GAS 0910
				GAS 0920
	DOUBLE PRECISION A, ALFA(NMAX), ANALM(NMAX), B			GAS 0930
	DOUBLE PRECISION C, CH4DIF(3), CH4TRY(3), CO2F			GAS 0940
	DOUBLE PRECISION CO2DIF(3), CO2TRY(3), CUNITS(NMAX)			GAS 0950
	DOUBLE PRECISION D, DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3			GAS 0960
	DOUBLE PRECISION DCH4, DDCH4, E, EXELT(35), FCCSAT, FIXIT, G			GAS 0970
	DOUBLE PRECISION H2SDIF(3), H2STRY(3), HTOT, HTOTI, J			GAS 0980
	DOUBLE PRECISION KHCH4, KHC02, KHH2S, KCH4OL, KCO2OL, KH2SOL			GAS 0990
	DOUBLE PRECISION KCH4W, KCO2W, KH2SW			GAS 1000
	DOUBLE PRECISION M(NMAX), MNACLD, OHTOT, OHTOTI			GAS 1010
	DOUBLE PRECISION ORGCH4, ORGCO2, ORGH2S, ORGT1			GAS 1020
	DOUBLE PRECISION PCH4W, PCO2W, PH2SW, PH, PH2O, DSEP, PTOTAL			GAS 1030
	DOUBLE PRECISION ROOT, SCO2, STEP(4)			GAS 1040
	DOUBLE PRECISION TC, TCH4M, TCO2M, TH2SM			GAS 1050
	DOUBLE PRECISION TCO2O, TCO2V, TCO2W			GAS 1060
	DOUBLE PRECISION TCH4O, TCH4V, TCH4W			GAS 1070
	DOUBLE PRECISION TH2SO, TH2SV, TH2SW			GAS 1080
	DOUBLE PRECISION TEST, TITR(11), TK, TOTEL(5), WROIL			GAS 1090
				GAS 1100
	EXTERNAL KHCH4, KHC02, KHH2S, POLY, PAGE			GAS 1110
				GAS 1120
	INTRINSIC DABS, DLOG10, DSIGN			GAS 1130
				GAS 1140
	COMMON /DIST / TCO2M, TCH4M, TH2SM, WROIL, KCH4OL, KCO2OL,			GAS 1150
	KH2SOL, IPHASE, DSEP			GAS 1160
	COMMON /EXTOT / EXELT, TOTEL, TITR			GAS 1170
	COMMON /FORM / IPAGE, IPGLN			GAS 1180
	COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,			GAS 1190
	DCH4, DDCH4, IOPT, FIXIT			GAS 1200
	COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS			GAS 1210
	COMMON /TOTALS/ CO2F, HTOTI, OHTOTI			GAS 1220
	COMMON /ZPH / PHHIT, PPHHIT, JCO3, SCO2, HTOT, OHTOT			GAS 1230
				GAS 1240
	SAVE ORGT1, STEP, CO2DIF, CO2TRY, H2SDIF, H2STRY, CH4DIF, CH4TRY			GAS 1250
	SAVE TCO2O, TCO2V, TCO2W, ORGCO2, PCO2W, KCO2W			GAS 1260
	SAVE TCH4O, TCH4V, TCH4W, ORGCH4, PCH4W, KCH4W			GAS 1270
	SAVE TH2SO, TH2SV, TH2SW, ORGH2S, PH2SW, KH2SW			GAS 1280
				GAS 1290
C	=====			GAS 1300
	TK = TC + 273.15D00			GAS 1310
				GAS 1320
	KCO2W = KHC02 (TK, MNACLD)			GAS 1330
	KH2SW = KHH2S (TK, MNACLD)			GAS 1340
				GAS 1350
				GAS 1360

IF (IGAS .EQ. 1) THEN	GAS 1370
HTOTI = HTOT	GAS 1380
OHTOTI = OHTOT	GAS 1390
ORGH2S = ANALM(33)	GAS 1400
ORGCH4 = ANALM(285)	GAS 1410
ORGC02 = SC02	GAS 1420
ORGT1 = TOTEL(1)	GAS 1430
TCO2M = TCO2M + SC02	GAS 1440
TCH4M = TCH4M + ANALM(285)	GAS 1450
TH2SM = TH2SM + ANALM(33)	GAS 1460
TCO2W = ORGC02	GAS 1470
TCH4W = ORGCH4	GAS 1480
TH2SW = ORGH2S	GAS 1490
PCH4W = 1.0	GAS 1500
IF (TCH4M .GT. CPUMIN) THEN	GAS 1510
DO 10 I = 1, 5	GAS 1520
KCH4W = KHCH4 (TK, MNACLD, PCH4W)	GAS 1530
PCH4W = TCH4M / ((WROIL / KCH4OL) + (1.0 / KCH4W))	GAS 1540
IF (PCH4W .GT. PTOTAL) PCH4W = PTOTAL	GAS 1550
IF (PCH4W .LT. 1.0) PCH4W = 1.0	GAS 1560
10 CONTINUE	GAS 1570
ELSE	GAS 1580
KCH4W = 1.0D00	GAS 1590
PCH4W = 0.0D00	GAS 1600
END IF	GAS 1610
IF (TCO2M .LT. CPUMIN) KCO2W = 1.0D00	GAS 1620
IF (TH2SM .LT. CPUMIN) KH2SW = 1.0D00	GAS 1630
TCH4O = WROIL * (PCH4W / KCH4OL)	GAS 1640
TCH4W = TCH4M - TCH4O	GAS 1650
IF (TCH4W .LE. CPUMIN .AND. TCH4M .GT. CPUMIN) THEN	GAS 1660
TCH4W = TCH4M / 2.0D00	GAS 1670
TCH4O = TCH4W	GAS 1680
ELSE IF (TCH4W .LE. CPUMIN .AND. TCH4M .LE. CPUMIN) THEN	GAS 1690
TCH4W = 0.0	GAS 1700
TCH4O = 0.0	GAS 1710
END IF	GAS 1720
M(285) = TCH4W	GAS 1730
DO 20 I = 1, 4	GAS 1740
STEP(I) = 0.0	GAS 1750
20 CONTINUE	GAS 1760
END IF	GAS 1770
PCO2W = KCO2W * M(97)	GAS 1780
PCH4W = KCH4W * M(285)	GAS 1790
PH2SW = KH2SW * M(33)	GAS 1800
	GAS 1810
	GAS 1820
IF ((PH2O + PCO2W + PCH4W + PH2SW) .LT. PTOTAL) THEN	GAS 1830
IPHASE = 2	GAS 1840
TCO2O = WROIL * (PCO2W / KCO2OL)	GAS 1850
TCH4O = WROIL * (PCH4W / KCH4OL)	GAS 1860
TH2SO = WROIL * (PH2SW / KH2SOL)	GAS 1870
TCO2V = 0.0D00	GAS 1880
TCH4V = 0.0D00	GAS 1890
TH2SV = 0.0D00	GAS 1900
ELSE	GAS 1910
IPHASE = 3	GAS 1920
A = TCO2M - SC02 + M(97)	GAS 1930
B = TCH4M	GAS 1940

C = TH2SM - ANALM(33) + M(33)	GAS 1950
E = PTOTAL - PH2O	GAS 1960
D = E * ((WROIL/KCO2OL) + (1.0D00/KCO2W))	GAS 1970
G = E * ((WROIL/KCH4OL) + (1.0D00/KCH4W))	GAS 1980
J = E * ((WROIL/KH2SOL) + (1.0D00/KH2SW))	GAS 1990
CALL POLY(A, B, C, E, D, G, J, ROOT)	GAS 2000
D = D / E	GAS 2010
G = G / E	GAS 2020
J = J / E	GAS 2030
PCO2W = A / (D + ROOT)	GAS 2040
PCH4W = B / (G + ROOT)	GAS 2050
PH2SW = C / (J + ROOT)	GAS 2060
	GAS 2070
TCO2O = WROIL * (PCO2W / KCO2OL)	GAS 2080
TCH4O = WROIL * (PCH4W / KCH4OL)	GAS 2090
TH2SO = WROIL * (PH2SW / KH2SOL)	GAS 2100
	GAS 2110
TCO2V = PCO2W * ROOT	GAS 2120
TCH4V = PCH4W * ROOT	GAS 2130
TH2SV = PH2SW * ROOT	GAS 2140
	GAS 2150
A = PCO2W / KCO2W	GAS 2160
B = PCH4W / KCH4W	GAS 2170
C = PH2SW / KH2SW	GAS 2180
	GAS 2190
IF (A .GT. CPUMIN) THEN	GAS 2200
TCO2O = TCO2O * M(97) / A	GAS 2210
TCO2V = TCO2V * M(97) / A	GAS 2220
END IF	GAS 2230
	GAS 2240
IF (B .GT. CPUMIN) THEN	GAS 2250
TCH4O = TCH4O * M(285) / B	GAS 2260
TCH4V = TCH4V * M(285) / B	GAS 2270
END IF	GAS 2280
	GAS 2290
IF (C .GT. CPUMIN) THEN	GAS 2300
TH2SO = TH2SO * M(33) / C	GAS 2310
TH2SV = TH2SV * M(33) / C	GAS 2320
END IF	GAS 2330
END IF	GAS 2340
	GAS 2350
DONE = .TRUE.	GAS 2360
	GAS 2370
IF (TCO2M .GT. CPUMIN) THEN	GAS 2380
TEST = (TCO2O + TCO2V + SCO2) / TCO2M	GAS 2390
IF (TEST .LT. CPUMIN) TEST = CPUMIN	GAS 2400
IF (IGAS .GT. 3 .AND. DABS(DLOG10(TEST)) .GT. FCCSAT) THEN	GAS 2410
DO 30 I = 1, 2	GAS 2420
CO2TRY(I) = CO2TRY(I+1)	GAS 2430
CO2DIF(I) = CO2DIF(I+1)	GAS 2440
30 CONTINUE	GAS 2450
END IF	GAS 2460
TEST = TEST - 1.0D00	GAS 2470
I = IGAS	GAS 2480
IF (IGAS .GT. 3) I = 3	GAS 2490
CO2TRY(I) = TCO2W	GAS 2500
CO2DIF(I) = TEST	GAS 2510
IF (IGAS .EQ. 1) THEN	GAS 2520

IF (TEST .GT. -0.98) THEN	GAS 2530
STEP(1) = TCO2W * ((1.0 / (TEST + 1.0)) - 1.0)	GAS 2540
ELSE	GAS 2550
STEP(1) = TCO2M / 3.0	GAS 2560
END IF	GAS 2570
IF (DABS(STEP(1)) .LT. CPUMIN) STEP(1) = TCO2M * 1.0D-04	GAS 2580
ELSE	GAS 2590
IF ((CO2DIF(I) * CO2DIF(I-1)) .LE. 0.0) THEN	GAS 2600
STEP(1) = STEP(1) * (-0.40)	GAS 2610
END IF	GAS 2620
IF ((TCO2W + STEP(1)) .LT. 0.0) STEP(1) = TCO2W * (-0.90)	GAS 2630
IF ((TCO2W + STEP(1)) .GT. TCO2M)	GAS 2640
STEP(1) = (TCO2M - TCO2W) * 0.90	GAS 2650
END IF	GAS 2660
STEP(1) = (-1.0) * DSIGN(STEP(1), TEST)	GAS 2670
TEST = TEST + 1.0D00	GAS 2680
IF (DABS(DLOG10(TEST)) .GT. FCCSAT) THEN	GAS 2690
DONE = .FALSE.	GAS 2700
TCO2W = TCO2W + STEP(1)	GAS 2710
END IF	GAS 2720
END IF	GAS 2730
	GAS 2740
IF (TH2SM .GT. CPUMIN) THEN	GAS 2750
TEST = (TH2SO + TH2SV + ANALM(33)) / TH2SM	GAS 2760
IF (TEST .LT. CPUMIN) TEST = CPUMIN	GAS 2770
	GAS 2780
IF (IGAS .GT. 3 .AND. DABS(DLOG10(TEST)) .GT. FCCSAT) THEN	GAS 2790
DO 40 I = 1, 2	GAS 2800
H2STRY(I) = H2STRY(I+1)	GAS 2810
H2SDIF(I) = H2SDIF(I+1)	GAS 2820
40 CONTINUE	GAS 2830
END IF	GAS 2840
	GAS 2850
TEST = TEST - 1.0D00	GAS 2860
I = IGAS	GAS 2870
IF (IGAS .GT. 3) I = 3	GAS 2880
H2STRY(I) = TH2SW	GAS 2890
H2SDIF(I) = TEST	GAS 2900
	GAS 2910
IF (IGAS .EQ. 1) THEN	GAS 2920
IF (TEST .GT. -0.98) THEN	GAS 2930
STEP(2) = TH2SW * ((1.0 / (TEST + 1.0)) - 1.0)	GAS 2940
ELSE	GAS 2950
STEP(2) = TH2SM / 3.0	GAS 2960
END IF	GAS 2970
IF (DABS(STEP(2)) .LT. CPUMIN) STEP(2) = TH2SM * 1.0D-04	GAS 2980
ELSE	GAS 2990
IF ((H2SDIF(I) * H2SDIF(I-1)) .LE. 0.0) THEN	GAS 3000
STEP(2) = STEP(2) * (-0.40)	GAS 3010
END IF	GAS 3020
IF ((TH2SW + STEP(2)) .LT. 0.0) STEP(2) = TH2SW * (-0.90)	GAS 3030
IF ((TH2SW + STEP(2)) .GT. TH2SM)	GAS 3040
STEP(2) = (TH2SM - TH2SW) * 0.90	GAS 3050
END IF	GAS 3060
	GAS 3070
STEP(2) = (-1.0) * DSIGN(STEP(2), TEST)	GAS 3080
TEST = TEST + 1.0D00	GAS 3090
	GAS 3100

IF (DABS(DLOG10(TEST)) .GT. FCCSAT) THEN	GAS 3110
DONE = .FALSE.	GAS 3120
TH2SW = TH2SW + STEP(2)	GAS 3130
END IF	GAS 3140
END IF	GAS 3150
IF (TCH4M .GT. CPUMIN) THEN	GAS 3160
TEST = (TCH4O + TCH4V + ANALM(285)) / TCH4M	GAS 3170
IF (TEST .LT. CPUMIN) TEST = CPUMIN	GAS 3180
	GAS 3190
	GAS 3200
IF (IGAS .GT. 3 .AND. DABS(DLOG10(TEST)) .GT. FCCSAT) THEN	GAS 3210
DO 50 I = 1, 2	GAS 3220
CH4TRY(I) = CH4TRY(I+1)	GAS 3230
CH4DIF(I) = CH4DIF(I+1)	GAS 3240
50 CONTINUE	GAS 3250
END IF	GAS 3260
	GAS 3270
TEST = TEST - 1.0D00	GAS 3280
I = IGAS	GAS 3290
IF (IGAS .GT. 3) I = 3	GAS 3300
CH4TRY(I) = TCH4W	GAS 3310
CH4DIF(I) = TEST	GAS 3320
	GAS 3330
IF (IGAS .EQ. 1) THEN	GAS 3340
IF (TEST .GT. -0.98) THEN	GAS 3350
STEP(3) = TCH4W * ((1.0 / (TEST + 1.0)) - 1.0)	GAS 3360
ELSE	GAS 3370
STEP(3) = TCH4M / 3.0	GAS 3380
END IF	GAS 3390
IF (DABS(STEP(3)) .LT. CPUMIN) STEP(3) = TCH4M * 1.0D-04	GAS 3400
ELSE	GAS 3410
IF ((CH4DIF(I) * CH4DIF(I-1)) .LE. 0.0) THEN	GAS 3420
STEP(3) = STEP(3) * (-0.40)	GAS 3430
END IF	GAS 3440
IF ((TCH4W + STEP(3)) .LT. 0.0) STEP(3) = TCH4W * (-0.90)	GAS 3450
IF ((TCH4W + STEP(3)) .GT. TCH4M)	GAS 3460
STEP(3) = (TCH4M - TCH4W) * 0.90	GAS 3470
END IF	GAS 3480
STEP(3) = (-1.0) * DSIGN(STEP(3), TEST)	GAS 3490
TEST = TEST + 1.0D00	GAS 3500
IF (DABS(DLOG10(TEST)) .GT. FCCSAT) THEN	GAS 3510
DONE = .FALSE.	GAS 3520
TCH4W = TCH4W + STEP(3)	GAS 3530
END IF	GAS 3540
END IF	GAS 3550
	GAS 3560
IF (DONE .OR. IGAS .EQ. IMAX) THEN	GAS 3570
IPHASE = 0	GAS 3580
CALL PAGE	GAS 3590
IPGLN = IPGLN + 6	GAS 3600
WRITE (UNO,1000)	GAS 3610
IPGLN = IPGLN + 3	GAS 3620
WRITE (UNO, 1010) SCO2, TCO2O, TCO2V, TCO2M, PCO2W	GAS 3630
WRITE (UNO, 1020) TCH4W, TCH4O, TCH4V, TCH4M, PCH4W	GAS 3640
WRITE (UNO, 1030) TH2SW, TH2SO, TH2SV, TH2SM, PH2SW	GAS 3650
IPGLN = IPGLN + 9	GAS 3660
WRITE (UNO, 1040) KCO2W, KCO2OL, KCH4W, KCH4OL, KH2SW, KH2SOL	GAS 3670
IPGLN = IPGLN + 3	GAS 3680

WRITE (UNO, 1050) WROIL, FCCSAT	GAS 3690
DCO2 = 0.0	GAS 3700
DH2S = 0.0	GAS 3710
DCH4 = 0.0	GAS 3720
ELSE	GAS 3730
TOTEL(3) = TCO2W	GAS 3740
HTOTI = ORGT1	GAS 3750
	GAS 3760
DCO2 = TCO2W - ORGCO2	GAS 3770
EXELT(29) = TCO2W	GAS 3780
TITR(1) = TCO2W	GAS 3790
ANALM(7) = TCO2W	GAS 3800
ANALM(98) = 0.0	GAS 3810
	GAS 3820
DH2S = TH2SW - ORGH2S	GAS 3830
EXELT(25) = TH2SW	GAS 3840
TITR(7) = TH2SW	GAS 3850
ANALM(33) = TH2SW	GAS 3860
	GAS 3870
DCH4 = TCH4W - ORGCH4	GAS 3880
ANALM(285) = TCH4W	GAS 3890
M(285) = TCH4W	GAS 3900
	GAS 3910
IF (IPRIN2 .EQ. 0) RETURN	GAS 3920
IF (IGAS .EQ. 1 .OR. IPGLN .GT. 45) CALL PAGE	GAS 3930
IPGLN = IPGLN + 7	GAS 3940
WRITE (UNO, 1060)	GAS 3950
IPGLN = IPGLN + 4	GAS 3960
I = IGAS	GAS 3970
IF (IGAS .GT. 3) I = 3	GAS 3980
WRITE (UNO, 1010) CO2TRY(I), TCO2O, TCO2V, TCO2M, PCO2W, TCO2W	GAS 3990
WRITE (UNO, 1020) CH4TRY(I), TCH4O, TCH4V, TCH4M, PCH4W, TCH4W	GAS 4000
WRITE (UNO, 1030) H2STRY(I), TH2SO, TH2SV, TH2SM, PH2SW, TH2SW	GAS 4010
END IF	GAS 4020
RETURN	GAS 4030
	GAS 4040
1000 FORMAT(//, ' ***** COMPOSITION OF CO-EXISTING GAS, '	GAS 4050
. , ' OIL, AND WATER ***** '	GAS 4060
. //, 19X, 'Total Moles in', 12X, 'Sum in Water', 3X	GAS 4070
. , 'Pressure', /, 10X, 'Water', 8X, 'Oil', 10X, 'Gas'	GAS 4080
. , 7X, 'Oil and Gas', 5X, '(bars)', /, 5X, 65('='))	GAS 4090
1010 FORMAT(' CO2 ', 6(E12.5, 1X))	GAS 4100
1020 FORMAT(' CH4 ', 6(E12.5, 1X))	GAS 4110
1030 FORMAT(' H2S ', 6(E12.5, 1X))	GAS 4120
1040 FORMAT(///, ' HENRY LAW CONSTANTS used for',	GAS 4130
. ' Calculations', //	GAS 4140
. ' K(CO2/H2O) = ', E12.5, 7X, 'K(CO2/OIL) = ', E12.5, /,	GAS 4150
. ' K(CH4/H2O) = ', E12.5, 7X, 'K(CH4/OIL) = ', E12.5, /,	GAS 4160
. ' K(H2S/H2O) = ', E12.5, 7X, 'K(H2S/OIL) = ', E12.5, /)	GAS 4170
1050 FORMAT(/, ' Oil to Water ratio (WROIL) = ', E12.5,	GAS 4180
. /, ' Convergence Factor (FCCSAT) = ', E12.5)	GAS 4190
1060 FORMAT(//, ' ***** COMPOSITION OF CO-EXISTING GAS, '	GAS 4200
. , ' OIL, AND WATER ***** '	GAS 4210
. /, ' *****CALCULATED PRE-STEP VALUES',	GAS 4220
. ' *****'	GAS 4230
. //, 19X, 'Total Moles in', 12X, 'Sum in Water', 3X,	GAS 4240
. , 'Pressure', 3X, 'Next Guess for',	GAS 4250
. /, 10X, 'Water', 8X, 'Oil', 10X, 'Gas',	GAS 4260

.	7X,'Oil and Gas',5X,'(bars)',4X,'Moles in Water',	GAS 4270
.	/,5X,65('=')	GAS 4280
END		GAS 4290

	INTEGER FUNCTION GETUNT (NAME)	GET 0010
C	=====	GET 0020
C	This function determines if a file is opened and return the unit	GET 0030
C	it is opened under. If the file is not opened it will open the	GET 0040
C	the file and return the unit it was opened under	GET 0050
C	-----	GET 0060
C	BASE INT Starting choice for file unit	GET 0070
C	NAME CHA Name of file	GET 0080
C	OPEN LOG Determines if file opened under name	GET 0090
C	UNTNUM INT File unit number	GET 0100
C	YES LOG Determines if file opened under unit	GET 0110
C	-----	GET 0120
	INTEGER BASE, UNTNUM	GET 0130
	LOGICAL OPEN, YES	GET 0140
	CHARACTER * 80 NAME	GET 0150
		GET 0160
C	=====	GET 0170
	BASE = 40	GET 0180
	INQUIRE (FILE = NAME, NUMBER = UNTNUM, OPENED = OPEN)	GET 0190
		GET 0200
	IF (.NOT. OPEN) THEN	GET 0210
		GET 0220
10	INQUIRE (UNIT = BASE, OPENED = YES)	GET 0230
	IF (YES) THEN	GET 0240
	BASE = BASE + 1	GET 0250
	GO TO 10	GET 0260
	END IF	GET 0270
	OPEN (BASE, FILE = NAME, STATUS = 'UNKNOWN')	GET 0280
	GETUNT = BASE	GET 0290
	ELSE	GET 0300
	GETUNT = UNTNUM	GET 0310
	END IF	GET 0320
		GET 0330
	RETURN	GET 0340
	END	GET 0350

	SUBROUTINE GUESS (XX, FXX, NEWX, NPTS)	GUE 0010
C	=====	GUE 0020
C	Calculate the value of X where FUN(X) = 0	GUE 0030
C		GUE 0040
C	Input values ... X - NPTS values of X	GUE 0050
C		GUE 0060
C	FX - NPTS values of FUN(X). MUST be ordered	GUE 0070
C	from lowest to highest.	GUE 0080
C	NPTS - number of X, FUN(X) pairs	GUE 0090
C		GUE 0100

C	Returned values ...	GUE 0110
C	NEWX - "Guessed" value of X where FUN(X) is zero	GUE 0120
C		GUE 0130
C	Uses method of Lagrangian interpolation. Note that we solve	GUE 0140
C	using FX as the x variable, and X as the Y variable, and then	GUE 0150
C	interpolate for a value of FX = 0.0	GUE 0160
C	-----	GUE 0170
C	A DBL Intermediate calculation	GUE 0180
C	B DBL Intermediate calculation	GUE 0190
C	FX DBL Local storage of FXX	GUE 0200
C	FXX DBL Values of the function of X	GUE 0210
C	I INT Loop variable	GUE 0220
C	IHIGH INT Pointer to value just above root	GUE 0230
C	ILOW INT Pointer to value just below the root	GUE 0240
C	J INT Loop variable	GUE 0250
C	JHIGH INT Pointer to value just above the root	GUE 0260
C	JLOW INT Pointer to value just below the root	GUE 0270
C	NEWX DBL New value of x where f(x) = 0	GUE 0280
C	NPTS INT Number of points	GUE 0290
C	START INT Restricts the range of points looked at	GUE 0300
C	STOP INT Restricts the range of points looked at	GUE 0310
C	X DBL Local storage of XX	GUE 0320
C	XX DBL Ordinate values	GUE 0330
C	-----	GUE 0340
	INTEGER NPTS, I, J, START, STOP, IHIGH, JHIGH, ILOW, JLOW	GUE 0350
		GUE 0360
	DOUBLE PRECISION XX(*), FXX(*), NEWX, A, B	GUE 0370
	DOUBLE PRECISION X(30), FX(30)	GUE 0380
		GUE 0390
	INTRINSIC DABS	GUE 0400
		GUE 0410
		GUE 0420
C	=====	GUE 0430
	START = 1	GUE 0440
	STOP = NPTS	GUE 0450
		GUE 0460
	DO 10 I = START, STOP	GUE 0470
	X(I) = XX(I)	GUE 0480
	FX(I) = FXX(I)	GUE 0490
	10 CONTINUE	GUE 0500
		GUE 0510
		GUE 0520
	50 CONTINUE	GUE 0530
	NEWX = 0.0	GUE 0540
	DO 200 I = START, STOP	GUE 0550
	A = 1.0D00	GUE 0560
	B = 1.0D00	GUE 0570
	DO 100 J = START, STOP	GUE 0580
	IF (J .NE. I) THEN	GUE 0590
	A = A * (FX(I) - FX(J))	GUE 0600
	B = B * (-1.0D00) * FX(J)	GUE 0610
	END IF	GUE 0620
	100 CONTINUE	GUE 0630
	NEWX = NEWX + (X(I) * B / A)	GUE 0640
	200 CONTINUE	GUE 0650
		GUE 0660
C	-----	GUE 0670
C	Check for a "fish hook" function...ie: new value of X must be	GUE 0680

C	between previous bounding values. If not, recalculate using	GUE 0690
C	one less order polynomial than present try.	GUE 0700
C	-----	GUE 0710
	IHIGH = STOP	GUE 0720
	ILOW = START	GUE 0730
	JHIGH = STOP	GUE 0740
	JLOW = START	GUE 0750
		GUE 0760
		GUE 0770
	DO 300 I = START+1, STOP	GUE 0780
	IF (FX(I) .LT. 0.0) THEN	GUE 0790
	IF (DABS(X(IHIGH) - X(ILOW)) .GT. DABS(X(IHIGH) - X(I)))	GUE 0800
	ILOW = I	GUE 0810
	IF (DABS(X(JHIGH) - X(JLOW)) .LT. DABS(X(JHIGH) - X(I)))	GUE 0820
	JLOW = I	GUE 0830
	ELSE	GUE 0840
	IF (DABS(X(IHIGH) - X(ILOW)) .GT. DABS(X(I) - X(ILOW)))	GUE 0850
	IHIGH = I	GUE 0860
	IF (DABS(X(JHIGH) - X(JLOW)) .LT. DABS(X(I) - X(JLOW)))	GUE 0870
	JHIGH = I	GUE 0880
	END IF	GUE 0890
300	CONTINUE	GUE 0900
		GUE 0910
	IF ((NEWX .LT. X(ILOW) .AND. NEWX .LT. X(IHIGH)) .OR.	GUE 0920
	(NEWX .GT. X(ILOW) .AND. NEWX .GT. X(IHIGH))) THEN	GUE 0930
	IF (DABS(X(JHIGH)-X(IHIGH)) .GT. DABS(X(JLOW)-X(ILOW))) THEN	GUE 0940
	J = JHIGH	GUE 0950
	ELSE	GUE 0960
	J = JLOW	GUE 0970
	END IF	GUE 0980
	IF (J .LT. STOP) THEN	GUE 0990
	DO 400 I = J, (STOP-1)	GUE 1000
	X(I) = X(I+1)	GUE 1010
	FX(I) = FX(I+1)	GUE 1020
400	CONTINUE	GUE 1030
	END IF	GUE 1040
	STOP = STOP - 1	GUE 1050
	GO TO 50	GUE 1060
	END IF	GUE 1070
		GUE 1080
	RETURN	GUE 1090
	END	GUE 1100

	SUBROUTINE INPUT (UNI, TEMP, HITEMP, DNS, PHHIT, IEXCH, ICO2,	INP 0010
	MIXFLG)	INP 0020
C	=====	INP 0030
C	This routine reads in one set of data at a time.	INP 0040
C	-----	INP 0050
C	ACTUAL INT Calculated index value	INP 0060
C	ADEX INT Flag for surface chemistry option	INP 0070
C	ALK INT Flag for distribution of carbonate species	INP 0080
C	AMOL DBL Molality of aqueous/mineral species added	INP 0090
C	ANALM DBL Analyzed molality of species i	INP 0100
C	ANS CHA Determines if ion exchange or adsorption	INP 0110

C	ANS1	INT	Number of complexes for added anion #1	INP 0120
C	ANS2	INT	Number of complexes for added anion #2	INP 0130
C	AVOG	DBL	Avogadro's number	INP 0140
C	CEC	DBL	Cation exchange capacity	INP 0150
C	COEF	DBL	Stoichiometric coefficient and ID number	INP 0160
C	CONV1	DBL	Tolerance factor for convergence of anions	INP 0170
C	CONV2	DBL	Tolerance factor for hydronium mass-balance	INP 0180
C	CPUMIN	DBL	Smallest positive real value program uses	INP 0190
C	CUNITS	DBL	Analytical input concentration	INP 0200
C	DCH4	DBL	Concentration of CH4 lost up annulas	INP 0210
C	DDCH4	DBL	Concentration of CH4 lost before pH measurement	INP 0220
C	DCO2	DBL	Concentration of CO2 lost up annulas	INP 0230
C	DDCO2	DBL	Concentration of CO2 lost before pH measurement	INP 0240
C	DH2S	DBL	Concentration of H2S lost up annulas	INP 0250
C	DDH2S	DBL	Concentration of H2S lost before pH measurement	INP 0260
C	DNH3	DBL	Concentration of NH3 lost up annulas	INP 0270
C	DDNH3	DBL	Concentration of NH3 lost before pH measurement	INP 0280
C	DENS	DBL	Density	INP 0290
C	DFRAC1	DBL	Smallest fraction of soln 1 mixed with soln 2	INP 0300
C	DHA	DBL	Ion size parameter	INP 0310
C	DINC	DBL	Increment of solution 1 to be added	INP 0320
C	DNA	DBL	Temporary ion size parameter for added ions	INP 0330
C	DNS	CHA	Determines if density should be calculated	INP 0340
C	DP	DBL	Dissolution/precipitation switch	INP 0350
C	DSEP	DBL	Density of oil at 15 degree C	INP 0360
C	EHM	DBL	Measured Eh in volts	INP 0370
C	EHMC	DBL	Measured Eh using the Calomel electrode	INP 0380
C	EMFZSC	DBL	Measured Eh using the Zobell's solution	INP 0390
C	FBOIL	DBL	Fraction of solution boiled-off as steam	INP 0400
C	FCCSAT	DBL	Tolerance factor for pH and CO2 options	INP 0410
C	FIXIT	DBL	Fixing value in the CO2 option	INP 0420
C	FLAGS	INT	Selection flags for calculation of redox equil.	INP 0430
C	GEOETH	INT	Flag to select geothermometer	INP 0440
C	GFW	DBL	Gram formula weight of aqueous species	INP 0450
C	HIGHKT	DBL	K(T) at temp 2 for added options	INP 0460
C	HITEMP	DBL	In-situ temperature	INP 0470
C	I	INT	Loop counting variable	INP 0480
C	IBMIX	INT	Switch for mixing option	INP 0490
C	ICCSAT	INT	Switch for pH option	INP 0500
C	ICO2	INT	Switch for CO2 option	INP 0510
C	IDDP	INT	Id number of the mineral to be dissolved/ppt	INP 0520
C	IDMIX	INT	Id number of the aqueous species to be added	INP 0530
C	IDN	INT	Id numbers of the ISCOMP components adsorption	INP 0540
C	IDSAT	INT	Id number of the mineral to be equilibrated	INP 0550
C	IEXCH	INT	Switch for exchange option	INP 0560
C	ILP	INT	Index list of the analytical species	INP 0570
C	ILQ	INT	Index list of the complexing cations	INP 0580
C	ILR	INT	Index list of the complexing anions	INP 0590
C	IMCO3	INT	Selects CO2 option	INP 0600
C	INDEX	INT	Reference index for added ions	INP 0610
C	INFORM	INT	Flag to print all the log K values in data base	INP 0620
C	INMIX	INT	Total number of mixtures of two solution mixed	INP 0630
C	INSP	INT	Total number of surface sites for adsorption	INP 0640
C	IOPT	INT	Switch for co2/h option	INP 0650
C	IPAGE	INT	Current page number of output file	INP 0660
C	IPGLN	INT	Current line number of the output file	INP 0670
C	IPHASE	INT	Switch for oil/water/gas calculations	INP 0680
C	IPIT	INT	Flag to use pitzer activity coefficients	INP 0690

C	IPRIN1	INT	Flag for printing iteration of anions	INP 0700
C	IPRIN2	INT	Flag for printing hydronium balance	INP 0710
C	IRXDP	INT	Id number of the aqueous species to be added	INP 0720
C	ISCHG	INT	Charge of each surface site for adsorption	INP 0730
C	ISCOMP	INT	Total number of components in dissociation	INP 0740
C	ITIC	INT	Hitemp distribution of carbonate species	INP 0750
C	ITMIX	INT	Switch for the mineral saturation option	INP 0760
C	ITT	INT	Number of aqueous species to add/sub with water	INP 0770
C	J	INT	Loop counting variable	INP 0780
C	KCH4OL	DBL	Henry's law coefficient for CH4 in oil	INP 0790
C	KCO2OL	DBL	Henry's law coefficient for CO2 in oil	INP 0800
C	KH2SOL	DBL	Henry's law coefficient for H2S in oil	INP 0810
C	KRXN	DBL	K for dissociation reaction of surface species	INP 0820
C	LINE	INT	Line count used for error location	INP 0830
C	LOWKT	DBL	Log K(T) at temp 1 for added options	INP 0840
C	MBASE	DBL	Equivalence Mole Fraction (initial) on surface	INP 0850
C	MINCO	DBL	Stoichiometric coefficient for added minerals	INP 0860
C	MININD	INT	Index number of the added mineral	INP 0870
C	MINLOG	DBL	Log K values for added minerals	INP 0880
C	MXMNK	INT	Total number of mineral log k values	INP 0890
C	MXSP	INT	Total number of aqueous species	INP 0900
C	NAME	CHA	Name of each complex formed by association	INP 0910
C	NDUM	INT	Id of mineral/aqueous complex with K(T) changed	INP 0920
C	NMAX	INT	General array dimension to allow easy expansion	INP 0930
C	NOSE	INT	Number of species in the equation	INP 0940
C	NUFLAG	INT	Sets the activity coefficients of neutral species	INP 0950
C	NUMCOM	INT	Number of complex the ion is associated with	INP 0960
C	NUMINS	INT	Number of minerals added	INP 0970
C	ODUM	CHA	Switch to indicate a mineral/aqueous complex	INP 0980
C	OK	INT	Error flag for Lagrange interpolation routine	INP 0990
C	OUTIN	CHA	Name of restart file name	INP 1000
C	PAGE1	CHA	Names of aqueous species	INP 1010
C	PAGE3	CHA	Names of solubility constants	INP 1020
C	PH	DBL	Measured pH of the solution	INP 1030
C	PHHIT	INT	Hitemp pH switch	INP 1040
C	PRESS	DBL	Total pressure	INP 1050
C	RATIO	INT	Flag for printing activity ratios of elements	INP 1060
C	RXDP	DBL	Molal amount of the aqueous species added	INP 1070
C	SAREA	DBL	Total surface area per kilogram of solvent	INP 1080
C	SPN	CHA	Name of each surface species adsorption	INP 1090
C	TAREA	DBL	Site density per unit area adsorption	INP 1100
C	TCH4M	DBL	Moles CH4 distributed between oil, water, vapor	INP 1110
C	TCO2M	DBL	Moles CO2 distributed between oil, water, vapor	INP 1120
C	TEMP	DBL	Temperature of the solution when pH was measured	INP 1130
C	TH2SM	DBL	Moles H2S distributed between oil, water, vapor	INP 1140
C	TIC	DBL	Concentration of total inorganic carbon	INP 1150
C	TITLE	CHA	Name of the sample	INP 1160
C	TOF	CHA	Places a form feed in output file	INP 1170
C	UNI	INT	File unit assigned for input file	INP 1180
C	UNITS	CHA	Units of concentration	INP 1190
C	UNO	INT	File unit assigned for output file	INP 1200
C	WROIL	DBL	Oil to water weight ratio	INP 1210
C	XD	DBL	Holds Log K's for additional anions & cations	INP 1220
C	XDUM	DBL	New log K(T) value	INP 1230
C	Z	INT	Charge of aqueous species	INP 1240
C				INP 1250
				INP 1260
				INP 1270

INTEGER NMAX, UNO

DOUBLE PRECISION AVOG, CPUMIN	INP 1280
	INP 1290
PARAMETER (NMAX = 340, UNO = 6)	INP 1300
PARAMETER (AVOG = 6.022D+23, CPUMIN = 1.0D-35)	INP 1310
	INP 1320
INTEGER ACTUAL, ALK, ANS1, ANS2, FLAGS(6), GEOTH	INP 1330
INTEGER I, IBMIX, ICCSAT, ICO2, IDDP, IDMX(50)	INP 1340
INTEGER IDN(10,10), IDSAT, IEXCH, ISCHG(10), ILP(33)	INP 1350
INTEGER ILQ(15), ILR(13), IMCO3, IMIX, INDEX, INFORM, INMIX, INSP	INP 1360
INTEGER IOPT, IPAGE, IPGLN, IPHASE, IPIT, IPRIN1, IPRIN2	INP 1370
INTEGER IRXDP(10), ISCOMP(10), ITIC, ITMIX, ITT	INP 1380
INTEGER J, LINE, MININD(8,5), MIXFLG, MXMNK, MXSP, NDUM(12), NOSE	INP 1390
INTEGER NUFLAG, NUMCOM, NUMINS, OK, PHHIT, RATIO, UNI, Z(NMAX)	INP 1400
	INP 1410
CHARACTER * 1 ADEX, CR, DNS, ODUM(12), TOF	INP 1420
CHARACTER * 5 UNITS	INP 1430
CHARACTER * 8 NAME, PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)	INP 1440
CHARACTER * 10 SPN(10)	INP 1450
CHARACTER * 40 TITMIX	INP 1460
CHARACTER * 80 DUMMY, MIXFLE, OUTIN, TITLE	INP 1470
	INP 1480
DOUBLE PRECISION ALFA(NMAX), AMOL(50), ANALM(NMAX)	INP 1490
DOUBLE PRECISION CEC, COEF(10,10), CONV1, CONV2, CUNITS(NMAX)	INP 1500
DOUBLE PRECISION DCH4, DCO2, DDCH4, DDCO2, DDH2S, DDNH3, DEBYE	INP 1510
DOUBLE PRECISION DENS, DFRAC1, DH2S, DINC, DHA(NMAX), DNA, DNH3	INP 1520
DOUBLE PRECISION DP, EHM, EPMC, EMFZSC, FBOIL, FCCSAT, FIXIT	INP 1530
DOUBLE PRECISION GFW(NMAX), HIGHKT, HITEMP, KCH4OL, KCO2OL	INP 1540
DOUBLE PRECISION KH2SOL, KRXN(10), LOWKT	INP 1550
DOUBLE PRECISION M(NMAX), MBASE(10), MINCO(9,5)	INP 1560
DOUBLE PRECISION MINLOG(2,5), PH, PRESS, DSEP, RXDP(10)	INP 1570
DOUBLE PRECISION SAREA, TAREA, TCH4M, TCO2M, TEMP	INP 1580
DOUBLE PRECISION TH2SM, TIC, WROIL, X, XD(2,45), XDUM(12)	INP 1590
	INP 1600
EXTERNAL DEBYE, PAGE	INP 1610
	INP 1620
INTRINSIC DABS, IABS	INP 1630
	INP 1640
COMMON /AL / NDUM, XDUM	INP 1650
COMMON /AMM / IDMX, AMOL, ITMIX, INMIX, DFRAC1, DINC, FBOIL	INP 1660
COMMON /BASIC / DENS, PRESS, EHM, EPMC, EMFZSC, TIC, FCCSAT, XD,	INP 1670
NUMCOM, NUMINS, MINLOG, MINCO, MININD, CONV1,	INP 1680
CONV2	INP 1690
COMMON /CH / ODUM	INP 1700
COMMON /DIST / TCO2M, TCH4M, TH2SM, WROIL, KCH4OL, KCO2OL,	INP 1710
KH2SOL, IPHASE, DSEP	INP 1720
COMMON /EXCHAN/ COEF, MBASE, KRXN, CEC, TAREA,	INP 1730
SAREA, IDN, ISCHG, ISCOMP, INSP	INP 1740
COMMON /FLAGCM/ ALK, ITIC, ICCSAT, IMCO3, ITT, ANS1, ANS2,	INP 1750
NUFLAG, IPIT, FLAGS, INFORM, RATIO, GEOTH,	INP 1760
IPRIN1, IPRIN2	INP 1770
COMMON /FMFD / TOF, CR, TITMIX	INP 1780
COMMON /FORM / IPAGE, IPGLN	INP 1790
COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,	INP 1800
DCH4, DDCH4, IOPT, FIXIT	INP 1810
COMMON /IMM / IBMIX, IMIX	INP 1820
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	INP 1830
COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	INP 1840
COMMON /NAMES2/ SPN	INP 1850

COMMON /NAMES3/ MIXFLE, OUTIN, TITLE, UNITS, ADEX	INP 1860
COMMON /SAT / IDDP, IDSAT, DP, RXDP, IRXDP	INP 1870
COMMON /TABCOM/ MXSP, MXMNK, GFW, Z, DHA	INP 1880
	INP 1890
DATA ILP /3, 4, 22, 1, 2, 18, 14, 12, 5, 6, 33, 7, 98, 30, 29,	INP 1900
136, 32, 31, 26, 15, 25, 27, 16, 23, 21, 13, 28, 169,	INP 1910
210, 48, 246, 265, 285/	INP 1920
DATA ILQ /8, 8, 8, 14, 15, 1, 16, 18, 4, 2, 23, 3, 25, 26, 27/	INP 1930
DATA ILR /5, 6, 7, 9, 29, 30, 48, 98, 101, 246, 265, 0, 0/	INP 1940
	INP 1950
C -----	INP 1960
	INP 1970
C -----	INP 1980
C Get basic input data	INP 1990
C -----	INP 2000
	INP 2010
LINE = 1	INP 2020
READ (UNI, 9000, END = 160) TITLE	INP 2030
	INP 2040
CALL PAGE	INP 2050
WRITE (UNO, 9010) TITLE	INP 2060
IPGLN = IPGLN + 1	INP 2070
	INP 2080
LINE = LINE + 1	INP 2090
READ (UNI, 9020, ERR = 150) TEMP, HITEMP, DENS, PRESS	INP 2100
	INP 2110
LINE = LINE + 1	INP 2120
READ (UNI, 9020, ERR = 150) PH, EHM, EHMC, EMFZSC, UNITS	INP 2130
	INP 2140
C -----	INP 2150
C Check to make sure the units are correct	INP 2160
C -----	INP 2170
	INP 2180
OK = 0	INP 2190
	INP 2200
DO 1 I=1,5	INP 2210
IF (UNITS(I:I).EQ.'m') UNITS(I:I)='M'	INP 2220
IF (UNITS(I:I).EQ.'g') UNITS(I:I)='G'	INP 2230
IF (UNITS(I:I).EQ.'l') UNITS(I:I)='L'	INP 2240
IF (UNITS(I:I).EQ.'p') UNITS(I:I)='P'	INP 2250
IF (UNITS(I:I).EQ.'o') UNITS(I:I)='O'	INP 2260
IF (UNITS(I:I).EQ.'e') UNITS(I:I)='E'	INP 2270
IF (UNITS(I:I).EQ.'q') UNITS(I:I)='Q'	INP 2280
IF (UNITS(I:I).EQ.'k') UNITS(I:I)='K'	INP 2290
1 CONTINUE	INP 2300
	INP 2310
IF (UNITS .EQ. 'MG/L ') THEN	INP 2320
OK = 1	INP 2330
ELSE IF (UNITS .EQ. 'PPM ') THEN	INP 2340
OK = 1	INP 2350
ELSE IF (UNITS .EQ. 'MOL/L') THEN	INP 2360
OK = 1	INP 2370
ELSE IF (UNITS .EQ. 'MOL/K') THEN	INP 2380
OK = 1	INP 2390
ELSE IF (UNITS .EQ. 'MEQ/L') THEN	INP 2400
OK = 1	INP 2410
ELSE	INP 2420
OK = 0	INP 2430

END IF	INP 2440
IF (OK .NE. 1) THEN	INP 2450
WRITE (UNO, 9160) TOF	INP 2460
WRITE (UNO, '(A,A5,A)') 'Must use proper units. "',	INP 2470
UNITS, '" are not recognized.'	INP 2480
STOP	INP 2490
END IF	INP 2500
	INP 2510
	INP 2520
WRITE (UNO, 9030) ' TEMP', ' HITEMP', ' DENS', ' PRESS'	INP 2530
WRITE (UNO, 9040) TEMP, HITEMP, DENS, PRESS	INP 2540
WRITE (UNO, 9030) ' PH', ' EHM', ' EHMC', ' EMFZSC'	INP 2550
WRITE (UNO, 9050) PH, EHM, EHMC, EMFZSC	INP 2560
WRITE (UNO, 9060) UNITS	INP 2570
IPGLN = IPGLN + 5	INP 2580
	INP 2590
C -----	INP 2600
C Get concentration of species	INP 2610
C -----	INP 2620
	INP 2630
LINE = LINE + 1	INP 2640
READ (UNI, 9070, ERR = 150) (CUNITS(ILP(I)), I = 1, 7)	INP 2650
WRITE (UNO, 9080) 'Na', 'K', 'Li', 'Ca',	INP 2660
'Mg', 'Fe', 'Al',	INP 2670
WRITE (UNO, 9050) (CUNITS(ILP(I)), I = 1, 7)	INP 2680
IPGLN = IPGLN + 2	INP 2690
	INP 2700
LINE = LINE + 1	INP 2710
READ (UNI, 9070, ERR = 150) (CUNITS(ILP(I)), I = 8, 13), TIC	INP 2720
WRITE (UNO, 9080) 'SiO2', 'Cl', 'SO4', 'H2S',	INP 2730
'HCO3', 'CO3', 'TIC',	INP 2740
WRITE (UNO, 9050) (CUNITS(ILP(I)), I = 8, 13), TIC	INP 2750
IPGLN = IPGLN + 2	INP 2760
	INP 2770
LINE = LINE + 1	INP 2780
READ (UNI, 9070, ERR = 150) (CUNITS(ILP(I)), I = 14, 20)	INP 2790
WRITE (UNO, 9080) 'F', 'PO4', 'NO3', 'NH3',	INP 2800
'B', 'Sr', 'Ba',	INP 2810
WRITE (UNO, 9050) (CUNITS(ILP(I)), I = 14, 20)	INP 2820
IPGLN = IPGLN + 2	INP 2830
	INP 2840
LINE = LINE + 1	INP 2850
READ (UNI, 9070, ERR = 150) (CUNITS(ILP(I)), I = 21, 26)	INP 2860
WRITE (UNO, 9080) 'Pb', 'Zn', 'Cu', 'Mn',	INP 2870
'Hg', 'Ag',	INP 2880
WRITE (UNO, 9050) (CUNITS(ILP(I)), I = 21, 26)	INP 2890
IPGLN = IPGLN + 2	INP 2900
	INP 2910
LINE = LINE + 1	INP 2920
READ (UNI, 9070, ERR = 150) (CUNITS(ILP(I)), I = 27, 29)	INP 2930
WRITE (UNO, 9080) 'As', 'U', 'V',	INP 2940
WRITE (UNO, 9050) (CUNITS(ILP(I)), I = 27, 29)	INP 2950
IPGLN = IPGLN + 2	INP 2960
	INP 2970
LINE = LINE + 1	INP 2980
READ (UNI, 9070, ERR = 150) (CUNITS(ILP(I)), I = 30, 33)	INP 2990
WRITE (UNO, 9080) 'Acetate', 'Oxalate', 'Succinate', 'CH4'	INP 3000
WRITE (UNO, 9050) (CUNITS(ILP(I)), I = 30, 33)	INP 3010

IPGLN = IPGLN + 2	INP 3020
	INP 3030
C -----	INP 3040
C Adjust B and As to the forms the program uses	INP 3050
C -----	INP 3060
IF (UNITS .EQ. 'PPM ' .OR. UNITS .EQ. 'MG/L ') THEN	INP 3070
CUNITS(31) = CUNITS(31) * 5.720	INP 3080
CUNITS(28) = CUNITS(28) * 1.668	INP 3090
CUNITS(169) = CUNITS(169) * 1.134	INP 3100
CUNITS(210) = CUNITS(210) * 1.942	INP 3110
END IF	INP 3120
	INP 3130
	INP 3140
C -----	INP 3150
C Carbon, High temperature carbon option	INP 3160
C -----	INP 3170
LINE = LINE + 1	INP 3180
READ (UNI, 9100, ERR = 150) ALK, ITIC	INP 3190
WRITE (UNO, 9130) ' ALK ', ' ITIC '	INP 3200
WRITE (UNO, 9110) ALK, ITIC	INP 3210
IPGLN = IPGLN + 2	INP 3220
	INP 3230
	INP 3240
C -----	INP 3250
C Gas addition option	INP 3260
C -----	INP 3270
DDCO2 = 0.0	INP 3280
DCO2 = 0.0	INP 3290
DDNH3 = 0.0	INP 3300
DNH3 = 0.0	INP 3310
DDH2S = 0.0	INP 3320
DH2S = 0.0	INP 3330
DDCH4 = 0.0	INP 3340
DCH4 = 0.0	INP 3350
	INP 3360
LINE = LINE + 1	INP 3370
READ (UNI, 9070, ERR = 150) DDCO2, DDH2S, DDNH3, DDCH4	INP 3380
WRITE (UNO, 9080) ' DCO2 ', ' DH2S ', ' DNH3 ', ' DCH4 '	INP 3390
WRITE (UNO, 9050) DDCO2, DDH2S, DDNH3, DDCH4	INP 3400
IPGLN = IPGLN + 2	INP 3410
	INP 3420
C -----	INP 3430
C pH and co2 saturation option	INP 3440
C -----	INP 3450
LINE = LINE + 1	INP 3460
READ (UNI, 9100, ERR = 150) ICCSAT, IMCO3, FIXIT, FCCSAT	INP 3470
WRITE (UNO, 9080) ' ICCSAT ', ' IMCO3 ', ' FIXIT ', ' FCCSAT '	INP 3480
WRITE (UNO, 9110) ICCSAT, IMCO3, FIXIT, FCCSAT	INP 3490
IPGLN = IPGLN + 2	INP 3500
	INP 3510
	INP 3520
IF (IMCO3 .EQ. 0) ICO2 = 0	INP 3530
IF (IMCO3 .GT. 0) ICO2 = 1	INP 3540
	INP 3550
IF (FCCSAT .LT. CPUMIN) FCCSAT = 2.0D-3	INP 3560
IF (FCCSAT .GT. 0.1) FCCSAT = 0.05	INP 3570
	INP 3580
C -----	INP 3590

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C      Gas-water-oil option                                INP 3600
C -----| INP 3610
                                           INP 3620
      LINE = LINE + 1                                       INP 3630
      READ (UNI, 9070, ERR = 150) TCO2M, TCH4M, TH2SM, WROIL, INP 3640
                                           KCO2OL, KCH4OL, KH2SOL, DSEP INP 3650
      WRITE (UNO, 9080) 'TCO2M ', 'TCH4M ', 'TH2SM ', 'WROIL ', INP 3660
                                           'KCO2OL ', 'KCH4OL ', 'KH2SOL ', 'DSEP ' INP 3670
      WRITE (UNO, 9050) TCO2M, TCH4M, TH2SM, WROIL, KCO2OL, INP 3680
                                           KCH4OL, KH2SOL, DSEP INP 3690
      IPGLN = IPGLN + 2                                       INP 3700
      IF (DABS(KCO2OL) .LT. CPUMIN) KCO2OL = 1.0             INP 3710
      IF (DABS(KCH4OL) .LT. CPUMIN) KCH4OL = 1.0             INP 3720
      IF (DABS(KH2SOL) .LT. CPUMIN) KH2SOL = 1.0             INP 3730
                                           INP 3740
C -----| INP 3750
C      Read and write data for ion exchange or adsorption INP 3760
C -----| INP 3770
                                           INP 3780
      LINE = LINE + 1                                       INP 3790
      READ (UNI, 9160, ERR = 150) ADEX                      INP 3800
      WRITE (UNO, '(A, A1)') ' Adsorption/Exchange option (N=no) = ', INP 3810
                                           ADEX INP 3820
      IF (ADEX .EQ. 'a' .OR. ADEX .EQ. 'A') THEN             INP 3830
        ADEX = 'A'                                           INP 3840
      ELSE IF (ADEX .EQ. 'e' .OR. ADEX .EQ. 'E') THEN         INP 3850
        ADEX = 'E'                                           INP 3860
      ELSE                                                     INP 3870
        ADEX = 'N'                                           INP 3880
      END IF                                                  INP 3890
      X = 0.0                                                 INP 3900
      IF (ADEX .EQ. 'A') THEN                                  INP 3910
        IEXCH = 1                                             INP 3920
        WRITE (UNO, 9220) ' Adsorption (Double layer model)' INP 3930
        WRITE (UNO, 9080) ' CEC ', ' TAREA ', ' SAREA ', ' INSP ' INP 3940
                                           INP 3950
      LINE = LINE + 1                                       INP 3960
      READ (UNI, 9150) CEC, TAREA, SAREA, INSP              INP 3970
      WRITE (UNO, 9240) CEC, TAREA, SAREA, INSP             INP 3980
                                           INP 3990
      WRITE (UNO, 9090) ' NAME ', ' CHARGE ', INP 4000
                                           'Fract. Surf. Sites ' INP 4010
                                           INP 4020
      IPGLN = IPGLN + 4                                       INP 4030
      DO 10 I = 1, INSP                                       INP 4040
        LINE = LINE + 1                                       INP 4050
        READ (UNI, 9200, ERR = 150) ISCHG(I), MBASE(I), SPN(I) INP 4060
        LINE = LINE + 1                                       INP 4070
                                           INP 4080
        WRITE (UNO, 9250) SPN(I), ISCHG(I), MBASE(I)         INP 4090
                                           INP 4100
      LINE = LINE + 1                                       INP 4110
      READ (UNI, 9210, ERR = 150) KRXN(I), ISCOMP(I), INP 4120
        (COEF(I,J), IDN(I,J), J=1,ISCOMP(I)) INP 4130
                                           INP 4140
      X = X + MBASE(I)                                       INP 4150
      IPGLN = IPGLN + 1                                       INP 4160
      IF (IPGLN .GT. 58) CALL PAGE INP 4170

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10	CONTINUE	INP 4180
		INP 4190
	IF (DABS(1.0D00 - X) .GT. 0.001) THEN	INP 4200
	WRITE (UNO, '(A, A, A)')	INP 4210
.	' ERROR in absorption/ion exchange',	INP 4220
.	' data. The sum of fraction of',	INP 4230
.	' surface sites is not 1.0'	INP 4240
	STOP	INP 4250
	END IF	INP 4260
		INP 4270
	WRITE (UNO, '(11X, A, A)') 'K = 1. *',	INP 4280
.	' * Coef * ID + '	INP 4290
		INP 4300
	DO 20 I = 1, INSP	INP 4310
	WRITE (UNO, 9260) KRXN(I), SPN(I), (COEF(I,J), IDN(I,J),	INP 4320
.	J = 1, ISCOMP(I))	INP 4330
	IPGLN = IPGLN + 1	INP 4340
	IF (IPGLN .GT. 57) CALL PAGE	INP 4350
20	CONTINUE	INP 4360
	ELSE IF (ADEX .EQ. 'E') THEN	INP 4370
	IEXCH = 2	INP 4380
	WRITE (UNO, 9220) 'Ion Exchange: '	INP 4390
	WRITE (UNO, 9080) ' CEC ', ' TAREA ', ' SAREA ', ' INSP '	INP 4400
		INP 4410
	LINE = LINE + 1	INP 4420
	READ (UNI, 9150) CEC, TAREA, SAREA, INSP	INP 4430
	WRITE (UNO, 9240) CEC, TAREA, SAREA, INSP	INP 4440
		INP 4450
	WRITE (UNO, 9090) ' NAME ', ' CHARGE ',	INP 4460
.	'Fract. Surf. Sites '	INP 4470
		INP 4480
	IPGLN = IPGLN + 4	INP 4490
	DO 30 I = 1, INSP	INP 4500
	LINE = LINE + 1	INP 4510
	READ (UNI, 9200, ERR = 150) ISCHG(I), MBASE(I), SPN(I)	INP 4520
	LINE = LINE + 1	INP 4530
		INP 4540
	WRITE (UNO, 9250) SPN(I), ISCHG(I), MBASE(I)	INP 4550
		INP 4560
	X = X + MBASE(I)	INP 4570
	LINE = LINE + 1	INP 4580
	READ (UNI, 9210, ERR = 150) KRXN(I), ISCOMP(I),	INP 4590
.	(COEF(I,J), IDN(I,J), J=1,ISCOMP(I))	INP 4600
		INP 4610
	IPGLN = IPGLN + 1	INP 4620
	IF (IPGLN .GT. 57) CALL PAGE	INP 4630
30	CONTINUE	INP 4640
		INP 4650
	IF (DABS(1.0D00 - X) .GT. 0.001) THEN	INP 4660
	WRITE (UNO, '(A, A, A)')	INP 4670
.	' ERROR in absorption/ion exchange',	INP 4680
.	' data. The sum of fraction of',	INP 4690
.	' surface sites is not 1.0'	INP 4700
	STOP	INP 4710
	END IF	INP 4720
		INP 4730
	WRITE (UNO, '(11X, A, A)') 'K = 1. *',	INP 4740
.	' * Coef * ID + '	INP 4750

DO 40 I = 1, INSP	INP 4760
WRITE (UNO, 9260) KRXN(I), SPN(I), (COEF(I,J), IDN(I,J),	INP 4770
J = 1, ISCOMP(I))	INP 4780
IPGLN = IPGLN + 1	INP 4790
IF (IPGLN .GT. 57) CALL PAGE	INP 4800
40 CONTINUE	INP 4810
END IF	INP 4820
IF (IEXCH .GT. 0) THEN	INP 4830
IF (CEC .LE. CPUMIN) CEC = TAREA * SAREA * 1000.0 / AVOG	INP 4840
END IF	INP 4850
	INP 4860
	INP 4870
	INP 4880
C -----	INP 4890
C Precipitation/mixing/boiling option	INP 4900
C -----	INP 4910
C IF (MIXFLG .EQ. 0) THEN set all values read equal to zero	INP 4920
C -----	INP 4930
	INP 4940
IF (IPGLN .GT. 59) CALL PAGE	INP 4950
IDDP = 0	INP 4960
IDSAT = 0	INP 4970
	INP 4980
LINE = LINE + 1	INP 4990
READ (UNI, 9100, ERR = 150) IBMIX, ITMIX	INP 5000
IF (IPGLN .GT. 59) CALL PAGE	INP 5010
IPGLN = IPGLN + 2	INP 5020
WRITE (UNO, 9130) 'IBMIX', 'ITMIX'	INP 5030
WRITE (UNO, 9110) IBMIX, ITMIX	INP 5040
IF (MIXFLG .NE. 0) THEN	INP 5050
IF (IPGLN .GT. 59) CALL PAGE	INP 5060
IPGLN = IPGLN + 2	INP 5070
IF (IBMIX .EQ. 1) THEN	INP 5080
WRITE (UNO, 9710)	INP 5090
ELSE IF (IBMIX .EQ. 2) THEN	INP 5100
WRITE (UNO, 9720)	INP 5110
ELSE IF (IBMIX .EQ. 3) THEN	INP 5120
WRITE (UNO, 9730)	INP 5130
END IF	INP 5140
END IF	INP 5150
IF (IBMIX .EQ. 1) THEN	INP 5160
IF (ITMIX .GT. 0) THEN	INP 5170
LINE = LINE + 1	INP 5180
IF (MIXFLG .EQ. 0) THEN	INP 5190
WRITE (UNO, 9080) ' SPECIES', 'MOLALITY'	INP 5200
IPGLN = IPGLN + 1	INP 5210
IF (IPGLN .GT. 59) CALL PAGE	INP 5220
END IF	INP 5230
DO 50 I = 1, ITMIX	INP 5240
LINE = LINE + 1	INP 5250
READ (UNI, 9290, ERR = 150) IDMIX(I), AMOL(I)	INP 5260
IF (MIXFLG .EQ. 0) THEN	INP 5270
WRITE (UNO, 9490) PAGE1(IDMIX(I)), AMOL(I)	INP 5280
IPGLN = IPGLN + 1	INP 5290
IF (IPGLN .GT. 59) CALL PAGE	INP 5300
ELSE	INP 5310
IDMIX(I) = 0	INP 5320
AMOL(I) = 0.0	INP 5330

	END IF	INP 5340
50	CONTINUE	INP 5350
	ELSE IF (ITMIX .EQ. 0) THEN	INP 5360
	LINE = LINE + 1	INP 5370
	READ (UNI, 9270, ERR = 150) IDSAT, IDDP, DP	INP 5380
	IF (MIXFLG .EQ. 0) THEN	INP 5390
	WRITE (UNO, 9420) PAGE3(IDSAT), IDSAT	INP 5400
	IPGLN = IPGLN + 1	INP 5410
	IF (IPGLN .GT. 59) CALL PAGE	INP 5420
	END IF	INP 5430
	IF (IDDP .EQ. 0) THEN	INP 5440
	LINE = LINE + 1	INP 5450
	READ (UNI, 9280, ERR = 150) ITT	INP 5460
	IF (MIXFLG .EQ. 0) THEN	INP 5470
	WRITE (UNO, 9440)	INP 5480
	IPGLN = IPGLN + 1	INP 5490
	IF (IPGLN .GT. 59) CALL PAGE	INP 5500
	END IF	INP 5510
	DO 60 I = 1, ITT	INP 5520
	LINE = LINE + 1	INP 5530
	READ (UNI, 9290, ERR = 150) IRXDP(I), RXDP(I)	INP 5540
	IF (MIXFLG .EQ. 0) THEN	INP 5550
	WRITE (UNO, 9460) IRXDP(I), PAGE1(IRXDP(I)), RXDP(I)	INP 5560
	IPGLN = IPGLN + 1	INP 5570
	IF (IPGLN .GT. 59) CALL PAGE	INP 5580
	END IF	INP 5590
60	CONTINUE	INP 5600
	IF (MIXFLG .EQ. 0) THEN	INP 5610
	WRITE (UNO, 9450) DP	INP 5620
	IPGLN = IPGLN + 1	INP 5630
	IF (IPGLN .GT. 59) CALL PAGE	INP 5640
	ELSE	INP 5650
	IDSAT = 0	INP 5660
	IDDP = 0	INP 5670
	ITT = 0	INP 5680
	DP = 0.0	INP 5690
	END IF	INP 5700
	ELSE	INP 5710
	IF (MIXFLG .EQ. 0) THEN	INP 5720
	WRITE (UNO, 9430) PAGE3(IDDP), IDDP	INP 5730
	IPGLN = IPGLN + 1	INP 5740
	IF (IPGLN .GT. 59) CALL PAGE	INP 5750
	ELSE	INP 5760
	IDDP = 0	INP 5770
	END IF	INP 5780
	END IF	INP 5790
	ELSE IF (ITMIX .LT. 0) THEN	INP 5800
	LINE = LINE + 1	INP 5810
	READ (UNI, 9290, ERR = 150) IDDP, AMOL(1)	INP 5820
	IF (MIXFLG .EQ. 0) THEN	INP 5830
	WRITE (UNO, 9140) 'IDDP ', 'AMOL(1) '	INP 5840
	WRITE (UNO, 9410) IDDP, AMOL(1)	INP 5850
	IPGLN = IPGLN + 2	INP 5860
	IF (IPGLN .GT. 59) CALL PAGE	INP 5870
	ELSE	INP 5880
	IDDP = 0	INP 5890
	AMOL(1) = 0.0	INP 5900
	END IF	INP 5910

END IF	INP 5920
IF (MIXFLG .EQ. 1) MIXFLG = 0	INP 5930
ELSE IF (IBMIX .EQ. 3) THEN	INP 5940
IF (MIXFLG .EQ. 0) THEN	INP 5950
LINE = LINE + 1	INP 5960
READ (UNI, 9070, ERR = 150) FBOIL	INP 5970
WRITE (UNO, 9470) FBOIL	INP 5980
IPGLN = IPGLN + 1	INP 5990
IF (IPGLN .GT. 59) CALL PAGE	INP 6000
ELSE	INP 6010
READ (UNI, '(A80)') DUMMY	INP 6020
MIXFLG = 0	INP 6030
END IF	INP 6040
	INP 6050
ELSE IF (IBMIX .EQ. 2) THEN	INP 6060
IF (MIXFLG .EQ. 0) THEN	INP 6070
LINE = LINE + 1	INP 6080
READ (UNI, 9290, ERR = 150) INMIX, DFRAC1, DINC, MIXFLE	INP 6090
IPGLN = IPGLN + 2	INP 6100
IF (IPGLN .GT. 59) CALL PAGE	INP 6110
WRITE (UNO, 9480) INMIX, DFRAC1, DINC	INP 6120
IF (MIXFLE .NE. ' ') THEN	INP 6130
WRITE (UNO, 9481) MIXFLE(1:40)	INP 6140
ELSE	INP 6150
WRITE (UNO, 9482)	INP 6160
END IF	INP 6170
MIXFLG = 1	INP 6180
ELSE	INP 6190
READ (UNI, '(A80)') DUMMY	INP 6200
MIXFLG = 0	INP 6210
END IF	INP 6220
END IF	INP 6230
	INP 6240
C -----	INP 6250
C Optional user Read in miscellaneous options	INP 6260
C -----	INP 6270
	INP 6280
LINE = LINE + 1	INP 6290
READ (UNI, 9180, ERR = 150) (ODUM(I), NDUM(I), XDUM(I), I = 1, 6)	INP 6300
WRITE (UNO, 9340) TEMP	INP 6310
WRITE (UNO, 9190) (ODUM(I), NDUM(I), XDUM(I), I = 1, 6)	INP 6320
IPGLN = IPGLN + 2	INP 6330
IF (IPGLN .GT. 59) CALL PAGE	INP 6340
	INP 6350
LINE = LINE + 1	INP 6360
READ (UNI, 9180, ERR = 150) (ODUM(I), NDUM(I), XDUM(I), I = 7, 12)	INP 6370
WRITE (UNO, 9340) HITEMP	INP 6380
WRITE (UNO, 9190) (ODUM(I), NDUM(I), XDUM(I), I = 7, 12)	INP 6390
IPGLN = IPGLN + 2	INP 6400
IF (IPGLN .GT. 59) CALL PAGE	INP 6410
	INP 6420
C -----	INP 6430
C Read user defined anions	INP 6440
C -----	INP 6450
	INP 6460
LINE = LINE + 1	INP 6470
READ (UNI, 9300, ERR = 150) ANS1, ANS2	INP 6480
WRITE (UNO, 9130) 'ANS1', 'ANS2'	INP 6490

WRITE (UNO, 9110) ANS1, ANS2	INP 6500
IPGLN = IPGLN + 2	INP 6510
IF (IPGLN .GT. 59) CALL PAGE	INP 6520
	INP 6530
DO 70 I = 1, 45	INP 6540
XD(1,I) = 0.0D0	INP 6550
XD(2,I) = 0.0D0	INP 6560
70 CONTINUE	INP 6570
	INP 6580
IF (ANS1 .EQ. 0 .AND. ANS2 .NE. 0) THEN	INP 6590
ANS1 = ANS2	INP 6600
ANS2 = 0	INP 6610
END IF	INP 6620
	INP 6630
IF (ANS1 .GT. 0) THEN	INP 6640
WRITE (UNO, 9500) 'NAME', 'CONC', 'GFW', 'CHARGE', 'DHA'	INP 6650
LINE = LINE + 1	INP 6660
READ (UNI, 9360, ERR = 150) CUNITS(MXSP+1), GFW(MXSP+1),	INP 6670
Z(MXSP+1), DHA(MXSP+1), PAGE1(MXSP+1)	INP 6680
WRITE (UNO, 9380) PAGE1(MXSP+1), CUNITS(MXSP+1), GFW(MXSP+1),	INP 6690
Z(MXSP+1), DHA(MXSP+1)	INP 6700
IPGLN = IPGLN + 2	INP 6710
IF (IPGLN .GT. 59) CALL PAGE	INP 6720
WRITE (UNO, 9400)	INP 6730
IPGLN = IPGLN + 1	INP 6740
	INP 6750
DO 80 I = 1, ANS1	INP 6760
LINE = LINE + 1	INP 6770
READ (UNI, 9370, ERR = 150) INDEX, DNA, LOWKT, HIGHKT, NAME	INP 6780
WRITE (UNO, 9390) NAME, INDEX, LOWKT, HIGHKT, DNA	INP 6790
IPGLN = IPGLN + 1	INP 6800
IF (IPGLN .GT. 59) CALL PAGE	INP 6810
	INP 6820
ACTUAL = MXSP + INDEX	INP 6830
PAGE1(ACTUAL) = NAME	INP 6840
	INP 6850
XD(1,INDEX) = LOWKT	INP 6860
XD(2,INDEX) = HIGHKT	INP 6870
	INP 6880
GFW(ACTUAL) = GFW(MXSP+1) + GFW(ILQ(INDEX))	INP 6890
IF (INDEX .EQ. 3) GFW(ACTUAL) = GFW(ACTUAL) + GFW(ILQ(INDEX))	INP 6900
	INP 6910
Z(ACTUAL) = Z(MXSP+1) + Z(ILQ(INDEX))	INP 6920
IF (INDEX .EQ. 3) Z(ACTUAL) = Z(ACTUAL) + Z(ILQ(INDEX))	INP 6930
	INP 6940
DHA(ACTUAL) = DEBYE (Z(ACTUAL), DNA)	INP 6950
	INP 6960
80 CONTINUE	INP 6970
END IF	INP 6980
	INP 6990
IF (ANS2 .NE. 0) THEN	INP 7000
WRITE (UNO, 9500) 'NAME', 'CONC', 'GFW', 'CHARGE', 'DHA'	INP 7010
LINE = LINE + 1	INP 7020
READ (UNI, 9360, ERR = 150) CUNITS(MXSP+16), GFW(MXSP+16),	INP 7030
Z(MXSP+16), DHA(MXSP+16), PAGE1(MXSP+16)	INP 7040
WRITE (UNO, 9380) PAGE1(MXSP+16), CUNITS(MXSP+16), GFW(MXSP+16),	INP 7050
Z(MXSP+16), DHA(MXSP+16)	INP 7060
IPGLN = IPGLN + 2	INP 7070

IF (IPGLN .GT. 59) CALL PAGE	INP 7080
WRITE (UNO, 9400)	INP 7090
IPGLN = IPGLN + 1	INP 7100
DO 90 I = 1, ANS2	INP 7110
LINE = LINE + 1	INP 7120
READ (UNI, 9370, ERR = 150) INDEX, DNA, LOWKT, HIGHKT, NAME	INP 7130
WRITE (UNO, 9390) NAME, INDEX, LOWKT, HIGHKT, DNA	INP 7140
IPGLN = IPGLN + 1	INP 7150
IF (IPGLN .GT. 59) CALL PAGE	INP 7160
	INP 7170
ACTUAL = MXSP + INDEX + 15	INP 7180
PAGE1(ACTUAL) = NAME	INP 7190
	INP 7200
XD(1, INDEX+15) = LOWKT	INP 7210
XD(2, INDEX+15) = HIGHKT	INP 7220
	INP 7230
GFW(ACTUAL) = GFW(MXSP+16) + GFW(ILQ(INDEX))	INP 7240
IF (INDEX .EQ. 3) GFW(ACTUAL) = GFW(ACTUAL) + GFW(ILQ(INDEX))	INP 7250
	INP 7260
Z(ACTUAL) = Z(MXSP+16) + Z(ILQ(INDEX))	INP 7270
IF (INDEX .EQ. 3) Z(ACTUAL) = Z(ACTUAL) + Z(ILQ(INDEX))	INP 7280
	INP 7290
DHA(ACTUAL) = DEBYE (Z(ACTUAL), DNA)	INP 7300
	INP 7310
90 CONTINUE	INP 7320
END IF	INP 7330
	INP 7340
C -----	INP 7350
C Read user defined cations	INP 7360
C -----	INP 7370
	INP 7380
LINE = LINE + 1	INP 7390
READ (UNI, 9510) NUMCOM, Z(MXSP+31), DHA(MXSP+31), GFW(MXSP+31),	INP 7400
CUNITS(MXSP+31), PAGE1(MXSP+31)	INP 7410
IF (NUMCOM .GT. 0) THEN	INP 7420
WRITE (UNO, 9520) 'NAME', 'CHARGE', 'DHA', 'GFW', 'CONC'	INP 7430
WRITE (UNO, 9530) PAGE1(MXSP+31), Z(MXSP+31), DHA(MXSP+31),	INP 7440
GFW(MXSP+31), CUNITS(MXSP+31)	INP 7450
IPGLN = IPGLN + 2	INP 7460
IF (IPGLN .GT. 59) CALL PAGE	INP 7470
ILR(12) = MXSP + 1	INP 7480
ILR(13) = MXSP + 16	INP 7490
	INP 7500
DO 100 I = 1, NUMCOM	INP 7510
WRITE (UNO, 9540) 'NAME', 'DHA', 'LOWKT', 'HIGHKT'	INP 7520
READ (UNI, 9550) INDEX, DNA, LOWKT, HIGHKT, NAME	INP 7530
WRITE (UNO, 9560) INDEX, NAME, DNA, LOWKT, HIGHKT	INP 7540
IPGLN = IPGLN + 2	INP 7550
IF (IPGLN .GT. 59) CALL PAGE	INP 7560
	INP 7570
ACTUAL = MXSP + INDEX + 30	INP 7580
	INP 7590
PAGE1(ACTUAL) = NAME	INP 7600
Z(ACTUAL) = Z(MXSP+31) + Z(ILR(INDEX-1))	INP 7610
	INP 7620
DHA(ACTUAL) = DEBYE (Z(ACTUAL), DNA)	INP 7630
	INP 7640
GFW(ACTUAL) = GFW(MXSP+31) + GFW(ILR(INDEX-1))	INP 7650

ACTUAL = 30 + INDEX	INP 7660
	INP 7670
XD(1,ACTUAL) = LOWKT	INP 7680
XD(2,ACTUAL) = HIGHKT	INP 7690
100 CONTINUE	INP 7700
END IF	INP 7710
	INP 7720
	INP 7730
C -----	INP 7740
C Read user defined minerals	INP 7750
C -----	INP 7760
	INP 7770
LINE = LINE + 1	INP 7780
READ (UNI, 9270, ERR = 150) NUMINS	INP 7790
IPGLN = IPGLN + 1	INP 7800
IF (IPGLN .GT. 59) CALL PAGE	INP 7810
WRITE (UNO, *) ' Number of Additional Minerals = ', NUMINS	INP 7820
	INP 7830
DO 120 I = 1, 5	INP 7840
MINLOG(1,I) = 999.9	INP 7850
MINLOG(2,I) = 999.9	INP 7860
DO 110 J = 1, 9	INP 7870
MINCO(J,I) = 0.0	INP 7880
IF (J .LE. 8) MININD(J,I) = 0	INP 7890
110 CONTINUE	INP 7900
120 CONTINUE	INP 7910
	INP 7920
DO 140 I = 1, NUMINS	INP 7930
LINE = LINE + 1	INP 7940
READ (UNI, 9570, ERR = 150) MINLOG(1,I), MINLOG(2,I),	INP 7950
MINCO(9,I), PAGE3(MXMNK+I)	INP 7960
LINE = LINE + 1	INP 7970
READ (UNI, 9210, ERR = 150) (MINCO(J,I), MININD(J,I), J = 1, 8)	INP 7980
	INP 7990
IPGLN = IPGLN + 3	INP 8000
IF (IPGLN .GT. 59) CALL PAGE	INP 8010
	INP 8020
NOSE = 0	INP 8030
DO 130 J = 1, 8	INP 8040
IF (MINCO(J,I) .GT. 0) NOSE = NOSE + 1	INP 8050
130 CONTINUE	INP 8060
	INP 8070
WRITE (UNO, 9580) PAGE3(MXMNK+I), 'Log K at T1 = ',	INP 8080
MINLOG(1,I), 'Log K at T2 = ', MINLOG(2,I)	INP 8090
WRITE (UNO, 9590) (MINCO(J,I), '*', PAGE1(MININD(J,I))), ' + ',	INP 8100
J = 1, NOSE), MINCO(9,I)	INP 8110
140 CONTINUE	INP 8120
	INP 8130
C -----	INP 8140
C Assign flags and convergence factors	INP 8150
C -----	INP 8160
	INP 8170
LINE = LINE + 1	INP 8180
READ (UNI, 9300, ERR = 150) NUFLAG, IPIT, (FLAGS(I), I = 1, 6)	INP 8190
WRITE (UNO, 9310) NUFLAG, IPIT	INP 8200
WRITE (UNO, 9320) 'Fe', 'Cu', 'Hg', 'Mn', 'U', 'V',	INP 8210
(FLAGS(I), I = 1, 6)	INP 8220
IPGLN = IPGLN + 2	INP 8230

IF (IPGLN .GT. 59) CALL PAGE	INP 8240
	INP 8250
LINE = LINE + 1	INP 8260
READ (UNI, 9600, ERR = 150) INFORM, RATIO, GEOTH, IPRIN1, IPRIN2,	INP 8270
OUTIN	INP 8280
	INP 8290
LINE = LINE + 1	INP 8300
READ (UNI, 9070, ERR = 150) CONV1, CONV2	INP 8310
	INP 8320
IF (CONV2 .LT. 1.0D-08 .OR. CONV2 .GT. 1.0D-2) CONV2 = 0.5D-04	INP 8330
IF (CONV1 .LT. 1.0D-08 .OR. CONV1 .GT. 1.0D-2) CONV1 = 0.5D-04	INP 8340
	INP 8350
WRITE (UNO, 9350)	INP 8360
WRITE (UNO, 9080) ' INFORM ', ' RATIO ', ' GEOTH ',	INP 8370
' IPRIN1 ', ' IPRIN2 '	INP 8380
WRITE (UNO, 9120) INFORM, RATIO, GEOTH, IPRIN1, IPRIN2	INP 8390
IF (OUTIN .NE. ' ') THEN	INP 8400
WRITE(UNO, 9610) OUTIN	INP 8410
IPGLN = IPGLN + 1	INP 8420
END IF	INP 8430
WRITE (UNO, 9330) CONV1, CONV2	INP 8440
IPGLN = IPGLN + 4	INP 8450
	INP 8460
C -----	INP 8470
C Set defaults	INP 8480
C -----	INP 8490
IF (DENS .LT. CPUMIN) THEN	INP 8500
DNS = 'U'	INP 8510
DENS = 1.0D0	INP 8520
ELSE	INP 8530
DNS = 'Y'	INP 8540
END IF	INP 8550
	INP 8560
	INP 8570
IF (DABS(HITEMP-TEMP) .LE. CPUMIN) HITEMP = 0.0D00	INP 8580
IF (HITEMP .GT. CPUMIN) PHHIT = 1	INP 8590
	INP 8600
C -----	INP 8610
C If the gas or co2 option is to be used, initialize this	INP 8620
C option so that it is performed after the hi-temperature	INP 8630
C option, if requested, is performed.	INP 8640
C -----	INP 8650
IOPT = 0	INP 8660
	INP 8670
	INP 8680
IF (DABS(DDCO2) .GT. CPUMIN .OR. DABS(DDNH3) .GT. CPUMIN .OR.	INP 8690
DABS(DDH2S) .GT. CPUMIN .OR. DABS(DDCH4) .GT. CPUMIN)	INP 8700
IOPT = 2	INP 8710
	INP 8720
IF (ICO2 .GT. 0 .AND. IMCO3 .GT. 0) THEN	INP 8730
IOPT = 1	INP 8740
ELSE	INP 8750
ICO2 = 0	INP 8760
END IF	INP 8770
	INP 8780
IF (TCO2M .GT. CPUMIN .OR. TCH4M .GT. CPUMIN	INP 8790
.OR. TH2SM .GT. CPUMIN) IPHASE = 2	INP 8800
	INP 8810

IPGLN = 60	INP 8820
	INP 8830
RETURN	INP 8840
	INP 8850
C -----	INP 8860
C Error Messages	INP 8870
C -----	INP 8880
	INP 8890
150 CONTINUE	INP 8900
WRITE (UNO, 9160) TOF	INP 8910
WRITE (UNO, 9170) LINE	INP 8920
STOP	INP 8930
	INP 8940
	INP 8950
C -----	INP 8960
C Out of data	INP 8970
C If there are no more data sets in file assigned to unit 5, stop.	INP 8980
C -----	INP 8990
	INP 9000
160 CLOSE (UNI)	INP 9010
CLOSE (UNO)	INP 9020
STOP	INP 9030
	INP 9040
C -----	INP 9050
C Format statements	INP 9060
C -----	INP 9070
	INP 9080
9000 FORMAT (A80)	INP 9090
9010 FORMAT (' ***** INPUT DATA ECHO ***** ',//,' TITLE : ',A80)	INP 9100
9020 FORMAT (4E10.4, A5)	INP 9110
9030 FORMAT (2X, 6(A10, 2X))	INP 9120
9040 FORMAT (2X, 5(E10.4, 2X), A5)	INP 9130
9050 FORMAT (2X,10(E10.4, 2X))	INP 9140
9060 FORMAT (' CONCENTRATION UNITS : ', 2X, A5)	INP 9150
9070 FORMAT (8E10.4)	INP 9160
9080 FORMAT (2X, 10(2X, A, 2X))	INP 9170
9090 FORMAT (2X, 10(2X, A))	INP 9180
9100 FORMAT (2I2, 2E10.4)	INP 9190
9110 FORMAT (2X,2(3X,I3,4X),E12.5,2X,F12.4)	INP 9200
9120 FORMAT (2X, 6(5X, I2, 5X))	INP 9210
9130 FORMAT (5X, A8, 2X, A8)	INP 9220
9140 FORMAT (A8, 2X, A8)	INP 9230
9150 FORMAT (3E10.4, I3)	INP 9240
9160 FORMAT (A1)	INP 9250
9170 FORMAT (5X,'ERROR IN READING REQUIRED INPUT LINE NO. ', I2,	INP 9260
./,' Program Stop')	INP 9270
9180 FORMAT (6(A1, I4, E10.4))	INP 9280
9190 FORMAT (6(1X, A1, 1X, I4, 1X, E10.4,3X))	INP 9290
9200 FORMAT (I4, E10.4, A10)	INP 9300
9210 FORMAT (11(E10.4, I3))	INP 9310
9220 FORMAT (' Surface Chemistry input for ',A)	INP 9320
9230 FORMAT (2X, 3(E12.4, 2X), 3X, I3)	INP 9330
9240 FORMAT (2X, 3(E10.4, 2X), 3X, I3)	INP 9340
9250 FORMAT (2X, A10, 6X, I3, 4X, E10.4)	INP 9350
9260 FORMAT (4X, F10.4, 3X, A, 4(5(5X, E12.5, 2X, I3), /))	INP 9360
9270 FORMAT (2I4,E10.4)	INP 9370
9280 FORMAT (I4,F12.0)	INP 9380
9290 FORMAT (I4, 2E10.4, A80)	INP 9390

9300	FORMAT (8I2, A80)	INP 9400
9310	FORMAT (' FLAG FOR ACTIVITY COEFF OF NEUTRAL SPECIES: ', I2, /,	INP 9410
.	' FLAG FOR ACTIVITY COEFF BY PITZERS EQUATIONS: ', I2)	INP 9420
9320	FORMAT (' FLAGS FOR CALCULATING REDOX SPECIES: ', /,	INP 9430
.	6(2X, A2), /,	INP 9440
.	6(2X, I2))	INP 9450
9330	FORMAT (' TOLERANCE FACTORS: ', 2X, 'CONV1 = ', E12.4, 2X,	INP 9460
.	'CONV2 = ', E12.4)	INP 9470
9340	FORMAT (' LOG KT TO BE CHANGED AT TEMP = ', F6.2)	INP 9480
9350	FORMAT (' PRINTING OPTIONS:')	INP 9490
9360	FORMAT (2E10.4, I2, E10.4, A8)	INP 9500
9370	FORMAT (I2, 3E10.4, A8)	INP 9510
9380	FORMAT (1X, A8, 4X, E10.4, 2X, E10.4, 6X, I4, 4X, E10.4)	INP 9520
9390	FORMAT (1X, A8, 4X, I4, 4X, E10.4, 2X, E10.4, 2X, E10.4)	INP 9530
9400	FORMAT (4X, 'NAME', 4X, 'INDEX', 5X, 'LOWKT', 7X, 'HIGHKT',	INP 9540
.	6X, 'DHA ')	INP 9550
9410	FORMAT (2X, I4, 2X, E10.4)	INP 9560
9420	FORMAT (' MINERAL TO BE DISSOLVED/PRECIPITATED TO SATURATION:',	INP 9570
.	' ', A8, 5X, ' Index number: ', I3)	INP 9580
9430	FORMAT (' MINERAL TO BE DISSOLVED/PRECIPITATED:', 15X,	INP 9590
.	A8, 5X, ' Index number: ', I3)	INP 9600
9440	FORMAT (' REACTION FOR SATURATION: ', 3X, 'ID#', 3X,	INP 9610
.	'Species ', 5X, 'STOICH COEFF')	INP 9620
9450	FORMAT (' Step direction/scaling factor = ', E12.5)	INP 9630
9460	FORMAT (' ', 29X, I3, 3X, A8, 5X, E12.5)	INP 9640
9470	FORMAT (' FRACTION OF BOILING: ', F12.4)	INP 9650
9480	FORMAT (1X, ' Number of mixtures = ', I3, ' starting at',	INP 9660
.	' fraction of solution one = ', F12.4,	INP 9670
.	' using a step increment of: ', F12.4)	INP 9680
9481	FORMAT (1X, ' and reading the second water composition from',	INP 9690
.	' the file ', A)	INP 9700
9482	FORMAT (1X, ' and reading the second water composition from',	INP 9710
.	' /, ' the data set following this one. ')	INP 9720
9490	FORMAT (3X, A8, 5X, E12.5)	INP 9730
9500	FORMAT (3X, A4, 8X, A4, 8X, A3, 8X, A6, 8X, A3)	INP 9740
9510	FORMAT (2I2, 3E10.4, A8)	INP 9750
9520	FORMAT (3X, A4, 7X, A6, 5X, A3, 5X, A3, 5X, A4)	INP 9760
9530	FORMAT (1X, A8, 5X, I2, 5X, F4.1, 5X, F8.3, 5X, 1P, E10.4)	INP 9770
9540	FORMAT (3X, A6, 7X, A3, 5X, A5, 5X, A5)	INP 9780
9550	FORMAT (I2, 3E10.4, A8)	INP 9790
9560	FORMAT (1X, I2, 2X, A8, 3(5X, E10.4))	INP 9800
9570	FORMAT (3E10.4, A8)	INP 9810
9580	FORMAT (1X, A8, 5X, A14, F7.2, 5X, A14, F7.2)	INP 9820
9590	FORMAT (1X, 9(F5.2, A1, A8, A3))	INP 9830
9600	FORMAT (5I2, A80)	INP 9840
9610	FORMAT (' Restart information will be written to the file ',	INP 9850
.	A)	INP 9860
9710	FORMAT (' Because the Mixing option was chosen in the previous'	INP 9870
.	' data set, ', /,	INP 9880
.	' the DISSOLUTION/PRECIPITATION option will not be',	INP 9890
.	' performed on this data set.')	INP 9900
9720	FORMAT (' Because the Mixing option was chosen in the previous'	INP 9910
.	' data set, ', /,	INP 9920
.	' the MIXING information will not be read from this'	INP 9930
.	' data set.')	INP 9940
9730	FORMAT (' Because the Mixing option was chosen in the previous'	INP 9950
.	' data set, ', /,	INP 9960
.	' the BOILING option will not be performed on this data',	INP 9970

END ' set.')

INP 9980
INP 9990

	SUBROUTINE INTIAL (OK, ALK, INFORM, RATIO, GAMMA, TEMP, HITEMP,	INT 0010
	PRESS, HTOTI, OHTOTI, ICO2, IMCO3, IBMIX,	INT 0020
	FCCSAT, IEXCH, ISAT, IPHNUM, JCCST)	INT 0030
C	=====	INT 0040
C	This routine initializes certain values when each new data	INT 0050
C	set is read into solmneqf.	INT 0060
C	-----	INT 0070
C	ALFA DBL Activity of aqueous species i	INT 0080
C	ALK INT Flag for distribution of carbonate species	INT 0090
C	CEC DBL Cation exchange capacity	INT 0100
C	COEF DBL Stoichiometric coefficient and Id number	INT 0110
C	CUNITS DBL Analytical input concentration	INT 0120
C	DCH4 DBL Concentration of CH4 lost up annulus	INT 0130
C	DDCH4 DBL Concentration of CH4 lost before pH measurement	INT 0140
C	DCO2 DBL Concentration of CO2 lost up annulus	INT 0150
C	DDCO2 DBL Concentration of CO2 lost before pH measurement	INT 0160
C	DH2S DBL Concentration of H2S lost up annulus	INT 0170
C	DDH2S DBL Concentration of H2S lost before pH measurement	INT 0180
C	DNH3 DBL Concentration of NH3 lost up annulus	INT 0190
C	DDNH3 DBL Concentration of NH3 lost before pH measurement	INT 0200
C	DSEP DBL Density of oil at 15 degree C	INT 0210
C	FCCSAT DBL Tolerance factor for pH and CO2 options	INT 0220
C	GAMMA DBL Activity coefficient	INT 0230
C	HITEMP DBL In-situ temperature	INT 0240
C	HTOTI DBL Sum of H in system	INT 0250
C	I INT Loop counting variable	INT 0260
C	IBMIX INT Switch for mixing option	INT 0270
C	ICO2 INT Switch for co2 option	INT 0280
C	IEXCH INT Switch for exchange/adsorption option	INT 0290
C	IMCO3 INT Selects CO2 option	INT 0300
C	INFORM INT Flag to print all the log K values in data base	INT 0310
C	IOPT INT Switch for CO2 option	INT 0320
C	IPHASE INT Gas/Oil/Water gas redistribution	INT 0330
C	IPHNUM INT Counter used in PHCALC	INT 0340
C	IRXDP INT Id number of the aqueous species to be added	INT 0350
C	ISAT INT Counter used in CO2OPT	INT 0360
C	JCCST INT Switch indicating if PHOPT called 1s5 time	INT 0370
C	JCO3 INT Switch to control printing of some headings	INT 0380
C	KT1 DBL Equilibrium constant of the aqueous reactions	INT 0390
C	M DBL Calculated molality of aqueous species	INT 0400
C	MBASE DBL Equivalence Mole Fraction (initial) on surface	INT 0410
C	NDUM INT Id of mineral/aqueous complex with K(T) changed	INT 0420
C	NMAX INT General array dimension to allow easy expansion	INT 0430
C	ODUM CHA Switch to indicate a mineral/aqueous complex	INT 0440
C	OHTOTI DBL Sum of hydroxide in system	INT 0450
C	OK INT Error flag for Lagrange interpolation routine	INT 0460
C	PHHIT INT Switch for ph iteration	INT 0470
C	PPHHIT INT Switch for ph iterations	INT 0480
C	PRESS DBL Total pressure	INT 0490
C	RATIO INT Flag for printing activity ratios of elements	INT 0500
C	RXDP DBL Molal amount of the aqueous species added	INT 0510

C	SCO2	DBL	Sum of CO2 species	INT 0520
C	TAREA	DBL	Site density per unit area	INT 0530
C	TCH4M	DBL	Moles CH4 distributed between oil, water, vapor	INT 0540
C	TCO2M	DBL	Moles CO2 distributed between oil, water, vapor	INT 0550
C	TEMP	DBL	Temperature of the solution when pH was measured	INT 0560
C	TH2SM	DBL	Moles H2S distributed between oil, water, vapor	INT 0570
C	XDUM	DBL	New log K(T) value	INT 0580
C	-----			INT 0590
				INT 0600
	INTEGER NMAX			INT 0610
	PARAMETER (NMAX = 340)			INT 0620
				INT 0630
	INTEGER ALK, I, IBMIX, ICO2, IDDP, IDN(10,10), IDSAT, IEXCH			INT 0640
	INTEGER IMCO3, INFORM, INSP, IPHASE, IPHNUM, IOPT, IRXDP(10)			INT 0650
	INTEGER ISAT, ISCHG(10), ISCOMP(10), JCO3, NDUM(12), OK			INT 0660
	INTEGER PHHIT, PPHIT, RATIO			INT 0670
				INT 0680
	CHARACTER * 1 ODUM(12)			INT 0690
				INT 0700
	DOUBLE PRECISION ALFA(NMAX), ANALM(NMAX), CEC, COEF(10,10)			INT 0710
	DOUBLE PRECISION CUNITS(NMAX), DCH4, DDCH4, DCO2, DDCO2			INT 0720
	DOUBLE PRECISION DH2S, DDH2S, DNH3, DDNH3, DP, FCCSAT, FIXIT			INT 0730
	DOUBLE PRECISION GAMMA(NMAX), HITEMP, HTOT, HTOTI, JCCST			INT 0740
	DOUBLE PRECISION KCH4OL, KCO2OL, KH2SOL, KRXN(10)			INT 0750
	DOUBLE PRECISION KT1(NMAX), M(NMAX), MBASE(10)			INT 0760
	DOUBLE PRECISION OHTOT, OHTOTI, PH, PRESS, DSEP, RXDP(10)			INT 0770
	DOUBLE PRECISION SAREA, SCO2, TAREA, TCH4M, TCO2M, TH2SM			INT 0780
	DOUBLE PRECISION TEMP, WROIL, XDUM(12)			INT 0790
				INT 0800
	COMMON /AL / NDUM, XDUM			INT 0810
	COMMON /CH / ODUM			INT 0820
	COMMON /DIST / TCO2M, TCH4M, TH2SM, WROIL, KCH4OL, KCO2OL,			INT 0830
	KH2SOL, IPHASE, DSEP			INT 0840
	COMMON /EXCHAN/ COEF, MBASE, KRXN, CEC, TAREA, SAREA, IDN,			INT 0850
	ISCHG, ISCOMP, INSP			INT 0860
	COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,			INT 0870
	DCH4, DDCH4, IOPT, FIXIT			INT 0880
	COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS			INT 0890
	COMMON /SAT / IDDP, IDSAT, DP, RXDP, IRXDP			INT 0900
	COMMON /TTK / KT1			INT 0910
	COMMON /ZPH / PHHIT, PPHIT, JCO3, SCO2, HTOT, OHTOT			INT 0920
				INT 0930
C	-----			INT 0940
				INT 0950
	IF (IBMIX .LE. 0) THEN			INT 0960
	DO 10 I = 1, 12			INT 0970
	ODUM(I) = ' '			INT 0980
	NDUM(I) = 0			INT 0990
	XDUM(I) = 0.0D0			INT 1000
10	CONTINUE			INT 1010
				INT 1020
	DO 20 I = 1, NMAX			INT 1030
	KT1(I) = 0.0D0			INT 1040
20	CONTINUE			INT 1050
				INT 1060
				INT 1070
	JCCST = 0			INT 1080
	PHHIT = 0			INT 1090

INFORM = 0	INT 1100
HITEMP = 0.0D0	INT 1110
OHTOTI = 0.0D0	INT 1120
ALK = 0	INT 1130
TEMP = 0.0D0	INT 1140
HTOTI = 0.0D0	INT 1150
RATIO = 0	INT 1160
PRESS = 0.0D0	INT 1170
END IF	INT 1180
	INT 1190
IPHNUM = 0	INT 1200
OK = 0	INT 1210
DDCO2 = 0.0D0	INT 1220
DDH2S = 0.0D0	INT 1230
DDNH3 = 0.0D0	INT 1240
DDCH4 = 0.0D0	INT 1250
DCO2 = 0.0D0	INT 1260
DH2S = 0.0D0	INT 1270
DNH3 = 0.0D0	INT 1280
DCH4 = 0.0D0	INT 1290
IOPT = 0	INT 1300
ICO2 = 0	INT 1310
IMCO3 = 0	INT 1320
FCCSAT = 0.05D0	INT 1330
TCO2M = 0.0D0	INT 1340
TCH4M = 0.0D0	INT 1350
TH2SM = 0.0D0	INT 1360
IPHASE = 0	INT 1370
DSEP = 0.0D0	INT 1380
PPHHIT = 0	INT 1390
JCO3 = 0	INT 1400
ISAT = 0	INT 1410
IEXCH = 0	INT 1420
CEC = 0.0D0	INT 1430
TAREA = 0.0D0	INT 1440
	INT 1450
DO 40 I = 1, NMAX	INT 1460
CUNITS(I) = 0.0D0	INT 1470
M(I) = 0.0D0	INT 1480
ALFA(I) = 0.0D0	INT 1490
GAMMA(I) = 1.0D0	INT 1500
40 CONTINUE	INT 1510
	INT 1520
DO 50 I = 1, 10	INT 1530
RXDP(I) = 0.0	INT 1540
IRXDP(I) = 0	INT 1550
50 CONTINUE	INT 1560
	INT 1570
RETURN	INT 1580
END	INT 1590

	DOUBLE PRECISION FUNCTION KHCH4 (TK, MNACLD, P)	KH4 0010
C	=====	KH4 0020
C	Calculates the henry's law coefficient for methane	KH4 0030


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C -----|KH4 0040
C   MNACLD   DBL   Sum of Molality * charge / 2      |KH4 0050
C   P        DBL   Partial pressure of methane       |KH4 0060
C   TK        DBL   Temperature in kelvin            |KH4 0070
C -----|KH4 0080
C   DOUBLE PRECISION MNACLD, TK, P                    |KH4 0090
C   INTRINSIC DEXP                                    |KH4 0100
C                                                     |KH4 0110
C =====|KH4 0120
C                                                     |KH4 0130
C   KHCH4 = 26.187D0 + (0.13647D-2 * P)                |KH4 0140
C   .      - (26.991D-3 * TK) + (11.69D-2 * MNACLD)    |KH4 0150
C   .      - (3380.7D0 / TK) - (24.09D-2 / MNACLD)     |KH4 0160
C   .      - (27.79D-2 / P) + (19.19D-5 * P / MNACLD)  |KH4 0170
C   .      - (14.28D-2 * P / TK) + (27.78D-5 * TK * MNACLD) |KH4 0180
C                                                     |KH4 0190
C   KHCH4 = DEXP(KHCH4)                                |KH4 0200
C                                                     |KH4 0210
C   RETURN                                             |KH4 0220
C   END                                               |KH4 0230

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DOUBLE PRECISION FUNCTION KHCO2 (T, MU)                KHC 0010
C =====|KHC 0020
C   Calculates the henry's law coefficient for CO2      |KHC 0030
C -----|KHC 0040
C   MU        DBL   Ionic strength of solution         |KHC 0050
C   T         DBL   Temperature in kelvin              |KHC 0060
C -----|KHC 0070
C   DOUBLE PRECISION MU, T                              |KHC 0080
C   INTRINSIC DEXP, DLOG                                |KHC 0090
C                                                     |KHC 0100
C =====|KHC 0110
C                                                     |KHC 0120
C   KHCO2 = 20.244D0 - (0.016323D0 * T)                |KHC 0130
C   .      - (1.0312D0 * MU) - (3629.7 / T)             |KHC 0140
C   .      + (0.4445D0 / MU) + (0.12806D-2 * T * MU)    |KHC 0150
C   .      + (255.90D0 * MU / T) - (0.16060D-2 * T / MU) |KHC 0160
C                                                     |KHC 0170
C   KHCO2 = DEXP(KHCO2)                                |KHC 0180
C                                                     |KHC 0190
C   RETURN                                             |KHC 0200
C   END                                               |KHC 0210

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DOUBLE PRECISION FUNCTION KHH2S (TK, M1)              KHH 0010
C =====|KHH 0020
C   Calculates the henry's law coefficient for H2S      |KHH 0030
C -----|KHH 0040
C   M1        DBL   Sum of Molality * charge / 2      |KHH 0050
C   TK        DBL   Temperature in kelvin              |KHH 0060
C -----|KHH 0070

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DOUBLE PRECISION TK, M1	KHH 0080
INTRINSIC DEXP	KHH 0090
	KHH 0100
	KHH 0110
C =====	KHH 0120
KHH2S = 11.416D0	KHH 0130
- (0.007013D0 * TK)	KHH 0140
+ (0.2905D0 * M1)	KHH 0150
- (2067.7D0 / TK)	KHH 0160
+ (.5705D0 / M1)	KHH 0170
- (.0001574D0 * TK * M1)	KHH 0180
- (46.20D0 * M1 / TK)	KHH 0190
- (.001777D0 * TK / M1)	KHH 0200
	KHH 0210
KHH2S = DEXP(KHH2S)	KHH 0220
RETURN	
END	

DOUBLE PRECISION FUNCTION KHNH3 (TK)	KHN 0010
C =====	KHN 0020
C Calculates the henry's law coefficient for ammonia	KHN 0030
C -----	KHN 0040
C TK DBL Temperature in kelvin	KHN 0050
C -----	KHN 0060
	KHN 0070
DOUBLE PRECISION TK	KHN 0080
INTRINSIC DLOG	KHN 0090
	KHN 0100
C =====	KHN 0110
KHNH3 = -1816.602D0/TK + 2.27770D0 * DLOG(TK) - 73.0179D-4 * TK	KHN 0120
- 6.4609	KHN 0130
	KHN 0140
KHNH3 = 10.0D0**KHNH3	KHN 0150
	KHN 0160
	KHN 0170
RETURN	KHN 0180
END	KHN 0190

SUBROUTINE LAGINT (XT, YT, X, Y, MAXK, NDIM, OK)	LAG 0010
C =====	LAG 0020
C Lagrange interpolation routine.	LAG 0030
C -----	LAG 0040
C Variables	LAG 0050
C -----	LAG 0060
C C DBL Calculates the interpolation constants	LAG 0070
C CPUMAX DBL Largest positive real value program uses	LAG 0080
C CPUMIN DBL Smallest positive real value program uses	LAG 0090
C DIF INT Difference between upper and lower bound	LAG 0100
C I INT Loop counting variable	LAG 0110
C K INT Fixes the interpolation range	LAG 0120
C LO INT Finds lower bound of interpolation range	LAG 0130
C MAXK INT Total number of values to be found	LAG 0140

C	MID	INT	Finds midpoint of interpolation range	LAG 0150
C	N	INT	Number of temperature points	LAG 0160
C	NDIM	INT	Identifies array dimension	LAG 0170
C	OK	INT	Error flag for Lagrange interpolation routine	LAG 0180
C	UNO	INT	File unit assigned for output file	LAG 0190
C	UP	INT	Finds upper bound of interpolation range	LAG 0200
C	W	DBL	Holds temperature values around point of interest	LAG 0210
C	X	DBL	The temperature point of interest	LAG 0220
C	XT	DBL	Array of temperature values	LAG 0230
C	Y	DBL	Final interpolated values at given temperature	LAG 0240
C	YT	DBL	Data array holding values for temperature point	LAG 0250
C	-----			LAG 0260
	INTEGER UNO			LAG 0270
	DOUBLE PRECISION CPUMIN			LAG 0280
	PARAMETER (UNO = 6, CPUMIN = 1.0D-35)			LAG 0290
				LAG 0300
	INTEGER DIF, I, K, LO, MAXK, MID, N, NDIM, OK, UP			LAG 0310
				LAG 0320
	DOUBLE PRECISION C(4), W(10), X, XT(11), Y(NDIM), YT(NDIM,11)			LAG 0330
				LAG 0340
	INTRINSIC DABS			LAG 0350
				LAG 0360
				LAG 0370
C	=====			LAG 0380
	N = 11			LAG 0390
	LO = 1			LAG 0400
	UP = N			LAG 0410
	MID = 1			LAG 0420
				LAG 0430
				LAG 0440
	DO 10 I = 1, MAXK			LAG 0450
	Y(I) = 0.0			LAG 0460
10	CONTINUE			LAG 0470
				LAG 0480
	IF (X.GT.XT(N) .OR. X.LT.XT(1)) GO TO 90			LAG 0490
	OK = 1			LAG 0500
				LAG 0510
20	CONTINUE			LAG 0520
	DIF = UP - LO			LAG 0530
	IF (DIF .LE .2) GO TO 30			LAG 0540
	MID = (UP + LO + 1) / 2			LAG 0550
	GO TO 40			LAG 0560
				LAG 0570
30	CONTINUE			LAG 0580
	IF (DIF .EQ. 0) GO TO 70			LAG 0590
	MID = LO + 1			LAG 0600
				LAG 0610
40	CONTINUE			LAG 0620
	IF ((DABS(X-XT(MID))) .LT. CPUMIN) GO TO 70			LAG 0630
	IF ((X-XT(MID)) .LT. 0.0D0) GO TO 50			LAG 0640
				LAG 0650
C	-----			LAG 0660
C	X > XT(MID)			LAG 0670
C	-----			LAG 0680
				LAG 0690
	LO = MID			LAG 0700
	GO TO 20			LAG 0710
				LAG 0720

50 CONTINUE	LAG 0730
IF ((DABS(X-XT(MID-1))) .GT. CPUMIN) GO TO 60	LAG 0740
	LAG 0750
C -----	LAG 0760
C X = XT(MID-1)	LAG 0770
C -----	LAG 0780
	LAG 0790
MID = MID - 1	LAG 0800
GO TO 70	LAG 0810
	LAG 0820
60 CONTINUE	LAG 0830
IF ((XT(MID-1)-X) .LT. CPUMIN) GO TO 70	LAG 0840
	LAG 0850
C -----	LAG 0860
C X < XT(MID-1)	LAG 0870
C -----	LAG 0880
	LAG 0890
UP = MID	LAG 0900
GO TO 20	LAG 0910
	LAG 0920
70 CONTINUE	LAG 0930
K = MID - 2	LAG 0940
IF (K .LT. 1) K = 1	LAG 0950
IF ((K+3) .GT. N) K = N - 3	LAG 0960
	LAG 0970
W(1) = X - XT(K)	LAG 0980
W(2) = X - XT(K+1)	LAG 0990
W(3) = X - XT(K+2)	LAG 1000
W(4) = X - XT(K+3)	LAG 1010
W(5) = XT(K) - XT(K+1)	LAG 1020
W(6) = XT(K) - XT(K+2)	LAG 1030
W(7) = XT(K) - XT(K+3)	LAG 1040
W(8) = XT(K+1) - XT(K+2)	LAG 1050
W(9) = XT(K+1) - XT(K+3)	LAG 1060
W(10) = XT(K+2) - XT(K+3)	LAG 1070
	LAG 1080
DO 80 I = 1, MAXK	LAG 1090
C(1) = YT(I,K) / (W(5) * W(6) * W(7))	LAG 1100
C(2) = -YT(I,K+1) / (W(5) * W(8) * W(9))	LAG 1110
C(3) = YT(I,K+2) / (W(6) * W(8) * W(10))	LAG 1120
C(4) = -YT(I,K+3) / (W(7) * W(9) * W(10))	LAG 1130
	LAG 1140
Y(I) = C(1) * W(2) * W(3) * W(4) + C(2) * W(1) * W(3) * W(4) +	LAG 1150
C(3) * W(1) * W(2) * W(4) + C(4) * W(1) * W(2) * W(3)	LAG 1160
80 CONTINUE	LAG 1170
	LAG 1180
RETURN	LAG 1190
	LAG 1200
C -----	LAG 1210
C Error messages	LAG 1220
C -----	LAG 1230
90 CONTINUE	LAG 1240
OK = 0	LAG 1250
	LAG 1260
IF (X .GT. XT(N)) WRITE (UNO, 100) X, XT(N)	LAG 1270
	LAG 1280
100 FORMAT (//, ' ', 'X-OUT IN LAGINT X=', E13.6, 2X, 'XT(N)=', E13.6)	LAG 1290
	LAG 1300

IF (X .LT. XT(1)) WRITE (UNO, 110) X, XT(1)	LAG 1310
110 FORMAT (//, ' ', 'X-OUT IN LAGINT X=', E13.6, 2X, 'XT(1)=', E13.6)	LAG 1320
	LAG 1330
RETURN	LAG 1340
END	LAG 1350

INTEGER FUNCTION LENGTH (STRING)	LEN 0010
C =====	LEN 0020
C Returns the length of the non-blank portion of a character	LEN 0030
C variable	LEN 0040
C -----	LEN 0050
C L INT Length pointer	LEN 0060
C STRING CHA Variable for which the length is to be determined	LEN 0070
C -----	LEN 0080
INTEGER L	LEN 0090
CHARACTER * 80 STRING	LEN 0100
	LEN 0110
C =====	LEN 0120
L = 80	LEN 0130
	LEN 0140
	LEN 0150
10 CONTINUE	LEN 0160
IF (L .GT. 1 .AND. STRING(L:L) .EQ. ' ') THEN	LEN 0170
L = L - 1	LEN 0180
GO TO 10	LEN 0190
END IF	LEN 0200
	LEN 0210
IF (STRING(L:L) .NE. ' ') THEN	LEN 0220
LENGTH = L	LEN 0230
ELSE	LEN 0240
LENGTH = 1	LEN 0250
END IF	LEN 0260
	LEN 0270
RETURN	LEN 0280
	LEN 0290
END	LEN 0300

SUBROUTINE MIXER (TEMP, M1, PRESS, DENS, ICALL, ISALT, IRUN,	MIX 0010
MXSP, FCCSAT, PH2O, IPRIN2, MXMNK)	MIX 0020
C =====	MIX 0030
C Precipitation/dissolution, Mixing, and Boiling options	MIX 0040
C -----	MIX 0050
C A1MIX DBL HTOT, OHTOT, TIC of first solution/original water	MIX 0060
C ADD DBL The amount of material being added/subtracted	MIX 0070
C ADDMIN DBL Record of the amount of mineral added	MIX 0080
C ADENS DBL Density of first water in mixing	MIX 0090
C ALFA DBL Activity of aqueous species i	MIX 0100
C AMOL DBL Amount in moles to be added	MIX 0110
C ANALM DBL Analyzed molality of species i	MIX 0120
C ANMMIX DBL Stored values for first water	MIX 0130

C	ATEMP	DBL	Temperature of solution A	MIX 0140
C	B2MIX	DBL	HTOT, OHTOT, TIC of second water	MIX 0150
C	BDENS	DBL	Density of second water in mixing	MIX 0160
C	BNMMIX	DBL	Stored values for second water	MIX 0170
C	BTEMP	DBL	Temperature of solution B	MIX 0180
C	BUFFER	CHA	Buffer for Character manipulation	MIX 0190
C	COFFAC	DBL	Component Coef. for dissolving phase	MIX 0200
C	CPUMIN	DBL	Smallest positive real value program uses	MIX 0210
C	CROSS	LOG	Have we crossed the root yet?	MIX 0220
C	DELTA	DBL	Temperary storage to find min. component	MIX 0230
C	DENS	DBL	Density	MIX 0240
C	DFRAC1	DBL	Smallest fraction of soln 1 mixed with soln 2	MIX 0250
C	DIF	DBL	Difference used in testing	MIX 0260
C	DINC	DBL	Increment of solution 1 to be added	MIX 0270
C	DONE	LOG	Are we done?	MIX 0280
C	DP	DBL	Dissolution/precipitation switch	MIX 0290
C	DUM2	CHA	Character array with names of gases	MIX 0300
C	EQC	DBL	Equivalent amount of carbon in 1 mole of comp.	MIX 0310
C	EQH	DBL	Equivalent amount of hydrogen in 1 mole of comp.	MIX 0320
C	ERROR	LOG	Is everything ok?	MIX 0330
C	EXELT	DBL	Total mass of components	MIX 0340
C	FBOIL	DBL	Fraction of solution boiled-off as steam	MIX 0350
C	FCCSAT	DBL	Tolerance factor for pH and CO2 options	MIX 0360
C	FFB	DBL	Fraction of boiling (1 / (1-fboil))	MIX 0370
C	FMIX	DBL	Mixtures to be examined	MIX 0380
C	HEQ	DBL	Coef. for H containing components	MIX 0390
C	I	INT	Loop variable	MIX 0400
C	IADD	INT	Index for positioning in adding mineral arrays	MIX 0410
C	IBOIL	INT	Index of number of boiling points stored	MIX 0420
C	IBTOT	INT	Count for number of boiling iterations	MIX 0430
C	ICALL	INT	Switch for calling this routine	MIX 0440
C	ICD	INT	Index for mineral being dissolved	MIX 0450
C	ICS	INT	Index for mineral to saturate with	MIX 0460
C	IDDP	INT	Id number of the mineral to be dissolved/ppt	MIX 0470
C	IDMIN	INT	Id number of the mineral to be dissolved/ppt	MIX 0480
C	IDMIX	INT	Id number of the aqueous species to be added	MIX 0490
C	IDSAT	INT	Id number of the mineral to be equilibrated	MIX 0500
C	IHID	INT	Index of H containing components	MIX 0510
C	INDX	INT	Index used for checking components	MIX 0520
C	INMIX	INT	Total number of mixtures of two solution mixed	MIX 0530
C	IPGLN	INT	Current line number of the output file	MIX 0540
C	IPRIN2	INT	Print switch	MIX 0550
C	IRUN	INT	Keeps track if this is first or second mixture	MIX 0560
C	IRXDP	INT	Id number of the aqueous species to be added	MIX 0570
C	ISALT	INT	Switch used in mixer to indicate option	MIX 0580
C	ISTF	INT	Temp. storage used in reading	MIX 0590
C	ITMIX	INT	Switch for the mineral saturation option	MIX 0600
C	J	INT	Loop variable	MIX 0610
C	JJ	INT	Loop variable and counter	MIX 0620
C	K	INT	Loop variable and counter	MIX 0630
C	KCH4	DBL	Henrys law coef for CH4	MIX 0640
C	KCO2	DBL	Henrys law coef for CO2	MIX 0650
C	KH2S	DBL	Henrys law coef for H2S	MIX 0660
C	KNH3	DBL	Henrys law coef for NH3	MIX 0670
C	LOGKT2	DBL	Log K for minerals at specified temperature	MIX 0680
C	M	DBL	Calculated molality of aqueous species	MIX 0690
C	M1	DBL	Sum of Molality * charge / 2	MIX 0700
C	MINDIM	INT	Parameter ... dimension of various arrays	MIX 0710

C	MINDP	LOG	Switch ... dissolving a mineral?	MIX 0720
C	MINSAT	LOG	Switch ... saturating with a mineral?	MIX 0730
C	MXMNK	INT	Total number of mineral log k values	MIX 0740
C	MXSP	INT	Total number of aqueous species	MIX 0750
C	NGAST	DBL	Values guessed for root	MIX 0760
C	NL	DBL	Number of moles in liquid	MIX 0770
C	NMAX	INT	General array dimension to allow easy expansion	MIX 0780
C	NV	DBL	Number of moles in vapour	MIX 0790
C	PAGE1	CHA	Names of aqueous species	MIX 0800
C	PAGE3	CHA	Names of solubility constants	MIX 0810
C	PH2O	DBL	Pressure of water	MIX 0820
C	PRESS	DBL	Total pressure	MIX 0830
C	R	DBL	Gas constant	MIX 0840
C	REVERS	LOG	OK to reverse direction in root finding?	MIX 0850
C	RXDP	DBL	Molal amount of the aqueous species added	MIX 0860
C	SIMIN	DBL	SI of mineral being saturated with. Tested.	MIX 0870
C	STEP	DBL	Amount of volatile to add/remove from liquid	MIX 0880
C	STEPSZ	DBL	Scaling factor (parameter) in diss/ppt minerals	MIX 0890
C	STF	DBL	Temp. storage used in reading	MIX 0900
C	STOFAC	DBL	Stoich. Coef. for material being added/removed	MIX 0910
C	TEMP	DBL	Current temperature	MIX 0920
C	TITMIX	CHA	Title for mixtures	MIX 0930
C	TITR	DBL	Iteration array in DISTRB, used for guesses	MIX 0940
C	TK	DBL	Temperature in K	MIX 0950
C	TOF	CHA	Places a form feed in output file	MIX 0960
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	MIX 0970
C	TRY	DBL	Next amount of volitiles in h2o (used in boiling)	MIX 0980
C	UNO	INT	File unit assigned for output file	MIX 0990
C	UNR	INT	Unit to read data file	MIX 1000
C	VDEN	DBL	Vapour density	MIX 1010
C	VRCH4	DBL	Volatility ratio for CH4	MIX 1020
C	VRCO2	DBL	Volatility ratio for CO2	MIX 1030
C	VRH2S	DBL	Volatility ratio for H2S	MIX 1040
C	VRNH3	DBL	Volatility ratio for NH3	MIX 1050
C	VRT	DBL	Used in calculated volatility ratio	MIX 1060
C	X	DBL	Temperary storage	MIX 1070
C	-----			MIX 1080
	INTEGER MINDIM, NMAX, UNO, UNR			MIX 1090
	DOUBLE PRECISION CPUMIN, R, STEPSZ			MIX 1100
	PARAMETER (MINDIM = 20, NMAX = 340, UNO = 6, UNR = 12)			MIX 1110
	PARAMETER (CPUMIN = 1.0D-35, R = 83.14241D-3, STEPSZ = 1.0D-02)			MIX 1120
				MIX 1130
				MIX 1140
C	-----			MIX 1150
C	R is 83.15 (bar cm**3 / deg mole) times divided by 1000			MIX 1160
C	(1 kg water). The density of the gas is in cm**3/gram, hense			MIX 1170
C	55.51 is implied.			MIX 1180
C	-----			MIX 1190
				MIX 1200
	INTEGER I, IADD, IBOIL, IBTOT, ICALL, ICD, ICS			MIX 1210
	INTEGER IDDP, IDMIX(50), IDMIN(10), IDSAT, IDSP(10)			MIX 1220
	INTEGER IHID(10), INDX, INMIX, IPAGE, IPGLN, IPRIN2			MIX 1230
	INTEGER IRUN, IRXDP(10), ISALT, ISTF(10), ITMIX			MIX 1240
	INTEGER J, JJ, K, MXMNK, MXSP			MIX 1250
				MIX 1260
	LOGICAL DONE, MINSAT, MINDP, ERROR, CROSS, REVERS			MIX 1270
				MIX 1280
	CHARACTER * 1 TOF, CR			MIX 1290

CHARACTER * 5 DUM2(4)	MIX 1300
CHARACTER * 8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)	MIX 1310
CHARACTER * 40 TITMIX, BUFFER	MIX 1320
	MIX 1330
DOUBLE PRECISION ATCPRD, ADD, ADMIN(MINDIM), ADENS, ALFA(NMAX)	MIX 1340
DOUBLE PRECISION AMOL(50), ANALM(NMAX), ANMMIX(NMAX), ATEMP	MIX 1350
DOUBLE PRECISION AIMIX(5), BDENS, BNMMIX(NMAX), BTEMP, B2MIX(5)	MIX 1360
DOUBLE PRECISION COFFAC(10), CUNITS(NMAX)	MIX 1370
DOUBLE PRECISION DELTA, DENS, DFRAC1, DIF(4,9), DINC, DP	MIX 1380
DOUBLE PRECISION EQC, EQH, EXELT(35)	MIX 1390
DOUBLE PRECISION FBOIL, FCCSAT, FFB, FMIX(10)	MIX 1400
DOUBLE PRECISION HEQ(10), LOGKT1(NMAX), LOGKT2(NMAX)	MIX 1410
DOUBLE PRECISION KCH4, KHCH4, KCO2, KHCO2, KH2S, KHH2S	MIX 1420
DOUBLE PRECISION KNH3, KHNH3, M(NMAX), M1, NGAST(9), NL(4), NV(4)	MIX 1430
DOUBLE PRECISION PH, PH2O, PRESS, RXDP(10)	MIX 1440
DOUBLE PRECISION SIMIN(MINDIM), STEP(4), STF(10), STOFAC(10)	MIX 1450
DOUBLE PRECISION TEMP, TITR(11), TK, TOTEL(5), TRY(4,9)	MIX 1460
DOUBLE PRECISION VDEN, VRT, VRCH4, VRCO2, VRH2S, VRNH3, X	MIX 1470
	MIX 1480
EXTERNAL ATCPRD, DPVT, GUESS, KHCH4, KHCO2, KHH2S, KHNH3, SORTA	MIX 1490
EXTERNAL PAGE	MIX 1500
	MIX 1510
INTRINSIC DABS, INDEX, LEN, MIN	MIX 1520
	MIX 1530
COMMON /ALOGK / LOGKT1, LOGKT2	MIX 1540
COMMON /AMM / IDMIX, AMOL, ITMIX, INMIX, DFRAC1, DINC, FBOIL	MIX 1550
COMMON /EXTOT / EXELT, TOTEL, TITR	MIX 1560
COMMON /FMFD / TOF, CR, TITMIX	MIX 1570
COMMON /FORM / IPAGE, IPGLN	MIX 1580
COMMON /MM / ANMMIX, AIMIX, B2MIX, FMIX, BNMMIX, ADENS, BDENS, ATEMP, BTEMP	MIX 1590
	MIX 1600
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	MIX 1610
COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	MIX 1620
COMMON /SAT / IDDP, IDSAT, DP, RXDP, IRXDP	MIX 1630
	MIX 1640
SAVE ADMIN, COFFAC, CROSS, DIF, DONE	MIX 1650
SAVE IADD, IBOIL, IBTOT, ICS, ICD, IDMIN, IDSP	MIX 1660
SAVE MINDP, MINSAT, NGAST, NL, NV, REVERS, SIMIN, STEP, STOFAC	MIX 1670
SAVE TRY, VRCH4, VRCO2, VRH2S, VRNH3	MIX 1680
	MIX 1690
DATA HEQ /1.0, 1.0, -1.0, 4.0, 2.0, -3.0, -1.0, 2.0, 1.0, 0.0/	MIX 1700
DATA IHID / 7, 8, 9, 12, 28, 31, 32, 33, 49, 0/	MIX 1710
DATA DUM2 /' CO2', ' NH3', ' H2S', ' CH4'/	MIX 1720
	MIX 1730
C =====	MIX 1740
	MIX 1750
C -----	MIX 1760
C Store solution parameters if first call	MIX 1770
C totel: (1) = htot; (2) = ohtot; (3) = tic	MIX 1780
C -----	MIX 1790
	MIX 1800
IF (ICALL .EQ. 1) THEN	MIX 1810
DO 10 I = 1, 5	MIX 1820
AIMIX(I) = TOTEL(I)	MIX 1830
10 CONTINUE	MIX 1840
	MIX 1850
DO 20 I = 1, MXSP + 44	MIX 1860
ANMMIX(I) = ANALM(I)	MIX 1870

20	CONTINUE	MIX 1880
		MIX 1890
	ADENS = DENS	MIX 1900
	ATEMP = TEMP	MIX 1910
	END IF	MIX 1920
		MIX 1930
C	-----	MIX 1940
C	icall = 1; isalt = 0 -- first call for mixing two solutions	MIX 1950
C	icall = 1; isalt = 1 -- first call for mixing species	MIX 1960
C	icall = 1; isalt = 2 -- first call for boiling a solution	MIX 1970
C	icall = 1; isalt = 3 -- first call for diss/precip. of a mineral	MIX 1980
C	-----	MIX 1990
		MIX 2000
	IF (ICALL .EQ. 1 .AND. ISALT .EQ. 0) THEN	MIX 2010
	IF (IPGLN .GT. 55) CALL PAGE	MIX 2020
	IPGLN = IPGLN + 4	MIX 2030
	WRITE (UNO,1250)	MIX 2040
	IRUN = 1	MIX 2050
	RETURN	MIX 2060
	ELSE IF (ICALL .EQ. 1 .AND. ISALT .EQ. 1 .AND. ITMIX .GT. 0) THEN	MIX 2070
	IF (IPGLN .GT. (59-8-ITMIX)) CALL PAGE	MIX 2080
	IPGLN = IPGLN + 5	MIX 2090
	WRITE (UNO, 1070)	MIX 2100
	DO 40 I = 1, ITMIX	MIX 2110
	INDX = IDMIX(I)	MIX 2120
	IF (INDX .EQ. 11) INDX = 12	MIX 2130
	EQH = 0.0D00	MIX 2140
	DO 30 J = 1,9	MIX 2150
	IF (INDX .EQ. IHID(J)) EQH = HEQ(J)	MIX 2160
30	CONTINUE	MIX 2170
	IF (DABS(EQH) .GT. CPUMIN) TOTEL(1) = TOTEL(1) +	MIX 2180
	(EQH * AMOL(I))	MIX 2190
		MIX 2200
	EQC = 0.0	MIX 2210
	IF (INDX .EQ. 7) EQC = 1.0	MIX 2220
	IF (INDX .EQ. 98) EQC = 1.0	MIX 2230
	IF (INDX .EQ. 207) EQC = 1.0	MIX 2240
	IF (INDX .EQ. 208) EQC = 2.0	MIX 2250
	IF (INDX .EQ. 209) EQC = 3.0	MIX 2260
	IF (DABS(EQC) .GT. CPUMIN) TOTEL(3) = TOTEL(3) +	MIX 2270
	(EQC * AMOL(I))	MIX 2280
		MIX 2290
	ANALM(INDX) = ANALM(INDX) + AMOL(I)	MIX 2300
	IPGLN = IPGLN + 1	MIX 2310
	WRITE (UNO,1080) INDX, PAGE1(INDX), AMOL(I), EQH, EQC	MIX 2320
		MIX 2330
	IF (ANALM(INDX) .LT. 0.0 .AND. ANMMIX(INDX) .GT. 0.0) THEN	MIX 2340
	WRITE (UNO, 1100) PAGE1(INDX), AMOL(I), ANMMIX(INDX)	MIX 2350
	STOP	MIX 2360
	END IF	MIX 2370
		MIX 2380
40	CONTINUE	MIX 2390
	IPGLN = IPGLN + 3	MIX 2400
	WRITE (UNO,1090)	MIX 2410
	ICALL = 3	MIX 2420
	J = 0	MIX 2430
		MIX 2440
	DO 50 I = 1, 28	MIX 2450

J = J + 1	MIX 2460
IF (J .EQ. 8) J = 12	MIX 2470
IF (J .EQ. 17) J = 18	MIX 2480
IF (J .EQ. 19) J = 21	MIX 2490
IF (J .EQ. 24) J = 25	MIX 2500
IF (J .EQ. 34) J = 48	MIX 2510
IF (J .EQ. 49) J = 169	MIX 2520
IF (J .EQ. 170) J = 210	MIX 2530
EXELT(I) = ANALM(J)	MIX 2540
50 CONTINUE	MIX 2550
	MIX 2560
EXELT(29) = ANALM(7)	MIX 2570
EXELT(30) = ANALM(246)	MIX 2580
EXELT(31) = ANALM(265)	MIX 2590
EXELT(32) = ANALM(136)	MIX 2600
EXELT(33) = ANALM(MXSP+1)	MIX 2610
EXELT(34) = ANALM(MXSP+16)	MIX 2620
EXELT(35) = ANALM(MXSP+31)	MIX 2630
	MIX 2640
TITR(1) = EXELT(29)	MIX 2650
TITR(2) = EXELT(6)	MIX 2660
TITR(3) = EXELT(22)	MIX 2670
TITR(4) = EXELT(21)	MIX 2680
TITR(5) = EXELT(5)	MIX 2690
TITR(6) = EXELT(26)	MIX 2700
TITR(7) = EXELT(25)	MIX 2710
TITR(8) = EXELT(30)	MIX 2720
TITR(9) = EXELT(31)	MIX 2730
TITR(10) = EXELT(33)	MIX 2740
TITR(11) = EXELT(34)	MIX 2750
	MIX 2760
RETURN	MIX 2770
END IF	MIX 2780
	MIX 2790
C -----	MIX 2800
C Precipitation / dissolution of a mineral	MIX 2810
C -----	MIX 2820
	MIX 2830
C -----	MIX 2840
C On first call, read the dissolution reactions of the minerals,	MIX 2850
C one at a time, and store the one required. If we are dissolving	MIX 2860
C /ppt a fixed amount of mineral, this will be the only call.	MIX 2870
C -----	MIX 2880
	MIX 2890
C -----	MIX 2900
C The following open statement have been changed out by	MIX 2910
C Ernie Perkins (ORSD, ARC) in order to allow an command	MIX 2920
C proceedure under VMS 4.5 on DEC VAX's to assign the files	MIX 2930
C external to the program.	MIX 2940
C -----	MIX 2950
	MIX 2960
IF ((ISALT .EQ. 3 .OR. (ISALT .EQ. 1 .AND. ITMIX .LT. 0)) .AND.	MIX 2970
ICALL .EQ. 1) THEN	MIX 2980
ANMMIX(7) = TOTEL(3)	MIX 2990
OPEN (UNR, FILE = 'RXN.TBL', STATUS = 'OLD', IOSTAT = K)	MIX 3000
C OPEN (UNR, STATUS = 'OLD', shared, readonly, IOSTAT = K)	MIX 3010
IF (K .NE. 0) THEN	MIX 3020
IF (IPGLN .GE. 55) CALL PAGE	MIX 3030

IPGLN = IPGLN + 4	MIX 3040
WRITE (UNO, 1030)	MIX 3050
STOP	MIX 3060
END IF	MIX 3070
	MIX 3080
MINSAT = .FALSE.	MIX 3090
MINDP = .FALSE.	MIX 3100
IF (IDDP .EQ. 0) MINDP = .TRUE.	MIX 3110
IF (IDSAT .EQ. 0) MINSAT = .TRUE.	MIX 3120
	MIX 3130
ERROR = .FALSE.	MIX 3140
DO 80 J = 1, MXMNK	MIX 3150
READ (UNR, 1000, IOSTAT=K) I, (STF(JJ), ISTF(JJ), JJ=1,10)	MIX 3160
IF (K .NE. 0) THEN	MIX 3170
IF (IPGLN .GT. 55) CALL PAGE	MIX 3180
IPGLN = IPGLN + 5	MIX 3190
WRITE (UNO, 1040) J	MIX 3200
STOP	MIX 3210
END IF	MIX 3220
IF (.NOT. MINSAT) THEN	MIX 3230
IF (IDSAT .EQ. I) THEN	MIX 3240
MINSAT = .TRUE.	MIX 3250
ICS = 0	MIX 3260
DO 60 K = 1, 10	MIX 3270
IDSP(K) = ISTF(K)	MIX 3280
COFFAC(K) = STF(K)	MIX 3290
IF (DABS(COFFAC(K)) .GT. CPUMIN) ICS = K	MIX 3300
CONTINUE	MIX 3310
IF (STF(1) .GT. 900.) THEN	MIX 3320
ERROR = .TRUE.	MIX 3330
IF (IPGLN .GT. 56) CALL PAGE	MIX 3340
IPGLN = IPGLN + 3	MIX 3350
WRITE (UNO, 1050) PAGE3(I)	MIX 3360
END IF	MIX 3370
END IF	MIX 3380
END IF	MIX 3390
IF (.NOT. MINDP) THEN	MIX 3400
IF (IDDP .EQ. I) THEN	MIX 3410
MINDP = .TRUE.	MIX 3420
ICD = 0	MIX 3430
DO 70 K = 1, 10	MIX 3440
IDMIN(K) = ISTF(K)	MIX 3450
STOFAC(K) = STF(K)	MIX 3460
IF (DABS(STOFAC(K)) .GT. CPUMIN) ICD=K	MIX 3470
CONTINUE	MIX 3480
IF (STF(1) .GT. 900.) THEN	MIX 3490
ERROR = .TRUE.	MIX 3500
IF (IPGLN .GT. 56) CALL PAGE	MIX 3510
IPGLN = IPGLN + 3	MIX 3520
WRITE (UNO, 1050) PAGE3(I)	MIX 3530
END IF	MIX 3540
END IF	MIX 3550
END IF	MIX 3560
	MIX 3570
C -----	MIX 3580
C In the absence of an ANSI standard WHILE statement	MIX 3590
C -----	MIX 3600
	MIX 3610

80	IF (MINSAT .AND. MINDP) GO TO 90	MIX 3620
	CONTINUE	MIX 3630
	IF (.NOT. MINSAT) THEN	MIX 3640
	IF (IPGLN .GT. 54) CALL PAGE	MIX 3650
	IPGLN = IPGLN + 5	MIX 3660
	WRITE (UNO, 1010) IDSAT	MIX 3670
	END IF	MIX 3680
		MIX 3690
	IF (.NOT. MINDP) THEN	MIX 3700
	IF (IPGLN .GT. 54) CALL PAGE	MIX 3710
	IPGLN = IPGLN + 5	MIX 3720
	WRITE (UNO, 1020) IDDP	MIX 3730
	END IF	MIX 3740
		MIX 3750
	IF ((.NOT. MINDP .OR. .NOT. MINSAT) .OR. ERROR) STOP	MIX 3760
		MIX 3770
90	CONTINUE	MIX 3780
	IF (IDSAT .EQ. 0) MINSAT = .FALSE.	MIX 3790
	IF (IDDP .EQ. 0) MINDP = .FALSE.	MIX 3800
		MIX 3810
	CLOSE (UNR)	MIX 3820
		MIX 3830
	END IF	MIX 3840
		MIX 3850
		MIX 3860
C	-----	MIX 3870
C	The appropriate reactions have been found. Make titles.	MIX 3880
C	Prepare the first step/take the first step	MIX 3890
C		MIX 3900
C	IDDP > 0 IDSAT > 0 ITMIX = 0 Dissolve/ppt IDDP til saturation	MIX 3910
C	with IDSAT	MIX 3920
C	IDDP = 0 IDSAT > 0 ITMIX = 0 dissolve/remove aqueous components	MIX 3930
C	til saturation with IDSAT	MIX 3940
C	IDDP > 0 IDSAT = 0 ITMIX < 0 dissolve a specified amount of	MIX 3950
C	IDSAT (note that this is specified	MIX 3960
C	by ICALL=1, ISALT=1, and ITMIX<0)	MIX 3970
C	-----	MIX 3980
	IF (ISALT .EQ. 3 .AND. ITMIX .EQ. 0 .AND. MINSAT	MIX 3990
	.AND. ICALL .EQ. 1 .AND. MINDP) THEN	MIX 4000
	IF (DP .LT. (CPUMIN * (-1.0))) THEN	MIX 4010
	TITMIX = PAGE3(IDDP)///' PRECIPITATED	MIX 4020
	ELSE IF (DP .GT. CPUMIN) THEN	MIX 4030
	TITMIX = PAGE3(IDDP)///' DISSOLVED	MIX 4040
	ELSE	MIX 4050
	TITMIX = PAGE3(IDDP)///' PPT/DISS	MIX 4060
	END IF	MIX 4070
	ELSE IF (ISALT .EQ. 3 .AND. ITMIX .EQ. 0 .AND. MINSAT	MIX 4080
	.AND. ICALL .EQ. 1 .AND. .NOT. MINDP) THEN	MIX 4090
		MIX 4100
		MIX 4110
C	-----	MIX 4120
C	If we are adding components, make up name, use * for	MIX 4130
C	non-trivial blanks, remove all other blanks, then	MIX 4140
C	change * to blank	MIX 4150
C	-----	MIX 4160
		MIX 4170
	K = 1	MIX 4180
	ICD = 0	MIX 4190

DO 130 I = 1, 10	MIX 4200
IF (IRXDP(I) .NE. 0) THEN	MIX 4210
IDMIN(I) = IRXDP(I)	MIX 4220
ICD = ICD + 1	MIX 4230
STOFAC(I) = RXDP(I)	MIX 4240
END IF	MIX 4250
IF (IRXDP(I) .NE. 0 .AND. K .LE. LEN(TITMIX)) THEN	MIX 4260
IF (K .NE. 1) THEN	MIX 4270
BUFFER(1:1) = '*'	MIX 4280
ELSE	MIX 4290
BUFFER(1:1) = ' '	MIX 4300
END IF	MIX 4310
WRITE (BUFFER(2:11), '(F10.3)') RXDP(I)	MIX 4320
BUFFER(12:22) = ' (' // PAGE1(IRXDP(I)) // ')'	MIX 4330
	MIX 4340
100 CONTINUE	MIX 4350
JJ = INDEX(BUFFER, '0 ')	MIX 4360
IF (JJ .NE. 0) THEN	MIX 4370
BUFFER(JJ:JJ) = ' '	MIX 4380
GO TO 100	MIX 4390
END IF	MIX 4400
110 CONTINUE	MIX 4410
JJ = INDEX(BUFFER, '. ')	MIX 4420
IF (JJ .NE. 0) THEN	MIX 4430
BUFFER(JJ:JJ) = ' '	MIX 4440
GO TO 110	MIX 4450
END IF	MIX 4460
DO 120 JJ = 1, 22	MIX 4470
IF (BUFFER(JJ:JJ) .NE. ' ' .AND.	MIX 4480
K .LE. LEN(TITMIX)) THEN	MIX 4490
TITMIX(K:K) = BUFFER(JJ:JJ)	MIX 4500
K = K + 1	MIX 4510
ELSE IF (K .GT. LEN(TITMIX)) THEN	MIX 4520
K = LEN(TITMIX)	MIX 4530
TITMIX(K-2:K) = '...'	MIX 4540
K = K + 10	MIX 4550
GO TO 110	MIX 4560
END IF	MIX 4570
120 CONTINUE	MIX 4580
END IF	MIX 4590
130 CONTINUE	MIX 4600
	MIX 4610
DO 140 I = 1, K	MIX 4620
IF (TITMIX(I:I) .EQ. '*') TITMIX(I:I) = ' '	MIX 4630
140 CONTINUE	MIX 4640
	MIX 4650
ELSE IF (ITMIX .LT. 0 .AND. ICALL .EQ. 1 .AND. ISALT .EQ. 1) THEN	MIX 4660
IF (IPGLN .GT. (59-8-ITMIX)) CALL PAGE	MIX 4670
IPGLN = IPGLN + 5	MIX 4680
WRITE (UNO,1110) PAGE3(IDDP)	MIX 4690
DO 160 I = 1, 10	MIX 4700
INDX = IDMIN(I)	MIX 4710
IF (INDX .LE. 0) GO TO 160	MIX 4720
IF (INDX .EQ. 11) INDX = 12	MIX 4730
	MIX 4740
EQH = 0.0D00	MIX 4750
DO 150 J = 1, 9	MIX 4760
IF (INDX .EQ. IHID(J)) EQH = HEQ(J)	MIX 4770

150	CONTINUE	MIX 4780
	IF (DABS(EQH) .GT. CPUMIN) TOTEL(1) = TOTEL(1) + (AMOL(1) * STOFAC(I) *EQC)	MIX 4790 MIX 4800
	EQC = 0.0	MIX 4810
	IF (INDX .EQ. 7) EQC = 1.0	MIX 4820
	IF (INDX .EQ. 98) EQC = 1.0	MIX 4830
	IF (INDX .EQ. 207) EQC = 1.0	MIX 4840
	IF (INDX .EQ. 208) EQC = 2.0	MIX 4850
	IF (INDX .EQ. 209) EQC = 3.0	MIX 4860
	IF (DABS(EQC) .GT. CPUMIN) TOTEL(3) = TOTEL(3) + (AMOL(1) * STOFAC(I) * EQC)	MIX 4870 MIX 4880
	ANALM(INDX) = ANALM(INDX) + (AMOL(1) * STOFAC(I))	MIX 4890
	IPGLN = IPGLN + 1	MIX 4900
	WRITE (UNO,1080) INDX, PAGEL(INDX), (AMOL(1)*STOFAC(I)), EQH, EQC	MIX 4910 MIX 4920
	IF (ANALM(INDX) .LT. 0.0 .AND. ANMMIX(INDX) .GT. 0.0) THEN	MIX 4930
	WRITE (UNO, 1100) PAGEL(INDX), (AMOL(1) * STOFAC(I)), ANMMIX(INDX)	MIX 4940 MIX 4950
	STOP	MIX 4960
	END IF	MIX 4970
160	CONTINUE	MIX 4980
	IPGLN = IPGLN + 3	MIX 4990
	WRITE (UNO,1090)	MIX 5000
	ICALL = 3	MIX 5010
	J = 0	MIX 5020
	DO 170 I = 1, 28	MIX 5030
	J = J + 1	MIX 5040
	IF (J .EQ. 8) J = 12	MIX 5050
	IF (J .EQ. 17) J = 18	MIX 5060
	IF (J .EQ. 19) J = 21	MIX 5070
	IF (J .EQ. 24) J = 25	MIX 5080
	IF (J .EQ. 34) J = 48	MIX 5090
	IF (J .EQ. 49) J = 169	MIX 5100
	IF (J .EQ. 170) J = 210	MIX 5110
	EXELT(I) = ANALM(J)	MIX 5120
170	CONTINUE	MIX 5130
	EXELT(29) = ANALM(7)	MIX 5140
	EXELT(30) = ANALM(246)	MIX 5150
	EXELT(31) = ANALM(265)	MIX 5160
	EXELT(32) = ANALM(136)	MIX 5170
	EXELT(33) = ANALM(MXSP+1)	MIX 5180
	EXELT(34) = ANALM(MXSP+16)	MIX 5190
	EXELT(35) = ANALM(MXSP+31)	MIX 5200
	TITR(1) = EXELT(29)	MIX 5210
	TITR(2) = EXELT(6)	MIX 5220
	TITR(3) = EXELT(22)	MIX 5230
	TITR(4) = EXELT(21)	MIX 5240
	TITR(5) = EXELT(5)	MIX 5250
	TITR(6) = EXELT(26)	MIX 5260
	TITR(7) = EXELT(25)	MIX 5270
	TITR(8) = EXELT(30)	MIX 5280
		MIX 5290
		MIX 5300
		MIX 5310
		MIX 5320
		MIX 5330
		MIX 5340
		MIX 5350

TITR(9) = EXELT(31)	MIX 5360
TITR(10) = EXELT(33)	MIX 5370
TITR(11) = EXELT(34)	MIX 5380
RETURN	MIX 5390
ELSE IF (ICALL .EQ. 1 .AND. ISALT .EQ. 3) THEN	MIX 5400
IF (IPGLN .GT. 55) CALL PAGE	MIX 5410
IPGLN = IPGLN + 4	MIX 5420
WRITE (UNO, 1060) ITMIX, IDSAT, IDDP	MIX 5430
STOP	MIX 5440
END IF	MIX 5450
	MIX 5460
IF (IDDP .NE. 0 .AND. IPRIN2 .NE. 0) THEN	MIX 5470
IF (IPGLN .GT. 56) CALL PAGE	MIX 5480
IPGLN = IPGLN + 2	MIX 5490
WRITE (UNO,1120) PAGE3(IDDP), TITMIX(9:25)	MIX 5500
END IF	MIX 5510
	MIX 5520
C -----	MIX 5530
C Prepare first steps	MIX 5540
C -----	MIX 5550
	MIX 5560
IF (ISALT .EQ. 3 .AND. ITMIX .EQ. 0 .AND. ICALL .EQ. 1) THEN	MIX 5570
IADD = 1	MIX 5580
JJ = 1	MIX 5590
SIMIN(IADD) = ATCPRD (ICS, IDSP, COFFAC, ALFA)	MIX 5600
SIMIN(IADD) = SIMIN(IADD) - LOGKT2(IDSAT)	MIX 5610
ADDMIN(IADD) = 0.0	MIX 5620
IF (DABS(SIMIN(IADD)) .LT. FCCSAT) THEN	MIX 5630
ICALL = 1	MIX 5640
IF (IPGLN .GT. 55) CALL PAGE	MIX 5650
IPGLN = IPGLN + 3	MIX 5660
WRITE (UNO,1150) TITMIX, ADDMIN(IADD)	MIX 5670
RETURN	MIX 5680
END IF	MIX 5690
J = 0	MIX 5700
DELTA = 1000.0	MIX 5710
DO 190 I = 1, 10	MIX 5720
IF (IDSP(I) .NE. 0) THEN	MIX 5730
IF (M(IDSP(I)) .LT. DELTA .AND.	MIX 5740
M(IDSP(I)) .GT. CPUMIN) THEN	MIX 5750
DO 180 K = 1, 10	MIX 5760
IF (IDMIN(K) .EQ. IDSP(I)) THEN	MIX 5770
IF (STOFAC(K) .GT. 0) THEN	MIX 5780
J = 1	MIX 5790
ELSE	MIX 5800
J = -1	MIX 5810
END IF	MIX 5820
DELTA = M(IDSP(I))	MIX 5830
END IF	MIX 5840
180 CONTINUE	MIX 5850
END IF	MIX 5860
END IF	MIX 5870
190 CONTINUE	MIX 5880
	MIX 5890
IF (DABS(DP) .GT. CPUMIN) THEN	MIX 5900
ADD = STEPSZ * DP	MIX 5910
REVERS = .FALSE.	MIX 5920
ELSE IF ((SIMIN(IADD) .LT. 0.0 .AND. J .GE. 0) .OR.	MIX 5930

	(SIMIN(IADD) .GT. 0.0 .AND. J .LT. 0)) THEN	MIX 5940
	ADD = STEPSZ	MIX 5950
	REVERS = .TRUE.	MIX 5960
	ELSE	MIX 5970
	ADD = STEPSZ * (-1.0)	MIX 5980
	REVERS = .TRUE.	MIX 5990
	END IF	MIX 6000
	IF (DABS(DP) .LT. CPUMIN) DP = 1.0D00	MIX 6010
	ADDMIN(IADD+1) = ADD	MIX 6020
	CROSS = .FALSE.	MIX 6030
		MIX 6040
	ELSE IF (ISALT .EQ. 3 .AND. ICALL .GT. 1) THEN	MIX 6050
	IADD = IADD + 1	MIX 6060
	SIMIN(IADD) = ATCPRD (ICS, IDSP, COFFAC, ALFA)	MIX 6070
	SIMIN(IADD) = SIMIN(IADD) - LOGKT2(IDSAT)	MIX 6080
	IF (DABS(SIMIN(IADD)) .LT. FCCSAT) THEN	MIX 6090
	ICALL = 1	MIX 6100
	IF (IPGLN .GT. 55) CALL PAGE	MIX 6110
	IPGLN = IPGLN + 3	MIX 6120
	WRITE (UNO,1150) TITMIX, ADDMIN(IADD)	MIX 6130
	RETURN	MIX 6140
	END IF	MIX 6150
		MIX 6160
	IF (.NOT. CROSS) THEN	MIX 6170
	IF ((SIMIN(IADD) * SIMIN(IADD-1)) .LT. 0.0) THEN	MIX 6180
	CROSS = .TRUE.	MIX 6190
	ELSE IF (DABS(SIMIN(IADD)) .LT. DABS(SIMIN(IADD-1))) THEN	MIX 6200
	ADD = ADDMIN(IADD) * 10.0	MIX 6210
	REVERS = .FALSE.	MIX 6220
	ELSE IF (REVERS) THEN	MIX 6230
	ADD = ADD * (-0.5)	MIX 6240
	IF ((DABS(ADD - ADDMIN(IADD))) .LT. 1.0E-12) THEN	MIX 6250
	WRITE (UNO, 1140) PAGE3(IDSAT), SIMIN(IADD), ADDMIN(IADD)	MIX 6260
	STOP	MIX 6270
	END IF	MIX 6280
	ELSE	MIX 6290
	ADD = (ADDMIN(IADD) - ADDMIN(IADD-1)) / 2.0	MIX 6300
	IF ((DABS(ADD) - DABS(ADDMIN(IADD))) .LT. 1.0E-12) THEN	MIX 6310
	WRITE (UNO, 1140) PAGE3(IDSAT), SIMIN(IADD), ADDMIN(IADD)	MIX 6320
	STOP	MIX 6330
	END IF	MIX 6340
	END IF	MIX 6350
	END IF	MIX 6360
	JJ = IADD	MIX 6370
	IF (CROSS) THEN	MIX 6380
	CALL SORTA(ADDMIN, SIMIN, IADD, JJ)	MIX 6390
		MIX 6400
	DO 200 I = 2, IADD	MIX 6410
	J = I - 1	MIX 6420
	IF ((SIMIN(I) * SIMIN(J)) .LT. 0.0) GO TO 210	MIX 6430
200	CONTINUE	MIX 6440
		MIX 6450
	ELSE	MIX 6460
	J = 6	MIX 6470
	END IF	MIX 6480
210	IF (IADD .GT. 6) THEN	MIX 6490
	IF (J .GT. 3) THEN	MIX 6500
	DO 220 I = 1, IADD-1	MIX 6510

	SIMIN(I) = SIMIN(I+1)	MIX 6520
	ADDMIN(I) = ADDMIN(I+1)	MIX 6530
220	CONTINUE	MIX 6540
	JJ = JJ - 1	MIX 6550
	J = J - 1	MIX 6560
	END IF	MIX 6570
	IADD = IADD - 1	MIX 6580
	END IF	MIX 6590
	IF (CROSS) THEN	MIX 6600
	CALL GUESS(ADDMIN, SIMIN, ADD, IADD)	MIX 6610
	X = DABS(ADDMIN(J) - ADDMIN(J+1)) / 10000.0D00	MIX 6620
	IF (DABS (ADDMIN(J) - ADD) .LT. X .OR.	MIX 6630
	DABS (ADDMIN(J+1) - ADD) .LT. X) THEN	MIX 6640
	ADD = (ADDMIN(J) + ADDMIN(J+1)) / 2.0	MIX 6650
	END IF	MIX 6660
	END IF	MIX 6670
	ADDMIN(IADD+1) = ADD	MIX 6680
	END IF	MIX 6690
		MIX 6700
C	-----	MIX 6710
C	Change the original solution parameters for the new step and	MIX 6720
C	go back to calculate species distribution	MIX 6730
C	-----	MIX 6740
		MIX 6750
	IF (ISALT .EQ. 3) THEN	MIX 6760
230	CONTINUE	MIX 6770
	EQC = 0.0	MIX 6780
	EQH = 0.0	MIX 6790
	ANALM(7) = TOTEL(3)	MIX 6800
	ANALM(98) = 0.0	MIX 6810
	IF (DABS(DP) .LT. CPUMIN) DP = 1.0D00	MIX 6820
	DO 240 I = 1, ICD	MIX 6830
	J = IDMIN(I)	MIX 6840
	IF (J .EQ. 0) GO TO 240	MIX 6850
	IF (J .EQ. 11) J = 12	MIX 6860
	IF (J .EQ. 7 .OR. J .EQ. 8 .OR. J .EQ. 49) THEN	MIX 6870
	EQH = EQH + (STOFAC(I) * ADD)	MIX 6880
	ELSE IF (J .EQ. 28 .OR. J .EQ. 33 .OR. J .EQ. 97) THEN	MIX 6890
	EQH = EQH + (STOFAC(I) * ADD * 2.0D00)	MIX 6900
	ELSE IF (J .EQ. 12) THEN	MIX 6910
	EQH = EQH + (STOFAC(I) * ADD * 4.0D00)	MIX 6920
	ELSE IF (J .EQ. 32 .OR. J .EQ. 9) THEN	MIX 6930
	EQH = EQH - (STOFAC(I) * ADD)	MIX 6940
	ELSE IF (J .EQ. 31) THEN	MIX 6950
	EQH = EQH - (STOFAC(I) * ADD * 3.0D00)	MIX 6960
	END IF	MIX 6970
		MIX 6980
	IF (J .EQ. 7) EQC = (ADD * STOFAC(I)) + EQC	MIX 6990
	IF (J .EQ. 97) EQC = (ADD * STOFAC(I)) + EQC	MIX 7000
	IF (J .EQ. 98) EQC = (ADD * STOFAC(I)) + EQC	MIX 7010
	IF (J .EQ. 207) EQC = (ADD * STOFAC(I)) + EQC	MIX 7020
	IF (J .EQ. 208) EQC = (ADD * STOFAC(I) * 2.0) + EQC	MIX 7030
	IF (J .EQ. 209) EQC = (ADD * STOFAC(I) * 3.0) + EQC	MIX 7040
	IF (J .EQ. 97 .OR. J .EQ. 98 .OR. J .EQ. 207 .OR.	MIX 7050
	J .EQ. 208 .OR. J .EQ. 209) J = 7	MIX 7060
		MIX 7070
	ANALM(J) = ANMMIX(J) + (ADD * STOFAC(I))	MIX 7080
		MIX 7090

IF (J .NE. 8 .AND. J .NE. 9 .AND. J .NE. 10 .AND.	MIX 7100
(ADD * STOFAC(I)) .LT. 0.0 .AND.	MIX 7110
ANMMIX(J) .LE. CPUMIN) THEN	MIX 7120
WRITE (UNO, 1160)	MIX 7130
STOP	MIX 7140
END IF	MIX 7150
IF (J .NE. 8 .AND. J .NE. 9 .AND. J .NE. 10	MIX 7160
.AND. ANALM(J) .LE. 0.0) THEN	MIX 7170
ADD = (ANMMIX(J) / STOFAC(I)) * (-1.0)	MIX 7180
ADD = ADD - (ADD / (DABS(DP) * 10.0** (IADD+3)))	MIX 7190
ADDMIN(IADD+1) = ADD	MIX 7200
GO TO 230	MIX 7210
END IF	MIX 7220
	MIX 7230
240 CONTINUE	MIX 7240
TOTEL(1) = AlMIX(1) + EQH	MIX 7250
TOTEL(3) = AlMIX(3) + EQC	MIX 7260
IF (TOTEL(3) .GT. CPUMIN) THEN	MIX 7270
ANALM(7) = TOTEL(3)	MIX 7280
ANALM(98) = 0.0	MIX 7290
ELSE IF (AlMIX(3) .GT. CPUMIN) THEN	MIX 7300
ADD = ADD / 0.9	MIX 7310
ADDMIN(IADD+1) = ADD	MIX 7320
GO TO 230	MIX 7330
END IF	MIX 7340
ICALL = 3	MIX 7350
	MIX 7360
IF (IPRIN2 .NE. 0) THEN	MIX 7370
IF (IPGLN .GT. 55) CALL PAGE	MIX 7380
IPGLN = IPGLN + 3	MIX 7390
IF (IDDP .NE. 0) THEN	MIX 7400
WRITE (UNO,1130) PAGE3(IDSAT), SIMIN(JJ), TITMIX(1:40), ADD	MIX 7410
ELSE	MIX 7420
WRITE (UNO,1130) PAGE3(IDSAT), SIMIN(JJ), TITMIX(1:40), ADD	MIX 7430
END IF	MIX 7440
END IF	MIX 7450
	MIX 7460
J = 0	MIX 7470
DO 250 I = 1, 28	MIX 7480
J = J + 1	MIX 7490
IF (J .EQ. 8) J = 12	MIX 7500
IF (J .EQ. 17) J = 18	MIX 7510
IF (J .EQ. 19) J = 21	MIX 7520
IF (J .EQ. 24) J = 25	MIX 7530
IF (J .EQ. 34) J = 48	MIX 7540
IF (J .EQ. 49) J = 169	MIX 7550
IF (J .EQ. 170) J = 210	MIX 7560
EXELT(I) = ANALM(J)	MIX 7570
250 CONTINUE	MIX 7580
	MIX 7590
EXELT(29) = ANALM(7)	MIX 7600
EXELT(30) = ANALM(246)	MIX 7610
EXELT(31) = ANALM(265)	MIX 7620
EXELT(32) = ANALM(136)	MIX 7630
EXELT(33) = ANALM(MXSP+1)	MIX 7640
EXELT(34) = ANALM(MXSP+16)	MIX 7650
EXELT(35) = ANALM(MXSP+31)	MIX 7660
	MIX 7670

TITR(1) = EXELT(29)	MIX 7680
TITR(2) = EXELT(6)	MIX 7690
TITR(3) = EXELT(22)	MIX 7700
TITR(4) = EXELT(21)	MIX 7710
TITR(5) = EXELT(5)	MIX 7720
TITR(6) = EXELT(26)	MIX 7730
TITR(7) = EXELT(25)	MIX 7740
TITR(8) = EXELT(30)	MIX 7750
TITR(9) = EXELT(31)	MIX 7760
TITR(10) = EXELT(33)	MIX 7770
TITR(11) = EXELT(34)	MIX 7780
RETURN	MIX 7790
END IF	MIX 7800
	MIX 7810
C -----	MIX 7820
C Boiling routine -- Icall = 1 on the first call only	MIX 7830
C -----	MIX 7840
	MIX 7850
IF (ISALT .EQ. 2) THEN	MIX 7860
FFB = 1.0 - FBOIL	MIX 7870
IF (ICALL .EQ. 1) THEN	MIX 7880
WRITE (BUFFER, 1230) FBOIL	MIX 7890
READ (BUFFER, '(A)') TITMIX	MIX 7900
IF (IPGLN .GT. 53) CALL PAGE	MIX 7910
IPGLN = IPGLN + 4	MIX 7920
WRITE (UNO,1170) FBOIL	MIX 7930
	MIX 7940
C -----	MIX 7950
C Calculate the concentration of non-volatile species after boiling	MIX 7960
C -----	MIX 7970
	MIX 7980
DO 260 I = 1, MXSP+30	MIX 7990
ANALM(I) = ANMMIX(I) / FFB	MIX 8000
260 CONTINUE	MIX 8010
	MIX 8020
J = 0	MIX 8030
DO 270 I = 1, 28	MIX 8040
J = J + 1	MIX 8050
IF (J .EQ. 8) J = 12	MIX 8060
IF (J .EQ. 17) J = 18	MIX 8070
IF (J .EQ. 19) J = 21	MIX 8080
IF (J .EQ. 24) J = 25	MIX 8090
IF (J .EQ. 34) J = 48	MIX 8100
IF (J .EQ. 49) J = 169	MIX 8110
IF (J .EQ. 170) J = 210	MIX 8120
EXELT(I) = ANALM(J)	MIX 8130
270 CONTINUE	MIX 8140
	MIX 8150
EXELT(29) = ANALM(7)	MIX 8160
EXELT(30) = ANALM(246)	MIX 8170
EXELT(31) = ANALM(265)	MIX 8180
EXELT(32) = ANALM(136)	MIX 8190
EXELT(33) = ANALM(MXSP+1)	MIX 8200
EXELT(34) = ANALM(MXSP+16)	MIX 8210
EXELT(35) = ANALM(MXSP+31)	MIX 8220
	MIX 8230
TITR(1) = EXELT(29)	MIX 8240
TITR(2) = EXELT(6)	MIX 8250

TITR(3) = EXELT(22)	MIX 8260
TITR(4) = EXELT(21)	MIX 8270
TITR(5) = EXELT(5)	MIX 8280
TITR(6) = EXELT(26)	MIX 8290
TITR(7) = EXELT(25)	MIX 8300
TITR(8) = EXELT(30)	MIX 8310
TITR(9) = EXELT(31)	MIX 8320
TITR(10) = EXELT(33)	MIX 8330
TITR(11) = EXELT(34)	MIX 8340
	MIX 8350
C -----	MIX 8360
C If steam is being added, change appropriate parameters. quit	MIX 8370
C -----	MIX 8380
	MIX 8390
IF (FBOIL .LT. 0.D0) THEN	MIX 8400
TOTEL(1) = TOTEL(1) / FFB	MIX 8410
TOTEL(2) = TOTEL(2) / FFB	MIX 8420
TOTEL(3) = TOTEL(3) / FFB	MIX 8430
ANALM(7) = TOTEL(3)	MIX 8440
ANALM(98) = 0.0	MIX 8450
EXELT(29) = ANALM(7)	MIX 8460
TITR(1) = EXELT(29)	MIX 8470
ICALL = 3	MIX 8480
RETURN	MIX 8490
END IF	MIX 8500
	MIX 8510
C -----	MIX 8520
C Calculate the partitioning of volatile species (co2,nh3,h2s,ch4)	MIX 8530
C -----	MIX 8540
	MIX 8550
TK = TEMP + 273.15	MIX 8560
KH2S = KHH2S(TK, M1)	MIX 8570
KNH3 = KHNH3(TK)	MIX 8580
KCO2 = KHCO2(TK, M1)	MIX 8590
IF (PRESS .LT. PH20) PRESS = PH20	MIX 8600
	MIX 8610
X = 1.0D00	MIX 8620
KCH4 = KHCH4(TK, M1, X)	MIX 8630
	MIX 8640
C -----	MIX 8650
C Calculate vapor density (routine taken from drummond's program)	MIX 8660
C Calculate volatility ratios	MIX 8670
C -----	MIX 8680
	MIX 8690
M1 = M1 - 1.0D00	MIX 8700
CALL DPVT (TEMP, M1, PRESS, VDEN)	MIX 8710
M1 = M1 + 1.0D00	MIX 8720
	MIX 8730
VRT = VDEN * R * (TEMP + 273.15)	MIX 8740
VRCO2 = KCO2 / VRT	MIX 8750
VRNH3 = KNH3 / VRT	MIX 8760
VRH2S = KH2S / VRT	MIX 8770
VRCH4 = KCH4 / VRT	MIX 8780
IF (IPGLN .GT. 51) CALL PAGE	MIX 8790
IPGLN = IPGLN + 6	MIX 8800
WRITE (UNO,1190) ' KH2S = ', KH2S, ' KNH3 = ', KNH3,	MIX 8810
' KCO2 = ', KCO2, ' KCH4 = ', KCH4,	MIX 8820
' VRCO2 = ', VRCO2, ' VRNH3 = ', VRNH3,	MIX 8830

.	' VRH2S = ', VRH2S, ' VRCH4 = ', VRCH4,	MIX 8840
.	' VRT = ', VRT, ' VDEN = ', VDEN	MIX 8850
		MIX 8860
	IBTOT = 1	MIX 8870
	IBOIL = 1	MIX 8880
		MIX 8890
	DO 280 I = 1, 4	MIX 8900
	NV(I) = 0.0	MIX 8910
	NL(I) = 0.0	MIX 8920
	STEP(I) = 0.0	MIX 8930
280	CONTINUE	MIX 8940
		MIX 8950
	IF (AlMIX(3) .GT. CPUMIN) THEN	MIX 8960
	TRY(1,IBOIL) = TOTEL(3)	MIX 8970
	NL(1) = TOTEL(3)	MIX 8980
	NV(1) = VRCO2 * (M(97) / FFB) * FBOIL	MIX 8990
	DIF(1,IBOIL) = AlMIX(3) - (TOTEL(3) * FFB + NV(1))	MIX 9000
	STEP(1) = AlMIX(3) / ((TOTEL(3) * FFB) + NV(1))	MIX 9010
	NL(1) = (STEP(1) - 1.0D00) * NL(1)	MIX 9020
		MIX 9030
	IF (NL(1) .LT. CPUMIN) THEN	MIX 9040
	NL(1) = 0.1 * TRY(1,IBOIL)	MIX 9050
	STEP(1) = NL(1) - TRY(1,IBOIL)	MIX 9060
	END IF	MIX 9070
		MIX 9080
	IF (NL(1) .GT. AlMIX(3) * FFB) THEN	MIX 9090
	NL(1) = 0.9 * AlMIX(3) * FFB	MIX 9100
	STEP(1) = NL(1) - TRY(1,IBOIL)	MIX 9110
	END IF	MIX 9120
	END IF	MIX 9130
		MIX 9140
	IF (ANMMIX(32) .GT. CPUMIN) THEN	MIX 9150
	TRY(2,IBOIL) = ANALM(32)	MIX 9160
	NL(2) = ANALM(32)	MIX 9170
	NV(2) = VRNH3 * (M(147) / FFB) * FBOIL	MIX 9180
	DIF(2,IBOIL) = ANMMIX(32) - (ANALM(32) * FFB + NV(2))	MIX 9190
	STEP(2) = ANMMIX(32) / ((ANALM(32) * FFB) + NV(2))	MIX 9200
	NL(2) = (STEP(2) - 1.0D00) * NL(2)	MIX 9210
		MIX 9220
	IF (NL(2) .LT. CPUMIN) THEN	MIX 9230
	NL(2) = 0.1 * TRY(2,IBOIL)	MIX 9240
	STEP(2) = NL(2) - TRY(2,IBOIL)	MIX 9250
	END IF	MIX 9260
		MIX 9270
	IF (NL(2) .GT. (ANMMIX(32) * FFB)) THEN	MIX 9280
	NL(2) = 0.9 * ANMMIX(32) * FFB	MIX 9290
	STEP(2) = NL(2) - TRY(2,IBOIL)	MIX 9300
	END IF	MIX 9310
	END IF	MIX 9320
		MIX 9330
	IF (ANMMIX(33) .GT. CPUMIN) THEN	MIX 9340
	TRY(3,IBOIL) = ANALM(33)	MIX 9350
	NL(3) = ANALM(33)	MIX 9360
	NV(3) = VRH2S * (M(33) / FFB) * FBOIL	MIX 9370
	DIF(3,IBOIL) = ANMMIX(33) - (ANALM(33) * FFB + NV(3))	MIX 9380
	STEP(3) = ANMMIX(33) / ((ANALM(33) * FFB) + NV(3))	MIX 9390
	NL(3) = (STEP(3) - 1.0D00) * NL(3)	MIX 9400
		MIX 9410

IF (NL(3) .LT. CPUMIN) THEN	MIX 9420
NL(3) = 0.1 * TRY(3,IBOIL)	MIX 9430
STEP(3) = NL(3) - TRY(3,IBOIL)	MIX 9440
END IF	MIX 9450
	MIX 9460
IF (NL(2) .GT. (ANMMIX(33) * FFB)) THEN	MIX 9470
NL(3) = 0.9 * ANMMIX(33) * FFB	MIX 9480
STEP(3) = NL(3) - TRY(3,IBOIL)	MIX 9490
END IF	MIX 9500
END IF	MIX 9510
	MIX 9520
IF (ANMMIX(285) .GT. CPUMIN) THEN	MIX 9530
TRY(4,IBOIL) = ANALM(285)	MIX 9540
NL(4) = ANALM(285)	MIX 9550
NV(4) = VRCH4 * (M(285) / FFB) * FBOIL	MIX 9560
DIF(4,IBOIL) = ANMMIX(285) - (ANALM(285)*FFB + NV(4))	MIX 9570
STEP(4) = ANALM(285) / ((ANMMIX(285) * FFB) + NV(4))	MIX 9580
NL(4) = (STEP(4) - 1.0D00) * NL(4)	MIX 9590
	MIX 9600
IF (NL(4) .LT. CPUMIN) THEN	MIX 9610
NL(4) = 0.1 * TRY(4,IBOIL)	MIX 9620
STEP(4) = NL(4) - TRY(4,IBOIL)	MIX 9630
END IF	MIX 9640
	MIX 9650
IF (NL(4) .GT. (ANMMIX(285) * FFB)) THEN	MIX 9660
NL(4) = 0.9 * ANMMIX(285) * FFB	MIX 9670
STEP(4) = NL(4) - TRY(4,IBOIL)	MIX 9680
END IF	MIX 9690
END IF	MIX 9700
END IF	MIX 9710
	MIX 9720
IF (ICALL .EQ. 3) THEN	MIX 9730
IBOIL = IBOIL + 1	MIX 9740
IBTOT = IBTOT + 1	MIX 9750
IF (IBTOT .GT. 3) THEN	MIX 9760
IBOIL = 3	MIX 9770
DO 300 J = 1, 4	MIX 9780
DO 290 I = 2, IBOIL	MIX 9790
TRY(J,I-1) = TRY(J,I)	MIX 9800
DIF(J,I-1) = DIF(J,I)	MIX 9810
CONTINUE	MIX 9820
CONTINUE	MIX 9830
END IF	MIX 9840
	MIX 9850
TRY(1,IBOIL) = TOTEL(3)	MIX 9860
NV(1) = VRCO2 * M(97) * FBOIL	MIX 9870
DIF(1,IBOIL) = ALMIX(3) - ((TOTEL(3) * FFB) + NV(1))	MIX 9880
	MIX 9890
TRY(2,IBOIL) = ANALM(32)	MIX 9900
NV(2) = VRNH3 * M(147) * FBOIL	MIX 9910
DIF(2,IBOIL) = ANMMIX(32) - ((ANALM(32) * FFB) + NV(2))	MIX 9920
	MIX 9930
TRY(3,IBOIL) = ANALM(33)	MIX 9940
NV(3) = VRH2S * M(33) * FBOIL	MIX 9950
DIF(3,IBOIL) = ANMMIX(33) - ((ANALM(33) * FFB) + NV(3))	MIX 9960
	MIX 9970
TRY(4,IBOIL) = ANALM(285)	MIX 9980
NV(4) = VRCH4 * M(285) * FBOIL	MIX 9990

DIF(4,IBOIL) = ANMMIX(285) - ((ANALM(285) * FFB) + NV(4))	MIX10000
DONE = .TRUE.	MIX10010
DO 310 I = 1, 4	MIX10020
IF (I .EQ. 1) THEN	MIX10030
X = ALMIX(3)	MIX10040
ELSE IF (I .EQ. 2) THEN	MIX10050
X = ANMMIX(32)	MIX10060
ELSE IF (I .EQ. 3) THEN	MIX10070
X = ANMMIX(33)	MIX10080
ELSE IF (I .EQ. 4) THEN	MIX10090
X = ANMMIX(285)	MIX10100
END IF	MIX10110
IF (X .GT. CPUMIN) THEN	MIX10120
IF (DABS(DIF(I,IBOIL) / X) .GT. 0.01 .AND.	MIX10130
DABS(STEP(I)) .GT. (X * 0.01) .AND. IBTOT .LT. 20)	MIX10140
DONE = .FALSE.	MIX10150
IF ((DIF(I,IBOIL) * DIF(I,(IBOIL-1))) .LT. 0.0) THEN	MIX10160
STEP(I) = STEP(I) * (-0.5)	MIX10170
ELSE IF (DABS(DIF(I,IBOIL)) .GT. DABS(DIF(I,(IBOIL-1))))	MIX10180
THEN	MIX10190
STEP(I) = STEP(I) * (-0.8)	MIX10200
END IF	MIX10210
IF ((NL(I) + STEP(I)) .LE. 0.0) THEN	MIX10220
STEP(I) = NL(I) * (-0.90)	MIX10230
ELSE IF ((NL(I) + STEP(I)) .GE. (X/FFB)) THEN	MIX10240
STEP(I) = ((X/FFB) - NL(I)) * 0.90	MIX10250
END IF	MIX10260
NL(I) = NL(I) + STEP(I)	MIX10270
NV(I) = X - (NL(I) * FFB)	MIX10280
END IF	MIX10290
310 CONTINUE	MIX10300
IF (DONE) THEN	MIX10310
NGAST(1) = ALMIX(3)	MIX10320
NGAST(2) = ANMMIX(32)	MIX10330
NGAST(3) = ANMMIX(33)	MIX10340
NGAST(4) = ANMMIX(285)	MIX10350
NL(1) = ANALM(7)	MIX10360
NL(2) = ANALM(32)	MIX10370
NL(3) = ANALM(33)	MIX10380
NL(4) = ANALM(285)	MIX10390
IF (IPGLN .GT. 48) CALL PAGE	MIX10400
IPGLN = IPGLN + 10	MIX10410
WRITE (UNO,1180) FBOIL	MIX10420
WRITE (UNO,1210)	MIX10430
DO 320 I = 1, 4	MIX10440
IF (NGAST(I) .GT. CPUMIN) THEN	MIX10450
NV(I) = NGAST(I) - (NL(I) * FFB)	MIX10460
X = NV(I) * 100.00 / NGAST(I)	MIX10470
	MIX10480
	MIX10490
	MIX10500
	MIX10510
	MIX10520
	MIX10530
	MIX10540
	MIX10550
	MIX10560
	MIX10570

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ELSE
  X = 0.0
  NL(I) = 0.0
  NV(I) = 0.0
END IF
WRITE (UNO,1220) DUM2(I), NGASt(I), (NL(I) * FFB),
NL(I), NV(I), X
320 CONTINUE
ICALL = 1
RETURN
END IF
END IF

IF (IPRIN2 .NE. 0) THEN
  IF (IPGLN .GT. 50) CALL PAGE
  IPGLN = IPGLN + 10
  WRITE (UNO, 1200)
    NV(1), (NL(1)*FFB), NL(1), PAGE1(97), M(97),
    NV(2), (NL(2)*FFB), NL(2), PAGE1(147), M(147),
    NV(3), (NL(3)*FFB), NL(3), PAGE1(33), M(33),
    NV(4), (NL(4)*FFB), NL(4), PAGE1(285), M(285)
  END IF

  TOTEL(1) = (AlMIX(1) - (NV(1) * 2.0) - (NV(3) * 2.0)) / FFB
  TOTEL(2) = (AlMIX(2) - NV(2)) / FFB
  TOTEL(3) = NL(1)
  ANALM(32) = NL(2)
  ANALM(33) = NL(3)
  ANALM(285) = NL(4)
  ANALM(7) = TOTEL(3)
  ANALM(98) = 0.0

  EXELT(24) = ANALM(32)
  EXELT(25) = ANALM(33)
  EXELT(29) = ANALM(7)

  TITR( 1) = EXELT(29)
  TITR( 7) = EXELT(25)

  ICALL = 3
  RETURN
END IF

C -----
C The following routine is for mixing two solutions
C Store the parameters of the second solution
C -----
IF (ICALL .EQ. 2) THEN
  DO 330 I = 1, 10
    FMIX(I) = 0.0D0
    IF (I .LE. 5) B2MIX(I) = TOTEL(I)
330 CONTINUE

  DO 340 I = 1, MXSP+30
    BNMMIX(I) = ANALM(I)
340 CONTINUE

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	BDENS = DENS	MIX11160
	BTEMP = TEMP	MIX11170
		MIX11180
		MIX11190
C	-----	MIX11200
C	Calculate the no. of mixtures to be processed and the	MIX11210
C	proportions of the two solutions in each of the mixtures	MIX11220
C	-----	MIX11230
		MIX11240
	IF (INMIX .LE. 0) INMIX = 1	MIX11250
	IF (DABS(DINC) .LT. CPUMIN) DINC = DFRAC1	MIX11260
		MIX11270
	INMIX = MIN(INMIX, 10)	MIX11280
	DO 350 I = 1, INMIX	MIX11290
	IF (I .EQ. 1) THEN	MIX11300
	FMIX(I) = DFRAC1	MIX11310
	ELSE	MIX11320
	FMIX(I) = FMIX(I-1) + DINC	MIX11330
	END IF	MIX11340
	IF (FMIX(I) .LT. 0.0 .OR. FMIX(I) .GT. 1.00D00) THEN	MIX11350
	INMIX = I - 1	MIX11360
	GO TO 360	MIX11370
	END IF	MIX11380
350	CONTINUE	MIX11390
		MIX11400
360	CONTINUE	MIX11410
	IRUN = 0	MIX11420
	CALL PAGE	MIX11430
	IPGLN = IPGLN + 7	MIX11440
	WRITE (UNO,1240) DFRAC1, INMIX, DINC	MIX11450
	END IF	MIX11460
		MIX11470
	ICALL = 3	MIX11480
		MIX11490
	RETURN	MIX11500
		MIX11510
1000	FORMAT(I3,/,10(F10.4,I4))	MIX11520
1010	FORMAT(//,' ***** Mineral with i.d. number = ',I4,/,	MIX11530
	' which will be dissolved/precipitated',/,	MIX11540
	' could not be found in the reaction file.')	MIX11550
1020	FORMAT(//,' ***** Mineral with i.d. number = ',I4,/,	MIX11560
	' which the solution will be brought to',	MIX11570
	' equilibrium with',/,	MIX11580
	' could not be found in the reaction file.')	MIX11590
1030	FORMAT(//,' ***** OPEN failed for phase reactions file',	MIX11600
	' (often called RXN.TBL or something similar)',	MIX11610
	/, ' in routine MIXER. Check that the file ',	MIX11620
	' exists ... ')	MIX11630
1040	FORMAT(//,' ***** ERROR reading the reaction data file in ',	MIX11640
	' routine MIXER. The error occurred while',	MIX11650
	/, ' trying to read the ',I5,'th line. Either the file',	MIX11660
	' is corrupted or the end of file was reached',	MIX11670
	/, ' without having found the minerals to dissolve'	MIX11680
	' or precipitate.')	MIX11690
1050	FORMAT(//,' ***** No reaction data for ',A8, '*****',	MIX11700
	' Correct and rerun')	MIX11710
1060	FORMAT(//,' ***** Illegal values of ITMIX, IDSAT, IDDP passed',	MIX11720
	/, ' to MIXER when IBMIX = 0. Values are ',	MIX11730

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.          3(I2,1X), 'respectively.')
1070 FORMAT(//, '*** Net amount of salt/(aqueous component) to be',
.          ' added the solution *****', //,
.          ' SP #          MOLALITY          EQH          EQC')
1080 FORMAT(I4,2X,A,2X,D16.8,2X,F5.2,2X,F5.2)
1090 FORMAT(' *****',//)
1100 FORMAT(//, ' *****ERROR*****ERROR*****',
.          /,4X, A, ' was removed from the solution (',E12.5,
.          ') but this drove the moles negative.',
.          /, ' In this solution, no more than ', E12.5,
.          ' moles can be removed. ')
1110 FORMAT(//, '*** Net amount of mineral ',A,' to be',
.          ' added the solution ... modeled using *****', //,
.          ' SP #          MOLALITY          EQH          EQC')
1120 FORMAT(/,2X,A8,' will be ',A13,' to saturation ')
1130 FORMAT(/, ' Saturation Index (SI) = (',A,') = ',E10.4,
.          /, ' Reaction Step (moles of ',A,') = ',E10.4)
1140 FORMAT(//, ' *** Saturation with ',A,' not possible. ',
.          /, ' SI minimum found at SI = ',E12.5,
.          /, ' At last try, there was ',E12.5,
.          ' moles of material added.',
.          /, ' This may also be caused by specifying DP',
.          /, ' to be negative when only a positive value',
.          /, ' works (or vice versa) or DP was too small of',
.          /, ' a value.')
1150 FORMAT(/, ' Total moles of ',A25,' to achieve saturation: ',E10.4,
.          /)
1160 FORMAT(/, ' Attempt to have a negative amount of a component',
.          /, ' Check what is being added/removed from the water .')
1170 FORMAT(//, ' ***** This solution is to be boiled off *****',
.          /, ' Fraction of boiling = ',F7.2)
1180 FORMAT(' ***** BOILING CALCULATIONS ***** ',//,
.          5X, 'Fraction of solution lost by boiling: ',F5.2)
1190 FORMAT(//, ' Parameters used in Boiling ..... ',
.          /,4(5X,A,E12.5), /,4(5X,A,E12.5), /,2(5X,A,E12.5))
1200 FORMAT(/, ' For the next step, projected amount in the',
.          17X,'using the current values in the',
.          /,10X,'vapour',11X,'liquid',11X,'liquid',
.          10X,'aqueous solution of the species'
.          /,10X,'(moles)',10X,'(moles)',9X,'(molality)',
.          23X,'(molality)',
.          /, ' CO2 = ',3(E12.5,5X),2X,A8,7X,E12.5,
.          /, ' NH3 = ',3(E12.5,5X),2X,A8,7X,E12.5,
.          /, ' H2S = ',3(E12.5,5X),2X,A8,7X,E12.5,
.          /, ' CH4 = ',3(E12.5,5X),2X,A8,7X,E12.5,
.          /)
1210 FORMAT(/, 14X,' Gas species', 5X,'Total Moles ',
.          5X,'Moles in Liquid', 3X,'Molality in Liquid',
.          4X,'Moles in Vapour',
.          4X,'% Lost in Vapour', /)
1220 FORMAT(20X, A5, 5(5X,E12.5,3X),5X,F12.5)
1230 FORMAT(' (fraction of boiling :- ',2X,F4.2,')')
1240 FORMAT(//, ' ***** Mixing of the two previous solutions in',
.          ' the following proportions: ', /,
.          5X,' Initial fraction of solution 1 = ',F7.4,/,
.          17X,' Number of mixtures = ',I3,/,
.          ' and the increment between solutions = ',F7.4,/)
1250 FORMAT(//, ' *****This solution is to be mixed with the',

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MIX11740
MIX11750
MIX11760
MIX11770
MIX11780
MIX11790
MIX11800
MIX11810
MIX11820
MIX11830
MIX11840
MIX11850
MIX11860
MIX11870
MIX11880
MIX11890
MIX11900
MIX11910
MIX11920
MIX11930
MIX11940
MIX11950
MIX11960
MIX11970
MIX11980
MIX11990
MIX12000
MIX12010
MIX12020
MIX12030
MIX12040
MIX12050
MIX12060
MIX12070
MIX12080
MIX12090
MIX12100
MIX12110
MIX12120
MIX12130
MIX12140
MIX12150
MIX12160
MIX12170
MIX12180
MIX12190
MIX12200
MIX12210
MIX12220
MIX12230
MIX12240
MIX12250
MIX12260
MIX12270
MIX12280
MIX12290
MIX12300
MIX12310

```

' next solution.....', /)

END

MIX12320

MIX12330

MIX12340

SUBROUTINE NACALC (TC, CM, PE, RLG, P, GLO)			NAC 0010
C	=====		NAC 0020
C	Program chaos2.f4-a routine for calculating thermo. properties		NAC 0030
C	of nacl(aq) using pitzer's new model. 0.0-osmotic;		NAC 0040
C	-----		NAC 0050
C	AC	DBL Charge of the anions	NAC 0060
C	ALPHA	DBL Coefficient of thermal expansion	NAC 0070
C	AN	DBL Number of anions	NAC 0080
C	AP	DBL Debye-huckel osmotic parameter	NAC 0090
C	AVN	DBL Avogadro's number	NAC 0100
C	B0	DBL Beta zero parameter	NAC 0110
C	B1	DBL Beta one parameter	NAC 0120
C	BETAL	DBL Coefficient of compressibility	NAC 0130
C	BK	DBL Boltzmann's constant in erg/deg	NAC 0140
C	C	DBL C sub fee parameter	NAC 0150
C	CC	DBL Charge of the cations	NAC 0160
C	CI	DBL Ionic Strength	NAC 0170
C	CM	DBL Sum of Molality * charge / 2	NAC 0180
C	CN	DBL Number of cations	NAC 0190
C	DC	DBL Dielectric constant of water	NAC 0200
C	DCDT	DBL Derivative of dielectric constant water T	NAC 0210
C	DW	DBL Density of water	NAC 0220
C	E	DBL Electron charge in esu	NAC 0230
C	F1I	DBL Intermediate storage variable	NAC 0240
C	F2I	DBL Intermediate storage variable	NAC 0250
C	F3I	DBL Intermediate storage variable	NAC 0260
C	F4I	DBL Intermediate storage variable	NAC 0270
C	GLO	DBL Gibbs free energy per mole	NAC 0280
C	I	INT Loop variable	NAC 0290
C	P	DBL Fit constants	NAC 0300
C	P0	DBL Vapor pressure	NAC 0310
C	PE	DBL Pressure in bars	NAC 0320
C	PHI	DBL Osmotic coefficient	NAC 0330
C	PI	DBL The constant Pi	NAC 0340
C	PX	DBL Calculated pressure of water	NAC 0350
C	RLG	DBL Natural log of the activity coefficient	NAC 0360
C	SCI	DBL Square root of the ionic strength	NAC 0370
C	T	DBL Temperature in kelvin	NAC 0380
C	TC	DBL Temperature in celcius	NAC 0390
C	VF1	DBL Intermediate storage variable	NAC 0400
C	VF2	DBL Intermediate storage variable	NAC 0410
C	VF3	DBL Intermediate storage variable	NAC 0420
C	XP0	DBL Intermediate storage variable	NAC 0430
C	XP1	DBL Intermediate storage variable	NAC 0440
C	XP2	DBL Intermediate storage variable	NAC 0450
C	XP3	DBL Intermediate storage variable	NAC 0460
C	XP4	DBL Intermediate storage variable	NAC 0470
C	XP5	DBL Intermediate storage variable	NAC 0480
C	XP6	DBL Intermediate storage variable	NAC 0490
C	XP7	DBL Intermediate storage variable	NAC 0500

C	XP8	DBL	Intermediate storage variable	NAC 0510
C	XP9	DBL	Intermediate storage variable	NAC 0520
C	XS	DBL	Intermediate storage variable	NAC 0530
C	-----			NAC 0540
	INTEGER I			NAC 0550
				NAC 0560
				NAC 0570
	DOUBLE PRECISION AC, ALPHA, AN, AP, AVN			NAC 0580
	DOUBLE PRECISION BO, B1, BETAL, BK			NAC 0590
	DOUBLE PRECISION C, CC, CI, CM, CN			NAC 0600
	DOUBLE PRECISION DC, DCDT, DW, E			NAC 0610
	DOUBLE PRECISION F1I, F2I, F3I, F4I, GLO			NAC 0620
	DOUBLE PRECISION P(60), PO, PE, PI, PHI, PX			NAC 0630
	DOUBLE PRECISION RLG, SCI, T, TC			NAC 0640
	DOUBLE PRECISION VF1, VF2, VF3, XS			NAC 0650
	DOUBLE PRECISION XP0, XP1, XP2, XP3, XP4, XP5, XP6, XP7, XP8, XP9			NAC 0660
				NAC 0670
	EXTERNAL PSAT, WAPVT, WDBP			NAC 0680
				NAC 0690
	INTRINSIC DABS, DEXP, DLOG, DSQRT			NAC 0700
				NAC 0710
	DATA AVN, BK, E, PI /6.02251D+23, 1.38054D-16,			NAC 0720
	4.80298D-10, 3.1415926D+0/			NAC 0730
				NAC 0740
C	=====			NAC 0750
				NAC 0760
C	-----			NAC 0770
C	CC & AC = Cation and anion charge			NAC 0780
C	-----			NAC 0790
				NAC 0800
	CC = P(54)			NAC 0810
	AC = P(55)			NAC 0820
				NAC 0830
C	-----			NAC 0840
C	CN & AN = Number of cations and anions			NAC 0850
C	-----			NAC 0860
				NAC 0870
	CN = P(56)			NAC 0880
	AN = P(57)			NAC 0890
				NAC 0900
C	-----			NAC 0910
C	TC = Temp(C); CM = Molality; CI = Ionic Strength			NAC 0920
C	-----			NAC 0930
				NAC 0940
	T = TC + 273.15D+0			NAC 0950
	CI = (CC**2 * CN + AC**2 * AN) * CM / 2.0			NAC 0960
				NAC 0970
C	-----			NAC 0980
C	Calculate saturation vapor pressure, P0			NAC 0990
C	-----			NAC 1000
				NAC 1010
	CALL PSAT (TC, P0)			NAC 1020
				NAC 1030
C	-----			NAC 1040
C	If desired, set PE = P0			NAC 1050
C	-----			NAC 1060
				NAC 1070
	IF (PE .LT. 1.0) PE = P0			NAC 1080

		NAC 1090
C	-----	NAC 1100
C	Set PE = One bar. if temp. less than 100C	NAC 1110
C	-----	NAC 1120
	IF (TC .LT. 100.1) PE = 1.0	NAC 1130
		NAC 1140
		NAC 1150
	XP0 = P(18) + (P(19) * PE) + (P(20) * PE**2) + (P(21) * PE**3)	NAC 1160
	XP1 = P(23) + (P(24) * PE) + (P(25) * PE**2) + (P(26) * PE**3)	NAC 1170
	XP2 = P(27) + (P(28) * PE) + (P(29) * PE**2)	NAC 1180
	XP3 = P(30) + (P(31) * PE) + (P(32) * PE**2) + (P(33) * PE**3)	NAC 1190
	XP4 = P(34) + (P(35) * PE) + (P(36) * PE**2) + (P(37) * PE**3)	NAC 1200
	XP5 = P(43) + (P(44) * PE)	NAC 1210
	XP6 = P(46) + (P(47) * PE)	NAC 1220
	XP7 = P(48) + (P(49) * PE)	NAC 1230
	XP8 = P(50) + (P(51) * PE)	NAC 1240
	XP9 = P(52) + (P(53) * PE)	NAC 1250
		NAC 1260
C	-----	NAC 1270
C	Initialize loop to calculate density, DW	NAC 1280
C	-----	NAC 1290
	DW = 1.0	NAC 1300
	PX = 1.0	NAC 1310
	DO 10 I = 1, 100	NAC 1320
	CALL WAPVT (TC, DW, PX, BETAL, GLO, ALPHA)	NAC 1330
	XS = DW	NAC 1340
	DW = DW / DEXP(BETAL * (PX - PE))	NAC 1350
	IF (DABS((DW-XS)/XS) .LT. 1.0D-10) GO TO 20	NAC 1360
	10 CONTINUE	NAC 1370
		NAC 1380
		NAC 1390
C	-----	NAC 1400
C	Calculate dielectric properties of water	NAC 1410
C	-----	NAC 1420
		NAC 1430
	20 CONTINUE	NAC 1440
	CALL WDBP (TC, PE, DC, DCDT)	NAC 1450
		NAC 1460
C	-----	NAC 1470
C	AP = Debye-huckel osmotic parameter	NAC 1480
C	-----	NAC 1490
		NAC 1500
	AP = (1.0 / 3.0) * DSQRT(2.0 * PI * AVN * DW / 1000.0) * (E**2 / (DC * BK * T))**1.5	NAC 1510
		NAC 1520
		NAC 1530
C	-----	NAC 1540
C	Calculate functions of ionic strength	NAC 1550
C	-----	NAC 1560
		NAC 1570
	SCI = DSQRT(CI)	NAC 1580
	F1I = DEXP(-2.0 * SCI)	NAC 1590
		NAC 1600
C	-----	NAC 1610
C	Is RLG a heat quantity ?	NAC 1620
C	-----	NAC 1630
		NAC 1640
	F2I = SCI / (1.0 + 1.2 * SCI)	NAC 1650
	F3I = (2.0 / 1.2) * DLOG(1.0 + 1.2 * SCI)	NAC 1660

	F4I = (1.0 - (1.0 + 2.0 * SCI - 4.0 * CI / 2.0) * F1I) /	NAC 1670
	(4.0 * CI)	NAC 1680
		NAC 1690
C	-----	NAC 1700
C	Calculate valence factors	NAC 1710
C	-----	NAC 1720
		NAC 1730
	VF1 = CC * AC	NAC 1740
	VF2 = 2.0 * CN * AN / (CN + AN)	NAC 1750
	VF3 = 2.0 * (CN * AN)**1.5 / (CN + AN)	NAC 1760
		NAC 1770
C	-----	NAC 1780
C	B0, B1, & C are parameters BETA0, BETA1, & C(superscript phi) in	NAC 1790
C	pitzer's equations. B0, B1, & C are calculated as functions of	NAC 1800
C	temp. In terms of the adjustable parameters, P(I)	NAC 1810
C	-----	NAC 1820
		NAC 1830
	B0 = P(17) / T + XP0 + P(22) * DLOG(T) + XP1 * T + XP2 * T**2 +	NAC 1840
	XP3 / (T - 227.0) + XP4 / (680.0 - T)	NAC 1850
	B1 = P(38) / T + P(39) + P(40) * T + P(41) / (T - 227.0)	NAC 1860
	C = P(42) / T + XP5 + P(45) * DLOG(T) + XP6 * T + XP7 * T**2 +	NAC 1870
	XP8 / (T - 227.0) + XP9 / (680.0 - T)	NAC 1880
		NAC 1890
C	-----	NAC 1900
C	PHI = Osmotic Coefficient	NAC 1910
C	-----	NAC 1920
		NAC 1930
	PHI = 1.0 - VF1 * AP * F2I + CM * VF2 * (B0 + B1 * F1I) +	NAC 1940
	CM**2 * VF3 * C	NAC 1950
		NAC 1960
C	-----	NAC 1970
C	RLG = Ln Gamma	NAC 1980
C	-----	NAC 1990
		NAC 2000
	RLG = -VF1 * AP * (F2I + F3I) + CM * 2.0 * VF2 * (B0 + B1 * F4I) + 1.5 * CM**2 * VF3 * C	NAC 2010
		NAC 2020
		NAC 2030
	RETURN	NAC 2040
	END	NAC 2050

	SUBROUTINE PAGE	PAG 0010
C	=====	PAG 0020
C	Writes a form feed into output file, increments page number, and	PAG 0030
C	resets line count	PAG 0040
C	-----	PAG 0050
C	IPAGE INT Current page number of output file	PAG 0060
C	IPGLN INT Current line number of the output file	PAG 0070
C	TOF CHA Places a form feed in output file	PAG 0080
C	UNO INT File unit assigned for output file	PAG 0090
C	-----	PAG 0100
		PAG 0110
	INTEGER UNO	PAG 0120
	PARAMETER (UNO = 6)	PAG 0130
		PAG 0140

INTEGER IPAGE, IPGLN	PAG 0150
	PAG 0160
CHARACTER * 1 TOF, CR	PAG 0170
CHARACTER * 40 TITMIX	PAG 0180
	PAG 0190
COMMON /FMFD/ TOF, CR, TITMIX	PAG 0200
COMMON /FORM/ IPAGE, IPGLN	PAG 0210
	PAG 0220
C -----	PAG 0230
	PAG 0240
IPAGE = IPAGE + 1	PAG 0250
WRITE (UNO, 100) TOF, IPAGE	PAG 0260
IPGLN = 4	PAG 0270
	PAG 0280
RETURN	PAG 0290
	PAG 0300
100 FORMAT (A1,60X,' PAGE - ',I4,' - ',///)	PAG 0310
	PAG 0320
END	PAG 0330

SUBROUTINE PCLOGK (TCENT, PS, PRES, MXAQK, MXPC)	PCL 0010
C -----	PCL 0020
C Determines the pressure correction on log K values if pressure	PCL 0030
C is greater than vapor pressure of water	PCL 0040
C -----	PCL 0050
C A DBL Fit constants	PCL 0060
C AHI DBL Pressure correction fit parameter	PCL 0070
C AL DBL Fit constant	PCL 0080
C ALLOW DBL Pressure correction fit parameter	PCL 0090
C B DBL Intermediate storage variable	PCL 0100
C B0 DBL Fit constant	PCL 0110
C B1 DBL Fit constant	PCL 0120
C B2 DBL Fit constant	PCL 0130
C B4 DBL Fit constant	PCL 0140
C BB DBL Intermediate storage variable	PCL 0150
C BBO DBL Fit constant	PCL 0160
C BEETO DBL Coefficient of isothermal compressibility of	PCL 0170
C water at temperature T	PCL 0180
C BET DBL Fit constant	PCL 0190
C BETA0 DBL Compressibility of water at 5 degree increments	PCL 0200
C starting a 5 deg. along the saturation curve	PCL 0210
C BHI DBL Pressure correction fit parameter	PCL 0220
C BLOW DBL Pressure correction fit parameter	PCL 0230
C C DBL Fit constant	PCL 0240
C CHI DBL Pressure correction fit parameter	PCL 0250
C CLOW DBL Pressure correction fit parameter	PCL 0260
C CPUMIN DBL Smallest positive real value program uses	PCL 0270
C D DBL Fit constant	PCL 0280
C DELK DBL Correction factor to log K of aqueous species	PCL 0290
C DELKHI DBL Adjusted log k at 1000 bars	PCL 0300
C DELKLO DBL Adjusted log k at 500 bars	PCL 0310
C DELVR DBL Change in volume at 25 degrees	PCL 0320
C DELW DBL Log K adjustment to water reaction	PCL 0330
C DLRR0 DBL Intermediate storage variable	PCL 0340

C	DPR	DBL	Intermediate storage variable	PCL 0350
C	E	DBL	Fit constant	PCL 0360
C	ER	DBL	Intermediate storage variable	PCL 0370
C	GAM	DBL	Fit constant	PCL 0380
C	I	INT	Loop variable	PCL 0390
C	ICOUNT	INT	Keeps track of number of times density is calc.	PCL 0400
C	IDB0	INT	Temperature pointer to compressibility constant	PCL 0410
C	J	INT	Loop variable	PCL 0420
C	LOGKP	DBL	Correction factor to log K for the minerals	PCL 0430
C	LOGKT1	DBL	Log K for aqueous species at specified temp.	PCL 0440
C	LOGKT2	DBL	Log K for minerals at specified temperature	PCL 0450
C	MXAQK	INT	Total number of aqueous log k values	PCL 0460
C	MXPC	INT	Total number of mineral pressure constants	PCL 0470
C	N	INT	Loop variable	PCL 0480
C	NH2O	DBL	Number of water ionization reactions	PCL 0490
C	NMAX	INT	General array dimension to allow easy expansion	PCL 0500
C	P	DBL	Intermediate storage variable	PCL 0510
C	PADJ	DBL	Adjusted pressure (Total press. - Sat. press.)	PCL 0520
C	PPP	DBL	Intermediate storage variable	PCL 0530
C	PR	DBL	Intermediate storage variable	PCL 0540
C	PRES	DBL	Total pressure	PCL 0550
C	PS	DBL	Saturation pressure	PCL 0560
C	R	DBL	Gas constant in cm**3 * bar / gram * deg. K	PCL 0570
C	RO	DBL	Density of water at T along the saturation curve	PCL 0580
C	RCAL	DBL	Gas constant in therm cal / mole * deg. K	PCL 0590
C	RH	DBL	Intermediate storage variable	PCL 0600
C	RHN	DBL	Intermediate storage variable	PCL 0610
C	RHO	DBL	Density of water at P, T	PCL 0620
C	S	DBL	Intermediate storage variable	PCL 0630
C	T	DBL	Temperature in degrees K	PCL 0640
C	TAU	DBL	T / T critical	PCL 0650
C	TCENT	DBL	Temperature in degrees C	PCL 0660
C	TEST1	DBL	Test to check for proper density	PCL 0670
C	TEST2	DBL	Test to check for proper pressure	PCL 0680
C	UNO	INT	File unit assigned for output file	PCL 0690
C	VH2O	DBL	Change change of water at the saturation pressure	PCL 0700
C	VRIC	DBL	Isocoulombic volume change for the reaction	PCL 0710
C	Y	DBL	Intermediate storage variable	PCL 0720
C	-----			PCL 0730
	INTEGER NMAX, UNO			PCL 0740
	DOUBLE PRECISION CPUMIN			PCL 0750
	PARAMETER (NMAX = 340, UNO = 6, CPUMIN = 1.0D-35)			PCL 0760
				PCL 0770
	INTEGER I, ICOUNT, IDB0, J, MXAQK, MXPC, N			PCL 0780
				PCL 0790
	DOUBLE PRECISION A(9,7), AHI(200), AL, ALOW(200)			PCL 0800
	DOUBLE PRECISION B, B0, B1, B2, B4, BB, BBO, BEETO, BET			PCL 0810
	DOUBLE PRECISION BETA0(70), BHI(200), BLOW(200)			PCL 0820
	DOUBLE PRECISION C, CHI(200), CLOW(200)			PCL 0830
	DOUBLE PRECISION D, DELK, DELKHI(200), DELKLO(200), DELVR(NMAX)			PCL 0840
	DOUBLE PRECISION DELW, DLRRO, DPR, E, ER, GAM			PCL 0850
	DOUBLE PRECISION LOGKP, LOGKT1(NMAX), LOGKT2(NMAX)			PCL 0860
	DOUBLE PRECISION NH2O(NMAX)			PCL 0870
	DOUBLE PRECISION P, PADJ, PPP, PR, PRES, PS			PCL 0880
	DOUBLE PRECISION R, RO, RCAL, RH, RHN, RHO			PCL 0890
	DOUBLE PRECISION S, T, TAU, TCENT, TEST1, TEST2			PCL 0900
	DOUBLE PRECISION VH2O, VRIC, Y			PCL 0910
				PCL 0920

INTRINSIC DABS, DEXP, DLOG, DLOG10	PCL 0930
	PCL 0940
COMMON /ALOGK/ LOGKT1, LOGKT2	PCL 0950
COMMON /PTK / DELVR, NH2O, ALOW, BLOW, CLOW, AHI, BHI, CHI	PCL 0960
	PCL 0970
	PCL 0980
DATA AL, BET, GAM /11.0, 44.3333333, 3.5/	PCL 0990
DATA B0, C, D /.747862916, -.354078223, .007159876/	PCL 1000
DATA E / -.003528426/	PCL 1010
DATA BB0, B1, B2 /1.127833441, -.594400123, -5.010995915/	PCL 1020
DATA B4 / 0.636842555/	PCL 1030
DATA R, RCAL, VH2O /4.61518, 1.9872, 21.1/	PCL 1040
	PCL 1050
DATA A /0.0, 0.0, 68833.257944332, 0.0, 0.0, 0.0, 0.0,	PCL 1060
. 0.0, 0.0, -5306.2968529023, 178638.32875422,	PCL 1070
. -2563743.6613260, 11797433.655832, -31377774.947767,	PCL 1080
. 46561826.115608, -31555231.392127, 0.0, 6962522.0862664,	PCL 1090
. 22744.901424408, -395147.31563338, 4821257.5981415,	PCL 1100
. -21734810.110373, 52911910.757704, -72752773.275387,	PCL 1110
. 47929666.384584, 0.0, -10834900.096447, -26627.944829770,	PCL 1120
. 0.0, 217572.45522644, 0.0, -707304.18082074, 0.0, 0.0,	PCL 1130
. 0.0, 0.0, 7877.9333020687, 338038.84280753,	PCL 1140
. -3418301.6969660, 10829952.168620, -13802577.177877,	PCL 1150
. 4177424.6148294, 4091266.4781209, 0.0, -2272282.7401688,	PCL 1160
. 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,	PCL 1170
. -698.30527374994, -138550.50202703, 1222315.6417448,	PCL 1180
. -2544199.8064049, -2510991.4369001, 14016358.244614,	PCL 1190
. -13626369.388386, 0.0, 3836548.6000660/	PCL 1200
	PCL 1210
DATA BETA0 /49.48, 48.26, 47.19, 46.33, 45.60, 45.06, 44.69,	PCL 1220
. 44.46, 44.35, 44.36, 44.48, 44.69, 45.01, 45.41,	PCL 1230
. 45.89, 46.46, 47.10, 47.82, 48.62, 49.50, 50.46,	PCL 1240
. 51.50, 52.62, 53.83, 55.12, 56.51, 57.99, 59.58,	PCL 1250
. 61.28, 63.09, 65.03, 67.10, 69.32, 71.69, 74.24,	PCL 1260
. 76.96, 79.89, 83.04, 86.43, 90.09, 94.77, 99.45,	PCL 1270
. 104.12, 108.80, 113.48, 120.78, 128.07, 135.37, 142.46,	PCL 1280
. 149.96, 162.28, 174.59, 186.91, 199.22, 211.54, 235.04,	PCL 1290
. 258.55, 282.05, 305.55, 329.06, 384.78, 440.50, 496.21,	PCL 1300
. 551.93, 607.65, 825.89, 1044.13, 1262.37, 1480.61, 1698.85/	PCL 1310
	PCL 1320
C =====	PCL 1330
	PCL 1340
IDB0 = TCENT / 5	PCL 1350
BEETO = BETA0(IDB0) / 10.0**6.0	PCL 1360
T = TCENT + 273.15	PCL 1370
TAU = T / 647.073	PCL 1380
ICOUNT = 1	PCL 1390
P = PS	PCL 1400
	PCL 1410
10 CONTINUE	PCL 1420
B = B0 + C * DLOG(TAU) + D / TAU**3 + E / TAU**5	PCL 1430
BB = BB0 + B1 / TAU + B2 / TAU**2 + B4 / TAU**4	PCL 1440
RH = 1.0	PCL 1450
IF (P .LT. PS) RH = 0.001	PCL 1460
PPP = P - 1.0D0	PCL 1470
IF(DABS(PPP) .LT. 1.0D-10 .AND. T .GT. 647.25) RH = 0.001	PCL 1480
	PCL 1490
DO 40 I = 1, 100	PCL 1500

Y = RH * B / 4.0	PCL 1510
ER = DEXP(-RH)	PCL 1520
PR = 0.0	PCL 1530
DPR = 0.0	PCL 1540
DO 30 N = 1, 9	PCL 1550
S = A(N,1)	PCL 1560
DO 20 J = 2, 7	PCL 1570
S = S + A(N,J) / TAU**(J-1)	PCL 1580
20 CONTINUE	PCL 1590
PR = PR + S * (1 - ER)**(N-1)	PCL 1600
DPR = DPR + S * (1 - ER)**(N-1) * (2 + RH * (N * ER - 1) /	PCL 1610
(1 - ER))	PCL 1620
30 CONTINUE	PCL 1630
PR = RH**2 * ER * PR + RH * R * T * ((1 + AL * Y +	PCL 1640
BET * Y**2) / (1-Y)**3 + 4 * Y * (BB / B - GAM))	PCL 1650
DPR = RH * ER * DPR + R * T * ((1 + 2 * AL * Y +	PCL 1660
3 * BET * Y**2) / (1-Y)**3 + 3 * Y * (1 + AL * Y +	PCL 1670
BET * Y**2) / (1-Y)**4 + 8 * Y * (BB / B - GAM))	PCL 1680
RHN = RH + (P - PR) / DPR	PCL 1690
TEST1 = DABS((RHN - RH) / RHN)	PCL 1700
TEST2 = DABS((P - PR) / P)	PCL 1710
IF (TEST1 .LT. 1.0D-6 .AND. TEST2 .LT. 1.0D-5) GO TO 50	PCL 1720
RH = RHN	PCL 1730
40 CONTINUE	PCL 1740
WRITE (UNO, 100) T, P, RHN	PCL 1750
RETURN	PCL 1760
50 CONTINUE	PCL 1770
IF (ICOUNT .EQ. 1) THEN	PCL 1780
R0 = RHN	PCL 1790
P = PRES	PCL 1800
ICOUNT = ICOUNT + 1	PCL 1810
GO TO 10	PCL 1820
END IF	PCL 1830
RHO = RHN	PCL 1840
	PCL 1850
	PCL 1860
	PCL 1870
	PCL 1880
C -----	PCL 1890
C Calculate the effect of pressure on logk of water	PCL 1900
C -----	PCL 1910
	PCL 1920
DLRRO = DLOG10(RHO / R0)	PCL 1930
DELW = -19.0D0 * DLRRO	PCL 1940
LOGKT1(2) = LOGKT1(2) - DELW	PCL 1950
	PCL 1960
C -----	PCL 1970
C Adjust the logk of other species for the effect of pressure	PCL 1980
C -----	PCL 1990
	PCL 2000
DLRRO = DLRRO / (RCAL * T * BEETO)	PCL 2010
	PCL 2020
DO 60 I = 1, MXAQK	PCL 2030
IF (DABS(DELVR(I) - 0.0D0) .LT. 1.0D-10) GO TO 60	PCL 2040
VRIC = DELVR(I) + NH2O(I) * VH2O	PCL 2050
DELK = (VRIC / (-41.84D0) * DLRRO) - NH2O(I) * DELW	PCL 2060
LOGKT1(I) = LOGKT1(I) + DELK	PCL 2070
60 CONTINUE	PCL 2080

	PCL 2090
C -----	PCL 2100
C Adjust the logk of minerals using helgeson's data	PCL 2110
C -----	PCL 2120
PADJ = PRES - PS	PCL 2130
DO 90 I = 1, MXPC	PCL 2140
DELKLO(I) = ALOW(I) + BLOW(I) * TCENT + CLOW(I) * TCENT**6	PCL 2150
DELKHI(I) = AHI(I) + BHI(I) * TCENT + CHI(I) * TCENT**6	PCL 2160
	PCL 2170
IF ((500.0D0-PADJ) .LT. CPUMIN) THEN	PCL 2180
LOGKP = DELKLO(I) + ((DELKHI(I) - DELKLO(I)) *	PCL 2190
(PADJ - 500.0D0)) / 500.0D0	PCL 2200
ELSE	PCL 2210
LOGKP = DELKLO(I) * PADJ / 500.0D0	PCL 2220
END IF	PCL 2230
	PCL 2240
LOGKT2(I) = LOGKT2(I) + LOGKP	PCL 2250
90 CONTINUE	PCL 2260
	PCL 2270
RETURN	PCL 2280
	PCL 2290
100 FORMAT (/ , ' ** CONVERGENCE ON DENSITY NOT ACHIEVED ***' , / ,	PCL 2300
' PRESSURE CORRECTION FOR AQUEOUS AND SOLID' ,	PCL 2310
' EQUILIBRIA WILL NOT BE IMPLEMENTED ')	PCL 2320
	PCL 2330
END	PCL 2340
	PCL 2350

	PHC 0010
SUBROUTINE PHCALC (TEMP, HITEMP, CONV2, ITIC, ITWR, ISALT,	PHC 0020
IPHNUM, IPRIN2, *, *, *, *)	PHC 0030
C -----	PHC 0040
C Calculates pH when ever conditions change	PHC 0050
C -----	PHC 0060
C ALFA DBL Activity of aqueous species i	PHC 0070
C CO2F DBL Sum of CO2 plus CO2 lost from solution	PHC 0080
C CONV2 DBL Convergence test	PHC 0090
C CROSS LOG Have we crossed root yet?	PHC 0100
C CUNITS DBL Analytical input concentration	PHC 0110
C DCO2 DBL Concentration of CO2 lost before pH measurement	PHC 0120
C DH2S DBL Concentration of H2S lost before pH measurement	PHC 0130
C DIFTRY DBL Difference from root	PHC 0140
C DNH3 DBL Concentration of NH3 lost before pH measurement	PHC 0150
C DONE LOG Are we done yet?	PHC 0160
C HITEMP DBL In-situ temperature	PHC 0170
C HTOT DBL Total hydronium	PHC 0180
C HTOTI DBL Initial total hydronium	PHC 0190
C I INT Loop counter	PHC 0200
C II INT Counter and pointer	PHC 0210
C IOPT INT Switch for CO2 option	PHC 0220
C IPGLN INT Current line number of the output file	PHC 0230
C IPHNUM INT Counter used in PHCALC	PHC 0240
C IPRIN2 INT Flag for printing hydronium balance	PHC 0250
C ISALT INT Switch for what option	PHC 0260
C ITIC INT Hitemp distribution of carbonate species	

C	ITWR	INT	Switch to control printing of some headings	PHC 0270
C	JCO3	INT	Switch to control printing of some headings	PHC 0280
C	JJ	INT	Pointer to last point(s) calculated	PHC 0290
C	M	DBL	Calculated molality of aqueous species	PHC 0300
C	NDIM	INT	Identifies array dimension	PHC 0310
C	NMAX	INT	General array dimension to allow easy expansion	PHC 0320
C	OHTOT	DBL	Current sum of all OH- in solution	PHC 0330
C	OHTOTI	DBL	Target sum of all OH- in solution	PHC 0340
C	PH	DBL	Measured pH of the solution	PHC 0350
C	PHHIT	INT	HITEMP switch, used to control PHCALC	PHC 0360
C	PHINC	DBL	Parameter. Used to scale size of step	PHC 0370
C	PHTRY	DBL	Values of pH tried	PHC 0380
C	PPHHIT	INT	Switch to control calling PHCALC	PHC 0390
C	SCO2	DBL	Sum of CO2 species	PHC 0400
C	TEMP	DBL	Temperature of the solution when pH was measured	PHC 0410
C	TEST1	DBL	Current Hydronium-hydroxide balance	PHC 0420
C	TEST2	DBL	H - OH balance to shoot for	PHC 0430
C	TEST3	DBL	Test of how far are we from root	PHC 0440
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	PHC 0450
C	UNO	INT	File unit assigned for output file	PHC 0460
-----				PHC 0470
INTEGER NDIM, NMAX, UNO				PHC 0480
DOUBLE PRECISION PHINC				PHC 0490
PARAMETER (NDIM = 5, NMAX = 340, UNO = 6, PHINC = 1.0)				PHC 0500
				PHC 0510
INTEGER I, II, IOPT, IPAGE, IPGLN, IPHNUM, IPRIN2, ISALT				PHC 0520
INTEGER ITIC, ITWR, JCO3, JJ, PHHIT, PPHIT				PHC 0530
				PHC 0540
LOGICAL CROSS, DONE				PHC 0550
				PHC 0560
CHARACTER * 1 TOF, CR				PHC 0570
CHARACTER * 40 TITMIX				PHC 0580
				PHC 0590
				PHC 0600
DOUBLE PRECISION ALFA(NMAX), ANALM(NMAX), CO2F, CONV2				PHC 0610
DOUBLE PRECISION CUNITS(NMAX), DCH4, DDCH4, DCO2, DDCO2				PHC 0620
DOUBLE PRECISION DH2S, DDH2S, DNH3, DDNH3, DIFTRY(NDIM)				PHC 0630
DOUBLE PRECISION EXELT(35), FIXIT, HITEMP, HTOT, HTOTI				PHC 0640
DOUBLE PRECISION M(NMAX), OHTOT, OHTOTI, PH, PHTRY(NDIM)				PHC 0650
DOUBLE PRECISION SCO2, TEMP, TEST1, TEST2, TEST3				PHC 0660
DOUBLE PRECISION TITR(11), TOTEL(5)				PHC 0670
				PHC 0680
EXTERNAL GUESS, PAGE, SORTA				PHC 0690
				PHC 0700
INTRINSIC DABS, DLOG10, DSIGN				PHC 0710
				PHC 0720
COMMON /EXTOT / EXELT, TOTEL, TITR				PHC 0730
COMMON /FMFD / TOF, CR, TITMIX				PHC 0740
COMMON /FORM / IPAGE, IPGLN				PHC 0750
COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,				PHC 0760
DCH4, DDCH4, IOPT, FIXIT				PHC 0770
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS				PHC 0780
COMMON /TOTALS/ CO2F, HTOTI, OHTOTI				PHC 0790
COMMON /ZPH / PHHIT, PPHIT, JCO3, SCO2, HTOT, OHTOT				PHC 0800
				PHC 0810
SAVE CROSS, DIFTRY, JJ, PHTRY				PHC 0820
				PHC 0830
=====				PHC 0840

DONE = .FALSE.	PHC 0850
IF (PPHIT .NE. 1 .AND. PHHIT .EQ. 1) THEN	PHC 0860
IF (IPHNUM .LE. 0) THEN	PHC 0870
CROSS = .FALSE.	PHC 0880
END IF	PHC 0890
	PHC 0900
	PHC 0910
C -----	PHC 0920
C If this is the first round of Hi-T, initialize, and exit to	PHC 0930
C re-calculate the log K values and to setup the mass-balance	PHC 0940
C criteria.	PHC 0950
C -----	PHC 0960
IF (DABS(TEMP - HITEMP) .GT. 1.0D-10) THEN	PHC 0970
TEMP = HITEMP	PHC 0980
HTOTI = HTOT	PHC 0990
OHTOTI = OHTOT	PHC 1000
TOTEL(1) = HTOTI	PHC 1010
TOTEL(2) = OHTOTI	PHC 1020
TOTEL(3) = CO2F	PHC 1030
IF (ITIC .EQ. 1) ITIC = 2	PHC 1040
RETURN 1	PHC 1050
END IF	PHC 1060
	PHC 1070
ITWR = 1	PHC 1080
	PHC 1090
	PHC 1100
C -----	PHC 1110
C Get and test for convergence.	PHC 1120
C Use a difference if solution is neutral to avoid	PHC 1130
C a divide by zero.	PHC 1140
C -----	PHC 1150
TEST1 = HTOT - OHTOT	PHC 1160
TEST2 = HTOTI - OHTOTI + (2.0D0 * DCO2) + (2.0D0 * DH2S) - DNH3	PHC 1170
TEST3 = TEST1 - TEST2	PHC 1180
IF (DABS(TEST2) .GT. 1.0D-10 .AND. DABS(TEST1) .GT. 1.0D-10)	PHC 1190
THEN	PHC 1200
TEST3 = TEST3 / TEST2	PHC 1210
ELSE	PHC 1220
IF (DABS(TEST1) .GT. 1.0D-10) THEN	PHC 1230
TEST3 = TEST3 / TEST1	PHC 1240
ELSE IF (DABS(TEST2) .GT. 1.0D-35) THEN	PHC 1250
TEST3 = TEST3 / DSIGN(1.0D-10, TEST2)	PHC 1260
ELSE	PHC 1270
TEST3 = TEST3 / 1.0D-10	PHC 1280
END IF	PHC 1290
END IF	PHC 1300
	PHC 1310
IPHNUM = IPHNUM + 1	PHC 1320
JJ = IPHNUM	PHC 1330
IF (IPHNUM .EQ. 0) THEN	PHC 1340
ALFA(8) = 10.0D00**(-PH)	PHC 1350
RETURN 2	PHC 1360
END IF	PHC 1370
	PHC 1380
	PHC 1390
C -----	PHC 1400
C Store Values and Check if root has been found or crossed.	PHC 1410
C -----	PHC 1420

PHTRY(IPHNUM) = - DLOG10(ALFA(8))	PHC 1430
DIFTRY(IPHNUM) = TEST3	PHC 1440
IF (DABS(TEST2) .GT. 1.0D-08 .AND. DABS(TEST1) .GT. 1.0D-08)	PHC 1450
THEN	PHC 1460
IF (DABS(DIFTRY(IPHNUM)) .LT. CONV2) DONE = .TRUE.	PHC 1470
ELSE	PHC 1480
IF ((DABS(DIFTRY(IPHNUM))*1.0D-08) .LT. 1.0D-09) DONE = .TRUE.	PHC 1490
END IF	PHC 1500
IF (IPHNUM .GT. 1 .AND. .NOT. CROSS) THEN	PHC 1510
IF ((DIFTRY(IPHNUM) * DIFTRY(IPHNUM-1)) .LT. 0.0)	PHC 1520
CROSS = .TRUE.	PHC 1530
END IF	PHC 1540
C -----	PHC 1550
C If root has been found, sort into order	PHC 1560
C -----	PHC 1570
IF (CROSS) THEN	PHC 1580
CALL SORTA (PHTRY, DIFTRY, IPHNUM, JJ)	PHC 1590
IF (.NOT. DONE .AND. JJ .GT. 1) THEN	PHC 1600
IF ((DIFTRY(JJ) * DIFTRY(JJ-1)) .LT. 0.0) THEN	PHC 1610
IF (DABS(PHTRY(JJ) - PHTRY(JJ-1)) .LT. 5.0E-4)	PHC 1620
DONE = .TRUE.	PHC 1630
END IF	PHC 1640
END IF	PHC 1650
IF (.NOT. DONE .AND. JJ .LT. IPHNUM) THEN	PHC 1660
IF ((DIFTRY(JJ) * DIFTRY(JJ+1)) .LT. 0.0) THEN	PHC 1670
IF (DABS(PHTRY(JJ) - PHTRY(JJ+1)) .LT. 5.0E-4)	PHC 1680
DONE = .TRUE.	PHC 1690
END IF	PHC 1700
END IF	PHC 1710
END IF	PHC 1720
C -----	PHC 1730
C Due to small size only keep last NDIM-1 points	PHC 1740
C -----	PHC 1750
IF (IPHNUM .EQ. NDIM .AND. .NOT. DONE) THEN	PHC 1760
IF (.NOT. CROSS) THEN	PHC 1770
IPHNUM = (NDIM-1)	PHC 1780
DO 100 I = 1, (NDIM-1)	PHC 1790
PHTRY(I) = PHTRY(I+1)	PHC 1800
DIFTRY(I) = DIFTRY(I+1)	PHC 1810
100 CONTINUE	PHC 1820
JJ = JJ - 1	PHC 1830
END IF	PHC 1840
IF (CROSS) THEN	PHC 1850
DO 110 I = 1, (IPHNUM - 1)	PHC 1860
IF ((DIFTRY(I) * DIFTRY(I+1)) .LT. 0.0) II = I	PHC 1870
110 CONTINUE	PHC 1880
IF (II .GT. (IPHNUM / 2) .AND. JJ .NE. 1) THEN	PHC 1890
DO 120 I = 1, (NDIM-1)	PHC 1900
	PHC 1910
	PHC 1920
	PHC 1930
	PHC 1940
	PHC 1950
	PHC 1960
	PHC 1970
	PHC 1980
	PHC 1990
	PHC 2000

	PHTRY(I) = PHTRY(I+1)	PHC 2010
	DIFTRY(I) = DIFTRY(I+1)	PHC 2020
120	CONTINUE	PHC 2030
	JJ = JJ - 1	PHC 2040
	IPHNUM = NDIM - 1	PHC 2050
	ELSE	PHC 2060
	IPHNUM = NDIM - 1	PHC 2070
	END IF	PHC 2080
	END IF	PHC 2090
	END IF	PHC 2100
		PHC 2110
C	-----	PHC 2120
C	If root not yet crossed, keep trucking	PHC 2130
C	-----	PHC 2140
	IF (.NOT. DONE .AND. .NOT. CROSS) THEN	PHC 2150
	PH = PHTRY(IPHNUM)	PHC 2160
	IF (IPHNUM .EQ. 1) THEN	PHC 2170
	PH = PH - (DSIGN(1.0D00, (TEST2 - TEST1)) * PHINC)	PHC 2180
	ELSE	PHC 2190
	IF (DABS(DIFTRY(IPHNUM)) .GT. DABS(DIFTRY(IPHNUM-1))) THEN	PHC 2200
	PH = DIFTRY(IPHNUM)	PHC 2210
	DIFTRY(IPHNUM) = DIFTRY(IPHNUM-1)	PHC 2220
	DIFTRY(IPHNUM-1) = PH	PHC 2230
	PH = PHTRY(IPHNUM)	PHC 2240
	PHTRY(IPHNUM) = PHTRY(IPHNUM-1)	PHC 2250
	PHTRY(IPHNUM-1) = PH	PHC 2260
	PH = (2.0 * PHTRY(IPHNUM)) - PHTRY(IPHNUM-1)	PHC 2270
	JJ = IPHNUM - 1	PHC 2280
	ELSE	PHC 2290
	PH = (2.0 * PHTRY(IPHNUM)) - PHTRY(IPHNUM-1)	PHC 2300
	END IF	PHC 2310
	END IF	PHC 2320
	ALFA(8) = 10.0D00**(-PH)	PHC 2330
	END IF	PHC 2340
		PHC 2350
		PHC 2360
C	-----	PHC 2370
C	If root has been crossed, get new value of pH	PHC 2380
C	-----	PHC 2390
	IF (.NOT. DONE .AND. CROSS) THEN	PHC 2400
	CALL GUESS (PHTRY, DIFTRY, PH, IPHNUM)	PHC 2410
	ALFA(8) = 10.0D00**(-PH)	PHC 2420
	END IF	PHC 2430
		PHC 2440
		PHC 2450
C	-----	PHC 2460
C	Go and try again. Print if necessary	PHC 2470
C	-----	PHC 2480
	IF (.NOT. DONE) THEN	PHC 2490
	IF (IPRIN2 .NE. 0) THEN	PHC 2500
	IF (IPGLN .GT. 56) CALL PAGE	PHC 2510
	WRITE (UNO,1000) TEST2, TEST1, (TEST1 - TEST2), DIFTRY(JJ),	PHC 2520
	PHTRY(JJ), PH, (PH - PHTRY(JJ))	PHC 2530
	IPGLN = IPGLN + 3	PHC 2540
	END IF	PHC 2550
	RETURN 2	PHC 2560
	END IF	PHC 2570
		PHC 2580

		PHC 2590
C	-----	PHC 2600
C	Root has been found. Update appropriate variables and exit	PHC 2610
C	-----	PHC 2620
	PH = PHTRY(JJ)	PHC 2630
	IPHNUM = 0	PHC 2640
	IF (JCO3 .EQ. 1 .AND. IOPT .NE. 0) RETURN	PHC 2650
	IF (ISALT .GE. 2) RETURN 4	PHC 2660
	PPHHIT = 1	PHC 2670
	END IF	PHC 2680
		PHC 2690
		PHC 2700
	IF (PPHHIT .EQ. 1) THEN	PHC 2710
	IF (IOPT .EQ. 1) RETURN	PHC 2720
	TEST1 = HTOT - OHTOT	PHC 2730
	TEST2 = HTOTI - OHTOTI + (2.D0 * DCO2) + (2.0D0 * DH2S) - DNH3	PHC 2740
	IF (IPRIN2 .NE. 0) THEN	PHC 2750
	IF (IPGLN .GT. 53) CALL PAGE	PHC 2760
	WRITE (UNO,1010) PH, TEST2, TEST1, (TEST2 - TEST1)	PHC 2770
	IPGLN = IPGLN + 5	PHC 2780
	END IF	PHC 2790
	IF (JCO3 .EQ. 1) THEN	PHC 2800
	TOTEL(1) = TOTEL(1) + 2.0*DCO2	PHC 2810
	TOTEL(3) = TOTEL(3) + DCO2	PHC 2820
	END IF	PHC 2830
	RETURN 3	PHC 2840
	END IF	PHC 2850
		PHC 2860
C	-----	PHC 2870
C	Store some parameters for use in mixing / printing	PHC 2880
C	-----	PHC 2890
	IF (HTOTI .LT. 1.D-35) THEN	PHC 2900
	TOTEL(1) = HTOT	PHC 2910
	TOTEL(2) = OHTOT	PHC 2920
	ELSE	PHC 2930
	TOTEL(1) = HTOTI	PHC 2940
	TOTEL(2) = OHTOTI	PHC 2950
	END IF	PHC 2960
		PHC 2970
		PHC 2980
	TOTEL(3) = SCO2	PHC 2990
	TOTEL(4) = PH	PHC 3000
		PHC 3010
	IF (JCO3 .EQ. 1) THEN	PHC 3020
	TOTEL(1) = TOTEL(1) + 2.0*DCO2	PHC 3030
	TOTEL(3) = TOTEL(3) + DCO2	PHC 3040
	RETURN 2	PHC 3050
	END IF	PHC 3060
		PHC 3070
	RETURN	PHC 3080
		PHC 3090
1000	FORMAT (/ , ' (HTOTI-OHTOTI) = ',D16.8,' (HTOT-OHTOT) = ',D16.8,	PHC 3100
	, ' Difference = ',D16.8,' Test = ',D16.8,	PHC 3110
	, / , ' pH was: ', F8.4, ' New pH is: ', F8.4,	PHC 3120
	, ' Change = ', E12.5)	PHC 3130
1010	FORMAT (// , ' **** Convergence Achieved at pH= ', F8.4,	PHC 3140
	, / , ' (HTOTI-OHTOTI) = ',D16.8,	PHC 3150
	, ' (HTOT-OHTOT) = ', D16.8,	PHC 3160

Difference = ', D16.8, //)

PHC 3170

PHC 3180

END

PHC 3190

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SUBROUTINE PHOPT (ICCSAT, FCCSAT, ITWR, JCCST, *)          PHO 0010
C =====                                                PHO 0020
C   The following routine achieves CALCITE, DOLOMITE or SIDERITE | PHO 0030
C   saturation by adjusting pH. "ICCSAT" is equivalent to "IPHSAT" | PHO 0040
C   in the manual.                                           PHO 0050
C -----                                                PHO 0060
C   ALFA      DBL    Activity of aqueous species i          PHO 0070
C   CROSS     LOG    Have we crossed root yet?              PHO 0080
C   FCCSAT    DBL    Zero test                               PHO 0090
C   HFAC      DBL    Number of hydrogen ions in reaction from mineral | PHO 0100
C                   to dominate species                     PHO 0110
C   I         INT    Loop Variable and pointer              PHO 0120
C   ICCSAT    INT    Switch for pH option                   PHO 0130
C   IDK       INT    Index for log K of mineral (Cal, Dol, Sid) | PHO 0140
C   IID       INT    Index of dominate carbonate species    PHO 0150
C   IPGLN     INT    Current line number of the output file | PHO 0160
C   ITWR      INT    Switch to control printing of some headings | PHO 0170
C   JCCST     INT    Switch indicating if PHOPT called 1st time | PHO 0180
C   JJ        INT    Pointer to last value calculated       PHO 0190
C   KTF       DBL    Number of Carbonate groups in reaction | PHO 0200
C   LOGKT1    DBL    Log K for aqueous species at specified temp. | PHO 0210
C   LOGKT2    DBL    Log K for minerals at specified temperature | PHO 0220
C   LTTIAP    DBL    Log of activity product                PHO 0230
C   M         DBL    Calculated molality of aqueous species | PHO 0240
C   MAXCO2    DBL    Temp storage to determinate domin. Carb. species | PHO 0250
C   NMAX      INT    General array dimension to allow easy expansion | PHO 0260
C   NUM       INT    Number of SI/ pH points in arrays      PHO 0270
C   PH        DBL    Measured pH of the solution            PHO 0280
C   PHTRY     DBL    Values of pH tried                     PHO 0290
C   REVERS    LOG    Do we need to reverse to find root?    PHO 0300
C   SATNAM    CHA    Name of mineral to be saturated with   PHO 0310
C   SI        DBL    Current SI value                       PHO 0320
C   SITRY     DBL    Values of SIs obtained                 PHO 0330
C   STEP      DBL    Value used to change pH by            PHO 0340
C   TOFAR     LOG    Have we gone too far?                  PHO 0350
C   TTIAP     DBL    Activity product                       PHO 0360
C   TTKT      DBL    Log K for reaction                     PHO 0370
C   UNO       INT    File unit assigned for output file     PHO 0380
C -----                                                PHO 0390
C
C   INTEGER NMAX, UNO                                       PHO 0400
C   PARAMETER (NMAX = 340, UNO = 6)                         PHO 0410
C                                                           PHO 0420
C   INTEGER I, IAQ, ICCSAT, IDK, IID, IPAGE, IPGLN, ITWR    PHO 0430
C   INTEGER JJ, JCCST, NUM                                  PHO 0440
C                                                           PHO 0450
C   LOGICAL CROSS, TOFAR, REVERS                            PHO 0460
C                                                           PHO 0470
C   CHARACTER * 8 SATNAM(3)                                PHO 0480
C                                                           PHO 0490
C                                                           PHO 0500

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DOUBLE PRECISION ALFA(NMAX), ANALM(NMAX), CUNITS(NMAX), FCCSAT	PHO 0510
DOUBLE PRECISION HFAC, KTF, LOGKT1(NMAX), LOGKT2(NMAX), LTTIAP	PHO 0520
DOUBLE PRECISION M(NMAX), MAXCO2, PH, PHTRY(5), SI, SITRY(5)	PHO 0530
DOUBLE PRECISION STEP, TTIAP, TTKT	PHO 0540
	PHO 0550
EXTERNAL GUESS, PAGE, SORTA	PHO 0560
	PHO 0570
INTRINSIC DABS, DLOG10, DSIGN	PHO 0580
	PHO 0590
COMMON /ALOGK/ LOGKT1, LOGKT2	PHO 0600
COMMON /FORM / IPAGE, IPGLN	PHO 0610
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	PHO 0620
	PHO 0630
SAVE CROSS, NUM, PHTRY, REVERS, SITRY, STEP, TOFAR	PHO 0640
	PHO 0650
DATA SATNAM / 'CALCITE ', 'DOLOMITE', 'SIDERITE' /	PHO 0660
	PHO 0670
C =====	PHO 0680
	PHO 0690
C -----	PHO 0700
C Scan for the most abundant CO2 species	PHO 0710
C -----	PHO 0720
	PHO 0730
MAXCO2 = M(7)	PHO 0740
HFAC = ALFA(8)	PHO 0750
IID = 7	PHO 0760
	PHO 0770
DO 10 IAQ = 97, 98	PHO 0780
IF (M(IAQ) .GT. MAXCO2) THEN	PHO 0790
IF (IAQ .EQ. 97) HFAC = ALFA(8) ** 2.0	PHO 0800
IF (IAQ .EQ. 98) HFAC = 1.0	PHO 0810
MAXCO2 = M(IAQ)	PHO 0820
IID = IAQ	PHO 0830
END IF	PHO 0840
10 CONTINUE	PHO 0850
	PHO 0860
C -----	PHO 0870
C ICCSAT = 1 for Calcite; = 2 for Dolomite; = 3 for Siderite	PHO 0880
C	PHO 0890
C Assign the appropriate SI based on ICCSAT AND the most abundant	PHO 0900
C CO2 species	PHO 0910
C -----	PHO 0920
	PHO 0930
IF (ICCSAT .EQ. 1) THEN	PHO 0940
TTIAP = ALFA(1) * ALFA(IID) / HFAC	PHO 0950
LTTIAP = DLOG10(TTIAP)	PHO 0960
IDK = 24	PHO 0970
KTF = 1.0	PHO 0980
ELSE IF (ICCSAT .EQ. 2) THEN	PHO 0990
TTIAP = ALFA(1) * ALFA(2) * ALFA(IID)**2 / HFAC**2	PHO 1000
LTTIAP = DLOG10(TTIAP)	PHO 1010
IDK = 41	PHO 1020
KTF = 2.0	PHO 1030
ELSE	PHO 1040
TTIAP = ALFA(18) * ALFA(IID) / HFAC	PHO 1050
LTTIAP = DLOG10(TTIAP)	PHO 1060
IDK = 146	PHO 1070
KTF = 1.0	PHO 1080

END IF	PHO 1090
IF (IID .EQ. 98) TTKT = LOGKT2(IDK)	PHO 1100
IF (IID .EQ. 7) TTKT = LOGKT2(IDK) - KTF * LOGKT1(1)	PHO 1110
IF (IID .EQ. 97) TTKT = LOGKT2(IDK) - KTF * LOGKT1(1)	PHO 1120
	PHO 1130
	PHO 1140
	PHO 1150
C -----	PHO 1160
C First time here, initialize various switches, and get first	PHO 1170
C step.	PHO 1180
C -----	PHO 1190
	PHO 1200
IF (JCCST .LT. 1) THEN	PHO 1210
WRITE (UNO,1001) SATNAM(ICCSAT)	PHO 1220
IPGLN = IPGLN + 3	PHO 1230
IF (IPGLN .GT. 57) CALL PAGE	PHO 1240
NUM = 0	PHO 1250
STEP = -0.5	PHO 1260
CROSS = .FALSE.	PHO 1270
TOFAR = .FALSE.	PHO 1280
REVERS = .FALSE.	PHO 1290
JCCST = 1	PHO 1300
IF (IID .EQ. 98) THEN	PHO 1310
STEP = 0.5	PHO 1320
IF ((LTTIAP - TTKT) .GE. 0.0) STEP = -1.0	PHO 1330
ELSE	PHO 1340
KTF = 1.0	PHO 1350
IF (IID .EQ. 97) KTF = 2.0	PHO 1360
	PHO 1370
IF (IDK .EQ. 24) THEN	PHO 1380
STEP = TTKT - DLOG10(ALFA(1)) - DLOG10(ALFA(IID))	PHO 1390
STEP = STEP - (KTF * PH)	PHO 1400
STEP = STEP * 1.01 / KTF	PHO 1410
ELSE IF (IDK .EQ. 41) THEN	PHO 1420
STEP = TTKT - DLOG10(ALFA(1)) - DLOG10(ALFA(2))	PHO 1430
- (2.0 * DLOG10(ALFA(IID)))	PHO 1440
STEP = STEP - (2.0 * KTF * PH)	PHO 1450
STEP = STEP * 1.01 / (KTF * 2.0)	PHO 1460
ELSE IF (IDK .EQ. 146) THEN	PHO 1470
STEP = TTKT - DLOG10(ALFA(18)) - DLOG10(ALFA(IID))	PHO 1480
STEP = STEP - (KTF * PH)	PHO 1490
STEP = STEP * 1.01 / KTF	PHO 1500
END IF	PHO 1510
END IF	PHO 1520
END IF	PHO 1530
	PHO 1540
C -----	PHO 1550
C Check for saturation using the SI	PHO 1560
C If saturation not achieved, adjust pH	PHO 1570
C -----	PHO 1580
	PHO 1590
SI = LTTIAP - TTKT	PHO 1600
IF (DABS(SI) .GT. FCCSAT) THEN	PHO 1610
NUM = NUM + 1	PHO 1620
PHTRY(NUM) = PH	PHO 1630
SITRY(NUM) = SI	PHO 1640
JJ = NUM	PHO 1650
	PHO 1660

IF (NUM .GT. 1 .AND. .NOT. CROSS) THEN	PHO 1670
IF ((SI * SITRY(NUM-1)) .LT. 0.0) CROSS = .TRUE.	PHO 1680
END IF	PHO 1690
IF (.NOT. CROSS) THEN	PHO 1700
IF (NUM .GT. 1) THEN	PHO 1710
IF (DABS(SI) - DABS(SITRY(NUM-1)) .LE. 0.0) THEN	PHO 1720
STEP = STEP * 1.5	PHO 1730
REVERS = .FALSE.	PHO 1740
ELSE	PHO 1750
PH = PHTRY(NUM-1)	PHO 1760
SI = SITRY(NUM-1)	PHO 1770
PHTRY(NUM-1) = PHTRY(NUM)	PHO 1780
SITRY(NUM-1) = SITRY(NUM)	PHO 1790
PHTRY(NUM) = PH	PHO 1800
SITRY(NUM) = SI	PHO 1810
JJ = NUM - 1	PHO 1820
	PHO 1830
IF (REVERS) THEN	PHO 1840
STEP = STEP * (-0.3)	PHO 1850
ELSE	PHO 1860
IF (NUM .EQ. 2) THEN	PHO 1870
STEP = STEP * (-1.0)	PHO 1880
ELSE	PHO 1890
STEP = STEP * (0.5)	PHO 1900
END IF	PHO 1910
END IF	PHO 1920
	PHO 1930
REVERS = .TRUE.	PHO 1940
END IF	PHO 1950
END IF	PHO 1960
	PHO 1970
IF (DABS(STEP) .GT. 1.5) STEP = DSIGN(1.5D00, STEP)	PHO 1980
PH = PHTRY(NUM) + STEP	PHO 1990
	PHO 2000
IF (TOFAR) THEN	PHO 2010
WRITE (UNO,1002) SATNAM(ICCSAT), PH	PHO 2020
IPGLN = IPGLN + 3	PHO 2030
IF (IPGLN .GT. 57) CALL PAGE	PHO 2040
RETURN	PHO 2050
END IF	PHO 2060
	PHO 2070
IF (DABS(STEP) .LT. 0.01) THEN	PHO 2080
WRITE (UNO,1003) SATNAM(ICCSAT), PH	PHO 2090
IPGLN = IPGLN + 3	PHO 2100
IF (IPGLN .GT. 57) CALL PAGE	PHO 2110
RETURN	PHO 2120
END IF	PHO 2130
	PHO 2140
IF (PH .LT. 0.1) THEN	PHO 2150
PH = 0.1	PHO 2160
TOFAR = .TRUE.	PHO 2170
END IF	PHO 2180
	PHO 2190
IF (PH .GT. 13.9) THEN	PHO 2200
PH = 13.9	PHO 2210
TOFAR = .TRUE.	PHO 2220
END IF	PHO 2230
	PHO 2240

	IF (NUM .EQ. 4) THEN	PHO 2250
	DO 20 I = 2, 5	PHO 2260
	PHTRY(I-1) = PHTRY(I)	PHO 2270
	SITRY(I-1) = SITRY(I)	PHO 2280
20	CONTINUE	PHO 2290
	NUM = NUM - 1	PHO 2300
	JJ = JJ - 1	PHO 2310
	END IF	PHO 2320
	END IF	PHO 2330
	IF (CROSS) THEN	PHO 2340
	CALL SORTA (PHTRY, SITRY, NUM, JJ)	PHO 2350
	IF (NUM .GT. 3) THEN	PHO 2360
	IF ((SITRY(3) * SITRY(4)) .LT. 0.0) THEN	PHO 2370
	DO 30 I = 2, 4	PHO 2380
	SITRY(I-1) = SITRY(I)	PHO 2390
	PHTRY(I-1) = PHTRY(I)	PHO 2400
30	CONTINUE	PHO 2410
	NUM = NUM - 1	PHO 2420
	JJ = JJ - 1	PHO 2430
	ELSE IF ((SITRY(1) * SITRY(2)) .LT. 0.0) THEN	PHO 2440
	NUM = NUM - 1	PHO 2450
	ELSE IF (DABS(SITRY(1)) .GT. DABS(SITRY(4))) THEN	PHO 2460
	DO 40 I = 2, 4	PHO 2470
	SITRY(I-1) = SITRY(I)	PHO 2480
	PHTRY(I-1) = PHTRY(I)	PHO 2490
40	CONTINUE	PHO 2500
	NUM = NUM - 1	PHO 2510
	JJ = JJ - 1	PHO 2520
	ELSE	PHO 2530
	NUM = NUM - 1	PHO 2540
	END IF	PHO 2550
	END IF	PHO 2560
	CALL GUESS (PHTRY, SITRY, PH, NUM)	PHO 2570
	END IF	PHO 2580
	ALFA(8) = 10.0**(-PH)	PHO 2590
	WRITE (UNO,1004) SATNAM(ICCSAT), SITRY(JJ), PHTRY(JJ), PH	PHO 2600
	IPGLN = IPGLN + 3	PHO 2610
	IF (IPGLN .GT. 57) CALL PAGE	PHO 2620
	ITWR = 1	PHO 2630
	RETURN 1	PHO 2640
	END IF	PHO 2650
	RETURN	PHO 2660
1001	FORMAT (/ , ' Begining ',A8,' saturation by adjusting pH ',/)	PHO 2670
1002	FORMAT (//, ' ***** ',A8,' saturation NOT POSSIBLE for PH',	PHO 2680
	between 0.1 and 13.9; Last pH tried = ',F6.3)	PHO 2690
1003	FORMAT (//, ' ***** ',A8,' saturation NOT POSSIBLE for pH',	PHO 2700
	of ',F6.3,' as a staddle point seems to have',	PHO 2710
	been reached here.')	PHO 2720
1004	FORMAT (/ , ' Log SI (' ,A8,') = ',E13.4,' at a pH of ',F6.3,	PHO 2730
	Trying a new pH of ',F6.3,/)	PHO 2740
	END	PHO 2750
		PHO 2760
		PHO 2770
		PHO 2780
		PHO 2790
		PHO 2800
		PHO 2810
		PHO 2820

	SUBROUTINE PITZER (A, MU, MXSP, TEMP1, PGDCA, PGDNA, PG, TEMP,			PIT 0010
	PALFA, CO2TIT, Z, FLAG1)			PIT 0020
C	-----			PIT 0030
C	This routine calculates the pitzer activity coefficients.			PIT 0040
C	-----			PIT 0050
C	Local constants			PIT 0060
C	-----			PIT 0070
C	CPUMIN	DBL	Smallest value machine can represent	PIT 0080
C	NANI	INT	Number of Anions	PIT 0090
C	NCAT	INT	Number of Cations	PIT 0100
C	NMAX	INT	Number of aqueous species declariton	PIT 0110
C	NTEM	INT	Number of Temperatures	PIT 0120
C	UNP	INT	File unit of Pitzer Data	PIT 0130
C	-----			PIT 0140
C	Declare constants			PIT 0150
C	-----			PIT 0160
	INTEGER NANI, NCAT, NMAX, NTEM, UNP			PIT 0170
	DOUBLE PRECISION CPUMIN			PIT 0180
	PARAMETER (NCAT = 10, NANI = 5, NMAX = 340, NTEM = 11, UNP = 7)			PIT 0190
	PARAMETER (CPUMIN = 1.0D-35)			PIT 0200
				PIT 0210
C	-----			PIT 0220
C	Local variables			PIT 0230
C	-----			PIT 0240
C	A	DBL	Molal debeye-huckel coefficient	PIT 0250
C	ALFA	DBL	Activity of aqueous species i	PIT 0260
C	ANALM	DBL	Analyzed molality of species i	PIT 0270
C	ANI	INT	Selects anions with pitzer data	PIT 0280
C	B	DBL	B coefficient	PIT 0290
C	B0	DBL	Beta zero parameter for current temp	PIT 0300
C	B00	DBL	Array of B0's for all temps	PIT 0310
C	B1	DBL	Beta one parameter of current temp	PIT 0320
C	B11	DBL	Array of B1's for all temps	PIT 0330
C	BFEE	DBL	B sub fee coefficient	PIT 0340
C	BP	DBL	B prime coefficient	PIT 0350
C	BZ	DBL	Charge coefficient	PIT 0360
C	C	DBL	C coefficient	PIT 0370
C	CAT	INT	Selects cations with pitzer data	PIT 0380
C	CO2TIT	DBL	Analyzed molality of CO3 + HCO3	PIT 0390
C	CP	DBL	C sub fee parameter for current temp	PIT 0400
C	CPP	DBL	Array of CP's for all temps	PIT 0410
C	DIFF	DBL	Difference value for activities	PIT 0420
C	DONE	INT	Switch to determine when DIFF is OK	PIT 0430
C	ETHTA	DBL	E theta function for anions	PIT 0440
C	ETHTAP	DBL	E theta prime function for anions	PIT 0450
C	ETHTC	DBL	E theta function for cations	PIT 0460
C	ETHTCP	DBL	E theta prime function for cations	PIT 0470
C	F	DBL	Debye-huckel interaction term	PIT 0480
C	FEE	DBL	Osmotic coefficient	PIT 0490
C	FLAG1	INT	Water calculation flag	PIT 0500
C	G	DBL	Function to calculate coefficient values	PIT 0510
C	GP	DBL	Primed function to calculate coefficient values	PIT 0520
C	I	INT	Cation 1 loop variable	PIT 0530
C	II	INT	Cation loop variable	PIT 0540
C	ITER	INT	Iteration counter	PIT 0550
C	J	INT	Cation 2 loop variable	PIT 0560
C	K	INT	Anion 1 loop variable	PIT 0570
C	KK	INT	Anion loop variable	PIT 0580

C	KT1	DBL	Equilibrium constants for specified temp	PIT 0590
C	L	INT	Anion 2 loop variable	PIT 0600
C	LINE	CHA	Read in lines which contain no information	PIT 0610
C	LNGA	DBL	Ln anion gamma	PIT 0620
C	LNGC	DBL	Ln cation gamma	PIT 0630
C	LNGDCA	DBL	Ln gamma for divalent ions with no pitzer data	PIT 0640
C	LNGDNA	DBL	Ln gamma for monovalent ions with no pitzer data	PIT 0650
C	LOOP	INT	Loop Variable	PIT 0660
C	M	DBL	Calculated molality of aqueous species i	PIT 0670
C	MA	DBL	Moles of Anion	PIT 0680
C	MC	DBL	Moles of Cation	PIT 0690
C	MU	DBL	Ionic strength of aqueous solution	PIT 0700
C	MXSP	INT	Total number of aqueous species	PIT 0710
C	OHA	DBL	Hydroxide Activity	PIT 0720
C	PALFA	DBL	Pitzer activities	PIT 0730
C	PG	DBL	Pitzer gammas	PIT 0740
C	PGAMA	DBL	Pitzer Gammas for Anions	PIT 0750
C	PGAMC	DBL	Pitzer Gammas for Cations	PIT 0760
C	PGDCA	DBL	Gamma for divalent ions with no pitzer data	PIT 0770
C	PGDNA	DBL	Gamma for monovalent ions with no pitzer data	PIT 0780
C	PHIA	DBL	Phi anion coefficient	PIT 0790
C	PHIAP	DBL	Phi prime anion coefficient	PIT 0800
C	PHIC	DBL	Phi cation coefficient	PIT 0810
C	PHICP	DBL	Phi prime cation coefficient	PIT 0820
C	PSIA	DBL	Psi Anion-Anion-Cation parameter	PIT 0830
C	PSIAA	DBL	Array of PSIA for all Temps	PIT 0840
C	PSIC	DBL	Psi Cation-Cation-Anion parameter	PIT 0850
C	PSICC	DBL	Array of PSIC for all Temps	PIT 0860
C	SUM1	DBL	Internal sum for ln gamma calculations	PIT 0870
C	SUM2	DBL	Internal sum for ln gamma calculations	PIT 0880
C	SUM2A	DBL	Internal sum for ln gamma calculations	PIT 0890
C	SUM3	DBL	Internal sum for ln gamma calculations	PIT 0900
C	SUM4	DBL	Internal sum for ln gamma calculations	PIT 0910
C	SUM5	DBL	Internal sum for osmotic calculations	PIT 0920
C	SUM6	DBL	Internal sum for osmotic calculations	PIT 0930
C	SUM6A	DBL	Internal sum for osmotic calculations	PIT 0940
C	SUM7	DBL	Internal sum for osmotic calculations	PIT 0950
C	SUM7A	DBL	Internal sum for osmotic calculations	PIT 0960
C	SUM8	DBL	Internal sum for osmotic calculations	PIT 0970
C	TEMP	DBL	Array of 11 Temperatures	PIT 0980
C	TEMP1	DBL	Temperature of Interest	PIT 0990
C	THTA	DBL	Pitzer theta anion parameter	PIT 1000
C	THTAA	DBL	Array of THTA for all temps	PIT 1010
C	THTC	DBL	Pitzer theta cation parameter	PIT 1020
C	THTCC	DBL	Array of THTC for all temps	PIT 1030
C	TP	INT	Integer equivalent to temp(i)	PIT 1040
C	X	DBL	Independent variable in the G functions	PIT 1050
C	Z	INT	Charge of Aqueous Species i	PIT 1060
C	ZA	INT	Charge of the anions	PIT 1070
C	ZC	INT	Charge of the cations	PIT 1080
C	-----			PIT 1090
C	Declare variables			PIT 1100
C	-----			PIT 1110
	INTEGER ANI(NANI), CAT(NCAT), DONE, FLAG1			PIT 1120
	INTEGER I, II, ITER, J, K, KK, L, LOOP			PIT 1130
	INTEGER MXSP, TP, Z(NMAX), ZA(NANI), ZC(NCAT)			PIT 1140
				PIT 1150
	CHARACTER * 1 LINE			PIT 1160

	PIT 1170
DOUBLE PRECISION A, ALFA(NMAX), ANALM(NMAX), B(NCAT,NANI)	PIT 1180
DOUBLE PRECISION B0(NCAT,NANI), B00(NCAT,NANI,NTEM), B1(NCAT,NANI)	PIT 1190
DOUBLE PRECISION B11(NCAT,NANI,NTEM), BFEE(NCAT,NANI)	PIT 1200
DOUBLE PRECISION BP(NCAT,NANI), BZ	PIT 1210
DOUBLE PRECISION C(NCAT,NANI), CO2TIT, CP(NCAT,NANI)	PIT 1220
DOUBLE PRECISION CPP(NCAT,NANI,NTEM), CUNITS(NMAX), DIFF	PIT 1230
DOUBLE PRECISION ETHTA(NANI,NANI), ETHTAP(NANI,NANI)	PIT 1240
DOUBLE PRECISION ETHTC(NCAT,NCAT), ETHTGP(NCAT,NCAT), F, FEE	PIT 1250
DOUBLE PRECISION G, GP, KT1(NMAX), LNGA(NANI)	PIT 1260
DOUBLE PRECISION LNGC(NCAT), LNGDCA, LNGDNA, M(NMAX), MA(NANI)	PIT 1270
DOUBLE PRECISION MC(NCAT), MU, OHA, PALFA(NMAX)	PIT 1280
DOUBLE PRECISION PG(NMAX), PGAMA(NANI), PGAMC(NCAT), PGDCA, PGDNA	PIT 1290
DOUBLE PRECISION PH, PHIA(NANI,NANI), PHIAP(NANI,NANI)	PIT 1300
DOUBLE PRECISION PHIC(NCAT,NCAT), PHICP(NCAT,NCAT)	PIT 1310
DOUBLE PRECISION PSIA(NANI,NANI,NCAT), PSIAA(NANI,NANI,NCAT,NTEM)	PIT 1320
DOUBLE PRECISION PSIC(NCAT,NCAT,NANI), PSICC(NCAT,NCAT,NANI,NTEM)	PIT 1330
DOUBLE PRECISION SUM1, SUM2, SUM2A, SUM2B, SUM2C, SUM3, SUM4	PIT 1340
DOUBLE PRECISION SUM4B, SUM4C, SUM5, SUM6, SUM6A, SUM7, SUM7A	PIT 1350
DOUBLE PRECISION SUM8, TEMP(NTEM), TEMP1	PIT 1360
DOUBLE PRECISION THTA(NANI,NANI), THTAA(NANI,NANI,NTEM)	PIT 1370
DOUBLE PRECISION THTC(NCAT,NCAT), THTCC(NCAT,NCAT,NTEM), X	PIT 1380
	PIT 1390
EXTERNAL PTZINT	PIT 1400
	PIT 1410
INTRINSIC DABS, DEXP, DLOG, DSQRT, IABS	PIT 1420
	PIT 1430
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	PIT 1440
COMMON /TTK / KT1	PIT 1450
	PIT 1460
DATA ANI /5, 6, 7, 98, 9/	PIT 1470
DATA CAT /3, 4, 1, 2, 26, 15, 8, 14, 23, 27/	PIT 1480
	PIT 1490
C =====	PIT 1500
	PIT 1510
C -----	PIT 1520
C Open data table of pitzer coefficients	PIT 1530
C -----	PIT 1540
	PIT 1550
OPEN (UNP, FILE = 'PIT.TBL', STATUS = 'OLD')	PIT 1560
C OPEN (UNP, STATUS = 'OLD', shared, readonly)	PIT 1570
	PIT 1580
C -----	PIT 1590
C Initialize arrays of parameters and coefficients	PIT 1600
C -----	PIT 1610
	PIT 1620
DO 10 I = 1, NMAX	PIT 1630
PG(I) = 0.0D0	PIT 1640
10 CONTINUE	PIT 1650
	PIT 1660
DO 40 I = 1, NCAT	PIT 1670
DO 30 K = 1, NANI	PIT 1680
B0(I,K) = 0.0D0	PIT 1690
B1(I,K) = 0.0D0	PIT 1700
CP(I,K) = 0.0D0	PIT 1710
	PIT 1720
DO 20 TP = 1, NTEM	PIT 1730
B00(I,K,TP) = 0.0D0	PIT 1740

	B11(I,K,TP) = 0.0D0	PIT 1750
	CPP(I,K,TP) = 0.0D0	PIT 1760
20	CONTINUE	PIT 1770
		PIT 1780
30	CONTINUE	PIT 1790
40	CONTINUE	PIT 1800
		PIT 1810
	DO 70 I = 1, NCAT	PIT 1820
	DO 60 J = 1, NCAT	PIT 1830
	THTC(I,J) = 0.0D0	PIT 1840
		PIT 1850
	DO 50 TP = 1, NTEM	PIT 1860
	THTCC(I,J,TP) = 0.0D0	PIT 1870
50	CONTINUE	PIT 1880
		PIT 1890
60	CONTINUE	PIT 1900
70	CONTINUE	PIT 1910
		PIT 1920
	DO 100 K = 1, NANI	PIT 1930
	DO 90 L = 1, NANI	PIT 1940
	THTA(K,L) = 0.0D0	PIT 1950
		PIT 1960
	DO 80 TP = 1, NTEM	PIT 1970
	THTAA(K,L,TP) = 0.0D0	PIT 1980
80	CONTINUE	PIT 1990
		PIT 2000
90	CONTINUE	PIT 2010
100	CONTINUE	PIT 2020
		PIT 2030
	DO 140 I = 1, NCAT	PIT 2040
	DO 130 J = 1, NCAT	PIT 2050
	DO 120 K = 1, NANI	PIT 2060
	PSIC(I,J,K) = 0.0D0	PIT 2070
		PIT 2080
	DO 110 TP = 1, NTEM	PIT 2090
	PSICC(I,J,K,TP) = 0.0D0	PIT 2100
110	CONTINUE	PIT 2110
		PIT 2120
120	CONTINUE	PIT 2130
130	CONTINUE	PIT 2140
140	CONTINUE	PIT 2150
		PIT 2160
	DO 180 K = 1, NANI	PIT 2170
	DO 170 L = 1, NANI	PIT 2180
	DO 160 I = 1, NCAT	PIT 2190
	PSIA(K,L,I) = 0.0D0	PIT 2200
		PIT 2210
	DO 150 TP = 1, NTEM	PIT 2220
	PSIAA(K,L,I,TP) = 0.0D0	PIT 2230
150	CONTINUE	PIT 2240
		PIT 2250
160	CONTINUE	PIT 2260
170	CONTINUE	PIT 2270
180	CONTINUE	PIT 2280
		PIT 2290
	DO 190 I = 1, NCAT	PIT 2300
	LNGC (I) = 0.0D0	PIT 2310
	IF (I .LE. NANI) LNGA (I) = 0.0D0	PIT 2320

190 CONTINUE	PIT 2330
	PIT 2340
C -----	PIT 2350
C Read in data	PIT 2360
C -----	PIT 2370
	PIT 2380
DO 195 I = 1, 3	PIT 2390
READ (UNP, '(A1)') LINE	PIT 2400
195 CONTINUE	PIT 2410
	PIT 2420
DO 220 I = 1, 6	PIT 2430
DO 210 TP = 1, NTEM	PIT 2440
READ (UNP, 200) (B00(I,K,TP), B11(I,K,TP), CPP(I,K,TP),	PIT 2450
K = 1, 4)	PIT 2460
200 FORMAT (12(F10.5))	PIT 2470
210 CONTINUE	PIT 2480
DO 215 J = 1, 4	PIT 2490
READ (UNP, '(A1)') LINE	PIT 2500
215 CONTINUE	PIT 2510
220 CONTINUE	PIT 2520
	PIT 2530
DO 240 I = 7, 10	PIT 2540
DO 230 TP = 1, 2	PIT 2550
READ (UNP, 200) (B00(I,K,TP), B11(I,K,TP), CPP(I,K,TP),	PIT 2560
K = 1, 4)	PIT 2570
230 CONTINUE	PIT 2580
DO 235 J = 1, 4	PIT 2590
READ (UNP, '(A1)') LINE	PIT 2600
235 CONTINUE	PIT 2610
240 CONTINUE	PIT 2620
	PIT 2630
DO 260 LOOP = 1, 9	PIT 2640
READ (UNP, 250) I, J, (THTCC(I,J,TP), TP = 1, 11)	PIT 2650
250 FORMAT (2(I2), 1X, 11(F10.5))	PIT 2660
260 CONTINUE	PIT 2670
	PIT 2680
DO 265 I = 1, 3	PIT 2690
READ (UNP, '(A1)') LINE	PIT 2700
265 CONTINUE	PIT 2710
	PIT 2720
DO 270 LOOP = 1, 9	PIT 2730
READ (UNP, 250) K, L, (THTAA(K,L,TP), TP = 1, 11)	PIT 2740
270 CONTINUE	PIT 2750
	PIT 2760
DO 275 I = 1, 3	PIT 2770
READ (UNP, '(A1)') LINE	PIT 2780
275 CONTINUE	PIT 2790
	PIT 2800
DO 290 LOOP = 1, 19	PIT 2810
READ (UNP, 280) I, J, K, (PSICC(I,J,K,TP), TP = 1, 11)	PIT 2820
280 FORMAT (3(I2), 1X, 11(F10.5))	PIT 2830
290 CONTINUE	PIT 2840
	PIT 2850
DO 295 I = 1, 3	PIT 2860
READ (UNP, '(A1)') LINE	PIT 2870
295 CONTINUE	PIT 2880
	PIT 2890
DO 300 LOOP = 1, 20	PIT 2900

READ (UNP, 280) K, L, I, (PSIAA(K,L,I,TP), TP = 1, 11)	PIT 2910
300 CONTINUE	PIT 2920
CLOSE (UNP)	PIT 2930
	PIT 2940
	PIT 2950
C -----	PIT 2960
C Interpolate values from table to proper temperature	PIT 2970
C -----	PIT 2980
	PIT 2990
CALL PTZINT (TEMP, TEMP1, B0, B00, B1, B11, CP, CPP, THTC, THTCC,	PIT 3000
THTA, THTAA, PSIC, PSICC, PSIA, PSIAA)	PIT 3010
	PIT 3020
C -----	PIT 3030
C Initialize E sub theta functions	PIT 3040
C -----	PIT 3050
	PIT 3060
DO 320 I = 1, NCAT	PIT 3070
DO 310 J = 1, NCAT	PIT 3080
ETHTC(I,J) = 0.0D0	PIT 3090
ETHTCP(I,J) = 0.0D0	PIT 3100
310 CONTINUE	PIT 3110
320 CONTINUE	PIT 3120
	PIT 3130
DO 340 K = 1, NANI	PIT 3140
DO 330 L = 1, NANI	PIT 3150
ETHTA(K,L) = 0.0D0	PIT 3160
ETHTAP(K,L) = 0.0D0	PIT 3170
330 CONTINUE	PIT 3180
340 CONTINUE	PIT 3190
	PIT 3200
C -----	PIT 3210
C Initialize moles and charge for anions and cations	PIT 3220
C -----	PIT 3230
	PIT 3240
DO 350 I = 1, NCAT	PIT 3250
MC(I) = 0.0D0	PIT 3260
ZC(I) = 0	PIT 3270
IF (I .LE. NANI) THEN	PIT 3280
MA(I) = 0.0D0	PIT 3290
ZA(I) = 0	PIT 3300
END IF	PIT 3310
350 CONTINUE	PIT 3320
	PIT 3330
C -----	PIT 3340
C To avoid zerodivide the molality of unknown components in	PIT 3350
C pitzer is set = 0.001 mole	PIT 3360
C -----	PIT 3370
	PIT 3380
DO 360 I = 1, NCAT	PIT 3390
ZC(I) = Z(CAT(I))	PIT 3400
MC(I) = ANALM(CAT(I))	PIT 3410
IF (FLAG1 .NE. 1 .AND. I .EQ. 7) MC(I) = ALFA(8)	PIT 3420
IF (MC(I) .LT. CPUMIN) MC(I) = 1.0D-3	PIT 3430
360 CONTINUE	PIT 3440
	PIT 3450
DO 370 K = 1, NANI	PIT 3460
ZA(K) = Z(ANI(K))	PIT 3470
MA(K) = ANALM(ANI(K))	PIT 3480

IF (FLAG1 .NE. 1 .AND. K .EQ. 5)	PIT 3490
MA(K) = KT1(2) * ALFA(10) / ALFA(8)	PIT 3500
IF (MA(K) .LT. CPUMIN) MA(K) = 1.0D-3	PIT 3510
370 CONTINUE	PIT 3520
	PIT 3530
C -----	PIT 3540
C Determine ionic strength	PIT 3550
C -----	PIT 3560
MU = 0.0D0	PIT 3570
BZ = 0.0D0	PIT 3580
	PIT 3590
	PIT 3600
DO 380 I = 1, MXSP + 44	PIT 3610
MU = MU + ANALM(I) * Z(I)**2	PIT 3620
IF (Z(I) .NE. 0) BZ = BZ + ANALM(I) * IABS(Z(I))	PIT 3630
380 CONTINUE	PIT 3640
	PIT 3650
MU = 0.5 * MU	PIT 3660
	PIT 3670
C -----	PIT 3680
C Calculate g functions assuming alpha = 2.0	PIT 3690
C -----	PIT 3700
X = 2 * DSQRT(MU)	PIT 3710
G = 2 * (1 - (1 + X) * DEXP(-X)) / (X**2)	PIT 3720
GP = -2 * (1 - (1 + X + (0.5 * X**2)) * DEXP(-X)) / X**2	PIT 3730
	PIT 3740
	PIT 3750
C -----	PIT 3760
C Determine B, B', and C coefficients assuming beta(2)MX = 0.0	PIT 3770
C -----	PIT 3780
	PIT 3790
DO 400 I = 1, NCAT	PIT 3800
DO 390 K = 1, NANI	PIT 3810
C(I,K) = 0.0D0	PIT 3820
B(I,K) = 0.0D0	PIT 3830
BP(I,K) = 0.0D0	PIT 3840
	PIT 3850
IF (MC(I) .LT. CPUMIN) GO TO 400	PIT 3860
IF (MA(K) .LT. CPUMIN) GO TO 390	PIT 3870
B(I,K) = B0(I,K) + B1(I,K) * G	PIT 3880
BP(I,K) = B1(I,K) * GP / MU	PIT 3890
	PIT 3900
IF (ZC(I) .EQ. 0) GO TO 400	PIT 3910
IF (ZA(K) .EQ. 0) GO TO 390	PIT 3920
C(I,K) = CP(I,K) / (2 * ((IABS(ZC(I) * ZA(K)))**0.5))	PIT 3930
390 CONTINUE	PIT 3940
400 CONTINUE	PIT 3950
	PIT 3960
C -----	PIT 3970
C Determine Phi and Phi' cation coefficients	PIT 3980
C -----	PIT 3990
	PIT 4000
DO 420 I = 1, NCAT	PIT 4010
DO 410 J = 1, NCAT	PIT 4020
PHIC(I,J) = 0.0D0	PIT 4030
PHICP(I,J) = 0.0D0	PIT 4040
	PIT 4050
IF (MC(I) .LT. CPUMIN) GO TO 420	PIT 4060

IF (MC(J) .LT. CPUMIN) GO TO 410	PIT 4070
PHIC(I,J) = THTC(I,J) + ETHTC(I,J)	PIT 4080
PHICP(I,J) = ETHTCP(I,J)	PIT 4090
410 CONTINUE	PIT 4100
420 CONTINUE	PIT 4110
	PIT 4120
	PIT 4130
C -----	PIT 4140
C Determine Phi and Phi' anion coefficients	PIT 4150
C -----	PIT 4160
DO 440 K = 1, NANI	PIT 4170
DO 430 L = 1, NANI	PIT 4180
PHIA(K,L) = 0.0D0	PIT 4190
PHIAP(K,L) = 0.0D0	PIT 4200
	PIT 4210
	PIT 4220
IF (MA(K) .LT. CPUMIN) GO TO 440	PIT 4230
IF (MA(L) .LT. CPUMIN) GO TO 430	PIT 4240
	PIT 4250
PHIA(K,L) = THTA(K,L) + ETHTA(K,L)	PIT 4260
PHIAP(K,L) = ETHTAP(K,L)	PIT 4270
430 CONTINUE	PIT 4280
440 CONTINUE	PIT 4290
	PIT 4300
C -----	PIT 4310
C Determine first summation term to solve equation for F	PIT 4320
C -----	PIT 4330
SUM1 = 0.0D0	PIT 4340
	PIT 4350
	PIT 4360
DO 460 I = 1, NCAT	PIT 4370
DO 450 K = 1, NANI	PIT 4380
SUM1 = SUM1 + MC(I) * MA(K) * BP(I,K)	PIT 4390
450 CONTINUE	PIT 4400
460 CONTINUE	PIT 4410
	PIT 4420
C -----	PIT 4430
C Determine second summation term to solve equation for F	PIT 4440
C -----	PIT 4450
SUM2 = 0.0D0	PIT 4460
	PIT 4470
	PIT 4480
DO 480 I = 1, (NCAT-1)	PIT 4490
DO 470 J = (I+1), NCAT	PIT 4500
SUM2 = SUM2 + MC(I) * MC(J) * PHICP(I,J)	PIT 4510
470 CONTINUE	PIT 4520
480 CONTINUE	PIT 4530
	PIT 4540
C -----	PIT 4550
C Determine third summation term to solve equation for F	PIT 4560
C -----	PIT 4570
SUM3 = 0.0D0	PIT 4580
	PIT 4590
	PIT 4600
DO 500 K = 1, (NANI-1)	PIT 4610
DO 490 L = (K+1), NANI	PIT 4620
SUM3 = SUM3 + MA(K) * MA(L) * PHIAP(K,L)	PIT 4630
490 CONTINUE	PIT 4640

500	CONTINUE	PIT 4650
		PIT 4660
C	-----	PIT 4670
C	Solve for F	PIT 4680
C	-----	PIT 4690
	F = -0.768 * A * ((DSQRT(MU) / (1 + 1.2 * DSQRT(MU))) +	PIT 4700
	(2 / 1.2) * DLOG(1 + 1.2 * DSQRT(MU))) + SUM1 + SUM2 + SUM3	PIT 4710
		PIT 4720
		PIT 4730
C	-----	PIT 4740
C	Start to solve for ln activity coefficient of the cations	PIT 4750
C	-----	PIT 4760
	ITER = 1	PIT 4770
		PIT 4780
		PIT 4790
	DO 620 II = 1, NCAT	PIT 4800
520	CONTINUE	PIT 4810
	IF (FLAG1 .EQ. 1 .AND. II .EQ. 7 .AND. ITER .EQ. 1)	PIT 4820
	M(8) = ALFA(8)	PIT 4830
	IF (MC(II) .LT. CPUMIN) GO TO 610	PIT 4840
		PIT 4850
C	-----	PIT 4860
C	First summation term for cation activity coefficients	PIT 4870
C	-----	PIT 4880
	SUM1 = 0.0D0	PIT 4890
		PIT 4900
		PIT 4910
	DO 530 K = 1, NANI	PIT 4920
	SUM1 = SUM1 + MA(K) * (2 * B(II,K) + BZ * C(II,K))	PIT 4930
530	CONTINUE	PIT 4940
		PIT 4950
C	-----	PIT 4960
C	Second summation term for cation activity coefficients	PIT 4970
C	-----	PIT 4980
		PIT 4990
	SUM2 = 0.0D0	PIT 5000
	SUM2B = 0.0D0	PIT 5010
	SUM2C = 0.0D0	PIT 5020
		PIT 5030
	DO 550 J = 1, NCAT	PIT 5040
	IF (II .EQ. J) GO TO 550	PIT 5050
	SUM2A = 0.0D0	PIT 5060
		PIT 5070
	DO 540 K = 1, NANI	PIT 5080
	IF (MC(J) .LT. CPUMIN) GO TO 540	PIT 5090
	SUM2A = SUM2A + MA(K) * PSIC(II,J,K)	PIT 5100
540	CONTINUE	PIT 5110
		PIT 5120
	SUM2 = SUM2 + MC(J) * (2 * PHIC(II,J) + SUM2A)	PIT 5130
		PIT 5140
	IF (J .EQ. 1 .OR. J .EQ. 3) THEN	PIT 5150
	SUM2B = SUM2 + 1.0D-3 * (2 * PHIC(II,J) + SUM2A)	PIT 5160
	SUM2C = SUM2 + 1.0D-3 * (2 * PHIC(II,J) + SUM2A)	PIT 5170
C	ELSE	PIT 5180
C	SUM2B = SUM2 + MC(J) * (2 * PHIC(II,J) + SUM2A)	PIT 5190
C	SUM2C = SUM2 + MC(J) * (2 * PHIC(II,J) + SUM2A)	PIT 5200
	END IF	PIT 5210
		PIT 5220

550	CONTINUE	PIT 5230
		PIT 5240
C	-----	PIT 5250
C	Third summation term for cation activity coefficients	PIT 5260
C	-----	PIT 5270
	SUM3 = 0.0D0	PIT 5280
		PIT 5290
		PIT 5300
	DO 570 K = 1, (NANI-1)	
	DO 560 L = (K+1), NANI	
	SUM3 = SUM3 + MA(K) * MA(L) * PSIA(K,L,II)	PIT 5330
560	CONTINUE	PIT 5340
570	CONTINUE	PIT 5350
		PIT 5360
C	-----	PIT 5370
C	Fourth summation term for cation activity coefficients	PIT 5380
C	-----	PIT 5390
	SUM4 = 0.0D0	PIT 5400
	SUM4B = 0.0D0	PIT 5410
	SUM4C = 0.0D0	PIT 5420
		PIT 5430
		PIT 5440
	DO 590 I = 1, NCAT	PIT 5450
	DO 580 K = 1, NANI	PIT 5460
	SUM4 = SUM4 + MC(I) * MA(K) * C(I,K)	PIT 5470
	IF (I .EQ. 1 .OR. I .EQ. 3) THEN	PIT 5480
	SUM4B = SUM4 + 1.0D-3 * MA(K) * C(I,K)	PIT 5490
	SUM4C = SUM4 + 1.0D-3 * MA(K) * C(I,K)	PIT 5500
C	ELSE	PIT 5510
C	SUM4B = SUM4 + MC(I) * MA(K) * C(I,K)	PIT 5520
C	SUM4C = SUM4 + MC(I) * MA(K) * C(I,K)	PIT 5530
	END IF	PIT 5540
580	CONTINUE	PIT 5550
590	CONTINUE	PIT 5560
		PIT 5570
	IF (II .EQ. 1) THEN	PIT 5580
	LNGDNA = F + SUM1 + SUM2C + SUM3 + SUM4C	PIT 5590
	PGDNA = DEXP(LNGDNA)	PIT 5600
	ELSE IF (II .EQ. 3) THEN	PIT 5610
	LNGDCA = 4 * F + SUM1 + SUM2B + SUM3 + 2*SUM4B	PIT 5620
	PGDCA = DEXP(LNGDCA)	PIT 5630
	END IF	PIT 5640
		PIT 5650
C	-----	PIT 5660
C	Add up components to solve for activity coefficient for the cation	PIT 5670
C	-----	PIT 5680
	LNGC(II) = ZC(II)**2 * F + SUM1 + SUM2 + SUM3 +	PIT 5690
	IABS(ZC(II)) * SUM4	PIT 5700
	PGAMC(II) = DEXP(LNGC(II))	PIT 5710
	PALFA(CAT(II)) = MC(II) * PGAMC(II)	PIT 5720
		PIT 5730
		PIT 5740
	IF (FLAG1 .NE. 1) GO TO 610	PIT 5750
		PIT 5760
	DONE = 1	PIT 5770
	M(8) = ALFA(8) / PGAMC(7)	PIT 5780
	DIFF = PALFA(CAT(7)) - ALFA(8)	PIT 5790
		PIT 5800

IF ((DABS(DIFF)-(5.0D-3*ALFA(8))) .LT. CPUMIN) GO TO 600	PIT 5810
DONE = 0	PIT 5820
ITER = ITER + 1	PIT 5830
	PIT 5840
	PIT 5850
600 CONTINUE	PIT 5860
IF (DONE .NE. 1) GO TO 520	PIT 5870
OHA = KT1(2) * ALFA(10) / ALFA(8)	PIT 5880
M(9) = OHA	PIT 5890
	PIT 5900
610 CONTINUE	PIT 5910
PG(CAT(II)) = PGAMC(II)	PIT 5920
620 CONTINUE	PIT 5930
	PIT 5940
C -----	PIT 5950
C Start to solve for ln activity coefficient of the anions	PIT 5960
C -----	PIT 5970
	PIT 5980
KK = 1	PIT 5990
630 CONTINUE	PIT 6000
IF (MA(KK) .LT. CPUMIN) GO TO 720	PIT 6010
	PIT 6020
C -----	PIT 6030
C First summation term for anion activity coefficients	PIT 6040
C -----	PIT 6050
	PIT 6060
SUM1 = 0.0D0	PIT 6070
	PIT 6080
DO 640 I = 1, NCAT	PIT 6090
SUM1 = SUM1 + MC(I) * (2 * B(I,KK) + BZ * C(I,KK))	PIT 6100
640 CONTINUE	PIT 6110
	PIT 6120
C -----	PIT 6130
C Second summation term for anion activity coefficients	PIT 6140
C -----	PIT 6150
	PIT 6160
SUM2 = 0.0D0	PIT 6170
	PIT 6180
DO 660 L = 1, NANI	PIT 6190
IF (L .EQ. KK) GO TO 660	PIT 6200
	PIT 6210
SUM2A = 0.0D0	PIT 6220
	PIT 6230
DO 650 I = 1, NCAT	PIT 6240
IF (MA(L) .LT. CPUMIN) GO TO 650	PIT 6250
SUM2A = SUM2A + MC(I) * PSIA(KK,L,I)	PIT 6260
650 CONTINUE	PIT 6270
	PIT 6280
SUM2 = SUM2 + MA(L) * (2 * PHIA(KK,L) + SUM2A)	PIT 6290
660 CONTINUE	PIT 6300
	PIT 6310
C -----	PIT 6320
C Third summation term for anion activity coefficients	PIT 6330
C -----	PIT 6340
	PIT 6350
SUM3 = 0.0D0	PIT 6360
	PIT 6370
DO 680 I = 1, (NCAT-1)	PIT 6380

	DO 670 J = (I+1), NCAT	PIT 6390
	SUM3 = SUM3 + MC(I) * MC(J) * PSIC(I,J,KK)	PIT 6400
670	CONTINUE	PIT 6410
680	CONTINUE	PIT 6420
		PIT 6430
C	-----	PIT 6440
C	Fourth summation term for anion activity coefficients	PIT 6450
C	-----	PIT 6460
	SUM4 = 0.0D0	PIT 6470
		PIT 6480
		PIT 6490
	DO 700 I = 1, NCAT	PIT 6500
	DO 690 K = 1, NANI	PIT 6510
	SUM4 = SUM4 + MC(I) * MA(K) * C(I,K)	PIT 6520
690	CONTINUE	PIT 6530
700	CONTINUE	PIT 6540
		PIT 6550
C	-----	PIT 6560
C	Add up components to solve for activity coefficient for the anion	PIT 6570
C	-----	PIT 6580
	LNGA(KK) = ZA(KK)**2 * F + SUM1 + SUM2 + SUM3 +	PIT 6590
	IABS(ZA(KK)) * SUM4	PIT 6600
	PGAMA(KK) = DEXP(LNGA(KK))	PIT 6610
	PALFA(ANI(KK)) = MA(KK) * PGAMA(KK)	PIT 6620
		PIT 6630
		PIT 6640
	IF (FLAG1 .NE. 1) GO TO 720	PIT 6650
		PIT 6660
	DONE = 1	PIT 6670
	M(9) = OHA / PGAMA(5)	PIT 6680
	DIFF = PALFA(ANI(5)) - OHA	PIT 6690
		PIT 6700
	IF ((DABS(DIFF)-(5.0D-3*OHA)) .LT. CPUMIN) GO TO 710	PIT 6710
		PIT 6720
	DONE = 0	PIT 6730
		PIT 6740
710	CONTINUE	PIT 6750
		PIT 6760
	IF (DONE .NE. 1) GO TO 630	PIT 6770
		PIT 6780
720	CONTINUE	PIT 6790
		PIT 6800
	IF (KK .EQ. 4 .AND. CO2TIT .GT. CPUMIN) THEN	PIT 6810
	MA(3) = CO2TIT / (1 + 2 * (KT1(1) * PGAMA(3)) /	PIT 6820
	(PGAMA(4)*ALFA(8)))	PIT 6830
	MA(4) = 5.0D-1 * (CO2TIT - MA(3))	PIT 6840
		PIT 6850
	IF (DABS(PALFA(ANI(3))-MA(3)*PGAMA(3)) .GT.	PIT 6860
	5.0D-3*PALFA(ANI(3))) KK = 3	PIT 6870
	IF (KK .EQ. 3) GO TO 630	PIT 6880
	IF (DABS(PALFA(ANI(4))-MA(4)*PGAMA(4)) .GT.	PIT 6890
	5.0D-3*PALFA(ANI(4))) GO TO 630	PIT 6900
	END IF	PIT 6910
		PIT 6920
	PG(ANI(KK)) = PGAMA(KK)	PIT 6930
	KK = KK + 1	PIT 6940
	IF (KK .LE. 5) GO TO 630	PIT 6950
		PIT 6960

C	-----	PIT 6970
C	Calculate the osmotic coefficient	PIT 6980
C	-----	PIT 6990
		PIT 7000
	DO 750 I = 1, NCAT	PIT 7010
	DO 740 K = 1, NANI	PIT 7020
	BFEE(I,K) = B0(I,K) + B1(I,K) * DEXP(-2.0 * DSQRT(MU))	PIT 7030
740	CONTINUE	PIT 7040
750	CONTINUE	PIT 7050
		PIT 7060
	SUM5 = 0.0D0	PIT 7070
		PIT 7080
	DO 770 I = 1, NCAT	PIT 7090
	DO 760 K = 1, NANI	PIT 7100
	SUM5 = SUM5 + (MC(I) * MA(K)) * (BFEE(I,K) + BZ * C(I,K))	PIT 7110
760	CONTINUE	PIT 7120
770	CONTINUE	PIT 7130
		PIT 7140
	SUM6 = 0.0D0	PIT 7150
		PIT 7160
	DO 800 I = 1, (NCAT-1)	PIT 7170
	DO 790 J = (I+1), NCAT	PIT 7180
	SUM6A = 0.0D0	PIT 7190
	DO 780 K = 1, NANI	PIT 7200
	SUM6A = SUM6A + MA(K) * PSIC(I,J,K)	PIT 7210
780	CONTINUE	PIT 7220
	SUM6 = SUM6 + (MC(I) * MC(J)) * (PHIC(I,J) + SUM6A)	PIT 7230
790	CONTINUE	PIT 7240
800	CONTINUE	PIT 7250
		PIT 7260
	SUM7 = 0.0D0	PIT 7270
		PIT 7280
	DO 830 K = 1, (NANI-1)	PIT 7290
	DO 820 L = (K+1), NANI	PIT 7300
	SUM7A = 0.0D0	PIT 7310
	DO 810 I = 1, NCAT	PIT 7320
	SUM7A = SUM7A + MC(I) * PSIA(K,L,I)	PIT 7330
810	CONTINUE	PIT 7340
	SUM7 = SUM7 + (MA(K) * MA(L)) * (PHIA(K,L) + SUM7A)	PIT 7350
820	CONTINUE	PIT 7360
830	CONTINUE	PIT 7370
		PIT 7380
	SUM8 = 0.0D0	PIT 7390
		PIT 7400
	DO 840 I = 1, NCAT	PIT 7410
	SUM8 = SUM8 + MC(I)	PIT 7420
840	CONTINUE	PIT 7430
		PIT 7440
	DO 845 I = 1, NANI	PIT 7450
	SUM8 = SUM8 + MA(I)	PIT 7460
845	CONTINUE	PIT 7470
		PIT 7480
	FEE = (-0.768 * A * MU) / (1 + 1.2 * DSQRT(MU))	PIT 7490
	FEE = FEE + SUM5 + SUM6 + SUM7	PIT 7500
	FEE = 1.0 + (2.0 * FEE) / SUM8	PIT 7510
		PIT 7520
C	-----	PIT 7530
C	Calculate the activity of water	PIT 7540

C	-----	PIT 7550
		PIT 7560
	ALFA(10) = 10**(-0.007823 * SUM8 * FEE)	PIT 7570
		PIT 7580
C	-----	PIT 7590
C	At this time pitzer data calculated for only (na,k,ca,mg,cl,so4)	PIT 7600
C	-----	PIT 7610
		PIT 7620
	DO 850 I = 7, NMAX	PIT 7630
	PALFA(I) = 0.0D0	PIT 7640
	PG(I) = 0.0D0	PIT 7650
850	CONTINUE	PIT 7660
		PIT 7670
	RETURN	PIT 7680
	END	PIT 7690
	SUBROUTINE POLY (A, B, C, E, D, G, J, ROOT)	POL 0010
C	=====	POL 0020
C	This routine solves the cubic equation which describes the	POL 0030
C	partitioning between gas, oil, and water.	POL 0040
C	Values defined in calling routine	POL 0050
C	-----	POL 0060
		POL 0070
	INTEGER UNO	POL 0080
	DOUBLE PRECISION CPUMIN	POL 0090
	PARAMETER (UNO = 6)	POL 0100
	PARAMETER (CPUMIN = 1.0D-35)	POL 0110
		POL 0120
	DOUBLE PRECISION A, B, C, D, E, F1, F2, F3, G, J, P	POL 0130
	DOUBLE PRECISION Q, R, S, ROOT, T, X, Z, Z1, Z2, Z3	POL 0140
		POL 0150
	INTRINSIC DABS, DACOS, DCOS, DMAX1, DSIN, DSQRT	POL 0160
		POL 0170
C	=====	POL 0180
		POL 0190
	X = (1.0D00 / 3.0D00)	POL 0200
		POL 0210
	Z1 = D + G + J - A - B - C	POL 0220
	Z1 = Z1 / E	POL 0230
		POL 0240
	Z2 = (D * G) + (D * J) + (G * J) - (A * G) - (A * J) - (B * D)	POL 0250
	- (B * J) - (C * D) - (C * G)	POL 0260
	Z2 = Z2 / (E**2)	POL 0270
		POL 0280
	Z3 = (D * G * J) - (A * G * J) - (B * D * J) - (C * D * G)	POL 0290
	Z3 = Z3 / (E**3)	POL 0300
		POL 0310
	Q = ((3.0 * Z2) - (Z1**2)) / 9.00D00	POL 0320
		POL 0330
	R = (9.0D00 * Z1 * Z2) - (27.00D00 * Z3) - (2.0D00 * Z1**3)	POL 0340
	R = R / 54.0D00	POL 0350
		POL 0360
	P = Q**3 + R**2	POL 0370
		POL 0380

```

IF (DABS(P) .LT. CPUMIN) THEN                                POL 0390
  F1 = (2.0D00 * (R**X))                                     POL 0400
  F1 = F1 - ( X * Z1)                                         POL 0410
  F2 = (-1.0D00) * (R**X) - (X * Z1)                         POL 0420
  F3 = F2                                                      POL 0430
ELSE IF (P .GT. 0.0D00) THEN                                  POL 0440
  S = (R + DSQRT(Q**3 + R**2))**X                             POL 0450
  T = (R - DSQRT(Q**3 + R**2))**X                             POL 0460
  F1 = S + T - (X * Z1)                                       POL 0470
  F2 = F1                                                      POL 0480
  F3 = F1                                                      POL 0490
ELSE IF (P .LT. 0.0D00) THEN                                  POL 0500
  Z = DACOS(R / (DSQRT(-1.0 * Q**3)))                         POL 0510
  Z = Z / 3.0D00                                              POL 0520
  F1 = (2.0D00 * DSQRT(-1.0 * Q) * DCOS(Z)) - (X * Z1)       POL 0530
  F2 = ((-1.0) * DSQRT(-1.0 * Q) * DCOS(Z)) - (X * Z1)       POL 0540
  F3 = ((-1.0) * DSQRT(-1.0 * Q) * DCOS(Z)) - (X * Z1)       POL 0550
  F3 = ((-1.0) * DSQRT(-1.0 * Q) * DCOS(Z)) - (X * Z1)       POL 0560
  F3 = ((-1.0) * DSQRT(-1.0 * Q) * DCOS(Z)) - (X * Z1)       POL 0570
  F3 = ((-1.0) * DSQRT(-1.0 * Q) * DCOS(Z)) - (X * Z1)       POL 0580
END IF                                                         POL 0590
ROOT = DMAX1(F1, F2, F3)                                     POL 0600
IF (ROOT .LE. 0.0) THEN                                       POL 0610
  WRITE (UNO, 1001)                                           POL 0620
  STOP                                                         POL 0630
END IF                                                         POL 0640
RETURN                                                         POL 0650
1001 FORMAT( //, 57('*'),/, ' ',56X,'*',/, ' * ERROR .... Call ', POL 0660
. 'E.H. Perkins, with complete problem *',/, POL 0670
. ' ',13X,'details. Error occurred during volatile *',/, POL 0680
. ' ',13X,'fractionation between water, oil and gas *',/, POL 0690
. ' ',13X,'phases. ',34X,'*',/, ' ',56X,'*',/, 57('*'),//) POL 0700
END                                                            POL 0710
                                                             POL 0720
                                                             POL 0730
                                                             POL 0740
                                                             POL 0750

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SUBROUTINE PRATIO (TITLE, PRESS, TEMP, DENS, UNITS, PCO2, GEOTH, PRA 0010
RATIO)                                                         PRA 0020
C ===== PRA 0030
C This routine prints mole ratios, log of active ratios, etc. PRA 0040
C ----- PRA 0050
C A1 DBL Temperary storage for intermediate values PRA 0060
C A2 DBL Temperary storage for intermediate values PRA 0070
C A3 DBL Temperary storage for intermediate values PRA 0080
C A4 DBL Temperary storage for intermediate values PRA 0090
C ALFA DBL Activity of aqueous species i PRA 0100
C ANALM DBL Analyzed molality of species i PRA 0110
C CO DBL Hold intermediate calculations PRA 0120
C CPUMIN DBL Smallest positive real value program uses PRA 0130
C CR CHA Inserts carriage returns in output PRA 0140
C CUNITS DBL Analytical input concentration PRA 0150
C DENS DBL Density PRA 0160

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C	DUM	DBL	Array to hold results for printing	PRA 0170
C	EXELT	DBL	Moles of components	PRA 0180
C	FD5	DBL	Number of Hydrogens in various activity ratios	PRA 0190
C	GEOTH	INT	Flag to print geothermometers	PRA 0200
C	I	INT	Loop variable/pointer	PRA 0210
C	ID1	INT	Index of species to make ratios	PRA 0220
C	ID2	INT	Index of species to make ratios	PRA 0230
C	ID3	INT	Index of species to make ratios	PRA 0240
C	ID4	INT	Index of species to make ratios	PRA 0250
C	IPGLN	INT	Current line number of the output file	PRA 0260
C	NMAX	INT	General array dimension to allow easy expansion	PRA 0270
C	PCO2	DBL	Partial Pressure of Carbon Dioxide	PRA 0280
C	PF	DBL	Holds intermediate calculations	PRA 0290
C	PH	DBL	Measured pH of the solution	PRA 0300
C	PRESS	DBL	Total pressure	PRA 0310
C	RATIO	INT	Flag for printing activity ratios of elements	PRA 0320
C	RMG	DBL	Holds intermediate calculations	PRA 0330
C	RMGD	DBL	Holds intermediate calculations	PRA 0340
C	SUBT	DBL	Array to hold calculated geothermometers	PRA 0350
C	TEMP	DBL	Temperature of the solution when pH was measured	PRA 0360
C	TITLE	CHA	Name of the sample	PRA 0370
C	TITMIX	CHA	TITLE for mixtures	PRA 0380
C	TITR	DBL	Iteration array in DISTRB, used for guesses	PRA 0390
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	PRA 0400
C	UNITS	CHA	Units of concentration	PRA 0410
C	UNO	INT	File unit assigned for output file	PRA 0420
C	-----			PRA 0430
	DOUBLE PRECISION CPUMIN			PRA 0440
	INTEGERS NMAX, UNO			PRA 0450
	PARAMETER (CPUMIN = 1.0D-35, UNO = 6)			PRA 0460
	PARAMETER (NMAX = 340)			PRA 0470
				PRA 0480
	INTEGERS I, ID1(10), ID2(10), ID3(10), ID4(6), IPAGE, IPGLN			PRA 0490
	INTEGERS GEOTH, RATIO			PRA 0500
				PRA 0510
	CHARACTER * 1 TOF, CR			PRA 0520
	CHARACTER * 5 UNITS			PRA 0530
	CHARACTER * 40 TITMIX			PRA 0540
	CHARACTER * 80 TITLE			PRA 0550
				PRA 0560
	DOUBLE PRECISION A1, A2, A3, A4, ALFA(NMAX), ANALM(NMAX)			PRA 0570
	DOUBLE PRECISION CO, CO2F, CUNITS(NMAX)			PRA 0580
	DOUBLE PRECISION DENS, DUM(10)			PRA 0590
	DOUBLE PRECISION HTOTI, EXELT(35), FD5(6), M(NMAX), OHTOTI			PRA 0600
	DOUBLE PRECISION PCO2, PF, PH, PRESS, RMG, RMGD, SUBT(21)			PRA 0610
	DOUBLE PRECISION TEMP, TITR(11), TOTEL(5)			PRA 0620
				PRA 0630
	INTRINSIC DABS, DLOG10, DSQRT			PRA 0640
	EXTERNAL PAGE			PRA 0650
				PRA 0660
	COMMON /EXTOT / EXELT, TOTEL, TITR			PRA 0670
	COMMON /FMFD / TOF, CR, TITMIX			PRA 0680
	COMMON /FORM / IPAGE, IPGLN			PRA 0690
	COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS			PRA 0700
	COMMON /TOTALS/ CO2F, HTOTI, OHTOTI			PRA 0710
				PRA 0720
	DATA ID1 / 1, 2, 3, 4, 14, 18, 6, 7, 1, 1/			PRA 0730
				PRA 0740

DATA ID2 / 32, 22, 4, 2, 26, 15, 6, 7, 8, 16/	PRA 0750
DATA ID3 / 3, 3, 3, 1, 1, 1, 20, 20, 20, 20/	PRA 0760
DATA ID4 / 1, 2, 3, 4, 14, 18/	PRA 0770
DATA FD5 / 2.0, 2.0, 1.0, 1.0, 3.0, 2.0/	PRA 0780
	PRA 0790
	PRA 0800
	PRA 0810
DO 10 I = 1, 10	PRA 0820
DUM(I) = 0.0	PRA 0830
10 CONTINUE	PRA 0840
	PRA 0850
IF (RATIO .EQ. 1) THEN	PRA 0860
CALL PAGE	PRA 0870
WRITE (UNO, 1000) TITLE, TEMP, TITMIX	PRA 0880
WRITE (UNO, 1010) CR	PRA 0890
WRITE (UNO, 1020) CR	PRA 0900
	PRA 0910
IF (EXELT(5) .GT. CPUMIN) THEN	PRA 0920
DO 20 I = 1, 8	PRA 0930
IF (ANALM(ID1(I)) .GT. CPUMIN) DUM(I) = EXELT(5) /	PRA 0940
ANALM(ID1(I))	PRA 0950
20 CONTINUE	PRA 0960
END IF	PRA 0970
	PRA 0980
IF (ANALM(2) .GT. CPUMIN) THEN	PRA 0990
DUM(9) = ANALM(1) / ANALM(2)	PRA 1000
IF (ANALM(3) .GT. CPUMIN) DUM(10) = DSQRT(ANALM(1)) / ANALM(3)	PRA 1010
END IF	PRA 1020
	PRA 1030
WRITE (UNO, 1030) (DUM(I), I = 1, 10)	PRA 1040
WRITE (UNO, 1040)	PRA 1050
WRITE (UNO, 1050) CR	PRA 1060
IPGLN = IPGLN + 3	PRA 1070
	PRA 1080
DO 25 I = 1, 10	PRA 1090
DUM(I) = 0.0D00	PRA 1100
25 CONTINUE	PRA 1110
	PRA 1120
DO 30 I = 1, 6	PRA 1130
IF (ANALM(ID2(I)) .GT. CPUMIN .AND.	PRA 1140
ANALM(ID3(I)) .GT. CPUMIN)	PRA 1150
DUM(I) = ANALM(ID2(I)) / ANALM(ID3(I))	PRA 1160
30 CONTINUE	PRA 1170
	PRA 1180
	PRA 1190
IF (EXELT(5) .GT. CPUMIN) THEN	PRA 1200
IF (ANALM(6) .GT. CPUMIN) DUM(7) = ANALM(6) / EXELT(5)	PRA 1210
IF (ANALM(7) .GT. CPUMIN) DUM(8) = ANALM(7) / EXELT(5)	PRA 1220
IF (EXELT(22) .GT. CPUMIN) DUM(9) = EXELT(22) / EXELT(5)	PRA 1230
IF (EXELT(23) .GT. CPUMIN) DUM(10) = EXELT(23) / EXELT(5)	PRA 1240
END IF	PRA 1250
	PRA 1260
WRITE (UNO, 1060) (DUM(I), I = 1, 10)	PRA 1270
WRITE (UNO, 1070) CR	PRA 1280
WRITE (UNO, 1080)	PRA 1290
WRITE (UNO, 1090) CR	PRA 1300
IPGLN = IPGLN + 7	PRA 1310
	PRA 1320

DO 40 I = 1, 6	PRA 1330
DUM(I) = 0.DO	PRA 1340
IF (ALFA(ID4(I)) .GT. CPUMIN) DUM(I) = DLOG10(ALFA(ID4(I)))	PRA 1350
+ (FD5(I) * PH)	PRA 1360
40 CONTINUE	PRA 1370
	PRA 1380
DUM(7) = 0.DO	PRA 1390
DUM(8) = 0.DO	PRA 1400
	PRA 1410
IF (ALFA(1) .GT. CPUMIN .AND. ALFA(2) .GT. CPUMIN)	PRA 1420
DUM(7) = DLOG10(ALFA(1) / ALFA(2))	PRA 1430
IF (ALFA(3) .GT. CPUMIN .AND. ALFA(4) .GT. CPUMIN)	PRA 1440
DUM(8) = DLOG10(ALFA(3) / ALFA(4))	PRA 1450
	PRA 1460
WRITE (UNO, 1100) (DUM(I), I = 1, 8)	PRA 1470
IPGLN = IPGLN + 1	PRA 1480
END IF	PRA 1490
	PRA 1500
IF (GEOTH .EQ. 1 .OR. RATIO .EQ. 1) THEN	PRA 1510
RMG = 0.0D0	PRA 1520
RMGD = 0.0D0	PRA 1530
CO = 0.0D0	PRA 1540
A1 = 0.0D0	PRA 1550
A2 = 0.0D0	PRA 1560
A3 = 0.0D0	PRA 1570
A4 = 0.0D0	PRA 1580
	PRA 1590
IF (ANALM(2) .GT. CPUMIN) RMG = ANALM(2) * 2 * 100 /	PRA 1600
(ANALM(2) * 2 + ANALM(1) * 2 + ANALM(4))	PRA 1610
IF (ANALM(1) .GT. CPUMIN) A1 = DLOG10(ANALM(1))	PRA 1620
IF (ANALM(3) .GT. CPUMIN) A3 = DLOG10(ANALM(3))	PRA 1630
IF (ANALM(4) .GT. CPUMIN) A4 = DLOG10(ANALM(4))	PRA 1640
	PRA 1650
A1 = 0.5 * A1	PRA 1660
A2 = A1	PRA 1670
	PRA 1680
IF (DABS(A1) .GT. CPUMIN .OR. DABS(A3) .GT. CPUMIN	PRA 1690
.OR. DABS(A4) .GT. CPUMIN) THEN	PRA 1700
A1 = A3 - A4 + (1.DO / 3.DO) * (A1 - A3)	PRA 1710
A2 = A3 - A4 + (4.DO / 3.DO) * (A2 - A3)	PRA 1720
	PRA 1730
IF (RATIO .EQ. 1) THEN	PRA 1740
WRITE (UNO, 1110) A1, A2	PRA 1750
IPGLN = IPGLN + 5	PRA 1760
END IF	PRA 1770
END IF	PRA 1780
END IF	PRA 1790
	PRA 1800
A3 = 0.0D0	PRA 1810
A4 = 0.0D0	PRA 1820
	PRA 1830
IF (GEOTH .EQ. 1) THEN	PRA 1840
IF (UNITS .EQ. 'MOL/L' .OR. UNITS .EQ. 'MOL/K') THEN	PRA 1850
WRITE (UNO, 1120)	PRA 1860
RETURN	PRA 1870
END IF	PRA 1880
	PRA 1890
C -----	PRA 1900

C	Calculation of the subsurface temperature "subt" of the sample	PRA 1910
C	from the chemical data.	PRA 1920
C	-----	PRA 1930
	IF (RATIO .NE. 1) CALL PAGE	PRA 1940
	DO 50 I = 1, 21	PRA 1950
	SUBT(I) = 0.D0	PRA 1960
50	CONTINUE	PRA 1970
		PRA 1980
	IF (CUNITS(12) .LT. CPUMIN) GO TO 60	PRA 1990
		PRA 2000
	IF (UNITS .EQ. 'MG/L ') THEN	PRA 2010
	CO = DLOG10(CUNITS(12) / DENS)	PRA 2020
	ELSE IF (UNITS .EQ. 'PPM ') THEN	PRA 2030
	CO = DLOG10(CUNITS(12))	PRA 2040
	END IF	PRA 2050
		PRA 2060
	SUBT(1) = 1.309D3 / (5.19D0 - CO) - 273.16D0	PRA 2070
	SUBT(2) = 1.522D3 / (5.75D0 - CO) - 273.16D0	PRA 2080
	SUBT(3) = 0.731D3 / (4.52D0 - CO) - 273.16D0	PRA 2090
	SUBT(8) = 1.032D3 / (4.69D0 - CO) - 273.16D0	PRA 2100
	SUBT(10) = 1.000D3 / (4.78D0 - CO) - 273.16D0	PRA 2110
		PRA 2120
	PF = 1.00 - 7.862D-5 * 2.718**(3.61D-3 * TEMP) * PRESS	PRA 2130
	CO = DLOG10(PF * ALFA(11) / ALFA(10)**2)	PRA 2140
		PRA 2150
	SUBT(16) = 1309.0D00 / (0.41 - CO) - 273.16D0	PRA 2160
	SUBT(17) = 1522.0D00 / (0.97 - CO) - 273.16D0	PRA 2170
	SUBT(18) = 1032.0D00 / (-0.09 - CO) - 273.16D0	PRA 2180
	SUBT(19) = -1000.0D00 / CO - 273.16D0	PRA 2190
		PRA 2200
	CO = PF * ALFA(11)	PRA 2210
	SUBT(21) = 731.0D00 / (-0.26 - DLOG10(CO)) - 273.16D0	PRA 2220
		PRA 2230
60	CONTINUE	PRA 2240
	IF (CUNITS(3) .GT. 0.0D0 .AND. CUNITS(4) .GT. 0.0D0)	PRA 2250
	SUBT(4) = 1.217D3 / (1.483D0 + DLOG10((CUNITS(3) /	PRA 2260
	CUNITS(4)))) - 273.16D0	PRA 2270
		PRA 2280
		PRA 2290
		PRA 2300
C	-----	PRA 2310
C	Calculation of paces geothermometer.	PRA 2320
C	-----	PRA 2330
	IF (PCO2 .GT. 1.0D-6) THEN	PRA 2340
	A4 = A2 - (-1.36 - 0.253 * DLOG10(PCO2))	PRA 2350
	SUBT(12) = 1.647D3 / (2.24D0 + A4) - 273.16	PRA 2360
	END IF	PRA 2370
		PRA 2380
	IF (A1 .GT. CPUMIN .AND. A2 .GT. CPUMIN) THEN	PRA 2390
	SUBT(5) = 1.647D3 / (2.24D0 + A1) - 273.16	PRA 2400
	SUBT(6) = 1.647D3 / (2.24D0 + A2) - 273.16	PRA 2410
	END IF	PRA 2420
		PRA 2430
	IF (RMG .LT. 0.5) THEN	PRA 2440
	SUBT(14) = SUBT(5)	PRA 2450
	GO TO 70	PRA 2460
	END IF	PRA 2470
		PRA 2480

IF (RMG .GT. 50.0 .OR. SUBT(6) .LT. 70.0) GO TO 70	PRA 2490
IF (SUBT(6) .LT. 100) THEN	PRA 2500
RMGD = SUBT(6)	PRA 2510
ELSE	PRA 2520
RMGD = SUBT(5)	PRA 2530
END IF	PRA 2540
IF (RMG .LT. 5.0) THEN	PRA 2550
SUBT(14) = RMGD - (-1.03 + 59.971 * DLOG10(RMG) + 145.05 *	PRA 2560
(DLOG10(RMG))**2 - 36711 * (DLOG10(RMG))**2 /	PRA 2570
(RMGD + 273.16D0) - 1.67D7 * DLOG10(RMG) /	PRA 2580
(RMGD + 273.16D0)**2)	PRA 2590
ELSE	PRA 2600
SUBT(14) = RMGD - (10.66 - 4.74 * RMG + 325.87 *	PRA 2610
DLOG10(RMG)**2 - (1.032D5 * DLOG10(RMG)**2) /	PRA 2620
(RMGD + 273.16D0) - (1.968D7 * DLOG10(RMG)**2 /	PRA 2630
(RMGD + 273.16D0)**2) + ((1.605D7 *	PRA 2640
DLOG10(RMG)**3) / (RMGD + 273.16D0)**2))	PRA 2650
END IF	PRA 2660
70 CONTINUE	PRA 2670
IF (CUNITS(2) .GT. CPUMIN .AND. CUNITS(22) .GT. CPUMIN) THEN	PRA 2680
IF (UNITS .EQ. 'MG/L ') A3 = DSQRT(CUNITS(2)) / CUNITS(22)	PRA 2690
IF (UNITS .EQ. 'PPM ')	PRA 2700
A3 = DSQRT(CUNITS(2) / DENS) / CUNITS(22)	PRA 2710
SUBT(7) = 2.2D3 / (5.47 + DLOG10(A3)) - 273.16D0	PRA 2720
END IF	PRA 2730
IF (CUNITS(3) .GT. CPUMIN .AND. CUNITS(22) .GT. CPUMIN)	PRA 2740
SUBT(9) = 1.59D3 / (DLOG10(CUNITS(3) / CUNITS(22)) + 0.779) -	PRA 2750
273.16D0	PRA 2760
DO 80 I = 1, 21	PRA 2770
IF (SUBT(I) .LT. CPUMIN) SUBT(I) = 999.0	PRA 2780
80 CONTINUE	PRA 2790
WRITE (UNO, 1130) CR, CR	PRA 2800
WRITE (UNO, 1140) SUBT(1), SUBT(16), SUBT(2), SUBT(17)	PRA 2810
WRITE (UNO, 1150) SUBT(8), SUBT(18), SUBT(10), SUBT(19)	PRA 2820
WRITE (UNO, 1160) SUBT(3), SUBT(21), SUBT(4), SUBT(5)	PRA 2830
WRITE (UNO, 1170) SUBT(6), SUBT(12)	PRA 2840
WRITE (UNO, 1180) SUBT(14), SUBT(7), SUBT(9)	PRA 2850
END IF	PRA 2860
IF (GEOTH .EQ. 1) GEOTH = 2	PRA 2870
RETURN	PRA 2880
1000 FORMAT (' SAMPLE IDENT - ', A80, 4X, 'TEMPERATURE = ', F8.2, /,	PRA 2890
20X, A40)	PRA 2900
1010 FORMAT (//, ' MOLE RATIOS (USING ANALYTICAL MOLALITY)', /, A1,	PRA 2910
39(' '), //, 8X, ' CL/CA', 8X, 'CL/MG', 8X, 'CL/NA',	PRA 2920
8X, 'CL/K', 8X, 'CL/AL', 8X, 'CL/FE', 7X, 'CL/SO4',	PRA 2930
6X, 'CL/HCO3', 5X, 'CA/MG', 7X, 'SQRT(CA)/NA')	PRA 2940
1020 FORMAT (A1, 3(8X, '____'), 8X, '____', 2(8X, '____'),	PRA 2950
7X, '____', 6X, '____', 5X, '____',	PRA 2960
	PRA 2970
	PRA 2980
	PRA 2990
	PRA 3000
	PRA 3010
	PRA 3020
	PRA 3030
	PRA 3040
	PRA 3050
	PRA 3060

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      7X, '_____' )
1030 FORMAT (1X, 10E13.4)
1040 FORMAT (/ , 8X, 'NH3/NA', 8X, 'LI/NA', 8X, 'K/NA', 8X, 'MG/CA',
      8X, 'SR/CA', 8X, 'BA/CA', 8X, 'SO4/CL', 8X, 'HCO3/CL',
      8X, 'F/CL', 8X, 'B/CL')
1050 FORMAT (A1, 8X, '_____', 8X, '_____', 8X, '_____', 8X, '_____',
      8X, '_____', 8X, '_____', 8X, '_____', 8X, '_____',
      8X, '_____', 8X, '_____')
1060 FORMAT (2X, 6E13.4, 2E14.4, 2E12.4)
1070 FORMAT (///, ' LOG OF ACTIVITY RATIOS', /, A1, 22(' '))
1080 FORMAT (8X, 'CA/H2', 8X, 'MG/H2', 9X, 'NA/H', 10X, 'K/H',
      8X, 'AL/H3', 8X, 'FE/H2', 8X, 'CA/MG', 9X, 'NA/K', A1)
1090 FORMAT (A1, 8X, '_____', 8X, '_____', 9X, '_____', 10X, '_____',
      8X, '_____', 8X, '_____', 8X, '_____', 9X, '_____')
1100 FORMAT (8E13.4)
1110 FORMAT (/ , ' LOG(NA/K)+1/3(LOG(SQRT(CA)/NA)) =', E10.3, /,
      ' LOG(NA/K)+4/3(LOG(SQRT(CA)/NA)) =', E10.3, //)
1120 FORMAT (//, ' NO TEMP. DATA IN MOL/L')
1130 FORMAT (//, ' CHEMICAL GEOTHERMOMETER TEMPERATURES (IN DEGREES',
      ' CENTIGRADE)', /, A1, 60(' '), /, 2X,
      ' ("999.0" INDICATES THAT A VALUE GREATER THAN 0.0 ',
      ' WAS NOT CALCULATED)', //, 45X,
      ' TEMP. WITH PRESSURE', /, ' TEMPERATURE', 29X,
      ' AND/OR ACTIVITY CORRECTION', /, A1, 62(' '), //)
1140 FORMAT (1X, F10.1, ' : QUARTZ (CONDUCTIVE) : ',
      1X, F10.1, T70, ' A. IF THE WATER IS BOILING OR STEAM',
      ' IS LOST DURING', /,
      1X, F10.1, ' : QUARTZ (ADIABATIC) : ',
      1X, F10.1, T70, ' THE SAMPLING OF GROUNDWATERS',
      ' THEN USE THE QUARTZ', /,
      T70, ' ADIABATIC TEMPERATURE.')
1150 FORMAT (1X, F10.1, ' : CHALCEDONY WITH SIO2 : ',
      1X, F10.1, T70, ' B. IF THERE IS NO STEAM LOSS THEN',
      ' USE THE QUARTZ', /,
      T70, ' CONDUCTIVE TEMPERATURE.', /,
      1X, F10.1, ' : ALFA CRISTOBALITE WITH SIO2 : ',
      1X, F10.1, T70, ' C. The Amorphous Silica Temperature',
      ' Should Be Considered', /,
      T70, ' When The Sample Is Saturated With',
      ' Amorphous Silica')
1160 FORMAT (1X, F10.1, ' : Amorphous Silica With SIO2 : ',
      1X, F10.1, T70, ' (THE DELTA G OF MINERAL NO. 275 IS',
      ' POSITIVE).', /,
      T70, ' D. IF THE IN SITU TEMPERATURE EXCEEDS',
      ' 150 DEGREES', /,
      T70, ' THEN THE NA/K TEMPERATURE MAY BE',
      ' USED.', /,
      1X, F10.1, ' : LOG (NA/K)',
      T70, ' E. ALTHOUGH THE 4/3 LOG TEMPERATURE IS',
      ' GENERALLY USED', /,
      1X, F10.1, ' : LOG (NA/K) + 1/3 LOG(SQRT(CA)/NA)',
      T70, ' WHEN THE TEMPERATURE IS LESS THAN',
      ' 100 DEGREES IT IS')
1170 FORMAT (1X, F10.1, ' : LOG (NA/K) + 4/3 LOG(SQRT(CA)/NA)',
      T70, ' CONSIDERED LESS RELIABLE THAN THE',
      ' 1/3 LOG TEMPERATURE.', /,
      1X, F10.1, ' : LOG (NA/K) + 4/3 LOG(SQRT(CA)/NA)',
      T70, ' F. THE ACTIVITIES OF H4SIO4 AND',

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.          ' WATER WILL BE COMPUTED', /, PRA 3650
.          24X, ' + 1.36+0.253*LOG(PCO2)', PRA 3660
.          T70, ' AT THE SURFACE TEMPERATURE ONLY IF', PRA 3670
.          ' THE HITEMP',/, PRA 3680
.          T70, ' OPTION IS SELECTED.') PRA 3690
1180 FORMAT (1X, F10.1, ' : MG CORRECTED 1/3 (NA-K-CA)', PRA 3700
.          T70, ' G. THE ORDER OF RELIABILITY OF THE', PRA 3710
.          ' CATION GEOTHERMOMETERS:', /, PRA 3720
.          T70, ' MG-LI>MG-CORRECTED NA-K-CA>NA-LI>', PRA 3730
.          'OTHERS', /, PRA 3740
.          1X, F10.1, ' : LOG (SQRT(MG)/LI)', PRA 3750
.          T70, ' H. DETAILS OF THE EQUATIONS AND', PRA 3760
.          ' PARAMETERS CAN BE', /, PRA 3770
.          1X, F10.1, ' : LOG (NA/LI)', PRA 3780
.          T70, ' FOUND IN KHARAKA AND MARINER,', PRA 3790
.          '1988).',/), PRA 3800
.          PRA 3810
END PRA 3820

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SUBROUTINE PRINTR (TITLE, EHM, UNITS, DENS, PRESS, GFW, TEMP, Z, PRI 0010
.          GAMMA, PH2O, PCO2, TDS, MU, MNACLD, SCO2, PRI 0020
.          HTOT, OHTOT, MXSP) PRI 0030
C ===== PRI 0040
C This routine prints the results of the iterations and the PRI 0050
C distribution of species. PRI 0060
C ----- PRI 0070
C ALFA DBL Activity of aqueous species i PRI 0080
C ALK1 DBL Various forms of Alkalinity (different units) PRI 0090
C ALK2 DBL " PRI 0100
C ALK3 DBL " PRI 0110
C ALK7 DBL " PRI 0120
C ANALM DBL Analyzed molality of species i PRI 0130
C C1 DBL PRI 0140
C CAR1 DBL Various forms of total/partial Carbon in solution PRI 0150
C CAR4 DBL " PRI 0160
C CFLG DBL " PRI 0170
C CPUMIN DBL Smallest positive real value program uses PRI 0180
C CR CHA Inserts carriage returns in output PRI 0190
C CU DBL Conversion factor between units PRI 0200
C CUNITS DBL Analytical input concentration PRI 0210
C DENS DBL Density PRI 0220
C DUM1 DBL Dummy variable for printing/storage PRI 0230
C DUM2 DBL Dummy variable for printing/storage PRI 0240
C DUM3 DBL Dummy variable for printing/storage PRI 0250
C DUM4 DBL Dummy variable for printing/storage PRI 0260
C EHM DBL Measured Eh in volts PRI 0270
C EXELT DBL Moles of components PRI 0280
C GAMMA DBL Activity coefficients PRI 0290
C GFW DBL Gram formula weight of aqueous species PRI 0300
C HTOT DBL Sum of the hydronium in solution PRI 0310
C I INT Loop variable PRI 0320
C IPGLN INT Current line number of the output file PRI 0330
C M DBL Calculated molality of aqueous species PRI 0340
C MNACLD DBL Sum of Molality * charge / 2 PRI 0350

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C	MU	DBL	Ionic strength of aqueous solution	PRI 0360
C	MXSP	INT	Total number of aqueous species	PRI 0370
C	NMAX	INT	General array dimension to allow easy expansion	PRI 0380
C	OHTOT	DBL	Sum of OH in the solution	PRI 0390
C	PAGE1	CHA	Names of aqueous species	PRI 0400
C	PCH4	DBL	(Partial) pressure of CH4 .. calculated	PRI 0410
C	PCO2	DBL	(Partial) pressure of CO2 .. calculated	PRI 0420
C	PH	DBL	Measured pH of the solution	PRI 0430
C	PH2O	DBL	Pressure of H2O (saturation curve)	PRI 0440
C	PH2S	DBL	(Partial) pressure of H2S .. calculated	PRI 0450
C	PNH3	DBL	(Partial) pressure of NH3 .. calculated	PRI 0460
C	PRESS	DBL	Total pressure	PRI 0470
C	PSS	DBL	Total Pressure for printing	PRI 0480
C	SCO2	DBL	TIC	PRI 0490
C	SUM2	DBL	Storage for printing	PRI 0500
C	SUM3	DBL	Storage for printing	PRI 0510
C	T	DBL	Temperature in K	PRI 0520
C	TDS	DBL	Total Dissolved Solids (UNITS = KG/L)	PRI 0530
C	TEMP	DBL	Temperature of the solution when pH was measured	PRI 0540
C	TITLE	CHA	Name of the sample	PRI 0550
C	TITMIX	CHA	Title for mixing runs	PRI 0560
C	TITR	DBL	Iteration array in DISTRB, used for guesses	PRI 0570
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	PRI 0580
C	UNITS	CHA	Units of concentration	PRI 0590
C	UNO	INT	File unit assigned for output file	PRI 0600
C	Z	INT	Charge of aqueous species	PRI 0610
-----				PRI 0620
	INTEGER NMAX, UNO			PRI 0630
	DOUBLE PRECISION CPUMIN			PRI 0640
	PARAMETER (NMAX = 340, UNO = 6, CPUMIN = 1.0D-35)			PRI 0650
				PRI 0660
	INTEGER I, IPAGE, IPGLN, MXSP, Z(NMAX)			PRI 0670
				PRI 0680
	DOUBLE PRECISION GAMMA(NMAX), GFW(NMAX), T			PRI 0690
				PRI 0700
	CHARACTER * 1 CR, TOF			PRI 0710
	CHARACTER * 5 UNITS			PRI 0720
	CHARACTER * 8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)			PRI 0730
	CHARACTER * 40 TITMIX			PRI 0740
	CHARACTER * 80 TITLE			PRI 0750
				PRI 0760
				PRI 0770
	DOUBLE PRECISION ALFA(NMAX), ALK1, ALK2, ALK3			PRI 0780
	DOUBLE PRECISION ALK7, ANALM(NMAX), C1			PRI 0790
	DOUBLE PRECISION CAR1, CAR4, CFLG			PRI 0800
	DOUBLE PRECISION CU, CUNITS(NMAX), DENS			PRI 0810
	DOUBLE PRECISION DUM1, DUM2, DUM3			PRI 0820
	DOUBLE PRECISION EHM, EXELT(35), HTOT			PRI 0830
	DOUBLE PRECISION KHCH4, KHCO2, KHH2S, KHNH3, M(NMAX), MNACLD			PRI 0840
	DOUBLE PRECISION MU, OHTOT, PCO2, PCH4, PH, PH2O, PH2S, PNH3			PRI 0850
	DOUBLE PRECISION PRESS, PSS, SCO2, SUM2, SUM3			PRI 0860
	DOUBLE PRECISION TDS, TEMP, TITR(11), TOTEL(5)			PRI 0870
				PRI 0880
	EXTERNAL KHCO2, KHCH4, KHH2S, KHNH3, PAGE			PRI 0890
				PRI 0900
	INTRINSIC DMAX1, DLOG10			PRI 0910
				PRI 0920
	COMMON /EXTOT / EXELT, TOTEL, TITR			PRI 0930

COMMON /FMFD / TOF, CR, TITMIX	PRI 0940
COMMON /FORM / IPAGE, IPGLN	PRI 0950
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	PRI 0960
COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	PRI 0970
	PRI 0980
C =====	PRI 0990
T = TEMP + 273.15	PRI 1000
	PRI 1010
TOTEL(1) = HTOT	PRI 1020
TOTEL(2) = OHTOT	PRI 1030
TOTEL(3) = SCO2	PRI 1040
	PRI 1050
	PRI 1060
CALL PAGE	PRI 1070
WRITE (UNO, 1060) TITLE, TITMIX	PRI 1080
WRITE (UNO, 1070)	PRI 1090
WRITE (UNO, 1080) CR	PRI 1100
IPGLN = IPGLN + 4	PRI 1110
	PRI 1120
C -----	PRI 1130
C Calculation of analytical cation-anion balance.	PRI 1140
C Printing of pH, Eh, temperature, and balance	PRI 1150
C -----	PRI 1160
DUM1 = 0.0D0	PRI 1170
DUM2 = 0.0D0	PRI 1180
DO 50 I = 1, MXSP + 44	PRI 1190
IF (Z(I) .GT. 0) THEN	PRI 1200
DUM1 = DUM1 + (Z(I) * ANALM(I))	PRI 1210
ELSE	PRI 1220
DUM2 = DUM2 - (Z(I) * ANALM(I))	PRI 1230
END IF	PRI 1240
50 CONTINUE	PRI 1250
DUM1 = DUM1 * (DENS - TDS) * 1.0D03	PRI 1260
DUM2 = DUM2 * (DENS - TDS) * 1.0D03	PRI 1270
	PRI 1280
	PRI 1290
WRITE (UNO,1090) PH, EHM, TEMP, DUM1, DUM2, (DUM1 - DUM2)	PRI 1300
IPGLN = IPGLN + 1	PRI 1310
	PRI 1320
C -----	PRI 1330
C Calculation of partial pressures	PRI 1340
C -----	PRI 1350
PCO2 = 0.0D0	PRI 1360
PNH3 = 0.0D0	PRI 1370
PCH4 = 0.0D0	PRI 1380
PH2S = 0.0D0	PRI 1390
	PRI 1400
	PRI 1410
IF (M(97) .GE. CPUMIN) PCO2 = M(97) * KHCO2(T, MNACLD)	PRI 1420
IF (M(33) .GE. CPUMIN) PH2S = M(33) * KHH2S(T, MNACLD)	PRI 1430
IF (M(285) .GE. CPUMIN) PCH4 = M(285) * KHCH4(T, MNACLD, 1.0D00)	PRI 1440
IF (M(147) .GE. CPUMIN) PNH3 = M(147) * KHNH3(T)	PRI 1450
	PRI 1460
PSS = DMAX1(1.0D00, PH2O, PRESS)	PRI 1470
	PRI 1480
C -----	PRI 1490
C Recalculation of cation-anion balance.	PRI 1500
C -----	PRI 1510

DUM1 = 0.0D0	PRI 1520
DUM2 = 0.0D0	PRI 1530
	PRI 1540
	PRI 1550
DO 10 I = 1, MXSP + 44	PRI 1560
IF (M(I) .LT. CPUMIN) M(I) = 0.0	PRI 1570
IF (Z(I) .LT. 0.0) THEN	PRI 1580
DUM2 = DUM2 - (Z(I) * M(I))	PRI 1590
ELSE	PRI 1600
DUM1 = DUM1 + (Z(I) * M(I))	PRI 1610
END IF	PRI 1620
10 CONTINUE	PRI 1630
	PRI 1640
C -----	PRI 1650
C Print total inorganic carbon as mg/l, ppm, and molality	PRI 1660
C -----	PRI 1670
	PRI 1680
DUM1 = DUM1 * (DENS - TDS) * 1.0D03	PRI 1690
DUM2 = DUM2 * (DENS - TDS) * 1.0D03	PRI 1700
WRITE (UNO, 1100) DUM1, DUM2, (DUM1 - DUM2),	PRI 1710
HTOT, OHTOT, (HTOT - OHTOT)	PRI 1720
WRITE (UNO, 1000)	PRI 1730
WRITE (UNO, 1010)	PRI 1740
WRITE (UNO, 1190) CR	PRI 1750
WRITE (UNO, 1020) DENS, (TDS * 1.0D6), MU, ALFA(10), PSS,	PRI 1760
PH2O, PCO2, PH2S, PCH4, PNH3	PRI 1770
IPGLN = IPGLN + 5	PRI 1780
	PRI 1790
SUM2 = M(7) + M(52) + M(56) + M(121) + M(132) + M(139)	PRI 1800
+ M(156)	PRI 1810
SUM3 = M(98) + M(51) + M(55) + M(114) + M(120) + M(138)	PRI 1820
+ M(140) + M(155) + M(207) + 2*M(208) + 3*M(209)	PRI 1830
	PRI 1840
DUM2 = SUM2 * 6.102D4 * (DENS - TDS)	PRI 1850
DUM3 = SUM3 * 6.001D4 * (DENS - TDS)	PRI 1860
DUM1 = DUM2 / DENS	PRI 1870
ALK7 = M(9) + M(28) + 3.0*M(29) + M(38) +	PRI 1880
2.0*M(39) + 4.0*M(40) + M(48) + 3.0*M(50) +	PRI 1890
M(53) + M(57) + M(69) + M(75) +	PRI 1900
2.0*M(76) + M(77) + M(85) + 2.0*M(86) +	PRI 1910
3.0*M(87) + 4.0*M(88) + M(89) + 2.0*M(90) +	PRI 1920
M(91) + 2.0*M(92) + 2.0*M(93) + M(94) +	PRI 1930
2.0*M(99)	PRI 1940
ALK7 = ALK7 +	PRI 1950
M(100) + M(101) + 2.0*M(102) + M(103) +	PRI 1960
M(118) + M(123) + M(135) + M(147) +	PRI 1970
M(154) + M(165) + 2.0*M(166) + M(170) +	PRI 1980
2.0*M(171) + 3.0*M(172) + 4.0*M(173) + 5.0*M(174) +	PRI 1990
2.0*M(182) + 4.0*M(183) + 6.0*M(184) + 8.0*M(185) +	PRI 2000
15.0*M(188) + M(189) + 2.0*M(190) + 2.0*M(191) +	PRI 2010
5.0*M(192) + 7.0*M(193)	PRI 2020
ALK7 = ALK7 +	PRI 2030
M(201) + 2.0*M(202) + 2.0*M(203) + M(204) +	PRI 2040
2.0*M(205) + 3.0*M(206) + 4.0*M(212) + 3.0*M(213) +	PRI 2050
2.0*M(214) + M(215) + 3.0*M(217) + M(220) +	PRI 2060
M(221) + 3.0*M(222) + M(223) + M(234) +	PRI 2070
M(239) + 2.0*M(240) + M(243) + M(245) +	PRI 2080
M(246) + M(250) + M(258) + 2.0*M(259)	PRI 2090

ALK7 = ALK7	PRI 2100
2.0*M(265) + M(266) + M(269) + M(289) +	PRI 2110
M(293) + 2.0*M(294) + M(295)	PRI 2120
ALK7 = ALK7 + M(MXSP+34) + M(MXSP+35) +	PRI 2130
3.0*M(MXSP+36) + M(MXSP+38) + 2.0*M(MXSP+39) +	PRI 2140
2.0*M(MXSP+41) + M(MXSP+40) + 2.0*M(MXSP+42)	PRI 2150
	PRI 2160
ALK7 = ALK7 + SUM2 + 2.0*SUM3	PRI 2170
	PRI 2180
ALK1 = ALK7 * 61.02 * 1000.0 * (DENS - TDS)	PRI 2190
ALK2 = ALK7 * 60.01 * 500.0 * (DENS - TDS)	PRI 2200
ALK3 = ALK7 * 100.08 * 500.0 * (DENS - TDS)	PRI 2210
	PRI 2220
CAR1 = 12.011D03 * SCO2 * (DENS - TDS)	PRI 2230
CAR4 = M(97) * GFW(97) * 1000.0 * (DENS - TDS)	PRI 2240
	PRI 2250
C -----	PRI 2260
C Print solute data.	PRI 2270
C -----	PRI 2280
	PRI 2290
WRITE (UNO, 1110)	PRI 2300
WRITE (UNO, 1120) CR	PRI 2310
WRITE (UNO, 1130)	PRI 2320
WRITE (UNO, 1140) CR	PRI 2330
WRITE (UNO, 1150)	PRI 2340
	PRI 2350
WRITE (UNO, 1160) ALK1, ALK2, ALK3, CAR1, (DUM2 + 2.0*DUM3),	PRI 2360
CAR4, DUM2, DUM3	PRI 2370
	PRI 2380
ALK1 = ALK1 / DENS	PRI 2390
ALK2 = ALK2 / DENS	PRI 2400
ALK3 = ALK3 / DENS	PRI 2410
CAR1 = CAR1 / DENS	PRI 2420
CAR4 = CAR4 / DENS	PRI 2430
DUM3 = DUM3 / DENS	PRI 2440
	PRI 2450
WRITE (UNO, 1170) ALK1, ALK2, ALK3, CAR1, (DUM1 + 2.0*DUM3),	PRI 2460
CAR4, DUM1, DUM3	PRI 2470
	PRI 2480
WRITE (UNO, 1180) ALK7, (ALK7/2.0), (ALK7/2.0), SCO2,	PRI 2490
(SUM2 + 2.0*SUM3), M(97), SUM2, SUM3	PRI 2500
	PRI 2510
IPGLN = IPGLN + 8	PRI 2520
	PRI 2530
WRITE (UNO, 1030)	PRI 2540
WRITE (UNO, 1200)	PRI 2550
WRITE (UNO, 1210) CR	PRI 2560
IPGLN = IPGLN + 4	PRI 2570
	PRI 2580
DO 20 I = 1, MXSP + 44	PRI 2590
CFLG = CUNITS(I)	PRI 2600
IF (CFLG .LT. CPUMIN .AND. M(I) .LT. CPUMIN) GO TO 20	PRI 2610
C1 = 0.0D0	PRI 2620
CU = 0.0D0	PRI 2630
IF (ALFA(I) .GT. CPUMIN) C1 = -DLOG10(ALFA(I))	PRI 2640
	PRI 2650
IF (CFLG .GE. CPUMIN) THEN	PRI 2660
IF (UNITS .EQ. 'MG/L ') THEN	PRI 2670

CU = CFLG / DENS	PRI 2680
ELSE IF (UNITS .EQ. 'PPM ') THEN	PRI 2690
CU = CFLG	PRI 2700
CFLG = CFLG * DENS	PRI 2710
ELSE	PRI 2720
CU = 1.0E3 * ANALM(I) * GFW(I) * (DENS-TDS) / DENS	PRI 2730
CFLG = CU * DENS	PRI 2740
END IF	PRI 2750
END IF	PRI 2760
DUM2 = 1.0E3 * M(I) * GFW(I) * (DENS-TDS)	PRI 2770
DUM1 = DUM2 / DENS	PRI 2780
	PRI 2790
	PRI 2800
IF (IPGLN .GT. 59) THEN	PRI 2810
CALL PAGE	PRI 2820
WRITE (UNO, 1030)	PRI 2830
WRITE (UNO, 1200)	PRI 2840
WRITE (UNO, 1210) CR	PRI 2850
IPGLN = IPGLN + 3	PRI 2860
END IF	PRI 2870
	PRI 2880
IF(I .EQ. 12 .OR. I .EQ. 32) THEN	PRI 2890
WRITE (UNO, 1040) I, PAGE1(I), CU, CFLG, ANALM(I)	PRI 2900
ELSE IF(ANALM(I) .GT. CPUMIN) THEN	PRI 2910
WRITE (UNO, 1040) I, PAGE1(I), CU, CFLG, ANALM(I),	PRI 2920
DUM1, DUM2, M(I), ALFA(I), GAMMA(I), C1	PRI 2930
ELSE	PRI 2940
WRITE (UNO, 1050) I, PAGE1(I), DUM1, DUM2, M(I), ALFA(I),	PRI 2950
GAMMA(I), C1	PRI 2960
END IF	PRI 2970
	PRI 2980
IPGLN = IPGLN + 1	PRI 2990
20 CONTINUE	PRI 3000
	PRI 3010
RETURN	PRI 3020
	PRI 3030
1000 FORMAT (/, 58X, 28('-'), 'PRESSURE', 28('-'), /,	PRI 3040
2X, 'DENSITY AT', 2X, 'TOTAL DISSOLVED', 5X, 'IONIC',	PRI 3050
7X, 'ACTIVITY', 4X, 'P TOTAL', 7X, 'PH2O', 7X,	PRI 3060
'PCO2', 7X, 'PH2S', 7X, 'PCH4', 7X, 'PNH3')	PRI 3070
1010 FORMAT (4X, 'INPUT T', 4X, 'SOLIDS (MG/L)', 5X, 'STRENGTH',	PRI 3080
5X, 'OF WATER', 5X, '(BARS)', 6X, '(BARS)', 5X, '(BARS)',	PRI 3090
5X, '(BARS)', 5X, '(BARS)', 5X, '(BARS)', A1)	PRI 3100
1020 FORMAT (2X, F9.4, 5X, F12.2, F13.5, 2X, F11.4, 3X, F10.4,	PRI 3110
3X, E10.4, 4(1X, E10.4))	PRI 3120
1030 FORMAT (19X, '-----ANALYZED-----',	PRI 3130
3X, '-----CALCULATED-----',	PRI 3140
17X, 'ACTIVITY', 5X, '-LOG10')	PRI 3150
1040 FORMAT (2X, I3, 2X, A8, 1X, 2F13.4, 5E13.4, F12.4, F11.4)	PRI 3160
1050 FORMAT (2X, I3, 2X, A8, 40X, 4E13.4, F12.4, F11.4)	PRI 3170
1060 FORMAT (' SAMPLE IDENT:- ', A80, /, 20X, A40)	PRI 3180
1070 FORMAT (/, 4X, 'PH', 9X, 'EH', 7X, 'TEMP', 18X, 'CATIONS',	PRI 3190
6X, 'ANIONS', 2X, 'DIFFERENCE (MEQ/L)',	PRI 3200
12X, '--- H - OH BALANCE (MOLES) -----')	PRI 3210
1080 FORMAT (A1, 2X, '____', 6X, '____', 5X, '____', 13X,	PRI 3220
____')	PRI 3230
1090 FORMAT (1X, F6.2, 2X, F10.4, 2X, F8.2, 8X, 'ANAL-', 1X,	PRI 3240
F10.4, 2X, F10.4, 2X, F10.4, 20X, 'HTOT', 8X,	PRI 3250

	'OHTOT', 5X, 'DIFFERENCE')	PRI 3260
1100	FORMAT (37X, 'CALC=', 1X, F10.4, 2X, F10.4, 2X, F10.4,	PRI 3270
	18X, E10.4, 2X, E10.4, 2X, E10.4)	PRI 3280
1110	FORMAT (/ , 72X, 'Dissolved Inorganic Carbon')	PRI 3290
1120	FORMAT (A1, 71X, '_____')	PRI 3300
1130	FORMAT (21X, 'Total Alkalinity as', 20X, 'as', 8X, 'HCO3-',	PRI 3310
	7X, 'H2CO3', 5X, 'Sum of', 5X, 'Sum of')	PRI 3320
1140	FORMAT (A1, 20X, '_____')	PRI 3330
1150	FORMAT (17X, 'HCO3-', 5X, 'CO3=', 7X, 'CaCO3', 17X, 'TIC',	PRI 3340
	5X, 'Alkalinity', 3X, 'species', 5X, 'HCO3-', 6X,	PRI 3350
	'CO3=')	PRI 3360
1160	FORMAT (7X, '(MG/L)=', 3(E10.4,1X), 10X, 5(E10.4, 1X))	PRI 3370
1170	FORMAT (8X, '(PPM)=', 3(E10.4,1X), 10X, 5(E10.4, 1X))	PRI 3380
1180	FORMAT (3X, '(MOLALITY)=', 3(E10.4,1X), 10X, 5(E10.4, 1X))	PRI 3390
1190	FORMAT (A1, 3X, '_____', 4X, '_____', 5X, '_____',	PRI 3400
	5X, '_____', 3X, '_____', 2X, '_____',	PRI 3410
	4(1X, '_____''))	PRI 3420
1200	FORMAT (7X, 'SPECIES', 9X, 'PPM', 9X, 'MG/L', 7X, 'MOLALITY',	PRI 3430
	8X, 'PPM', 9X, 'MG/L', 7X, 'MOLALITY', 5X, 'ACTIVITY',	PRI 3440
	7X, 'COEFF.', 3X, 'ACTIVITY')	PRI 3450
1210	FORMAT (A1, 6X, '_____', 5X, '_____', 2X, '_____',	PRI 3460
	3X, '_____', 3X, '_____', 3X, '_____',	PRI 3470
	3X, '_____', 3X, '_____', 4X, '_____',	PRI 3480
	3X, '_____'')	PRI 3490
		PRI 3500
END		PRI 3510

	SUBROUTINE PRNTAB (TITLE, TEMP, MXAQK)	PRN 0010
C	=====	PRN 0020
C	Print out of tables.	PRN 0030
C	-----	PRN 0040
C	I INT Loop variable	PRN 0050
C	LOGKT1 DBL Log K for aqueous species at specified temp.	PRN 0060
C	MXAQK INT Total number of aqueous log k values	PRN 0070
C	NMAX INT General array dimension to allow easy expansion	PRN 0080
C	PAGE1 CHA Names of aqueous species	PRN 0090
C	PAGE2 CHA Names of equilibrium constants	PRN 0100
C	TEMP DBL Temperature of the solution when pH was measured	PRN 0110
C	TITLE CHA Name of the sample	PRN 0120
C	TOF CHA Places a form feed in output file	PRN 0130
C	UNO INT File unit assigned for output file	PRN 0140
C	-----	PRN 0150
		PRN 0160
	INTEGER NMAX, UNO	PRN 0170
	PARAMETER (NMAX = 340, UNO = 6)	PRN 0180
		PRN 0190
	INTEGER I, IPAGE, IPGLN, J, MXAQK	PRN 0200
		PRN 0210
	CHARACTER * 1 TOF, CR	PRN 0220
	CHARACTER * 8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)	PRN 0230
	CHARACTER * 40 TITMIX	PRN 0240
	CHARACTER * 80 TITLE	PRN 0250
		PRN 0260
	DOUBLE PRECISION LOGKT1(NMAX), LOGKT2(NMAX)	PRN 0270

DOUBLE PRECISION TEMP	PRN 0280
	PRN 0290
EXTERNAL PAGE	PRN 0300
	PRN 0310
COMMON /ALOGK / LOGKT1, LOGKT2	PRN 0320
COMMON /FMFD / TOF, CR, TITMIX	PRN 0330
COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	PRN 0340
COMMON /FORM / IPAGE, IPGLN	PRN 0350
	PRN 0360
C -----	PRN 0370
	PRN 0380
J = ((MXAQK - 1) / 3) + 1	PRN 0390
	PRN 0400
DO 10 I = 1, J	PRN 0410
IF (I .EQ. 1 .OR. IPGLN .GT. 57) THEN	PRN 0420
CALL PAGE	PRN 0430
WRITE (UNO, 110) TITLE, TEMP	PRN 0440
WRITE (UNO, 120)	PRN 0450
WRITE (UNO, 130)	PRN 0460
IPGLN = IPGLN + 9	PRN 0470
END IF	PRN 0480
IPGLN = IPGLN + 1	PRN 0490
	PRN 0500
IF ((I+J+J) .LE. MxAQK) THEN	PRN 0510
WRITE (UNO, 140) I, PAGE2(I), LOGKT1(I),	PRN 0520
I+J, PAGE2(I+J), LOGKT1(I+J),	PRN 0530
I+J+J, PAGE2(I+J+J), LOGKT1(I+J+J)	PRN 0540
ELSE IF ((I+J) .LE. (MXAQK - (J - 1))) THEN	PRN 0550
WRITE (UNO, 140) I, PAGE2(I), LOGKT1(I),	PRN 0560
I+J, PAGE2(I+J), LOGKT1(I+J)	PRN 0570
ELSE	PRN 0580
WRITE (UNO, 140) I, PAGE2(I), LOGKT1(I)	PRN 0590
END IF	PRN 0600
	PRN 0610
10 CONTINUE	PRN 0620
	PRN 0630
RETURN	PRN 0640
	PRN 0650
110 FORMAT (' SAMPLE IDENT:- ', A80, /, ' TEMPERATURE = ', F6.2, ' C')	PRN 0660
120 FORMAT (//, 5X, '**TABLE OF LOG(KT) FOR THE AQUEOUS COMPLEXES**', /)	PRN 0670
130 FORMAT (/, 3(3X, 'I ', 'SPECIES', 11X, 'LOG K ', 10X), /)	PRN 0680
140 FORMAT (1X, 3(13, 2X, A8, 3X, F12.4, 12X))	PRN 0690
	PRN 0700
END	PRN 0710

SUBROUTINE PSAT (TC, PS)				PSA 0010
C	-----			PSA 0020
C	Calculates the saturation pressure for water			PSA 0030
C	(Keenan and others, 1969)			PSA 0040
C	-----			PSA 0050
C	F	DBL	Fit Coefficients	PSA 0060
C	I	INT	Loop index	PSA 0070
C	PCRT	DBL	Critical pressure (bars)	PSA 0080
C	PS	DBL	Saturation pressure	PSA 0090

C	S	DBL	Temperary storage	PSA 0100
C	TC	DBL	Temperature in deg. C	PSA 0110
C	TCRT	DBL	Critical Temperature (deg C)	PSA 0120
C	TR	DBL	1.0 / Temperature in deg K	PSA 0130
C	-----			PSA 0140
	INTEGER I			PSA 0150
				PSA 0160
	DOUBLE PRECISION F(8), PCRT, PS, S, TC, TCRT, TR			PSA 0170
				PSA 0180
	INTRINSIC DEXP			PSA 0190
				PSA 0200
	PARAMETER (TCRT=374.136D00, PCRT=220.88D00)			PSA 0210
				PSA 0220
	DATA F /-741.9242D0, -29.721D0, -11.55286D0, -8.685635D-1,			PSA 0230
	1.094098D-1, 4.3999D-1, 2.520658D-1, 5.218684D-2/			PSA 0240
				PSA 0250
				PSA 0260
C	=====			PSA 0270
	TR = 1.0D03 / (TC + 273.15D00)			PSA 0280
				PSA 0290
	S = 0.0D0			PSA 0300
	DO 10 I = 1, 8			PSA 0310
	S = S + F(I) * (0.65 - 0.01 * TC)**(I-1)			PSA 0320
10	CONTINUE			PSA 0330
				PSA 0340
	PS = PCRT * DEXP(1.0D-5 * TR * (TCRT - TC) * S)			PSA 0350
				PSA 0360
	RETURN			PSA 0370
	END			PSA 0380
				PSA 0390

	SUBROUTINE PTZINT (TEMP, TEMP1, B0, B00, B1, B11, CP, CPP, THTC,	PTZ 0010
	THGCC, THTA, THTAA, PSIC, PSICC, PSIA, PSIAA)	PTZ 0020
C	=====	PTZ 0030
C	This routine calculates the interpolated values of the	PTZ 0040
C	pitzer coeffiencients for routine pitzer. It uses the	PTZ 0050
C	routine tluvt to calculate the actual value.	PTZ 0060
C	-----	PTZ 0070
C	Future Modifications	PTZ 0080
C	-----	PTZ 0090
C	If and when more cation and anion data are incorporated into	PTZ 0100
C	the data tables the values of the parameters ncat and nani will	PTZ 0110
C	need to be increased.	PTZ 0120
C	-----	PTZ 0130
C	History	PTZ 0140
C	-----	PTZ 0150
C	J.D. DeBraal 06/87 Initial Coding	PTZ 0160
C	-----	PTZ 0170
C	Local Constants	PTZ 0180
C	-----	PTZ 0190
C	NANI INT Number of Anions	PTZ 0200
C	NCAT INT Number of Cations	PTZ 0210
C	NTEM INT Number of Temperatures	PTZ 0220
C	-----	PTZ 0230

C	Declare Constants			PTZ 0240
C	-----			PTZ 0250
	INTEGER	NANI,	NCAT,	NTEM
	PARAMETER	(NANI = 5, NCAT = 10, NTEM = 11)		PTZ 0260
				PTZ 0270
C	-----			PTZ 0280
C	Local Variables			PTZ 0290
C	-----			PTZ 0300
C	B0	(i,k)	DBL	Beta zero parameter for current temp
C	B00	(i,k,t)	DBL	Array of B0 for all temps
C	B1	(i,k)	DBL	Beta one parameter for current temp
C	B11	(i,k,t)	DBL	Array of B1 for all temps
C	CP	(i,k)	DBL	C super phi parameter for current temp
C	CPP	(i,k,t)	DBL	Array of CP for all temps
C	I		INT	Cation 1 loop variable
C	J		INT	Cation 2 loop variable
C	K		INT	Anion 1 loop variable
C	L		INT	Anion 2 loop variable
C	OK		INT	Error flag used in LAGINT
C	PSIA	(k,1,i)	DBL	PSI anion-anion-cation parameter
C	PSIAA	(k,1,i,t)	DBL	Array of PSIA for all temps
C	PSIC	(i,j,k)	DBL	PSI cation-cation-anion parameter
C	PSICC	(i,j,k,t)	DBL	Array of PSIC for all temps
C	TB0	(k,t)	DBL	Temporary B0 array with cation constant
C	TB1	(k,t)	DBL	Temporary B1 array with cation constant
C	TCP	(k,t)	DBL	Temporary CP array with cation constant
C	TEMP	(t)	DBL	Array of 11 temperatures
C	TEMP1		DBL	Temperature of interest
C	THTA	(i,k)	DBL	Pitzer theta anion parameter
C	THTAA	(i,k,t)	DBL	Array of THTA for all temps
C	THTC	(i,k)	DBL	Pitzer theta cation parameter
C	THTCC	(i,k,t)	DBL	Array of THTC for all temps
C	TMP	(t)	DBL	Interpolated value from LAGINT
C	TP		INT	Temperature loop variable
C	TPSIA	(i,t)	DBL	Temporary PSIA with anions constant
C	TPSIC	(k,t)	DBL	Temporary PSIC with cations constant
C	TTHTA	(1,t)	DBL	Temporary THTA with anion 1 constant
C	TTHTC	(j,t)	DBL	Temporary THTC with cation 1 constant
C	-----			PTZ 0610
C	Declare Variables			PTZ 0620
C	-----			PTZ 0630
	INTEGER	I, J, K, L, OK, TP		PTZ 0640
				PTZ 0650
	DOUBLE PRECISION	B0(NCAT,NANI), B00(NCAT,NANI,NTEM)		PTZ 0660
	DOUBLE PRECISION	B1(NCAT,NANI), B11(NCAT,NANI,NTEM)		PTZ 0670
	DOUBLE PRECISION	CP(NCAT,NANI), CPP(NCAT,NANI,NTEM)		PTZ 0680
	DOUBLE PRECISION	PSIA(NANI,NANI,NCAT), PSIAA(NANI,NANI,NCAT,NTEM)		PTZ 0690
	DOUBLE PRECISION	PSIC(NCAT,NCAT,NANI), PSICC(NCAT,NCAT,NANI,NTEM)		PTZ 0700
	DOUBLE PRECISION	TB0(NANI,NTEM), TB1(NANI,NTEM), TCP(NANI,NTEM)		PTZ 0710
	DOUBLE PRECISION	TEMP(NTEM), TEMP1		PTZ 0720
	DOUBLE PRECISION	THTA(NANI,NANI), THTAA(NANI,NANI,NTEM)		PTZ 0730
	DOUBLE PRECISION	THTC(NCAT,NCAT), THTCC(NCAT,NCAT,NTEM)		PTZ 0740
	DOUBLE PRECISION	TMP(NCAT)		PTZ 0750
	DOUBLE PRECISION	TPSIA(NCAT,NTEM), TPSIC(NANI,NTEM)		PTZ 0760
	DOUBLE PRECISION	TTHTA(NANI,NTEM), TTHTC(NCAT,NTEM)		PTZ 0770
C	-----			PTZ 0780
C	Routines			PTZ 0790
C	-----			PTZ 0800
C	LAGINT	SUB	Calculate a Value for Desired Temp	PTZ 0810

C	-----	PTZ 0820
	EXTERNAL LAGINT	PTZ 0830
C	-----	PTZ 0840
C	Initialize Variables	PTZ 0850
C	-----	PTZ 0860
	DATA TMP /NCAT*0.0/	PTZ 0870
C	=====	PTZ 0880
	DO 40 I = 1, NCAT	PTZ 0890
	DO 20 K = 1, NANI	PTZ 0900
	DO 10 TP = 1, NTEM	PTZ 0910
	TB0(K,TP) = B00(I,K,TP)	PTZ 0920
10	CONTINUE	PTZ 0930
20	CONTINUE	PTZ 0940
		PTZ 0950
	CALL LAGINT (TEMP, TB0, TEMP1, TMP, NANI, NANI, OK)	PTZ 0960
		PTZ 0970
		PTZ 0980
	DO 30 K = 1, NANI	PTZ 0990
	B0(I,K) = TMP(K)	PTZ 1000
30	CONTINUE	PTZ 1010
40	CONTINUE	PTZ 1020
		PTZ 1030
	DO 80 I = 1, NCAT	PTZ 1040
	DO 60 K = 1, NANI	PTZ 1050
	DO 50 TP = 1, NTEM	PTZ 1060
	TB1(K,TP) = B11(I,K,TP)	PTZ 1070
50	CONTINUE	PTZ 1080
60	CONTINUE	PTZ 1090
		PTZ 1100
	CALL LAGINT (TEMP, TB1, TEMP1, TMP, NANI, NANI, OK)	PTZ 1110
		PTZ 1120
		PTZ 1130
	DO 70 K = 1, NANI	PTZ 1140
	B1(I,K) = TMP(K)	PTZ 1150
70	CONTINUE	PTZ 1160
80	CONTINUE	PTZ 1170
		PTZ 1180
	DO 120 I = 1, NCAT	PTZ 1190
	DO 100 K = 1, NANI	PTZ 1200
	DO 90 TP = 1, NTEM	PTZ 1210
	TCP(K,TP) = CPP(I,K,TP)	PTZ 1220
90	CONTINUE	PTZ 1230
100	CONTINUE	PTZ 1240
		PTZ 1250
	CALL LAGINT (TEMP, TCP, TEMP1, TMP, NANI, NANI, OK)	PTZ 1260
		PTZ 1270
	DO 110 K = 1, NANI	PTZ 1280
	CP(I,K) = TMP(K)	PTZ 1290
110	CONTINUE	PTZ 1300
120	CONTINUE	PTZ 1310
		PTZ 1320
	DO 160 I = 1, NCAT	PTZ 1330
	DO 140 J = 1, NCAT	PTZ 1340
	DO 130 TP = 1, NTEM	PTZ 1350
	TTHTC(J,TP) = THTCC(I,J,TP)	PTZ 1360
130	CONTINUE	PTZ 1370
140	CONTINUE	PTZ 1380
		PTZ 1390
	CALL LAGINT (TEMP, TTHTC, TEMP1, TMP, NCAT, NCAT, OK)	

	DO 150 J = 1, NCAT	PTZ 1400
	THTC(I,J) = TMP(J)	PTZ 1410
150	CONTINUE	PTZ 1420
160	CONTINUE	PTZ 1430
		PTZ 1440
		PTZ 1450
	DO 200 K = 1, NANI	PTZ 1460
	DO 180 L = 1, NANI	PTZ 1470
	DO 170 TP = 1, NTEM	PTZ 1480
	THTA(L,TP) = THTAA(K,L,TP)	PTZ 1490
170	CONTINUE	PTZ 1500
180	CONTINUE	PTZ 1510
		PTZ 1520
	CALL LAGINT (TEMP, THTA, TEMP1, TMP, NCAT, NCAT, OK)	PTZ 1530
		PTZ 1540
	DO 190 L = 1, NANI	PTZ 1550
	THTA(K,L) = TMP(L)	PTZ 1560
190	CONTINUE	PTZ 1570
200	CONTINUE	PTZ 1580
		PTZ 1590
	DO 250 I = 1, NCAT	PTZ 1600
	DO 240 J = 1, NCAT	PTZ 1610
	DO 220 K = 1, NANI	PTZ 1620
	DO 210 TP = 1, NTEM	PTZ 1630
	TPSIC(K,TP) = PSICC(I,J,K,TP)	PTZ 1640
210	CONTINUE	PTZ 1650
220	CONTINUE	PTZ 1660
		PTZ 1670
	CALL LAGINT (TEMP, TPSIC, TEMP1, TMP, NANI, NANI, OK)	PTZ 1680
		PTZ 1690
	DO 230 K = 1, NANI	PTZ 1700
	PSIC(I,J,K) = TMP(K)	PTZ 1710
230	CONTINUE	PTZ 1720
240	CONTINUE	PTZ 1730
250	CONTINUE	PTZ 1740
		PTZ 1750
		PTZ 1760
	DO 300 K = 1, NANI	PTZ 1770
	DO 290 L = 1, NANI	PTZ 1780
	DO 270 I = 1, NCAT	PTZ 1790
	DO 260 TP = 1, NTEM	PTZ 1800
	TPSIA(I,TP) = PSIAA(K,L,I,TP)	PTZ 1810
260	CONTINUE	PTZ 1820
270	CONTINUE	PTZ 1830
		PTZ 1840
	CALL LAGINT (TEMP, TPSIA, TEMP1, TMP, NCAT, NCAT, OK)	PTZ 1850
		PTZ 1860
	DO 280 I = 1, NCAT	PTZ 1870
	PSIA(K,L,I) = TMP(K)	PTZ 1880
280	CONTINUE	PTZ 1890
290	CONTINUE	PTZ 1900
300	CONTINUE	PTZ 1910
		PTZ 1920
	RETURN	PTZ 1930
	END	

	DOUBLE PRECISION FUNCTION SEXP10 (X)	SEX 0010
C	=====	SEX 0020
C	If a number is too small to be raised to the power of ten,	SEX 0030
C	return zero, else raise it.	SEX 0040
C	-----	SEX 0050
		SEX 0060
	DOUBLE PRECISION X, CPUMIN, CPUMAX	SEX 0070
	PARAMETER (CPUMIN = 1.0D-35, CPUMAX = 1.0D+35)	SEX 0080
	INTRINSIC DLOG10	SEX 0090
		SEX 0100
C	=====	SEX 0110
		SEX 0120
	IF (X .GT. DLOG10(CPUMIN) .AND. X .LT. DLOG10(CPUMAX)) THEN	SEX 0130
	SEXP10 = 10.0D00**X	SEX 0140
	ELSE	SEX 0150
	SEXP10 = 0.0D00	SEX 0160
	END IF	SEX 0170
		SEX 0180
	RETURN	SEX 0190
	END	SEX 0200

	DOUBLE PRECISION FUNCTION SLOG10(X)	SLO 0010
C	=====	SLO 0020
C	If a number is too small to have it's log taken, return -999	SLO 0030
C	-----	SLO 0040
		SLO 0050
	DOUBLE PRECISION X, CPUMIN	SLO 0060
	PARAMETER (CPUMIN = 1.0D-35)	SLO 0070
	INTRINSIC DLOG10	SLO 0080
		SLO 0090
C	=====	SLO 0100
		SLO 0110
	IF (X .GT. CPUMIN) THEN	SLO 0120
	SLOG10 = DLOG10(X)	SLO 0130
	ELSE	SLO 0140
	SLOG10 = -999.9D00	SLO 0150
	END IF	SLO 0160
		SLO 0170
	RETURN	SLO 0180
	END	SLO 0190

	SUBROUTINE SORTA (A, B, INUM, IPOINT)	SOR 0010
C	=====	SOR 0020
C	A utility routine to sort arrays before using GUESS	SOR 0030
C	-----	SOR 0040
C	A DBL Array to be sorted based on matching value in B	SOR 0050
C	B DBL Sort this array (smallest to largest)	SOR 0060
C	I INT Index counter	SOR 0070
C	INUM INT Number of points to sort	SOR 0080
C	IPOINT INT Pointer to specific entry ... return	SOR 0090

C			new position		SOR 0100
C	J	INT	Index counter		SOR 0110
C	X	DBL	Temporary storage		SOR 0120
C	-----				SOR 0130
	INTEGER INUM, IPOINT, I, J				SOR 0140
	DOUBLE PRECISION A(*), B(*), X				SOR 0150
					SOR 0160
					SOR 0170
C	=====				SOR 0180
	IF (INUM .LE. 1) RETURN				SOR 0190
					SOR 0200
	DO 200 I = 1, (INUM-1)				SOR 0210
	DO 100 J = (I+1), INUM				SOR 0220
	IF (B(I) .GT. B(J)) THEN				SOR 0230
	X = A(J)				SOR 0240
	A(J) = A(I)				SOR 0250
	A(I) = X				SOR 0260
	X = B(J)				SOR 0270
	B(J) = B(I)				SOR 0280
	B(I) = X				SOR 0290
	IF (IPOINT .EQ. I) THEN				SOR 0300
	IPOINT = J				SOR 0310
	ELSE IF (IPOINT .EQ. J) THEN				SOR 0320
	IPOINT = I				SOR 0330
	END IF				SOR 0340
	END IF				SOR 0350
100	CONTINUE				SOR 0360
200	CONTINUE				SOR 0370
					SOR 0380
					SOR 0390
	RETURN				SOR 0400
	END				SOR 0410

	SUBROUTINE STORE (TEMP, HITEMP)				STO 0010
C	=====				STO 0020
C	Writes out current data values to create a restart file				STO 0030
C	-----				STO 0040
C	ADEX	INT	Flag for surface chemistry option		STO 0050
C	ALFA	DBL	Activity of aqueous species i		STO 0060
C	ALK	INT	Flag for distribution of carbonate species		STO 0070
C	AMOL	DBL	Molality of aqueous/mineral species added		STO 0080
C	ANALM	DBL	Analyzed molality of species i		STO 0090
C	ANS1	INT	Number of complexes for added anion #1		STO 0100
C	ANS2	INT	Number of complexes for added anion #2		STO 0110
C	CEC	DBL	Cation exchange capacity		STO 0120
C	COEF	DBL	Stoichiometric coefficient and Id number		STO 0130
C	CONV1	DBL	Tolerance factor for convergence of anions		STO 0140
C	CONV2	DBL	Tolerance factor for hydronium mass-balance		STO 0150
C	CPUMIN	DBL	Smallest positive real value program uses		STO 0160
C	CUNITS	DBL	Analytical input concentration		STO 0170
C	DCH4	DBL	Concentration of CH4 lost up annulas		STO 0180
C	DDCH4	DBL	Concentration of CH4 lost before pH measurement		STO 0190
C	DCO2	DBL	Concentration of CO2 lost up annulas		STO 0200
C	DDCO2	DBL	Concentration of CO2 lost before pH measurement		STO 0210

C	DH2S	DBL	Concentration of H2S lost up annulas	STO 0220
C	DDH2S	DBL	Concentration of H2S lost before pH measurement	STO 0230
C	DNH3	DBL	Concentration of NH3 lost up annulas	STO 0240
C	DDNH3	DBL	Concentration of NH3 lost before pH measurement	STO 0250
C	DENS	DBL	Density	STO 0260
C	DFRAC1	DBL	Smallest fraction of soln 1 mixed with soln 2	STO 0270
C	DHA	DBL	Ion size parameter	STO 0280
C	DINC	DBL	Increment of solution 1 to be added	STO 0290
C	DP	DBL	Dissolution/precipitation switch	STO 0300
C	DSEP	DBL	Density of oil at 15 degree C	STO 0310
C	EHM	DBL	Measured Eh in volts	STO 0320
C	EHMC	DBL	Measured Eh using the Calomel electrode	STO 0330
C	EMFZSC	DBL	Measured Eh using the Zobell's solution	STO 0340
C	EXELT	DBL	Moles of components	STO 0350
C	FBOIL	DBL	Fraction of solution boiled-off as steam	STO 0360
C	FCCSAT	DBL	Tolerance factor for pH and CO2 options	STO 0370
C	FIXIT	DBL	Fixing value in the CO2 option	STO 0380
C	FLAGS	INT	Selection flags for calculation of redox equil.	STO 0390
C	GEOHT	INT	Flag to select geothermometer	STO 0400
C	GFW	DBL	Gram formula weight of aqueous species	STO 0410
C	HITEMP	DBL	In-situ temperature	STO 0420
C	I	INT	Loop counting variable	STO 0430
C	IBMIX	INT	Switch for mixing option	STO 0440
C	ICCSAT	INT	Switch for pH option	STO 0450
C	IDDP	INT	Id number of the mineral to be dissolved/ppt	STO 0460
C	IDMIX	INT	Id number of the aqueous species to be added	STO 0470
C	IDN	INT	Id numbers of the ISCOMP components adsorption	STO 0480
C	IDSAT	INT	Id number of the mineral to be equilibrated	STO 0490
C	IMCO3	INT	Selects CO2 option	STO 0500
C	IMIX	INT	Switch used in MIXER routines	STO 0510
C	INFORM	INT	Flag to print all the log K values in data base	STO 0520
C	INMIX	INT	Total number of mixtures of two solution mixed	STO 0530
C	INSP	INT	Total number of surface sites for adsorption	STO 0540
C	IOPT	INT	Switch for co2/h option	STO 0550
C	IPAGE	INT	Current page number of output file	STO 0560
C	IPGLN	INT	Current line number of the output file	STO 0570
C	IPHASE	INT	Switch for oil/water/gas calculations	STO 0580
C	IPIT	INT	Flag to use pitzer activity coefficients	STO 0590
C	IPRIN1	INT	Flag for printing iteration of anions	STO 0600
C	IPRIN2	INT	Flag for printing hydronium balance	STO 0610
C	IRXDP	INT	Id number of the aqueous species to be added	STO 0620
C	ISCHG	INT	Charge of each surface site for adsorption	STO 0630
C	ISCOMP	INT	Total number of components in dissociation	STO 0640
C	ITIC	INT	Hitemp distribution of carbonate species	STO 0650
C	ITMIX	INT	Switch for the mineral saturation option	STO 0660
C	ITT	INT	Number of aqueous species to add/sub with water	STO 0670
C	J	INT	Loop counting variable	STO 0680
C	KCH4OL	DBL	Henry's law coefficient for CH4 in oil	STO 0690
C	KCO2OL	DBL	Henry's law coefficient for CO2 in oil	STO 0700
C	KH2SOL	DBL	Henry's law coefficient for H2S in oil	STO 0710
C	KRXN	DBL	K for dissociation reaction of surface species	STO 0720
C	MBASE	DBL	Equivalence Mole Fraction (initial) on surface	STO 0730
C	MINCO	DBL	Stoichiometric coefficient for added minerals	STO 0740
C	MININD	INT	Index number of the added mineral	STO 0750
C	MINLOG	DBL	Log K values for added minerals	STO 0760
C	MXMKN	INT	Total number of mineral log k values	STO 0770
C	MXSP	INT	Total number of aqueous species	STO 0780
C	NDUM	INT	Id of mineral/aqueous complex with K(T) changed	STO 0790

C	NMAX	INT	General array dimension to allow easy expansion	STO 0800
C	NUFLAG	INT	Sets the activity coefficients of neutral species	STO 0810
C	NUMCOM	INT	Number of complex the ion is associated with	STO 0820
C	NUMINS	INT	Number of minerals added	STO 0830
C	ODUM	CHA	Switch to indicate a mineral/aqueous complex	STO 0840
C	OUTIN	CHA	Name of restart file name	STO 0850
C	PAGE1	CHA	Names of aqueous species	STO 0860
C	PAGE3	CHA	Names of solubility constants	STO 0870
C	PH	DBL	Measured pH of the solution	STO 0880
C	PRESS	DBL	Total pressure	STO 0890
C	PTR	INT	Points to index number of the analytical species	STO 0900
C	RATIO	INT	Flag for printing activity ratios of elements	STO 0910
C	RXDP	DBL	Molal amount of the aqueous species added	STO 0920
C	SAREA	DBL	Total surface area per kilogram of solvent	STO 0930
C	SPN	CHA	Name of each surface species adsorption	STO 0940
C	TAREA	DBL	Site density per unit area adsorption	STO 0950
C	TCH4M	DBL	Moles CH4 distributed between oil, water, vapor	STO 0960
C	TCO2M	DBL	Moles CO2 distributed between oil, water, vapor	STO 0970
C	TEMP	DBL	Temperature of the solution when pH was measured	STO 0980
C	TH2SM	DBL	Moles H2S distributed between oil, water, vapor	STO 0990
C	TIC	DBL	Concentration of total inorganic carbon	STO 1000
C	TITLE	CHA	Name of the sample	STO 1010
C	TITR	DBL	Iteration array in DISTRB, used for guesses	STO 1020
C	TOTEL	DBL	Contains HTOT, OHTOT and Sum CO2	STO 1030
C	UN	INT	File unit assigned for output file	STO 1040
C	UNITS	CHA	Units of concentration	STO 1050
C	WROIL	DBL	Oil to water weight ratio	STO 1060
C	XD	DBL	Holds Log K's for additional anions & cations	STO 1070
C	XDUM	DBL	New log K(T) value	STO 1080
C	Z	INT	Charge of aqueous species	STO 1090
-----				STO 1100
	INTEGER NMAX			STO 1110
	DOUBLE PRECISION CPUMIN			STO 1120
	PARAMETER (CPUMIN = 1.0D-35, NMAX = 340)			STO 1130
				STO 1140
	INTEGER ALK, ANS1, ANS2, FLAGS(6), GEOTH, GETUNT, I			STO 1150
	INTEGER IBMIX, ICCSAT, IDDP, IDMIX(50)			STO 1160
	INTEGER IDN(10,10), IDSAT, IMCO3, IMIX			STO 1170
	INTEGER INFORM, INMIX, INSP, IOPT, IPHASE, IPIT			STO 1180
	INTEGER IPRIN1, IPRIN2, IRXDP(10), ISCHG(10)			STO 1190
	INTEGER ISCOMP(10), ITIC, ITMIX, ITT, J			STO 1200
	INTEGER MININD(8,5), MXSP, MXMNK, NDUM(12), NUFLAG			STO 1210
	INTEGER NUMCOM, NUMINS, PTR(33), RATIO, UN, Z(NMAX)			STO 1220
				STO 1230
	CHARACTER * 1 ADEX, ODUM(12)			STO 1240
	CHARACTER * 5 UNITS			STO 1250
	CHARACTER * 8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)			STO 1260
	CHARACTER * 10 SPN(10)			STO 1270
	CHARACTER * 80 MIXFLE, OUTIN, TITLE			STO 1280
				STO 1290
	DOUBLE PRECISION ALFA(NMAX), AMOL(50), ANALM(NMAX), CEC			STO 1300
	DOUBLE PRECISION COEF(10,10), CONV1, CONV2			STO 1310
	DOUBLE PRECISION CUNITS(NMAX), DCH4, DCO2, DH2S, DNH3			STO 1320
	DOUBLE PRECISION DDCH4, DDCO2, DDH2S, DDNH3			STO 1330
	DOUBLE PRECISION DENS, DFRAC1, DHA(NMAX), DINC			STO 1340
	DOUBLE PRECISION DP, DSEP, EHM, EPMC, EXELT(35)			STO 1350
	DOUBLE PRECISION EMFZSC, FBOIL, FCCSAT, FIXIT			STO 1360
	DOUBLE PRECISION GFW(NMAX), HITEMP			STO 1370

DOUBLE PRECISION KCH4OL, KCO2OL, KH2SOL	STO 1380
DOUBLE PRECISION KRXN(10), M(NMAX), MBASE(10), MINCO(9,5)	STO 1390
DOUBLE PRECISION MINLOG(2,5), PH, PRESS	STO 1400
DOUBLE PRECISION RXDP(10), SAREA, TAREA, TCH4M	STO 1410
DOUBLE PRECISION TCO2M, TEMP, TH2SM, TITR(11), TOTEL(5), TIC	STO 1420
DOUBLE PRECISION WROIL, XD(2,45), XDUM(12)	STO 1430
	STO 1440
INTRINSIC DABS	STO 1450
	STO 1460
EXTERNAL GETUNT	STO 1470
	STO 1480
	STO 1490
COMMON /AL / NDUM, XDUM	STO 1500
COMMON /AMM / IDMIX, AMOL, ITMIX, INMIX, DFRAC1, DINC, FBOIL	STO 1510
COMMON /BASIC / DENS, PRESS, EHM, EPMC, EMFZSC, TIC, FCCSAT, XD,	STO 1520
NUMCOM, NUMINS, MINLOG, MINCO, MININD, CONV1,	STO 1530
CONV2	STO 1540
COMMON /CH / ODUM	STO 1550
COMMON /DIST / TCO2M, TCH4M, TH2SM, WROIL, KCH4OL, KCO2OL,	STO 1560
& KH2SOL, IPHASE, DSEP	STO 1570
COMMON /EXCHAN/ COEF, MBASE, KRXN, CEC, TAREA, SAREA, IDN,	STO 1580
& ISCHG, ISCOMP, INSP	STO 1590
COMMON /EXTOT / EXELT, TOTEL, TITR	STO 1600
COMMON /FLAGCM/ ALK, ITIC, ICCSAT, IMCO3, ITT, ANS1, ANS2,	STO 1610
NUFLAG, IPIT, FLAGS, INFORM, RATIO, GEOTH,	STO 1620
IPRIN1, IPRIN2	STO 1630
COMMON /GAS / DCO2, DDCO2, DH2S, DDH2S, DNH3, DDNH3,	STO 1640
& DCH4, DDCH4, IOPT, FIXIT	STO 1650
COMMON /IMM / IBMIX, IMIX	STO 1660
COMMON /MOLS / PH, ANALM, M, ALFA, CUNITS	STO 1670
COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	STO 1680
COMMON /NAMES2/ SPN	STO 1690
COMMON /NAMES3/ MIXFLE, OUTIN, TITLE, UNITS, ADEX	STO 1700
COMMON /SAT / IDDP, IDSAT, DP, RXDP, IRXDP	STO 1710
COMMON /TABCOM/ MXSP, MXMNK, GFW, Z, DHA	STO 1720
	STO 1730
DATA PTR /3, 4, 22, 1, 2, 18, 14, 12, 5, 6, 33, 7, 98, 30, 29,	STO 1740
& 136, 32, 31, 26, 15, 25, 27, 16, 23, 21, 13, 28, 169,	STO 1750
& 210, 48, 246, 265, 285/	STO 1760
	STO 1770
C =====	STO 1780
	STO 1790
IF (OUTIN .EQ. ' ') THEN	STO 1800
RETURN	STO 1810
ELSE	STO 1820
UN = GETUNT (OUTIN)	STO 1830
END IF	STO 1840
	STO 1850
UNITS = 'MOL/K'	STO 1860
	STO 1870
TIC = TOTEL(3)	STO 1880
IF (TIC .GT. CPUMIN) THEN	STO 1890
ANALM(7) = 0.0D00	STO 1900
ANALM(98) = 0.0D00	STO 1910
ELSE	STO 1920
TIC = 0.0D00	STO 1930
END IF	STO 1940
	STO 1950

WRITE (UN, 9010) TITLE	STO 1960
WRITE (UN, 9030) TEMP, HITEMP, DENS, PRESS	STO 1970
WRITE (UN, 9030) PH, EHM, EHMC, EMFZSC, UNITS	STO 1980
WRITE (UN, 9080) (ANALM(PTR(I)), I = 1, 7)	STO 1990
WRITE (UN, 9080) (ANALM(PTR(I)), I = 8, 13), TIC	STO 2000
WRITE (UN, 9080) (ANALM(PTR(I)), I = 14, 20)	STO 2010
WRITE (UN, 9080) (ANALM(PTR(I)), I = 21, 26)	STO 2020
WRITE (UN, 9080) (ANALM(PTR(I)), I = 27, 29)	STO 2030
WRITE (UN, 9080) (ANALM(PTR(I)), I = 30, 33)	STO 2040
WRITE (UN, 9100) ALK, ITIC	STO 2050
WRITE (UN, 9080) DCO2, DH2S, DNH3, DCH4	STO 2060
WRITE (UN, 9100) ICCSAT, IMCO3, FIXIT, FCCSAT	STO 2070
WRITE (UN, 9080) TCO2M, TCH4M, TH2SM, WROIL,	STO 2080
& KCO2OL, KCH4OL, KH2SOL, DSEP	STO 2090
	STO 2100
WRITE (UN, 9160) ADEX	STO 2110
IF (ADEX .EQ. 'A' .OR. ADEX .EQ. 'E') THEN	STO 2120
WRITE (UN, 9150) CEC, TAREA, SAREA, INSP	STO 2130
DO 30 I = 1, INSP	STO 2140
WRITE (UN, 9200) ISCHG(I), MBASE(I), SPN(I)	STO 2150
WRITE (UN, 9210) KRXN(I), ISCOMP(I), (COEF(I,J),	STO 2160
& IDN(I,J), J = 1, ISCOMP(I))	STO 2170
30 CONTINUE	STO 2180
END IF	STO 2190
	STO 2200
I = 0	STO 2210
WRITE (UN, 9100) I, I	STO 2220
	STO 2230
WRITE (UN, 9180) (ODUM(I), NDUM(I), XDUM(I), I = 1, 6)	STO 2240
WRITE (UN, 9180) (ODUM(I), NDUM(I), XDUM(I), I = 7, 12)	STO 2250
	STO 2260
WRITE (UN, 9290) ANS1, ANS2	STO 2270
IF (ANS1 .GT. 0) THEN	STO 2280
WRITE (UN, 9350) ANALM(MXSP+1), GFW(MXSP+1), Z(MXSP+1),	STO 2290
& DHA(MXSP+1), PAGE1(MXSP+1)	STO 2300
DO 60 I = 2, 15	STO 2310
IF (DABS(XD(1,I)) .GT. CPUMIN .OR.	STO 2320
& DABS(XD(2,I)) .GT. CPUMIN) THEN	STO 2330
WRITE (UN, 9360) I, DHA(MXSP+I), XD(1,I), XD(2,I),	STO 2340
& PAGE1(MXSP+I)	STO 2350
END IF	STO 2360
60 CONTINUE	STO 2370
END IF	STO 2380
IF (ANS2 .GT. 0) THEN	STO 2390
WRITE (UN, 9350) ANALM(MXSP+16), GFW(MXSP+16), Z(MXSP+16),	STO 2400
& DHA(MXSP+16), PAGE1(MXSP+16)	STO 2410
DO 70 I = 2, 15	STO 2420
IF (DABS(XD(1,I+15)) .GT. CPUMIN .OR.	STO 2430
& DABS(XD(2,I+15)) .GT. CPUMIN) THEN	STO 2440
WRITE (UN, 9360) I+15, DHA(MXSP+I+15), XD(1,I+15),	STO 2450
& XD(2,I+15), PAGE1(MXSP+15+I)	STO 2460
END IF	STO 2470
70 CONTINUE	STO 2480
END IF	STO 2490
	STO 2500
IF (NUMCOM .GT. 0) THEN	STO 2510
WRITE (UN, 9500) NUMCOM, Z(MXSP+31), DHA(MXSP+31),	STO 2520
& GFW(MXSP+31), ANALM(MXSP+31), PAGE1(MXSP+31)	STO 2530

DO 80 I = 2, 14	STO 2540
IF (DABS(XD(1,I+30)) .GT. CPUMIN .OR.	STO 2550
& DABS(XD(2,I+30)) .GT. CPUMIN) THEN	STO 2560
WRITE (UN, 9360) I+30, DHA(MXSP+I+30), XD(1,I+30),	STO 2570
& XD(2,I+30), PAGE1(MXSP+30+I)	STO 2580
END IF	STO 2590
80 CONTINUE	STO 2600
ELSE	STO 2610
WRITE (UN, 9500) NUMCOM	STO 2620
END IF	STO 2630
WRITE (UN, 9360) NUMINS	STO 2640
DO 90 I = 1, NUMINS	STO 2650
IF (DABS(MINLOG(1,I)) .GT. CPUMIN .OR. DABS(MINLOG(2,I))	STO 2660
. .GT. CPUMIN) THEN	STO 2670
WRITE (UN, 9560) MINLOG(1,I), MINLOG(2,I),	STO 2680
. MINCO(9,I), PAGE3(MXMNK+I)	STO 2690
WRITE (UN, 9210) (MINCO(J,I), MININD(J,I), J = 1, 8)	STO 2700
END IF	STO 2710
90 CONTINUE	STO 2720
WRITE (UN, 9290) NUFLAG, IPIT, (FLAGS(I), I = 1, 6)	STO 2730
IF (GEOTH .GT. 0) GEOTH = 1	STO 2740
WRITE (UN, 9300) INFORM, RATIO, GEOTH, IPRIN1, IPRIN2	STO 2750
WRITE (UN, 9080) CONV1, CONV2	STO 2760
	STO 2770
	STO 2780
	STO 2790
RETURN	STO 2800
	STO 2810
C -----	STO 2820
C Format Statements	STO 2830
C -----	STO 2840
	STO 2850
9010 FORMAT (A80)	STO 2860
9030 FORMAT (4E10.4, A5)	STO 2870
9080 FORMAT (8E10.4)	STO 2880
9100 FORMAT (2I2, 2E10.4)	STO 2890
9150 FORMAT (3E10.4, I3)	STO 2900
9160 FORMAT (A1)	STO 2910
9180 FORMAT (6(A1, I4, E10.4))	STO 2920
9200 FORMAT (I4, E10.4, A10)	STO 2930
9210 FORMAT (11(E10.4, I3))	STO 2940
9270 FORMAT (2I4, E10.4)	STO 2950
9280 FORMAT (I4, 2E10.4)	STO 2960
9290 FORMAT (8I2)	STO 2970
9300 FORMAT (5I2, A80)	STO 2980
9350 FORMAT (2E10.4, I2, E10.4, A8)	STO 2990
9360 FORMAT (I2, 3E10.4, A8)	STO 3000
9500 FORMAT (2I2, 3E10.4, A8)	STO 3010
9560 FORMAT (5E10.4, A8)	STO 3020
	STO 3030
END	STO 3040

SUBROUTINE TABLES (MXAQK, BDAT, TK, TCO2, MXPC)	TAB 0010
C =====	TAB 0020

C	This routine reads in all required tables.	TAB 0030
C	-----	TAB 0040
C	AHI DBL Pressure correction fit parameter	TAB 0050
C	ALOW DBL Pressure correction fit parameter	TAB 0060
C	BDAT DBL B-dot as a function of temperature	TAB 0070
C	BHI DBL Pressure correction fit parameter	TAB 0080
C	BLOW DBL Pressure correction fit parameter	TAB 0090
C	CHI DBL Pressure correction fit parameter	TAB 0100
C	CLOW DBL Pressure correction fit parameter	TAB 0110
C	DELVR DBL Change in volume at 25 degrees	TAB 0120
C	DHA DBL Ion size parameter	TAB 0130
C	GFW DBL Gram formula weight of aqueous species	TAB 0140
C	I INT Loop variable	TAB 0150
C	J INT Loop variable	TAB 0160
C	LKT1 DBL Log K for aqueous species with temperature	TAB 0170
C	LKT2 DBL Log K for minerals with temperature	TAB 0180
C	MXAQK INT Total number of aqueous log k values	TAB 0190
C	MXMNK INT Total number of mineral log k values	TAB 0200
C	MXPC INT Total number of mineral pressure constants	TAB 0210
C	MXSP INT Total number of aqueous species	TAB 0220
C	N INT Index number	TAB 0230
C	NH2O DBL Number of water ionization reactions	TAB 0240
C	NMAX INT General array dimension to allow easy expansion	TAB 0250
C	PAGE1 CHA Names of aqueous species	TAB 0260
C	PAGE2 CHA Names of equilibrium constants	TAB 0270
C	PAGE3 CHA Names of solubility constants	TAB 0280
C	TCO2 DBL Activity coefficients of CO2 with temperature	TAB 0290
C	TK DBL Temperature steps used by program	TAB 0300
C	TOF CHA Places a form feed in output file	TAB 0310
C	UND INT File unit assigned for data tables	TAB 0320
C	UNO INT File unit assigned for output file	TAB 0330
C	Z INT Charge of aqueous species	TAB 0340
C	-----	TAB 0350
	INTEGER NMAX, UND, UNO	TAB 0360
	PARAMETER (NMAX = 340, UND = 10, UNO = 6)	TAB 0370
		TAB 0380
	INTEGER I, J, N, MXSP, MXAQK, MXMNK, MXPC, Z(NMAX)	TAB 0390
		TAB 0400
	CHARACTER * 1 TOF, CR	TAB 0410
	CHARACTER * 8 PAGE1(NMAX), PAGE2(NMAX), PAGE3(NMAX)	TAB 0420
	CHARACTER * 40 TITMIX	TAB 0430
		TAB 0440
	DOUBLE PRECISION AHI(200), ALOW(200), BDAT(10), BHI(200)	TAB 0450
	DOUBLE PRECISION BLOW(200), CHI(200), CLOW(200), DELVR(NMAX)	TAB 0460
	DOUBLE PRECISION DHA(NMAX), GFW(NMAX)	TAB 0470
	DOUBLE PRECISION LKT1(NMAX,11), LKT2(NMAX,11), NH2O(NMAX)	TAB 0480
	DOUBLE PRECISION TCO2(10), TK(11)	TAB 0490
		TAB 0500
	COMMON /FMFD / TOF, CR, TITMIX	TAB 0510
	COMMON /KK / LKT1, LKT2	TAB 0520
	COMMON /NAMES1/ PAGE1, PAGE2, PAGE3	TAB 0530
	COMMON /PTK / DELVR, NH2O, ALOW, BLOW, CLOW, AHI, BHI, CHI	TAB 0540
	COMMON /TABCOM/ MXSP, MXMNK, GFW, Z, DHA	TAB 0550
		TAB 0560
		TAB 0570
C	=====	TAB 0580
		TAB 0590
	OPEN (UND, FILE = 'DATA.TBL', STATUS = 'OLD')	TAB 0600

C	OPEN (UND, STATUS = 'OLD', shared, readonly)	TAB 0610
		TAB 0620
	READ (UND, 1000) MXSP, MXAQK, MXMKN, MXPC	TAB 0630
		TAB 0640
	DO 10 I = 1, MXSP	TAB 0650
	READ (UND, 1010, END = 70) N, PAGE1(I), Z(I), DHA(I), GFW(I)	TAB 0660
10	CONTINUE	TAB 0670
		TAB 0680
	DO 20 I = 1, MXAQK	TAB 0690
	READ (UND, 1020, END = 80) N, PAGE2(I), (LKT1(I,J), J = 1, 11)	TAB 0700
20	CONTINUE	TAB 0710
		TAB 0720
	DO 30 I = 1, MXMKN	TAB 0730
	READ (UND, 1020, END = 90) N, PAGE3(I), (LKT2(I,J), J = 1, 11)	TAB 0740
30	CONTINUE	TAB 0750
		TAB 0760
	READ (UND, 1030, END = 100) (BDAT(I), I = 1, 10)	TAB 0770
		TAB 0780
	READ (UND, 1040, END = 110) (TK(I), I = 1, 11)	TAB 0790
		TAB 0800
	READ (UND, 1050, END = 120) (TCO2(I), I = 1, 10)	TAB 0810
		TAB 0820
	DO 40 I = 1, MXPC	TAB 0830
	READ (UND, 1060, END = 130) ALOW(I), BLOW(I), CLOW(I),	TAB 0840
	AHI(I), BHI(I), CHI(I)	TAB 0850
	BLOW(I) = BLOW(I) * 1.0D-4	TAB 0860
	BHI(I) = BHI(I) * 1.0D-4	TAB 0870
	CLOW(I) = CLOW(I) * 1.0D-16	TAB 0880
	CHI(I) = CHI(I) * 1.0D-16	TAB 0890
40	CONTINUE	TAB 0900
		TAB 0910
	DO 50 I = 1, MXAQK	TAB 0920
	DELVR(I) = 0.0D0	TAB 0930
	NH2O(I) = 0.0D0	TAB 0940
	READ (UND, 1070, ERR = 140, END = 60) J, DELVR(J), NH2O(J)	TAB 0950
50	CONTINUE	TAB 0960
		TAB 0970
60	CONTINUE	TAB 0980
	CLOSE (UND)	TAB 0990
	RETURN	TAB 1000
		TAB 1010
C	=====	TAB 1020
		TAB 1030
70	CONTINUE	TAB 1040
	WRITE (UNO, 1080) TOF	TAB 1050
	WRITE (UNO, 1090)	TAB 1060
	STOP	TAB 1070
		TAB 1080
80	CONTINUE	TAB 1090
	WRITE (UNO, 1080) TOF	TAB 1100
	WRITE (UNO, 1100)	TAB 1110
	STOP	TAB 1120
		TAB 1130
90	CONTINUE	TAB 1140
	WRITE (UNO, 1080) TOF	TAB 1150
	WRITE (UNO, 1110)	TAB 1160
	STOP	TAB 1170
		TAB 1180

100	CONTINUE	TAB 1190
	WRITE (UNO, 1080) TOF	TAB 1200
	WRITE (UNO, 1120)	TAB 1210
	STOP	TAB 1220
		TAB 1230
110	CONTINUE	TAB 1240
	WRITE (UNO, 1080) TOF	TAB 1250
	WRITE (UNO, 1130)	TAB 1260
	STOP	TAB 1270
		TAB 1280
120	CONTINUE	TAB 1290
	WRITE (UNO, 1080) TOF	TAB 1300
	WRITE (UNO, 1140)	TAB 1310
	STOP	TAB 1320
		TAB 1330
130	CONTINUE	TAB 1340
	WRITE (UNO, 1080) TOF	TAB 1350
	WRITE (UNO, 1150)	TAB 1360
	STOP	TAB 1370
		TAB 1380
140	CONTINUE	TAB 1390
	WRITE (UNO, 1160) TOF	TAB 1400
	STOP	TAB 1410
		TAB 1420
1000	FORMAT (4I4)	TAB 1430
1010	FORMAT (I3, 1X, A8, 1X, I2, 1X, F3.1, 1X, F8.3)	TAB 1440
1020	FORMAT (I3, 1X, A8, 7(1X, F7.2) / 13X, 4(F7.2, 1X))	TAB 1450
1030	FORMAT (10(F5.3, 1X))	TAB 1460
1040	FORMAT (F3.1, 3(1X, F4.1), 7(1X, F5.1))	TAB 1470
1050	FORMAT (F3.1, 2(1X, F4.1), 7(1X, F5.1))	TAB 1480
1060	FORMAT (5(F8.3, 1X), F8.3)	TAB 1490
1070	FORMAT (I4, 2F8.3)	TAB 1500
1080	FORMAT (A1)	TAB 1510
1090	FORMAT (5X, 'ERROR IN READING TABLE-PAGE1', /, ' Program Stop')	TAB 1520
1100	FORMAT (5X, 'ERROR IN READING TABLE-PAGE2', /, ' Program Stop')	TAB 1530
1110	FORMAT (5X, 'ERROR IN READING TABLE-PAGE3', /, ' Program Stop')	TAB 1540
1120	FORMAT (5X, 'ERROR IN READING TABLE-BDAT ', /, ' Program Stop')	TAB 1550
1130	FORMAT (5X, 'ERROR IN READING TABLE-TK ', /, ' Program Stop')	TAB 1560
1140	FORMAT (5X, 'ERROR IN READING TABLE-TCO2 ', /, ' Program Stop')	TAB 1570
1150	FORMAT (5X, 'ERROR IN READING TABLE-PRESS', /, ' Program Stop')	TAB 1580
1160	FORMAT (A1, 5X, 'ERROR IN READING TABLE-PRESS (IONS) ', /, ' Program Stop')	TAB 1590
		TAB 1600
		TAB 1610
	END	TAB 1620

SUBROUTINE WAPVT (TC, X, P, BETA, G, ALPHA)				WAP 0010
C	=====			WAP 0020
C	Routine to calculate the properties of pure water			WAP 0030
C	from the steam tables of keenan et al (1969)			WAP 0040
C	-----			WAP 0050
C	A	DBL	Fit coefficients A(i,j)	WAP 0060
C	AF	DBL	Helmholtz free energy as a function of rho and T	WAP 0070
C	AF0	DBL	Intermediate storage variable	WAP 0080
C	ALPHA	DBL	Coefficient of thermal expansion	WAP 0090

C	BETA	DBL	Coefficient of compressibility	WAP 0100
C	C	DBL	Fit coefficients C(i)	WAP 0110
C	DIDX	DBL	First derivative of SI with respect to density	WAP 0120
C	DIDX2	DBL	Second derivative of SI with respect to density	WAP 0130
C	DKDX	DBL	First derivative of SK with respect to density	WAP 0140
C	DKDX2	DBL	Second derivative of SK with respect to density	WAP 0150
C	DPDT	DBL	Derivative of pressure with respect to temp.	WAP 0160
C	DPDTR	DBL	Derivative of Q by tau with constant rho	WAP 0170
C	DPDX	DBL	Derivative of pressure by density at constant T	WAP 0180
C	DQDTR	DBL	Intermediate storage variable	WAP 0190
C	DQDX	DBL	First derivative of Q by density at constant T	WAP 0200
C	DQDX2	DBL	Second derivative of Q by density at constant T	WAP 0210
C	DTDTR	DBL	First derivative of TJ with respect to Tau	WAP 0220
C	DTRDT	DBL	Derivative of TR with respect to temperature	WAP 0230
C	E	DBL	Fit constant	WAP 0240
C	FK	DBL	Intermediate storage variable	WAP 0250
C	G	DBL	Gibbs Free Energy in joules per mole	WAP 0260
C	I	INT	Loop variable	WAP 0270
C	J	INT	Loop variable	WAP 0280
C	MW	DBL	Molecular weight of water	WAP 0290
C	P	DBL	Pressure (bar)	WAP 0300
C	Q	DBL	Intermediate storage variable	WAP 0310
C	RC	DBL	R in j/ g K	WAP 0320
C	RP	DBL	R in bar cm(3)/g K	WAP 0330
C	SC	DBL	Intermediate storage variable	WAP 0340
C	SI	DBL	Sum of A(i,j) * TI(i), i=1,8 in Q	WAP 0350
C	SK	DBL	Sum of A(i,j), i=9,10 in Q	WAP 0360
C	T	DBL	Temperature in deg K	WAP 0370
C	TC	DBL	Temperature in deg C	WAP 0380
C	TCR	DBL	1000 / critical temperature of water in kelvin	WAP 0390
C	TF	DBL	Intermediate storage variable	WAP 0400
C	TI	DBL	Array of XTs to the (i-1)th power	WAP 0410
C	TJ	DBL	Intermediate storage variable	WAP 0420
C	TP	DBL	Tau(a,j)	WAP 0430
C	TR	DBL	1000 / current temperature of water in kelvin	WAP 0440
C	TT	DBL	Intermediate storage variable	WAP 0450
C	X	DBL	Density (g/cm3)	WAP 0460
C	XP	DBL	Density(a,j)	WAP 0470
C	XT	DBL	Intermediate storage variable	WAP 0480
C	-----			WAP 0490
	DOUBLE PRECISION MW			WAP 0500
	PARAMETER (MW = 18.0153D00)			WAP 0510
				WAP 0520
	INTEGER I, J			WAP 0530
				WAP 0540
	DOUBLE PRECISION A(10,7), AF, AF0, ALPHA, BETA, C(8)			WAP 0550
	DOUBLE PRECISION DIDX, DIDX2, DKDX, DKDX2, DPDT, DPDTR, DPDX			WAP 0560
	DOUBLE PRECISION DQDTR, DQDX, DQDX2, DTDTR, DTRDT			WAP 0570
	DOUBLE PRECISION E, FK, G, P, Q			WAP 0580
	DOUBLE PRECISION RC, RP, SC, SI, SK			WAP 0590
	DOUBLE PRECISION T, TC, TCR, TF, TI(8), TJ, TP, TR, TT			WAP 0600
	DOUBLE PRECISION X, XP, XT			WAP 0610
				WAP 0620
	INTRINSIC DEXP, DLOG			WAP 0630
				WAP 0640
	DATA TCR, E, RP/ 1.544912D+0, 4.8D+0, 4.6151D+0/			WAP 0650
	DATA C /1.857065D+3, 3.22912D+3, -4.19465D+2, 3.66649D+1,			WAP 0660
	-2.05516D+1, 4.85233D+0, 4.6D+1, -1.011249D+3/			WAP 0670

		WAP 0680
DATA A	/2.9492937D+1, -1.3213917D+2, 2.7464632D+2, -3.6093828D+2,	WAP 0690
.	3.4218431D+2, -2.4450042D+2, 1.5518535D+2, 5.9728487D+0,	WAP 0700
.	-4.1030848D+2, -4.1605860D+2, -5.1985860D+0, 7.7779182D+0,	WAP 0710
.	-3.3301902D+1, -1.6254622D+1, -1.7731074D+2, 1.2748742D+2,	WAP 0720
.	1.3746153D+2, 1.5597836D+2, 3.3731180D+2, -2.0988866D+2,	WAP 0730
.	6.8335354D+0, -2.6149751D+1, 6.5326396D+1, -2.6181978D+1,	WAP 0740
.	0.0D+0, 0.0D+0, 0.0D+0, 0.0D+0,	WAP 0750
.	-1.3746618D+2, -7.3396848D+2, -1.564104D-1, -7.2546108D-1,	WAP 0760
.	-9.2734289D+0, 4.3125840D+0, 0.0D+0, 0.0D+0,	WAP 0770
.	0.0D+0, 0.0D+0, 6.7874983D+0, 1.0401717D+1,	WAP 0780
.	-6.3972405D+0, 2.6409282D+1, -4.7740374D+1, 5.6323130D+1,	WAP 0790
.	0.0D+0, 0.0D+0, 0.0D+0, 0.0D+0,	WAP 0800
.	1.3687317D+2, 6.4581880D+2, -3.9661401D+0, 1.5453061D+1,	WAP 0810
.	-2.9142470D+1, 2.9568796D+1, 0.0D+0, 0.0D+0,	WAP 0820
.	0.0D+0, 0.0D+0, 7.9847970D+1, 3.9917570D+2,	WAP 0830
.	-6.9048554D-1, 2.7407416D+0, -5.1028070D+0, 3.9636085D+0,	WAP 0840
.	0.0D+0, 0.0D+0, 0.0D+0, 0.0D+0,	WAP 0850
.	1.3041253D+1, 7.1531353D+1/	WAP 0860
		WAP 0870
C	-----	WAP 0880
		WAP 0890
	RC = RP / 10.0D+0	WAP 0900
	T = TC + 273.15D00	WAP 0910
	TR = 1.0D+3 / T	WAP 0920
	TF = TR - TCR	WAP 0930
	FK = DEXP(-E * X)	WAP 0940
	SC = 0.0D+0	WAP 0950
		WAP 0960
C	-----	WAP 0970
C	Calculate psi sub 0	WAP 0980
C	-----	WAP 0990
		WAP 1000
	DO 10 I = 1, 6	WAP 1010
	SC = SC + C(I) / TR**(I-1)	WAP 1020
	10 CONTINUE	WAP 1030
		WAP 1040
	AFO = SC + C(7) * DLOG(T) + C(8) * DLOG(T / TR)	WAP 1050
		WAP 1060
C	-----	WAP 1070
C	Calculate Q term by term	WAP 1080
C	-----	WAP 1090
		WAP 1100
	Q = 0.0D+0	WAP 1110
	DQDX = 0.0D+0	WAP 1120
	DQDX2 = 0.0D+0	WAP 1130
	DPDTR = 0.0D+0	WAP 1140
	DQDTR = 0.0D+0	WAP 1150
		WAP 1160
	DO 50 J = 1, 7	WAP 1170
	IF (J .GT. 1) THEN	WAP 1180
	TP = 2.5D+0	WAP 1190
	XP = 1.0D+0	WAP 1200
	ELSE	WAP 1210
	TP = TCR	WAP 1220
	XP = 0.634D+0	WAP 1230
	END IF	WAP 1240
		WAP 1250

30	CONTINUE	WAP 1260
	XT = X - XP	WAP 1270
	TT = TR - TP	WAP 1280
	TI(1) = 1.0D+0	WAP 1290
		WAP 1300
	DO 40 I = 2, 8	WAP 1310
	TI(I) = TI(I-1) * XT	WAP 1320
40	CONTINUE	WAP 1330
		WAP 1340
	SI = A(1,J) + A(2,J) * TI(2) + A(3,J) * TI(3) + A(4,J) * TI(4) +	WAP 1350
	A(5,J) * TI(5) + A(6,J) * TI(6) + A(7,J) * TI(7) +	WAP 1360
	A(8,J) * TI(8)	WAP 1370
	DIDX = A(2,J) + 2.0*A(3,J) * TI(2) + 3.0*A(4,J) * TI(3) +	WAP 1380
	4.0*A(5,J) * TI(4) + 5.0*A(6,J) * TI(5) +	WAP 1390
	6.0*A(7,J) * TI(6) + 7.0*A(8,J) * TI(7)	WAP 1400
	DIDX2 = 2.0*A(3,J) + 6.0*A(4,J) * TI(2) + 12.0*A(5,J) * TI(3) +	WAP 1410
	20.0*A(6,J) * TI(4) + 30.0*A(7,J) * TI(5) +	WAP 1420
	42.0*A(8,J) * TI(6)	WAP 1430
		WAP 1440
	SK = FK * (A(9,J) + A(10,J) * X)	WAP 1450
	DKDX = FK * A(10,J) - E * SK	WAP 1460
	DKDX2 = -E * FK * A(10,J) - E * DKDX	WAP 1470
		WAP 1480
	TJ = TT**(J-2)	WAP 1490
	DTDTR = (J-2) * TT**(J-3)	WAP 1500
		WAP 1510
	Q = Q + TJ * (SI + SK)	WAP 1520
	DQDX = DQDX + TJ * (DIDX + DKDX)	WAP 1530
	DQDX2 = DQDX2 + TJ * (DIDX2 + DKDX2)	WAP 1540
	DPDTR = DPDTR + DTDTR * (SI + SK)	WAP 1550
	DQDTR = DQDTR + DTDTR * (DIDX + DKDX)	WAP 1560
50	CONTINUE	WAP 1570
		WAP 1580
	DPDTR = Q + TF * DPDTR	WAP 1590
	DQDTR = DQDX + TF * DQDTR	WAP 1600
	Q = TF * Q	WAP 1610
	DQDX = TF * DQDX	WAP 1620
	DQDX2 = TF * DQDX2	WAP 1630
	DTRDT = -1.0D+3 / T**2	WAP 1640
	DPDT = DTRDT * (DPDTR + DQDTR * X)	WAP 1650
		WAP 1660
	AF = AF0 + RC * T * (DLOG(X) + X * Q)	WAP 1670
		WAP 1680
	P = X * RP * T * (1.0D+0 + X * Q + X**2 * DQDX)	WAP 1690
		WAP 1700
	DPDX = P / X + X * RP * T * (Q + 3.0 * X * DQDX + X**2 * DQDX2)	WAP 1710
		WAP 1720
	BETA = 1.0 / (X * DPDX)	WAP 1730
		WAP 1740
	ALPHA = BETA * (P / T + T * RP * DPDT * X**2)	WAP 1750
		WAP 1760
	G = (AF + (P / X) * (RC / RP)) * MW	WAP 1770
		WAP 1780
	RETURN	WAP 1790
	END	WAP 1800

	SUBROUTINE WDBP (TC, P, DC, DCDT)	WDB 0010
C		WDB 0020
C	Routine to calculate the dielectric constant of water	WDB 0030
C	based on eq (1) of Bradley and Pitzer (1979)	WDB 0040
C	This equation is only valid for temperatures of 0-350 C	WDB 0050
C	and pressures up to 2000 bar at 70 C and lower and up to	WDB 0060
C	5000 bar greater than 70 C	WDB 0070
C	-----	WDB 0080
C	B DBL Intermediate storage variable	WDB 0090
C	C DBL Intermediate storage variable	WDB 0100
C	DC DBL Dielectric constant of water	WDB 0110
C	DCDT DBL Derivative of dielectric constant wrt T	WDB 0120
C	DCO DBL Intermediate storage variable	WDB 0130
C	DT1 DBL Intermediate storage variable	WDB 0140
C	DT2 DBL Intermediate storage variable	WDB 0150
C	DT3 DBL Intermediate storage variable	WDB 0160
C	P DBL Pressure in bars	WDB 0170
C	T DBL Temperature in deg k	WDB 0180
C	TC DBL Temperature in deg c	WDB 0190
C	U DBL Fit constants	WDB 0200
C	-----	WDB 0210
	DOUBLE PRECISION B, C, DC, DCDT, DCO, DT1, DT2, DT3	WDB 0220
	DOUBLE PRECISION P, T, TC, U(9)	WDB 0230
		WDB 0240
	INTRINSIC DEXP, DLOG	WDB 0250
		WDB 0260
	DATA U/ 3.4279D+2, -5.0866D-3, 9.4690D-7, -2.0525D+0,	WDB 0270
	3.1159D+3, -1.8289D+2, -8.0325D+3, 4.2142D+6,	WDB 0280
	2.1417D+0 /	WDB 0290
		WDB 0300
		WDB 0310
C	-----	WDB 0320
	T = TC + 273.15D+00	WDB 0330
	DCO = U(1) * DEXP(U(2)*T + U(3)*T**2)	WDB 0340
	C = U(4) + (U(5) / (U(6) + T))	WDB 0350
	B = U(7) + (U(8) / T) + (U(9) * T)	WDB 0360
	DC = DCO + (C * DLOG((B + P) / (B + 1.0D+3)))	WDB 0370
	DT1 = U(1) * (U(2) + (2.0 * U(3) * T))	WDB 0380
	* (DEXP((U(2) * T) + (U(3) * T**2)))	WDB 0390
	DT2 = (U(5) / (U(6) + T)**2) * DLOG((B+P) / (B + 1.0D+3))	WDB 0400
	DT3 = (C * (1.0D+3 - P) * (U(9) - (U(8)/T**2)))	WDB 0410
	/ ((B + P) * (B + 1.0D+3))	WDB 0420
	DCDT = DT1 - DT2 + DT3	WDB 0430
		WDB 0440
	RETURN	WDB 0450
	END	WDB 0460
		WDB 0470