

WATER AVAILABILITY, USE, AND ESTIMATED FUTURE WATER DEMAND IN THE UPPER DUCK RIVER BASIN, MIDDLE TENNESSEE

By SUSAN S. HUTSON

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CONVERSION FACTORS

	Multiply	To obtain	By
inch (in.)		25.4	millimeter
foot (ft)		0.3048	meter
mile (mi)		1.609	kilometer
acre-foot (acre-ft)		1,233	cubic meter
cubic foot (ft ³)		0.02832	cubic meter
cubic foot per second		0.02832	cubic meter per second
second (ft ³ /s)		0.64632	million gallons per day
gallon (gal)		0.003785	cubic meter
gallon per minute (gal/min)		0.06309	liter per second
gallon per day (gal/d)		0.003785	cubic meter per day
million gallons (Mgal)		0.3785	cubic meter
million gallons per day (Mgal/d)		0.04381	cubic meter per second

Water-use data are shown in million gallons per day and generally are rounded to three significant figures; percentages are rounded to two significant figures. Water-use data may not add to totals shown and percentages may not add to 100 because of rounding of individual values.

WATER AVAILABILITY, USE, AND ESTIMATED FUTURE WATER DEMAND IN THE UPPER DUCK RIVER BASIN, MIDDLE TENNESSEE

By Susan S. Hutson

Abstract

Water availability and use during 1989, and potential future water demands were determined for the upper Duck River basin in Middle Tennessee. The basin includes an area of about 1,700 square miles within the Highland Rim and Central Basin physiographic regions of Tennessee, where limestone rocks of Mississippian and Ordovician age predominate. The Duck River is the principal source of water in the basin, supplying a total of 18.9 million gallons per day (Mgal/d) in 1989 or 93 percent of the municipal supply to the cities of Tullahoma, Manchester, Lewisburg, Shelbyville, Columbia, and several smaller communities. Municipal water use increased 16 percent from 1980 to 1990 (from 18.0 to 20.9 Mgal/d). Socioeconomic data and future projections for development in the basin indicate that water demand will continue to increase during the next 25 years. Projections of potential future water demands in the basin for the years 1995, 2000, and 2015 were made using the Institute for Water Resources-Municipal and Industrial Needs System water-use models. The water-use models were calibrated using socioeconomic data for 1989, and were used to estimate water demands for future years. Water demands for year 1995 are estimated to increase 19 percent from 20.4 to 24.3 Mgal/d; for year 2000, 39 percent (from about 20.4 to 28.3 Mgal/d); and for year 2015, 91 percent (from 20.4 to 39.0 Mgal/d). Residential water demand for year 2015 is projected to increase by

122 percent, industrial demand by 93 percent, and commercial demand by 82 percent.

Increase in withdrawals from the Duck River throughout the basin would reduce minimum flows at key sites along the river. The reductions would increase through the year 2015. For an operational flow of 155 cubic feet per second (ft³/s) at Shelbyville, flow at Columbia would be reduced from 136 ft³/s in 1995 to 120 ft³/s in 2015. For a lower operational flow of 120 ft³/s at Shelbyville, flow at Columbia would decrease from 101 ft³/s in 1995 to 85.4 ft³/s in 2015.

The study also included an overview of the potential for developing the ground-water resources in the basin. Previous studies indicate that ground-water occurrence is irregular and difficult to predict because of the lack of homogeneity among the limestone rocks underlying the basin. Statistical analyses of yields to 5,938 wells in the basin showed that the highest yields occur in Coffee County, and that 75 percent of these wells produced less than 30 gallons per minute. However, measurements of the flow of the tributaries to Duck River show stream channel losses that indicate the potential for development of ground water does exist at specific sites.

INTRODUCTION

Water demand in the upper Duck River basin in Middle Tennessee increased significantly from 1980 to

1990. Water for domestic, industrial, and commercial uses from public-supply facilities (municipal use) increased from 18.0 million gallons per day (Mgal/d) in 1980 to 20.9 Mgal/d in 1990, or 16 percent. Projected residential, industrial, and commercial developments in the basin suggest that water use will continue to increase. Considerable uncertainty exists among officials from agencies in the basin and from the State of Tennessee whether existing water supplies are adequate to meet additional demands. Long-term projections are needed to determine if the Duck River, the principal source of water in the basin, can supply anticipated future demands.

In 1989, the U.S. Geological Survey (USGS) began an investigation to document trends in water availability and use in the upper Duck River basin. The study also included estimates of future water demands through year 2015. The project was conducted in cooperation with the Upper Duck River Development Agency and the Tennessee State Planning Office. This report summarizes the findings of the investigation.

Purpose and Scope

The purposes of this report are to:

- Summarize data on surface-water availability in the upper Duck River basin.
- Summarize available data on ground-water resources.
- Summarize the amount of water delivered to the principal customers within each public water-supply service area in the basin.
- Provide estimates of future water demand for the years 1995, 2000, and 2015.

The study area comprises the drainage area of the upper Duck River basin within Bedford, Coffee, Marshall, and Maury Counties, and part of southern Williamson County (fig. 1). The study was limited to this area because water demand from the Duck River

will most likely increase as a result of growth in these counties (Steven Parks, Director, Upper Duck River Development Agency, oral commun., 1989).

The investigation included an inventory of water use in the upper Duck River basin, and excludes any assessment of the availability of streamflow for maintaining water quality. Estimates of future water demands in the basin were made with the Institute for Water Resources-Municipal and Industrial Needs (IWR-MAIN) System water-use models designed by Planning and Management Consultants, Ltd. under contract with the U.S. Army Corps of Engineers, Institute for Water Resources (U.S. Army Corps of Engineers, 1988). The ground-water availability study was limited to an analysis of existing well records and the measurement of streamflow gains and losses (seepage investigations) along tributaries of the Duck River during two low-flow periods.

Approach

The following tasks were designed to accomplish the project objectives:

- Surface-water availability was evaluated using existing streamflow records, including periods of minimum flows.
- An inventory of wells in the study area, including a statistical analysis of yields to wells, was performed to analyze the potential for ground-water resources development. Measurements of streamflow during dry weather periods were conducted in two subbasins of the study area to provide additional data on ground-water resources.
- Municipal water use was analyzed using data collected for 1980, 1985, 1989, and 1990.
- The IWR-MAIN water-use models were calibrated for the study area using demographic and economic data for 1989. The calibrated models were used to estimate municipal water demands for the years 1995, 2000, and 2015.

HYDROGEOLOGIC SETTING

The upper Duck River basin drains parts of the Highland Rim and Central Basin physiographic regions of Tennessee (Miller, 1974) (fig. 2). The climate of the area is moderate, with annual rainfall averaging 46 inches per year. The river flows from the dissected limestone highlands in northern Coffee County into Normandy Reservoir, completed by the Tennessee Valley Authority (TVA) in 1976. The reservoir, with a capacity of 117,000 acre-feet, at normal maximum headwater elevation of 875 feet, is used for flood control, water supply, water-quality enhancements, and recreation. Downstream from Normandy Dam (fig. 1), the river flows into Bedford County and through the city of Shelbyville, where municipal water withdrawals averaged 3.90 Mgal/d during 1989. There are no major urban areas in the path of the river as it traverses Marshall County, although it supplied 2.71 Mgal/d during 1989 to Lewisburg and other smaller communities. The river then flows into Maury County and through the abandoned Columbia Dam (construction began in 1973 and was discontinued in 1983) (Jack L. Davis, Manager, Navigation and System Modification, Tennessee Valley Authority, oral commun., 1992) into the city of Columbia. Withdrawals in Columbia for municipal supplies averaged 8.48 Mgal/d during 1989. Total drainage area of the basin at the western Maury County boundary is about 1,700 square miles.

Minimum flows of the upper Duck River in Bedford, Marshall, and Maury Counties increased significantly since the construction of Normandy Reservoir. The 3-day 20-year (3Q20) minimum flow represents the lowest mean daily flow on a consecutive 3-day period with a recurrence interval of 20 years. Estimated values of 3Q20 at Shelbyville and Columbia before (Bingham, 1985) and after (U.S. Geological Survey files, Nashville) completion of the damsite are as follows:

Station	Before		Period of record	After		Period of record
	ft ³ /s	Mgal/d		ft ³ /s	Mgal/d	
Shelbyville	53.8	34.8	1949-76	71.3	46.1	1978-91
Columbia	15.1	9.8	1905-08 1921-76	95.4	61.7	1978-91

The different geologic and hydrographic conditions of the Highland Rim and Central Basin regions play an important role in the availability of ground-water resources in the area. The Highland Rim is underlain by chert and clay-rich limestone of the Warsaw Limestone and the Fort Payne Formation of Mississippian age (Miller, 1974). Although the occurrence of large quantities of ground water is variable and requires careful site selection, as much as 860 gallons per minute (gal/min) per well may be produced in a few places from the Fort Payne Formation (Burchett, 1977). Residuum in northeastern Bedford County, ranging in thickness from 10 to 80 feet, stores large quantities of ground water that discharges to tributaries in the basin. This discharge helps to maintain base flow in the Duck River as the river flows out of the Highland Rim region. In contrast, the Central Basin is underlain by the Murfreesboro, Ridley, Lebanon, Carters, and Bigby-Cannon Limestones of Ordovician age (Miller, 1974). The occurrence of ground water in these limestone rocks is extremely variable. The highest yields to wells occur at depths shallower than 150 feet in sheet-like dissolution openings, usually extending laterally a few thousand feet in any direction (Brahana and Hollyday, 1988). Yields to wells as high as 70 gal/min can occur within the Ridley Limestone (U.S. Geological Survey files, 1992). Residuum is usually less than 15 feet thick, stores little water, and as a consequence the natural base flow of the Duck River and its tributaries decreases downstream of Shelbyville (Burchett, 1977).

Ground-water use in the study area is for municipal and for domestic supply. The yields of several industrial wells that tap the Fort Payne Formation of the Highland Rim section in Coffee County are generally less than 100 gal/min.

WATER AVAILABILITY

Surface- and ground-water availability in the upper Duck River basin varies seasonally, annually, and geographically. The Duck River is the main source of municipally used surface water in the basin. Springs and wells of varying yields supplement the municipal water supply from the Duck River and provide water to domestic systems.

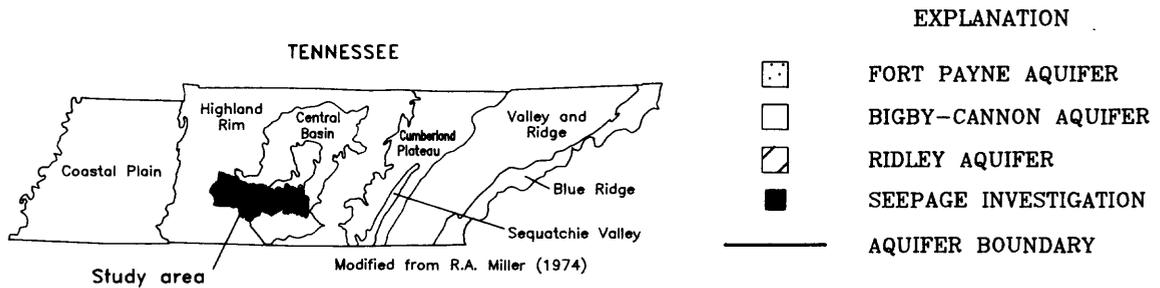
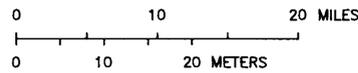
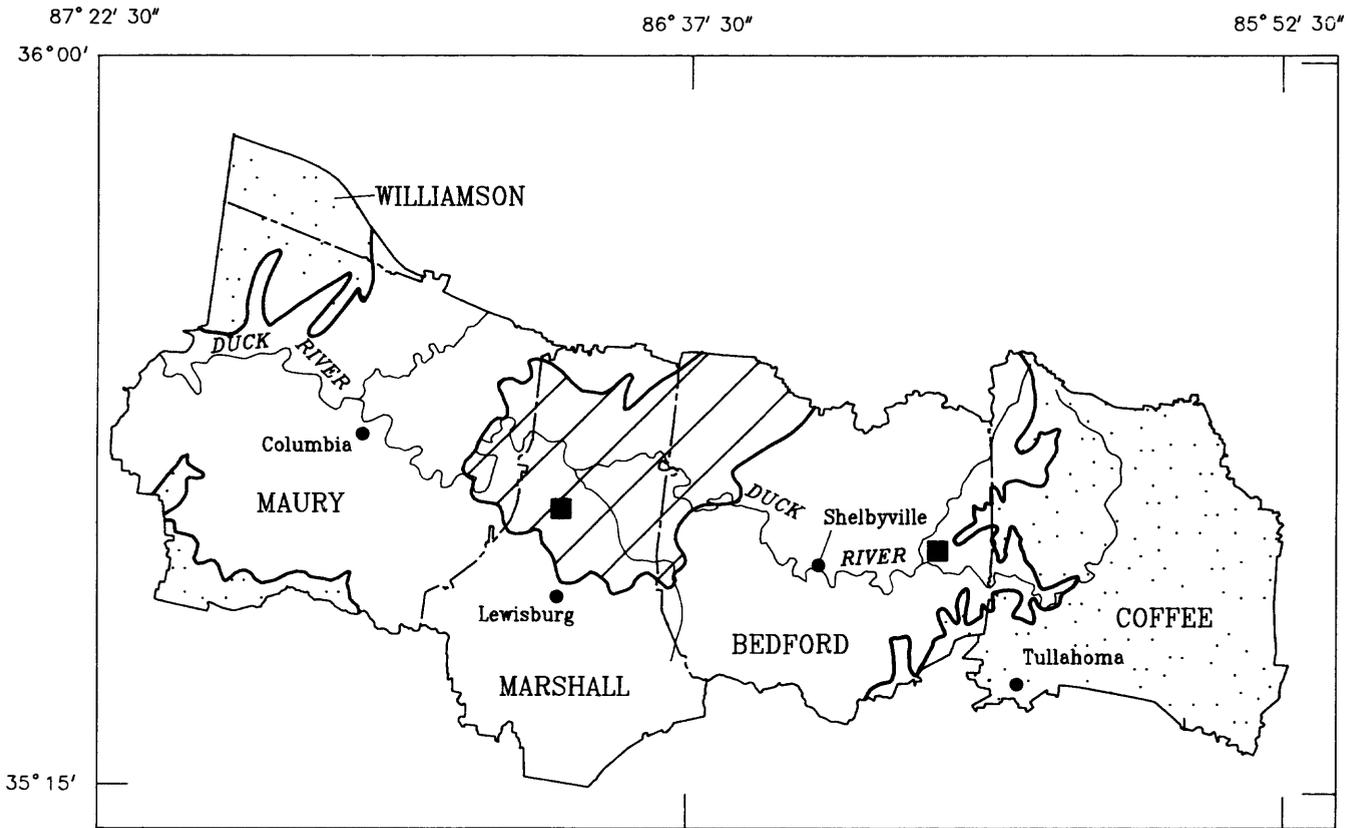


Figure 2. Physiographic regions, major aquifers, and seepage-investigation locations in the upper Duck River study area.

Surface Water

Normandy Dam, at river mile 248.6, has regulated the flow of the Duck River since January 1976. Flow releases are controlled to meet water supply and water-quality requirements downstream from the damsite. Releases from the reservoir have increased since 1981 to meet growing municipal demands and to maintain water quality at Shelbyville (river mile 221.4). Initially, a minimum winter release of 60 ft³/s (38.8 Mgal/d) was sustained. In 1987, the minimum winter flow was increased to 80 ft³/s (51.7 Mgal/d), and in January 1992, to 120 ft³/s (77.6 Mgal/d). Regulated summer flows at Shelbyville are higher, requiring a minimum flow of 155 ft³/s (100.2 Mgal/d) to ensure adequate water quality throughout the reach.

Low flows in the reach of the upper Duck River from Normandy Dam to the city of Columbia are used by Upper Duck River Development Agency and the Tennessee Valley Authority as an indicator of water availability. Low-flow statistics were obtained from analyzing 10 years of data (1979 to 1988) from USGS continuous-record gaging stations near Shelbyville (station 03598000) and downstream at Columbia (station 03599500). Analyses of the low-flow data show that:

- Minimum daily flow near Shelbyville is 72.0 ft³/s (46.5 Mgal/d); the minimum 3-day flow is 77.0 ft³/s (49.8 Mgal/d), recorded during October 1982.
- Minimum daily flow at Columbia is 86.0 ft³/s (55.6 Mgal/d); the minimum 3-day flow is 89.0 ft³/s (57.5 Mgal/d), recorded during October 1982.
- During the record drought of 1988, minimum daily flow near Shelbyville was 87.0 ft³/s (56.2 Mgal/d); at Columbia, 128 ft³/s (82.7 Mgal/d).

Ground Water

The elements of the study related to ground water were limited to:

- An inventory of well data to determine range of yields to wells within each county in the study area; and
- A seepage investigation in two subbasins to identify areas for potential ground-water development.

The scope of the project did not include an in-depth assessment of the ground-water resources in the study area. The information collected is inadequate to provide a practical assessment of the potential for development of additional ground-water supplies throughout the basin. The complex nature of the geology and ground-water flow in the limestone rock fractures underlying the basin will require additional investigation to properly assess the ground-water resources. Such an investigation would involve extensive data collection and test drilling.

A summary of yields to wells within the study area was compiled from files maintained by the USGS and the Tennessee Division of Water Supply (TDWS), Tennessee Department of Environment and Conservation (TDEC). The files contained records of 5,938 municipal, industrial, and domestic wells with a diameter of 6 inches or greater. Statistical analysis of yields from the wells in the inventory was performed. The values of the median and quartiles (25th and 75th percentile) are graphically displayed as box plots (fig. 3). Extreme values (those greater than 100 gal/min.) are not displayed so that the quartile ranges may be more clearly represented. In Bedford County, 9 wells had yields greater than 100 gal/min; Coffee County, 117 wells; Marshall County, 6 wells; and Maury County, 13 wells. The analyses showed that:

- Median yields to wells ranged from 5 gal/min in Maury County to 20 gal/min in Coffee County.
- Maximum yields were recorded from wells in Coffee County, with 25 percent of the wells

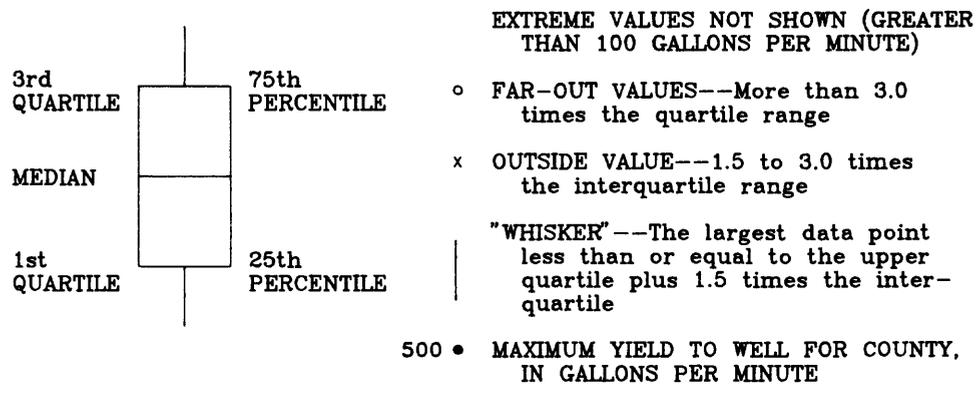
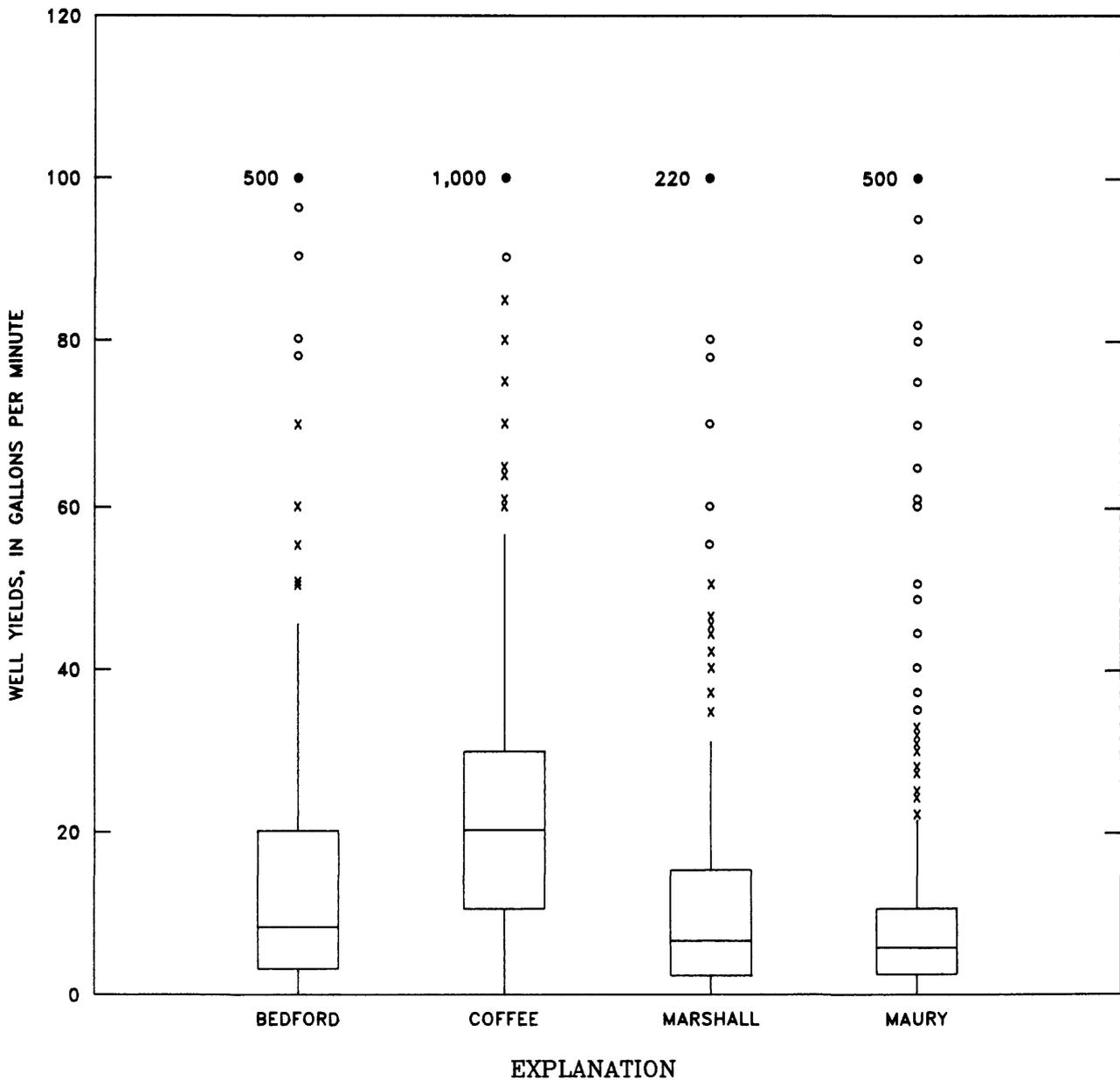


Figure 3. Distribution of yields to wells 100 gallons per minute and less by county in the upper Duck River basin.

exceeding 30 gal/min, and a maximum individual yield of 1,000 gal/min.

- Lowest yields were recorded in wells from Maury County, with 25 percent of the wells with yields of 12 gal/min or more. However, wells with yields as high as 500 gal/min have been drilled in the county.

The statistical analyses suggest that there is less likelihood that a well constructed in Maury County will have a yield as large as 100 gal/min as would a well constructed in Coffee County. However, the potential for ground-water development of a specific site in either county must be evaluated on factors pertinent to that site, rather than on statistical data of the entire county.

Seepage investigations can be used to screen potentially more productive areas from less productive areas within a ground-water basin prior to drilling (Burchett, 1977). The method uses discharge measurements made at selected points along a stream and its tributaries. The measurements must be made during a period of no surface runoff. Under this condition, streamflow is composed entirely of aquifer discharge. Using a large-scale map (preferably a 7¹/₂-minute topographic quadrangle map) to locate each measurement site, the drainage area for the site is measured and both the change in drainage area (ΔA) and the change in discharge (ΔQ) from the next site upstream are calculated. Relatively large values of the ratio of change in discharge to change in drainage area ($\Delta Q/\Delta A$, where ΔA is at least 0.01 mi²) reflect significant gains from the aquifer (or losses to the aquifer when the ratio results in a negative value), and indicate areas where water flows through the aquifer with a relative degree of ease. Rock or sediments in these areas has greater permeability than that in areas characterized by low $\Delta Q/\Delta A$ values, and potentially will provide greater yields of water to wells.

For this study, two seepage investigations were conducted: one at Hurricane Creek basin (Bedford County) and another at the East Fork of Big Rock Creek basin (Marshall County) (fig. 2). Analyses of the data from the studies (table 1) indicate several sites

with comparatively high ratios of $\Delta Q/\Delta A$, suggesting the potential for ground-water development in these subbasins. Discharge and area data are presented in Flohr and others (1991). A previous seepage investigation in several subbasins within Maury and Williamson Counties also showed several sites with potential for ground-water development (Lowery and others, 1987). Confirmation of the actual ground-water resources in these areas will require detailed investigations and test drilling.

Table 1. Seepage investigations in the upper Duck River basin

Site number	Site name	County	Aquifer	Date of measurement	Number of measurements
1	Spring Hill.	Maury and Williamson.	Bigby-Cannon.	4-21-87	45
2	Hurricane Creek.	Bedford	Bigby-Cannon.	4-04-90	33
3	East Fork of Big Rock Creek.	Marshall	Ridley	4-05-90	24

WATER USE

The upper Duck River basin is divided into four municipal water-service areas (WSA's)--Bedford, Coffee, Marshall, and Maury--whose boundaries closely coincide with their respective county boundaries (fig. 1). Municipal water use in the basin increased 16 percent from 1980 to 1990 (Alexander and others, 1984; Tennessee Division of Water Supply files, 1990; U.S. Geological Survey files, 1985, 1988, and 1990) (table 2). Correspondingly, the number of customer connections increased about 13 percent. Most of the increase occurred in recent years. The Maury WSA had an increase in water use of 11 percent from 1988 through 1990, the largest in the study area. Overall water use in the basin in the same period increased only 7.4 percent. These increases in water use are principally due to growth in the residential and industrial sectors.

Table 2. Water-service area withdrawals and number of customer connections

[Source: U.S. Geological Survey unpublished data, 1990]

Water-service area	Withdrawals, in million gallons per day					Number of connections	
	1980	1985	1988	1989	1990	1980	1990
Bedford	3.81	3.62	3.99	4.36	4.20	8,666	10,056
Coffee	3.50	3.62	3.94	3.83	3.95	10,780	12,121
Marshall	2.27	2.51	2.61	2.82	2.85	5,338	6,333
Maury	8.43	8.75	8.94	9.41	9.93	16,972	18,612
Basin totals	18.01	18.50	19.48	20.42	20.93	41,756	47,122

Weather affects the water-use patterns in the basin. During the summer season (May, June, July, and August) when temperatures are higher, water use increases because of outdoor use. If rainfall is below normal for the season, water use increases even more. Precipitation data from a weather station at Columbia and water-withdrawal records from the Columbia Water Department (Maury WSA) for a drought year (1988) were compared to data for a year with sufficient summer precipitation (1989) (fig. 4). During 1988, the total departure from normal rainfall during the summer season (May, June, July, and August) was -6.6 inches (U.S. Department of Commerce, 1989). Water use during this period of 1988 averaged 9.02 Mgal/d, or 13 percent above the 1988 annual average water use of 7.98 Mgal/d (table 3). In comparison, rainfall during the summer season of 1989 was 5.90 inches above normal (U.S. Department of Commerce, 1990). During this period, water use averaged 8.78 Mgal/d, or 3.5 percent above the 1989 annual average water use of 8.48 Mgal/d (U.S. Geological Survey files, 1989) (fig. 4).

The seasonal increase can be expressed also as a ratio of water use in summer to water use in winter. For the Columbia Water Department (Maury WSA), the ratio in 1988 was 1.21 (9.02 Mgal/d to

7.47 Mgal/d) (table 4). That is, for every 121 gallons per day used during the summer season, a household used 100 gallons per day during the winter season. Summer sprinkling (outdoor usage) accounts for the difference (Howe and Linaweaver, 1967).

Water use for the public-supply systems and municipally supplied industries in the study area for 1989 was estimated from an inventory of use. The inventory was conducted in 1990 in cooperation with TDWS. Twenty-four public-supply systems provided data detailing the source of supply; daily average-annual amount of water withdrawn or purchased (table 5); maximum daily withdrawal; population served; number of connections; distribution amounts to residential, commercial, and industrial users; conveyance losses; and free service. The municipally supplied industries provided data detailing their source(s) of supply, daily water usage, normal operation schedule, Standard Industrial Classification (SIC) categories, and number of employees. The results of the inventory indicated that:

- Municipal withdrawals during 1989 totaled 20.4 Mgal/d (table 2).
- The Duck River surface water accounted for 93 percent of the withdrawals (18.9 Mgal/d); the

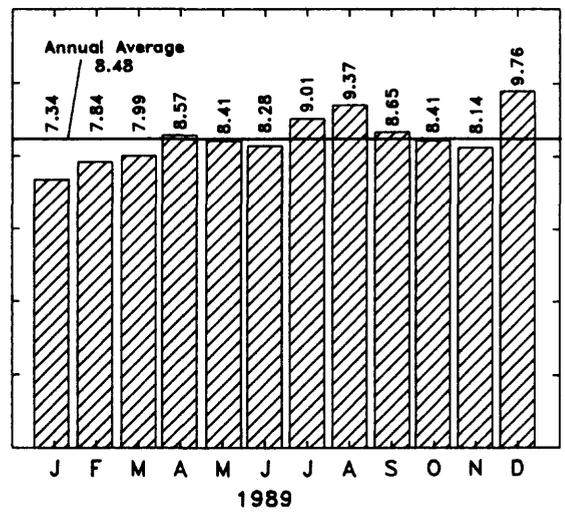
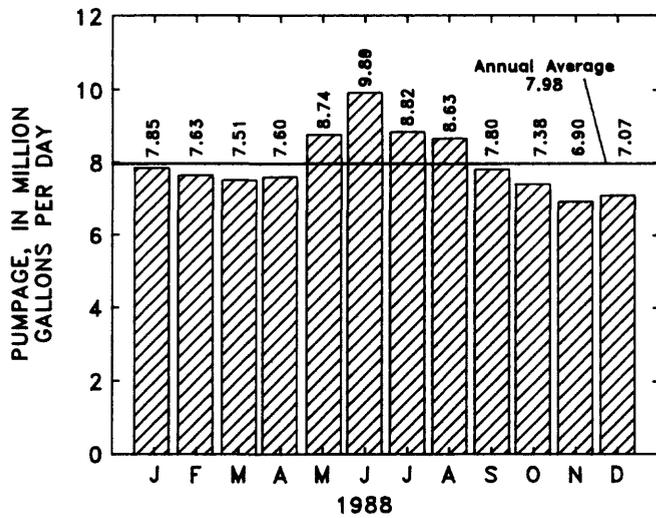
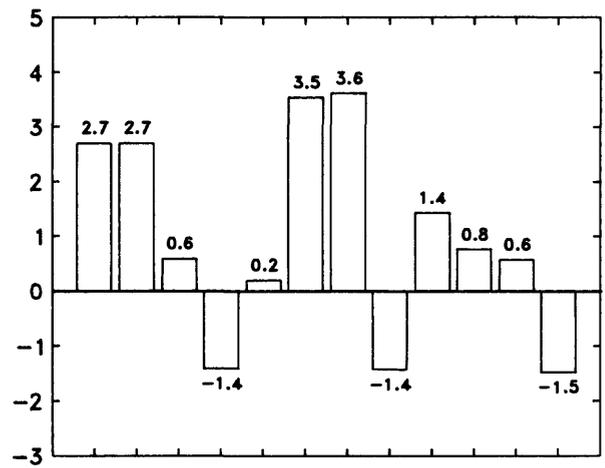
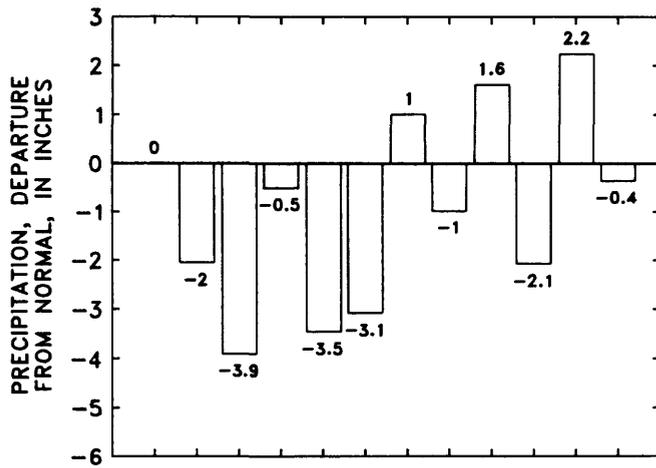


Figure 4. Monthly water withdrawals by Columbia Water Department and monthly departure from normal precipitation statistics for Columbia, Tennessee, for 1988 and 1989.

Table 3. Average daily water withdrawals by month for major public-supply systems during 1988

[Summer season usage (outdoor and indoor); and winter season usage (indoor)]

Month	Withdrawals, in million gallons per day, for indicated public water-supply system			
	Columbia Water Department	Lewisburg Water System	Shelbyville Water System	Duck River Utility Commission
Winter season				
January	7.85	2.39	2.96	3.92
February	7.63	2.28	2.72	3.84
March	7.51	2.31	2.50	3.80
April	7.60	2.43	2.61	3.90
September	7.80	2.51	2.88	3.87
October	7.38	2.49	2.66	3.59
November	6.90	2.48	2.73	3.30
December	7.07	2.52	2.84	3.48
Average	7.47	2.43	2.74	3.71
Summer season				
May	8.74	2.66	2.80	4.27
June	9.89	2.89	3.21	4.86
July	8.82	2.48	2.89	4.17
August	8.63	2.59	3.03	4.34
Average	9.02	2.66	2.98	4.41
Annual average	7.98	2.50	2.82	3.94

Table 4. Seasonal and maximum daily water-use ratios for major public-supply systems for 1988

[Summer, May through August; Winter, September through April; WD, Water Department; WS, Water System; UC, Utility Commission]

System	Daily average withdrawal, in million gallons per day				Ratio		
	Summer	Winter	Annual	Maximum	Summer/Winter	Summer/annual	Maximum/annual
Columbia WD	9.02	7.47	7.98	12.31	1.21	1.13	1.54
Lewisburg WS	2.66	2.43	2.50	3.81	1.09	1.06	1.52
Shelbyville WS	2.98	2.74	2.82	4.14	1.09	1.06	1.47
Duck River UC	4.41	3.71	3.94	5.74	1.19	1.12	1.46

Table 5. Public-supply facilities, source(s) of supply, and water use in the upper Duck River basin, Tennessee

[Mgal/d, million gallons per day; WSA, water-service area; __, no transaction; WS, Water System; Co., county; UD, Utility District; e, estimated; UC, Utility Commission; MCBPU, Marshall County Board of Public Utilities; WD, Water Department; and, MHP, mobile home park]

Facility	Source of supply (river mile)	Withdrawals, in Mgal/d	Purchased water, in Mgal/d
Bedford WSA			
Shelbyville Water System	Duck River (227.0)	3.22	—
Bedford County UD #1	Duck River (202.4)	.683	—
	Shelbyville WS		
Bedford County UD #2	Bedford Co. UD #1	—	0.080
	Wartrace WS		
Bell Buckle Water System	Wartrace WS	—	.140
Wartrace Water System	Cascade Spring	.452	—
Flat Creek Cooperative	Shelbyville WS	—	.140
Coffee WSA			
Manchester Water Department	Duck River UC	—	1.59
Tullahoma Board of Utilities	Duck River UC	—	2.10
Duck River Utility Commission	Duck River (255.0)	3.83	—
Hillsville Utility District	Manchester WD	—	.278
Shady Grove MHP	well	.007e	—
Stacy Anne's MHP	well	.007	—
Marshall WSA			
Chapel Hill Water System	MCBPU #1	—	0.000
	Town Well	0.114	—
Marshall County Board of Public Utilities	Lewisburg WS	—	.300
Cornersville Water Department	Lewisburg WS	—	.090
Petersburg Water System	Fayetteville WS	—	.050
Lewisburg Water System	Duck River (181.0)	2.71	—
Henry Horton State Park	MCBPU #1	—	.021
	Chapel Hill WS	—	—
Maury WSA			
Columbia Water Department	Duck River (133.7)	8.48	—
Mount Pleasant Water System #1	Spring	.930	—
Spring Hill Water Department	Columbia WD	—	.560
Maury County Water System	Columbia WD	—	.140
Mount Pleasant Water System #2	Columbia WD	—	.130
Hillsboro and Thompson Station Utility District	Spring Hill WD	—	.360

remaining 7 percent or 1.5 Mgal/d was withdrawn from springs and wells (table 5).

- Normandy Reservoir provided 20 percent of the surface water, or 3.83 Mgal/d (Duck River Utility Commission). The remaining 80 percent is withdrawn downstream of Normandy Reservoir at four public-supply intakes on the Duck River (Shelbyville, Bedford County Utility District, Lewisburg, and Columbia).
- During 1989, residential-sector water use accounted for 41 percent (8.36 Mgal/d) of total municipal water use; commercial, 10 percent (2.02 Mgal/d); industrial, 28 percent (5.64 Mgal/d); and, public/unaccounted water, 22 percent (4.4 Mgal/d) (table 6).

Table 6. Public-supply deliveries of water to various water-use sectors during 1989

[Mgal/d, million gallons per day]

Water-service area	Sector			
	Residential (Mgal/d)	Commercial (Mgal/d)	Industrial (Mgal/d)	Public/unaccounted (Mgal/d)
Bedford	1.62	0.192	0.957	1.59
Coffee	1.90	.503	.499	.931
Marshall	1.36	.215	.616	.629
Maury	3.48	1.11	3.57	1.25
Basin totals	8.36	2.02	5.64	4.40

WATER-DEMAND SIMULATION

Future municipal water demands within the upper Duck River basin were estimated using the Institute for Water Resources-Municipal and Industrial Needs System. Econometric demand and requirement (usually of the unit-use type) models calculated water demand as a function of socioeconomic parameters. Each of these parameters was projected for the future years for which water demand was estimated.

The IWR-MAIN System is used primarily to test assumptions and the effects that various assumptions or changes would have on water use in the basin rather than as a predictive tool to generate absolute values showing future water use. This use of the system and the basic assumptions about growth, land use, population, and technology determine the results. If the assumptions are changed (for example, population decreases in the area), the water-demand results will change. The results depend on the validity of the assumptions.

Model Description

The IWR-MAIN System is a water-demand forecasting system that contains a range of water-use models, socioeconomic-parameter generating procedures, and data-management techniques (U.S. Army Corps of Engineers, 1988). Nonmunicipal or rural water demand is not simulated by the IWR-MAIN System. The IWR-MAIN System architecture allows for spatial, sector, and seasonal disaggregation of a study area (fig. 5). The unit for spatial disaggregation is the WSA. This unit may correspond to a city-wide or county-wide public-supply facility or consist of all public-supply facilities within a county or basin. The system divides municipal water users within each WSA into four major sectors: residential, commercial, industrial, and public/unaccounted. Each sector is further disaggregated into a number of categories for simulation purposes (fig. 5). The seasonal dimensions of the system consider any one of the elements of annual average, winter or summer season, or maximum daily use for each sector and category.

The relation between the calibration and the simulation processes of the IWR-MAIN System is displayed graphically in figure 6. The schematic illustrates how the data modules (top) relate to the computational modules (middle) and to the results (bottom). The base-year data are used to produce future-year data by means of internal models that project growth for the various socioeconomic parameters. The growth in economic parameters (future data) also may be produced

INPUT DATA

Number of housing units by type, density and market-value range; average lot size; persons per household; and Composite Construction Cost Index

Number of employees by 3-digit Standard Industrial Classification (SIC) groups

Water and wastewater prices and rate structures; marginal price; bill difference

Climatic/weather conditions (moisture deficit)

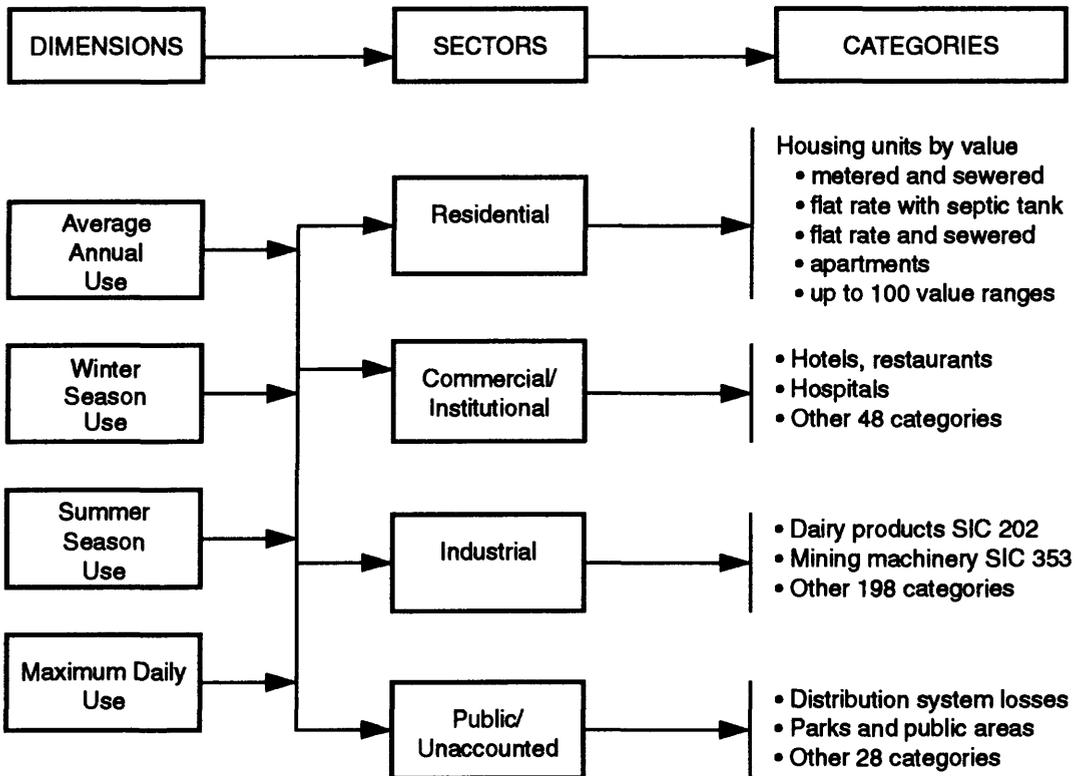
Residential population, income and employment

WATER-USE MODELS

Econometric equations
Unit-use requirement equations

LIBRARY DATA

DISAGGREGATED WATER USES

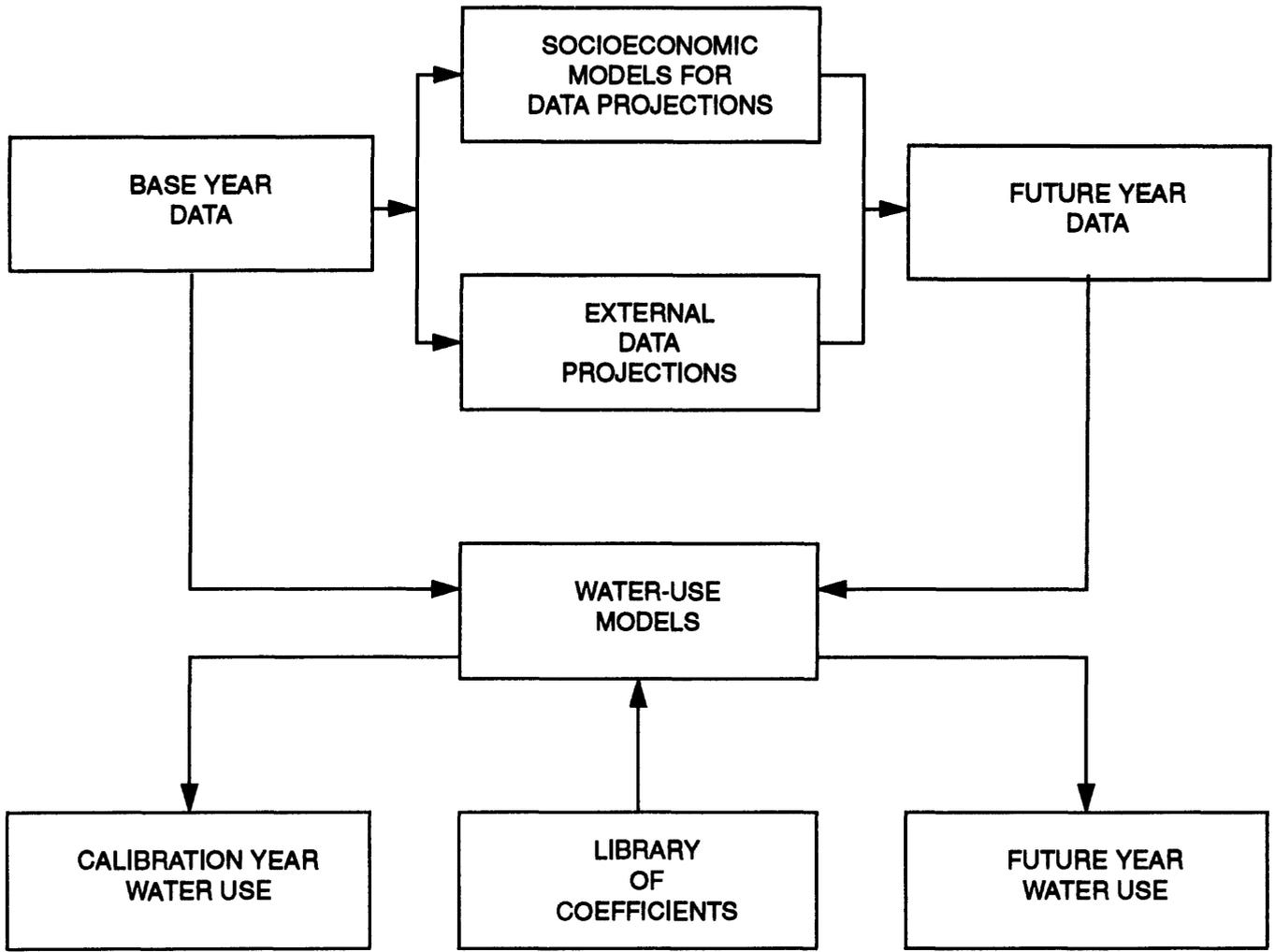


Modified from U.S. Army Corps of Engineers (1988)

Figure 5. Schematic describing the Institute for Water Resources-Municipal and Industrial Needs System architecture.

CALIBRATION

SIMULATION



Modified from U.S. Army Corps of Engineers (1988)

Figure 6. Schematic relating the calibration and simulation processes of the Institute for Water Resources-Municipal and Industrial Needs System to data, computational subroutine, library, and result modules.

externally by the user and added to the model. Base (or calibration) year data are incorporated into the water-use models to simulate base (or calibration) year water use. If the base and calibration year are different years, selected future-year data also are incorporated into the model. The water-use models are calibrated by adjusting the library values--model constants, parameter coefficients, climatic values--to

reflect local socioeconomic and climatic conditions. Base-year and future-year data are manipulated by the water-use models to calculate water demand for future years.

The 5.1 version of the IWR-MAIN System was used in this study (U.S. Army Corps of Engineers, 1988). The user's manual and system description

provides additional details for much of the discussion presented in this section of the report.

Demand Models

The econometric water-demand models relate socioeconomic parameters to water use for the residential, industrial, and commercial sectors (table 7). For the purposes of this study, these models were applied only to the residential sector. In this study, the residential sector was disaggregated into two categories: (1) metered and sewered, and (2) flat rate with septic tank (fig. 5). The number of housing units in each category is the significant variable driving the residential models. Housing value and price of water are the principal economic variables.

Table 7. Socioeconomic parameters input to the Institute for Water Resources-Municipal and Industrial Needs System

[SIC, Standard Industrial Classification]

Required base-year parameters	Future-year parameters
Number of residences by type and value range	Number of housing units by type and value range
Commercial and industrial employment by SIC	Commercial and industrial employment by SIC
Number of persons per household	Total employment ¹
Median household income	Median household income ¹
Resident population	Resident population ¹
Water and sewer rate structure	
Composite construction cost index	
Bill difference	
Climatic conditions	
Total population	

¹ Required model input.

Metered and Sewered Residential Model

Water demand for the metered and sewered (MW) category is calculated for each housing value range for the winter and summer seasons by applying multiple-

coefficient demand models containing elasticities for housing value and water use. Water use is then aggregated by the model to produce a weighted residential water use for the water-service area, including maximum daily and annual average use. Housing value acts as a proxy for income. Marginal price and bill difference (*Appendix A*) variables capture the effects of change in the water-rate structure on disposable income.

The MW winter-demand equation demonstrates a linear relation between quantity of water and various housing and pricing variables. As the following equation indicates, the projected quantity of water increases as the housing values increase; and water demand decreases as the marginal price of water and the effective annual bill difference increase.

$$(Q_D)_{ms} = (234 + 1.451 V/F_a - 45.9P_a - 2.59I_a)N_r, \quad (1)$$

where

- Q is water usage, in gallons per day;
- D is winter or indoor water use;
- ms is metered and sewered;
- 234 is y-intercept, number of gallons per household per day;
- V is average house value in a range of value per \$1,000;
- F_a is assessment factor;
- P_a is effective annual marginal price of water, in dollars per 1,000 gallons;
- I_a is effective annual marginal price of water, in dollars per billing period; and
- N_r is number of residences in value range r.

Summer usage includes indoor and outdoor usage. Outdoor usage is related to lawn or garden sprinkling, car washing, or other similar activity. Irrigable land and moisture deficit are variables which factor into the MW summer equation quantifying this additional usage as follows:

$$(Q_s)_{ms,e} = (385 + 2.876V/F_a - 285.8P_a - 4.35I_a + 157.77 * B * MD)N_r, \quad (2)$$

where

- is summer season;
- is east of the 100th meridian;
- 385 is y-intercept, number of gallons per person per day;
- P_s is effective summer marginal price of water, in dollars per 1,000 gallons;
- I_s is effective summer bill difference variable, in dollars per billing period;
- B is irrigable land per dwelling unit, in acres per unit;
- MD is summer-season moisture deficit, in inches; and

Q_s , V_s , F_s , B , and N_r are as defined in equation (1).

Irrigable land is a function of housing density and is derived from the following equation:

$$B = 0.803 * Hd^{-1.26} \quad (3)$$

where

- Hd is housing density, and
- B is as defined in equation (2).

Only the equation for the summer MW category includes weather conditions as a factor for influencing water demand. Precipitation and evapotranspiration values read from the IWR-MAIN Library of Climatic Variables produce values for the moisture deficit (MD) parameter. The latitude and longitude determine these precipitation and evapotranspiration values for each WSA (table 8). These climatic variables may be adjusted by the user to describe different climatic scenarios. Summer-season moisture deficit, MD , is calculated as follows:

$$MD = E - 0.6R \quad (4)$$

where

- E is summer-season potential evaporation, in inches; and
- R is summer-season precipitation, in inches.

Flat Rate with Septic Tank Residential Model

The flat rate with septic tank (FP) residential model estimates water use for the winter season as a function

Table 8. Climatological variables for the water-service areas

[Source: IWR-MAIN Library of Climatic Variables; rain and evapotranspiration measurements for the summer season (June, July, and August) based on long-term average weather data as of 1967]

Water-service area	Evapotranspiration		Precipitation (inches)
	Total (inches)	Maximum daily (inches)	
Bedford	17.25	0.29	11.00
Coffee	17.25	.29	11.00
Marshall	18.50	.29	10.50
Maury	18.50	.29	10.50

of persons per household and the number of housing units by value range. The equation constant, 30.2, represents the number of gallons per household per day. The FP category includes housing units that are occupied by customers who face a zero marginal price. This category is often used as a user-defined category to include, for example, housing units which are self-supplied. The equation is as follows:

$$(Q_D)_r = (30.2 + 39.5D_p)N_r \quad (5)$$

where

- r is flat rate with septic tank residential use,
- D_p is persons per household, and
- Q , D , and N_r are as defined in equation (1).

In the FP summer-usage equation, an exponential relation exists between housing value and water use. For each 1-percent increase in housing value, water use increases 0.783 percent. Also winter usage is a variable. The relation of water quantity to the variables is as follows:

$$(Q_s) = (0.41 * 44.573 * (V/F_s)^{0.783})N_r * 2.0 + (Q_D)_r \quad (6)$$

Q_s , V , F_s , N_r , D , and r are as defined in equations (1), (2), and (5).

Unit-Requirement Models

The unit-use requirement models estimate future water demand as a product of projected WSA

commercial and industrial employment and a value of per-employee water use. The unit-use coefficient is assumed to be fixed through time; that is, new technology is not a factor the model recognizes. Price elasticities are not factors in the models. Industrial water use is estimated as follows:

$$(Q_a)_n = (C_a)_n * P_n, \quad (7)$$

where

- a is average annual use;
- n is industrial use category;
- C is industrial water-use coefficient, in gallons per employee per day;
- P is water use parameter--employment; and
- Q is as defined in equation (1).

Data Preparation/Model Input

Housing and employment data were prepared as input to the water-use and socioeconomic models contained in the IWR-MAIN System. Several assumptions about the character of the data for the base and the calibration years and about the structure of socioeconomic conditions in future years were necessary to model the basin. These assumptions are detailed within the respective data sections.

The water-use models of the IWR-MAIN System used demographic and economic data provided externally by the user as well as parameter values generated internally by socioeconomic models in the system. Actual values of these parameters (table 7) are required for a base, or beginning year, and projected values of selected parameters for specified future years. The data were developed for each WSA (Bedford, Coffee, Marshall, and Maury) for the residential, commercial, and industrial sectors. This spatial disaggregation allowed the system to consider varying rates of sector growth within the basin, and to consider the effect of different rate structures on water use. Data were prepared for the base year, 1980; calibration year, 1989; and, future years, 1995, 2000, and 2015.

The socioeconomic models (referred to as housing or employment models) in the IWR-MAIN System generated future values for housing and employment. These models contain coefficients and elasticities developed from intensive statistical analyses of data sets representing a cross section of national housing and employment patterns (U.S. Army Corps of Engineers, 1988). Unlike the water-use models, these models are not calibrated by the user to reflect local socioeconomic conditions. Instead, data detailing local conditions are input to the IWR-MAIN System and override the parameter-generating algorithms.

For the purposes of this study, the base year (1980) and calibration year (1989) are two different years. Socioeconomic conditions had changed significantly between 1980 and 1989 and sufficient data were available for 1989 to calibrate that year. The quality of the water-use data also improved significantly from 1980 to 1989. Whereas the 1980 water-use data were insufficient to ensure a reliable calibration, a water-use inventory for 1989 provided sufficient data to satisfy modeling requirements.

Some base-year data are required to calibrate the water-use models in this study and some are required by the socioeconomic models to quantify initial housing and employment conditions (table 7). At a minimum, a water-demand forecast requires the user to input total population, total employment, and median income for each future year. For this study, the number of housing units by type and employment statistics for several categories were projected externally and added to the system for the forecasts.

For the public/unaccounted sector and for the maximum-daily use dimension, water use was estimated externally to the system. Public/unaccounted water was calculated as a percentage of the total municipal water use (fig. 5). For the calibration year, the percentage reflects the unaccounted amount observed for the major public-water facility in each WSA; for the future years, the percentage remains constant through time for each WSA at 15 percent. This 15 percent is close to the default value for the

IWR-MAIN System, 14.9 percent. For maximum daily water use, the ratio of maximum daily to annual average water use for 1988 (a drought year) (table 3) was applied to the total water use for the calibration and the future years. This estimated amount represents, therefore, maximum daily water use under drought conditions.

Housing Data

The residential sector of the IWR-MAIN System was disaggregated into two housing categories: MW and FP (fig. 5). For modeling the Duck River basin these housing categories were defined as follows:

- MW consists of specified, occupied housing units (housing units built on less than 10 acres of land without property attachment) (U.S. Department of Commerce, 1982a). These units are individually metered, but not necessarily sewered.
- The FP category was principally used to manage the housing-unit data that were not included in the MW category. It includes housing units which depend on domestic wells (self-supplied) for their water; nonspecified housing units [housing units situated on 10 acres or more or housing units attached to a commercial establishment (U.S. Department of Commerce, 1982a)]; and, mobile homes. FP water demand is not included in the municipal totals for water demand for the basin. FP water-use models were not calibrated for this study, because no actual water-use data existed to compare to a simulated water demand.

Base- and Calibration-Year Data

Several sources of data were used in preparing base-year input values required to construct the residential water-use models (table 7). The U.S. Census Bureau provided data enumerating: specified owner-occupied housing units by value range; renter-occupied units by range of contract rent; and occupied housing units in the county and urban areas served by public-supply systems or served by sewerage (U.S.

Department of Commerce, 1982a, 1983). The number of housing units by type (MW or FP) and value range that were input to the model for the base year 1980 resulted from the spatial analysis of these data sets (table 9). All renter-occupied units are included in the MW category. Renter-occupied units were combined with owner occupied units to yield total occupied units by value range. Contract rent was converted to housing value using the following equation:

$$F = \frac{(1 + i)^N}{i(1 + i)^N} \quad (8)$$

where

F is conversion factor,

i is 1980 discount rate, and

^N is number of months in mortgage period.

Equivalent housing value expressed in 1980 dollars is as follows:

$$V = R * F \quad (9)$$

where

V is equivalent housing value, and

R is monthly rent.

For the basin,

F = 66.353,

i = 0.015 (18 percent in 1980), and

^N = 360.

For the calibration year (1989), estimates of the total number of occupied housing units by WSA were provided by the Tennessee Housing Development Agency (Linda Lavagia, oral commun., 1990). The type of decennial data (U.S. Department of Commerce, 1982a) used to disaggregate the housing units by type (MW or FP) for 1980 was not available for 1989; therefore, the same proportions as determined for the base year were used for 1989 (table 9).

Housing density (fig. 5, table 7) for the central part of the city of Columbia (David Holderfield, Director of Grants and Planning for the City of Columbia, oral commun., 1991) was used as the housing density value for each WSA for the base, calibration, and future years. This density value is 6 units per acre. Housing density in each WSA is low compared to

Table 9. Number of occupied housing units by type

[WSA, Water-service area; MW, metered and sewered; FP, Flat rate with septic tank]

WSA	Housing units				
	1980	1989	1995	2000	2015
Bedford					
MW	6,713	8,060	10,519	12,028	14,240
FP	3,232	3,880	2,034	1,060	593
Coffee					
MW	10,401	12,489	14,916	16,348	18,227
FP	3,249	3,944	2,034	1,043	564
Marshall					
MW	5,215	6,351	7,361	8,639	10,222
FP	1,929	2,350	1,727	854	487
Maury					
MW	14,499	15,875	19,313	20,943	23,165
FP	2,792	3,131	1,566	647	716

housing density in the urban areas where most of the municipal water is delivered. Because the model uses housing density to calculate the amount of irrigable land, equation 3, and ultimately summer demand, a high housing density was necessary for each WSA to calibrate the expected summer usage.

The model is structured so that only one value for the housing density variable for the base, calibration, and future years can be specified for each model run. Changing the housing density value creates an alternative water-use scenario. Model input for the pricing and the climate variables have the same limits, wherein each pricing and climate specification represents a new set of model conditions and a different water-use scenario.

The U.S. Census Bureau provided statistics for resident population (fig. 5, table 7) for each WSA for

the base year (1980). The Department of Sociology, University of Tennessee, projected resident population for the calibration year (1989) (B.B. Vickers, University of Tennessee, 1990). Future-year projections resulted from the application of the growth equation to the 1980 census data and the 1990 preliminary census data (April 1990) (*Appendix B*) as follows:

$$POP_U_t = POP_U * e^{kt}, \quad (10)$$

where

- POP_{U_t} is future year population,
- POP_U is population as of 1980,
- e is the base of the natural logarithm
- k is growth constant, and
- t is projection time interval.

An inventory of water- and wastewater-rate structures for each system in each WSA was used to specify annual, summer season, and marginal price,

and to calculate bill difference for the base year (tables 7 and 10, and fig. 5). Rate-structure information for the period 1980-90 was compiled and the rates were expressed in 1980 constant dollars. The annual inventory of water- and wastewater-rate structures by Allen and Hoshall Consultants, provided supplemental rate data (1980 to 1990) (Allen and Hoshall Consultants, written commun., 1991).

Table 10. Marginal price and bill difference in 1980 dollars for the metered and sewerred housing category

Water-service area	Annual price per thousand gallons	Marginal price per thousand gallons	Bill difference per thousand gallons
Bedford	8.69	6.08	1.64
Coffee	2.89	2.59	4.57
Marshall	3.21	3.13	1.27
Maury	1.80	1.65	3.78

The rate structure imposed by the largest public supplier in each WSA was adopted as the determining rate structure for water demand in that WSA (table 10). Either this public supplier served most of the connections in the WSA or it distributed water to other systems, influencing their rate structure. The selected systems were Columbia Water Department (Maury WSA), Lewisburg Water System (Marshall WSA), Shelbyville Water System (Bedford WSA), and Tullahoma Utility Board (Coffee WSA).

Future-Year Data

For the future years (1995, 2000, and 2015), the number of total housing units was generated externally to the IWR-MAIN System (fig. 5, table 7). The external method uses the projected resident population for each future year and divides by the number of persons per household in 1990 (U.S. Census Bureau, written commun., 1990) (*Appendix B*). To project the number of housing units by type for each simulation interval (1989 to 1995; 1995 to 2000; and 2000 to 2015), the percent of FP housing units was decreased

by about 50 percent (table 9). For example, for the Bedford WSA, the FP housing units are 32.5 percent of the total housing units. For the first simulation interval (1989 to 1995), the percentage of FP units was reduced to 16.2 percent; the next interval (1995 to 2000), 8 percent; and the last interval (2000 to 2015), 4 percent. This reduction quantifies a water-use scenario reflecting an assumed rate of expansion for the public-supply systems and a corresponding rate of decrease for domestic self-supplied water within each WSA. This scenario also assumes that in the future none of the WSA's will be 100-percent supplied by public water.

For the calibration and future years, the number of housing units within a selected value range for a specified housing type (MW or FP) were generated by an internal econometric housing model (fig. 5, table 7). In calculating the percent of housing units for a selected value range, this housing model considered the rate of changes in median income and in population from the base year to the future year (U.S. Army Corps of Engineers, 1988) (table 11).

The only complete assessment of median household income in Tennessee occurs in each decennial census (fig. 5, table 7). The 1980 Census provided base year (1980) median household income. For the calibration and future years, median household income was projected using a multiplier derived from the average of the rate of change in per capita income in constant 1972 dollars projected by the Bureau of Economic Analysis, U.S. Department of Commerce (1988) (table 12). Six rates of change were projected from 1980 to 2015. These projected rates of change were used in conjunction with the 1979 median household income for each county as reported by the U.S. Census Bureau in 1980, which enabled the projection to be expressed in constant 1979 dollars. The multiplier was used as a measure of expected growth in median household income through the year 2015. The projected rates of change in per capita income ranged from 0.003 (1980-83) to 0.031 (1983-89) (Charles Brown, Director of Tennessee Data Center, oral commun., 1991).

Table 11. Projected metered and sewer occupied housing units by value range

[WSA, water-service area]

WSA Value range, in \$1,000 (1980 constant dollars)	Housing units			
	1989	1995	2000	2015
Bedford				
0.0 - 10.0	1,877	1,889	1,739	395
10.0 - 20.0	1,240	1,248	1,150	261
20.0 - 30.0	1,096	1,103	1,016	231
30.0 - 50.0	1,667	1,979	2,055	1,922
50.0 - 100.0	1,238	1,995	2,518	4,171
100.0 - 150.0	789	1,930	2,974	6,082
150.0 - 200.0	102	249	384	785
200.0 - 200.1	51	125	192	426
Coffee				
0.0 - 10.0	2,363	2,117	1,826	378
10.0 - 20.0	2,110	1,891	1,631	337
20.0 - 30.0	1,248	1,118	964	199
30.0 - 50.0	2,657	2,887	2,863	2,411
50.0 - 100.0	2,824	4,183	5,059	7,748
100.0 - 150.0	1,139	2,407	3,544	6,330
150.0 - 200.0	117	247	364	650
200.0 - 200.1	31	66	97	173
Marshall				
0.0 - 10.0	1,553	1,407	1,379	317
10.0 - 20.0	1,029	932	914	210
20.0 - 30.0	941	852	836	192
30.0 - 50.0	1,072	1,125	1,223	1,167
50.0 - 100.0	994	1,351	1,683	2,818
100.0 - 150.0	639	1,420	2,185	4,628
150.0 - 200.0	49	109	168	356
200.0 - 200.1	74	164	252	534
Maury				
0.0 - 10.0	2,465	2,181	1,928	413
10.0 - 20.0	3,186	2,819	2,493	524
20.0 - 30.0	1,644	1,455	1,286	276
30.0 - 50.0	3,166	3,467	3,475	2,953
50.0 - 100.0	3,073	4,406	4,973	7,282
100.0 - 150.0	1,788	3,809	5,185	8,943
150.0 - 200.0	347	739	1,006	1,743
200.0 - 200.1	206	439	597	1,030

Table 12. Median household income

[WSA, water-service area]

WSA	Median household income, in 1980 constant dollars				
	1980	1989	1995	2000	2015
Bedford	13,757	16,671	18,699	20,343	25,035
Coffee	14,331	17,366	19,479	21,191	26,077
Marshall	13,523	16,387	18,381	19,997	24,608
Maury	14,726	17,844	20,015	21,561	26,040

Employment Data

For the commercial sector, several SIC categories are grouped into one because the water-use coefficients for the categories are similar. For industry, a more comprehensive data base and a greater range of values for coefficients for the categories resulted in more disaggregation of the industrial categories than of the commercial categories. The number of commercial employment categories for the four WSA's range from 4 to 11. The number of categories for industry range from 13 to 30 (table 13).

Base- and Calibration-Year Data

The water-use models require employment statistics at the 3-digit SIC level for the commercial and industrial sectors whereas the employment model only requires this level of disaggregation for the base year. The most comprehensive data are published at the 2-digit SIC level by the Tennessee Department of Employment Security (1990, 1991). The U.S. Census of Population and Housing for 1980 (U.S. Department of Commerce, 1982b) provides total employment and employment by 2-digit SIC category for each WSA for the base year 1980. Employment statistics are sparse at the 3-digit SIC level. An unpublished water-use inventory (Tennessee Division of Water Supply, computer files, 1981) for 1980 enabled some disaggregation of industrial water users by 3-digit SIC code. In one major water-use category, metals and machinery (SIC 33), only about 25 percent of the employees were identified at the 3-digit SIC level. Therefore, the remaining employees (SIC 33) were assigned to a

3-digit SIC category that reflected the average water use per employee for the 2-digit category (U.S. Army Corps of Engineers, 1988).

The employment model requires total employment data for each WSA for 5 years before the base year, the base year, the calibration year, and each future year. The State Labor Force Summary provided total employment statistics from 1975 (5 years before the base year) to 1989 (Tennessee Department of Employment Security, 1990). The industrial water-use inventory conducted by TDWS in 1989 (U.S. Geological Survey unpublished data, 1990), the Directory of Manufacturers (White, 1989), the Community Economic Data publications (Tennessee Department of Economic and Community Development, 1988; 1989a; 1989b; 1989c; 1990), and Tennessee labor force estimates from the Tennessee Department of Employment Security (1990) provided a means of disaggregating the 2-digit employment water-use estimates, statistics to 3-digit statistics. For the calibration year water-use estimates, employment is disaggregated into 3-digit SIC categories.

Future-Year Data

Regression analysis predicted total employment for each WSA for 1995, 2000, and 2015 (*Appendix C*) (fig. 5, table 7). Information detailing plant closings, expansions, or initiations determined from 1990 industrial data were used to externally project changes to employment statistics in the 3-digit SIC categories. For those SIC categories for which no growth information was available, the employment model generated the future year statistics. The employment model reviews changes in total employment implied by base year and future year data to establish a compound rate of growth. Employment projections for each of the simulation periods result from applying this growth rate to the base-year employment total.

Model Calibration

Model calibration consists of inputting actual socioeconomic data for a period of time and simulating water use by various sectors of the municipal system. Actual water use is compared to simulated results to

Table 13. Model and calibration coefficients by employment categories for the Institute for Water Resources-Municipal and Industrial Needs System

[NC, no change to model coefficient; SIC, Standard Industrial Classification; values, in gallons per day per employee; --, not applicable]

Category	SIC	Model coefficient	Calibration coefficient			
			Bedford	Coffee	Marshall	Maury
Commercial sector						
Miscellaneous commercial.	--	47.2	19.1	24.1	167.0	248.0
Barbers and cleaning.	--	380.2	190.1	NC	NC	NC
Recreational facilities.	--	225.5	167	NC	NC	NC
Hotels and restaurants.	--	186.6	93	54.1	NC	NC
Parks	--	720.7	NC	NC	21,000	NC
Government	--	70.6	35.3	35.3	NC	NC
Utilities	--	6.7	NC	NC	NC	20
Industrial sector						
Meat products	201	343.8	331	NC	NC	NC
Dairy products	202	354.4	NC	NC	1,505	NC
Beverages	208	691.4	NC	200	NC	NC
Paperboard	265	91.3	NC	NC	112	NC
Plastics	282	333.3	NC	NC	363	NC
Soap	284	283.1	NC	NC	19	NC
Paints	285	254.7	NC	NC	130	1,329
Agricultural chemicals.	287	839.9	NC	NC	NC	1,650
Rubber products	306	144.9	NC	NC	152.5	NC
Plastics	307	206.2	200	68	152.5	2,034
Footwear	314	60.1	NC	NC	20	NC
Concrete	327	183.8	NC	NC	1,134	440.3
Nonmetallics	329	156.6	NC	NC	NC	375.1
Nonferrous	335	303.0	NC	NC	NC	479
rolling.	336	184.8	NC	NC	70	NC
Nonferrous foundry.	345	122.4	NC	NC	46	NC
Metal services	347	425.3	NC	NC	380.8	NC
Fabricated metal	349	102.6	NC	NC	47	NC
Metalworking	354	41.9	NC	NC	18.6	NC
Machinery	358	139.7	NC	NC	124	190
Electrical	362	189.9	NC	NC	NC	1,379
Vehicles	371	217.9	200	NC	51.8	NC
Boat building	373	110.1	NC	57	NC	NC
Toys	394	110.9	NC	69	NC	NC
Pens and pencils	395	102.4	NC	NC	43.3	NC
Miscellaneous	399	93.9	NC	69	NC	9,600

determine calibration accuracy. Two major steps comprise the calibration process:

- (1) Initial simulation using all the default parameters of the IWR-MAIN System; and
- (2) Analysis of the pattern of errors resulting when the simulated water demand is compared to the actual values, then adjusting equations as needed.

The year 1989 was selected for calibration because water use was inventoried for the public-supply systems and industries in the upper Duck River basin for that year. The water-use inventory provided a guide to adjusting the residential, commercial, and industrial constants and coefficients of the water-use models (tables 13 and 14).

Table 14. Model and calibration constants for the metered and sewered housing models

Metered and sewered housing models	Model constant	Calibration constant			
		Bedford	Coffee	Marshall	Maury
Winter season	234	541	217	294	235
Summer season	385	2,407	241	829	385

For this study, the IWR-MAIN System estimates of the residential water demand for each season exhibit a systematic error of overpredicting (or underpredicting) actual water use in the calibration year. The percent error is approximately the same for all years within each WSA. This pattern of prediction error indicates that residential water use in the study area is characterized by a higher (or lower) base use than that observed in the data that were used to derive the IWR-MAIN System demand models. A systematic error of overpredicting water use was noted in the Coffee WSA (table 15). In contrast, the simulated residential water demand for the Bedford, Marshall, and Maury WSA's was consistently lower. The simulated water demand for the Maury WSA was slightly less than the actual residential water use.

The winter and summer equation constants (y-intercepts) representing gallons per household per day were adjusted to calibrate the seasonal models. Summer and annual water usage for each WSA were calibrated to yield a ratio of about 1.04 to agree with the summer (May-August) and annual ratio for the Columbia Water System for 1989 (fig. 4). Columbia Water System closely mirrored the seasonal water use of the other major water systems in the basin.

For the industrial and commercial unit-use requirement models, the results of the initial calibration revealed the need to adjust the IWR-MAIN System default coefficients from the Library of Coefficients (U.S. Army Corps of Engineers, 1988). The coefficient defining the per employee water use in various commercial and industrial categories (table 13) required adjustment, with the commercial sector requiring the greatest adjustments. Per employee rates of use for the largest utility customers were verified using the data compiled from the 1989 survey. These included industries with high employment, high projected rate of growth, or large quantity users. Changes to the coefficients reflect local per employee use for a specific SIC or represent average employee use for aggregated SIC categories (table 13).

Model Reliability

The constants, coefficients, and elasticities in the water-use models were generally reliable in estimating residential water demand. For two of the WSA's, the

Table 15. Observed and modeled average annual water demand for metered and sewered housing for 1989

[Mgal/d, million gallons per day]

Water-service area	Observed value (Mgal/d)	Simulated water demand without adjustments (Mgal/d)	Simulated water demand with adjustments (Mgal/d)
Bedford	1.64	-0.89	1.64
Coffee	1.90	2.30	1.90
Marshall	1.36	.92	1.36
Maury	3.48	3.46	3.48

pricing elasticities exceeded the model values. For the Bedford WSA, water rates exceeded the range of the pricing elasticities developed from the national data sets. A negative water demand (-0.89 Mgal/d) resulted (table 15). For the Marshall WSA, the calibration underpredicted water use by 32.4 percent. For both WSA's, a large adjustment to the y-intercept of the seasonal equations was made (table 14). The large adjustment to the y-intercept for the residential equations necessary to offset or counterbalance the low elasticities may create some concern about reliability of the model. The alternative is to develop extensive local data to calculate a local set of elasticities. The developers of the model recommend adjusting the equations by the methods described rather than attempting to develop local data with limited resources (Eva M. Opitz, Planning and Management Consultants, Ltd., oral commun., 1991).

The housing model calculates the percent change in number of housing units within a value range based on the percent change in median income and in population from the base year to the future year. This relation between housing units and median income is the least reliable factor in this study and, therefore, open to question. The projected median income is based on projected per capita income (table 12). These two measures of income are not the same. Per capita income was used in this study because it was the best available projected income data. In Maury County, the percent change in projected median income from 1989 to 2015 was about 77 percent (\$14,726 to \$26,040) (table 12). Although the constant dollar amount was small (\$11,314), the percent change in the housing value range, 100.0-150.0 thousand dollars, was large enough that the shift was significant (table 11). For 1980, about 1 percent of the MW housing units were in this range; for 2015, 38.6 percent of the MW housing units were in this range. As demonstrated in equation 1, as housing value increases, water use increases. In the Maury WSA, per capita water use increased 38.9 percent [35 gallons per day (gal/d) from 1989 to 2015 (from 88 to 123 gal/d)] (table 16).

However, overall comparisons of the simulated residential water demand for the basin are acceptable and represent the specified model assumptions.

Table 16. Per capita use for the residential sector

Water service area	Per capita use, in gallons per person per day			
	1989	1995	2000	2015
Bedford	80	91	98	120
Coffee	62	70	75	89
Marshall	86	91	102	129
Maury	88	99	106	123

Results of Simulation

The calibrated models of the IWR-MAIN System were used to simulate water demand in the upper Duck River basin for the years 1995, 2000, and 2015. The results of the simulation (table 17) show that:

- Total average water demand in the basin could increase 19 percent by year 1995, 39 percent by year 2000, and 91 percent by year 2015. The largest increases could occur in the Maury WSA (112 percent);
- Residential demand by year 2015 could increase 122 percent, with the largest increase in the Bedford WSA (162 percent);
- Industrial demand by year 2015 could increase 93 percent, with the largest increase in the Maury WSA (114 percent); and
- Commercial demand could increase 82 percent, with the largest increase in the Maury WSA (115 percent).

Maximum daily water demand could increase 91 percent, with the largest potential increases in the Maury WSA (112 percent) followed by the Marshall WSA (100 percent).

Table 17. Simulated water demand, upper Duck River basin, by sector for 1989, 1995, 2000, and 2015

[Mgal/d, million gallons per day; WSA, water-service area]

Sector	1989 (Mgal/d)	1995 (Mgal/d)	2000 (Mgal/d)	2015 (Mgal/d)	Percent change 2015 over 1989
Bedford WSA					
Residential	1.64	2.41	2.97	4.29	162
Industrial	.96	1.06	1.18	1.54	60.0
Commercial	.19	.20	.21	.26	36.8
Public/unaccounted	1.58	.65	.77	1.07	-32.0
Total sector use	4.37	4.32	5.13	7.16	63.8
Percentage public/ unaccounted.	36.10	15.00	15.00	15.00	-58.4
Maximum daily	6.44	6.35	7.54	10.53	63.5
Coffee WSA					
Residential	1.90	2.54	3.00	3.98	109
Industrial	.50	.54	.58	.70	40.0
Commercial	.50	.53	.55	.61	22.0
Public/unaccounted	.93	.64	.73	.93	0.0
Total sector use	3.83	4.25	4.86	6.22	62.4
Percentage public/ unaccounted.	22.00	15.00	15.00	15.00	-31.8
Maximum daily	5.55	6.16	7.05	9.02	62.5
Marshall WSA					
Residential	1.36	1.78	2.24	3.31	143
Industrial	.61	.69	.79	1.03	68.9
Commercial	.22	.26	.30	.41	86.0
Public/unaccounted	.63	.49	.60	.88	39.7
Total sector use	2.82	3.22	3.93	5.63	99.6
Percentage public/ unaccounted.	22.30	15.00	15.00	15.00	-32.7
Maximum daily	4.29	4.89	5.97	8.56	99.5
Maury WSA					
Residential	3.48	4.74	5.44	7.06	103
Industrial	3.57	4.27	5.10	7.64	114
Commercial	1.11	1.64	1.79	2.39	115
Public/unaccounted	1.25	1.88	2.08	2.88	130
Total sector use	9.41	12.53	14.41	19.97	112
Percentage public/ unaccounted.	13.30	15.00	15.00	15.00	12.8
Maximum daily	14.49	19.30	21.30	29.60	112

Table 17. Simulated water demand, upper Duck River basin, by sector for 1989, 1995, 2000, and 2015--Continued

Sector	1989 (Mgal/d)	1995 (Mgal/d)	2000 (Mgal/d)	2015 (Mgal/d)	Percent change 2015 over 1989
Upper Duck					
Residential	8.38	11.47	13.65	18.64	122
Industrial	5.64	6.56	7.65	10.91	93.4
Commercial	2.02	2.63	2.85	3.67	81.7
Public/unaccounted	4.39	3.66	4.18	5.76	31.2
Total demand	20.43	24.32	28.33	38.98	90.8
Maximum daily	30.77	36.70	42.75	58.86	91.3

EFFECT OF WATER WITHDRAWALS ON STREAMFLOW

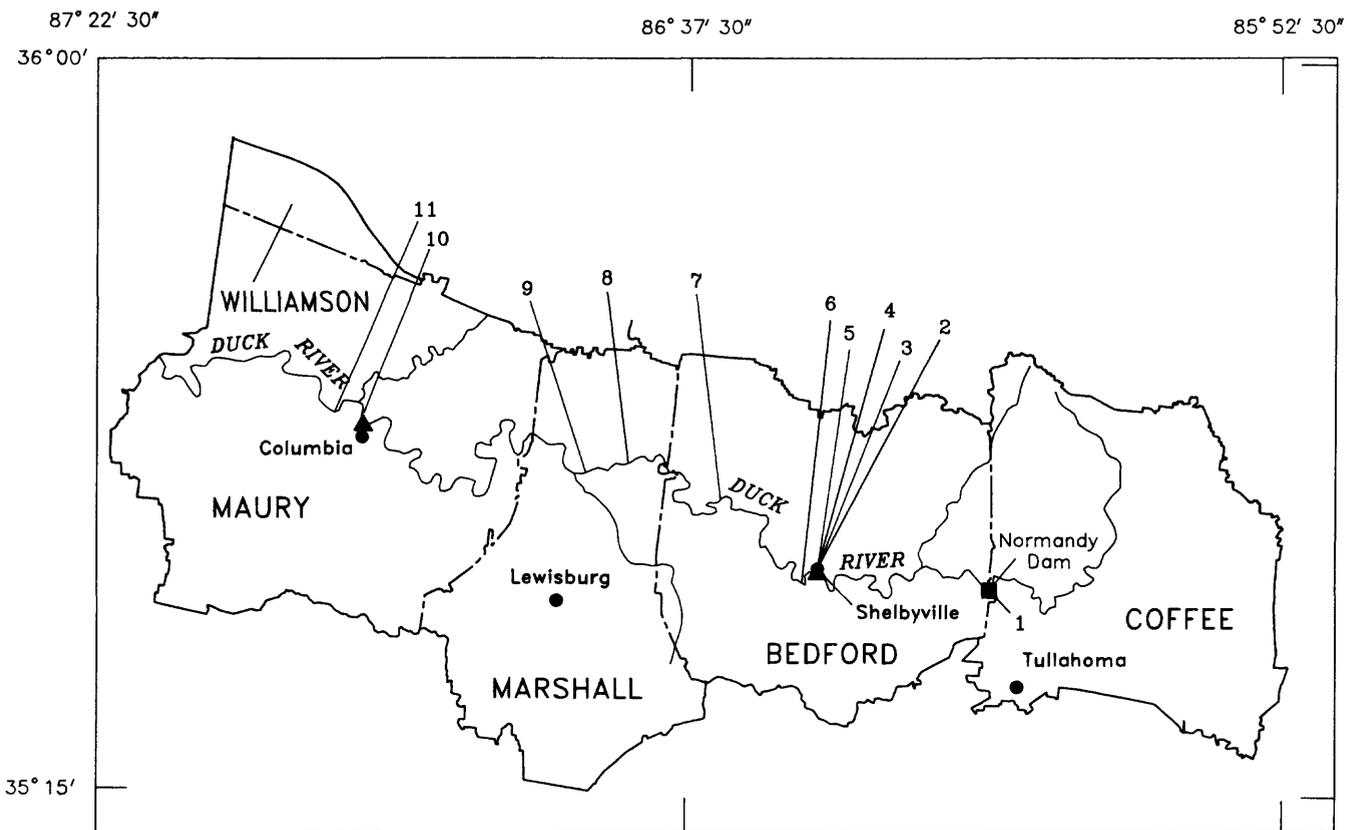
The effect of current and future municipal water withdrawals on streamflow in the upper Duck River was estimated at 11 locations from Normandy Dam to Columbia (fig. 7, table 18). A water budget for withdrawals and inflow discharges was calculated for two operational flow scenarios. The first scenario was for a summer minimum discharge of 155 ft³/s (100.2 Mgal/d); the second for a winter minimum discharge of 120 ft³/s (77.6 Mgal/d). The operational flows are measured at the USGS gage at Shelbyville. Projections show that simulated water demands and flows at key sites would be as follows:

- For an operational flow of 155 ft³/s (100.18 Mgal/d) at Shelbyville, flow at Columbia would be 134 ft³/s (87.6 Mgal/d) in 1995; 130 ft³/s (85.0 Mgal/d) in 2000; and 119 ft³/s (77.8 Mgal/d) for year 2015.
- For an operational flow of 120 ft³/s (77.56 Mgal/d) at Shelbyville, flow at Columbia would be 99.0 ft³/s (65.0 Mgal/d) in 1995; 95.0 ft³/s (62.4 Mgal/d) in 2000; and 83.7 ft³/s (55.2 Mgal/d) in 2015.

SUMMARY

The upper Duck River basin includes an area of about 1,700 square miles in Coffee, Bedford, Marshall, Maury Counties, and part of southern Williamson County in Middle Tennessee. Duck River, which is the principal source of municipal water supplies in the basin, has been regulated since 1976 at Normandy Reservoir. The reservoir, located in the headwaters of the basin near Tullahoma, is used for flood control, water-quality enhancements, low-flow augmentation, water supply, and recreation.

Water use in the basin increased 16 percent from 1980 to 1990 (18.0 Mgal/d to 20.9 Mgal/d). Socio-economic data for the area suggest that water demands will continue to increase in response to residential, industrial, and commercial development. Officials from the Upper Duck River Development Authority and the Tennessee State Planning Office are concerned about the capacity of the river to meet future water demands. In an attempt to address this concern, an investigation was conducted by the USGS from 1989 to 1991 to determine water use and availability in the basin and potential future water demands. The study also included an overview of the potential for developing the ground-water resources in the area.



EXPLANATION

- STUDY-AREA BOUNDARY
- - - - - WATER-SERVICE-AREA BOUNDARY--Each county water-service area is consistent with that county's political boundary, except for the Maury County water-service area that also includes part of southern Williamson County
- ▲ CONTINUOUS STREAMFLOW-GAGING STATION
- 1 SITE NUMBER

Figure 7. Water withdrawal and inflow discharge sites along the Duck River.

Table 18. Effect of water withdrawals and inflow discharges at various locations along the upper Duck River

[ft³/s, cubic feet second; Mgal/d, million gallons per day; 1 cubic foot per second = 0.646317 Mgal/d; -, withdrawal; +, discharge; --, no transaction. Site is a geographic reference point; site location: 1, Normandy Dam; 2, Shelbyville Water System (intake); 3, Shelbyville Water System (discharge); 4, U.S. Geological Survey gage; 5, Shelbyville Sewer Department; 6, industry; 7, Bedford County Utility District; 8, Chapel Hill Sewer System; 9, Lewisburg Water System; 10, U.S. Geological Survey gage; 11, Columbia Water Department]

Site number (see fig. 7)	River mile	1989		1995		2000		2015	
		Water use (Mgal/d)	Flow (Mgal/d)						
Summer operational flow, 155 ft³/s (100.18 Mgal/d), at river mile 221.4									
1	248.6	--	103.40	--	103.37	--	104.18	--	106.21
2	222.0	-3.22	100.18	-3.19	100.18	-4.00	100.18	-6.03	100.18
3	221.9	+ .06	100.24	+ .06	100.24	+ .06	100.24	+ .06	100.24
4	221.4	--	100.24	--	100.24	--	100.24	--	100.24
5	221.3	+1.79	102.03	+1.79	102.03	+1.79	102.03	+1.79	102.03
6	220.2	+ .80	102.83	+ .80	102.83	+ .80	102.83	+ .80	102.83
7	202.4	- .68	102.15	- .68	102.15	- .68	102.15	- .68	102.15
8	185.5	+ .20	102.35	+ .20	102.35	+ .20	102.35	+ .20	102.35
9	181.0	-2.71	99.64	-3.11	99.24	-3.82	98.53	-5.52	96.83
10	136.9	--	99.64	--	99.24	--	98.53	--	96.83
11	133.7	-8.48	91.16	-11.60	87.64	-13.48	85.05	-19.04	77.79
Winter operational flow, 120 ft³/s (77.56 Mgal/d), river mile 221.4									
1	248.6	--	80.78	--	80.75	--	81.56	--	83.59
2	222.0	-3.22	77.56	-3.19	77.56	-4.00	77.56	-6.03	77.56
3	221.9	+ .06	77.62	+ .60	77.62	+ .60	77.62	+ .06	77.62
4	221.4	--	77.62	--	77.62	--	77.62	--	77.62
5	221.3	+1.79	79.41	+ 1.79	79.41	+1.79	79.41	+1.79	79.41
6	220.2	+ .80	80.21	+ .80	80.21	+ .80	80.21	+ .80	80.21
7	202.4	- .68	79.53	- .68	79.53	- .68	79.53	- .68	79.53
8	185.5	+ .20	79.73	+ .20	79.73	+ .20	79.73	+ .20	79.73
9	181	-2.71	77.02	-3.11	76.62	-3.82	75.91	-5.52	74.21
10	136.9	--	77.02	--	76.62	--	75.91	--	74.21
11	133.7	-8.48	68.54	-11.60	65.02	-13.48	62.43	-19.04	55.17

The Duck River supplied an average of 18.9 Mgal/d in 1989 to utilities within four WSA's. The WSA's provide water for domestic, commercial, and industrial uses to Tullahoma, Manchester, Lewisburg, Shelbyville, Columbia, and several smaller communities in the basin. The number of customer connections increased about 13 percent from 1980 to 1990. During 1989, 93 percent (18.9 Mgal/d) of the total municipal withdrawals were from the Duck River;

the balance (about 7 percent or 1.5 Mgal/d) was supplied from springs and wells. Normandy Reservoir was the source of about 20 percent (3.83 Mgal/d) of the surface water supplied. Residential uses were about 41 percent (8.36 Mgal/d) of the total; commercial about 10 percent (2.02 Mgal/d); and industrial about 28 percent (5.64 Mgal/d). Other uses, including losses, were about 22 percent (4.40 Mgal/d). Water use varies seasonally. During a drought year, summer

water usage in the Maury WSA increased 21 percent over that of winter.

Low flows in the Duck River are augmented by releases from Normandy Reservoir. Winter low flows at Shelbyville are currently (1992) maintained at 77.6 Mgal/d; summer low flows at 100 Mgal/d. Discharges from the reservoir have been augmented since 1976 to maintain minimum flows, provide additional supplies, and enhance water quality. The 3Q20 discharge value changed from 34.8 Mgal/d to 46.1 Mgal/d at Shelbyville since regulation. At Columbia, the 3Q20 changed from 9.8 Mgal/d to 61.7 Mgal/d.

The potential for developing ground-water resources as an important component of the water supply is uncertain because data are insufficient to make a thorough assessment. The geology of the area is complex, with lack of homogeneity among the rocks underlying the area. Limestones of Mississippian and Ordovician age are the principal rocks, with residuum deposits in some areas. Yields to wells in the area vary significantly, ranging from <1 to as high as 860 gal/min. The most productive wells are located in Coffee County, in limestone rocks within the Highland Rim physiographic region. Analysis of well data indicates that 75 percent of these wells yield less than 30 gallons per minute. Two seepage investigations in subbasins to the Duck River indicate that local areas have potential for increased development of ground-water supplies, but additional testing and drilling would be required.

Projected future water demands in the basin were estimated with the IWR-MAIN System. The system uses a series of socioeconomic water-use algorithms to provide projections of future water demands. The model was calibrated to conditions as of 1989 and used to estimate water demands for the years 1995, 2000, and 2015.

Results from the water-use model projections indicate that water demands for the year 1995 would increase to 24.3 Mgal/d (19 percent); 2000, to 28.3 Mgal/d (39 percent); and 2015, to 39.0 Mgal/d (91 percent). For year 2015, residential water demand could increase by 122 percent; industrial water

demand, by 93 percent; and commercial water demand, by 82 percent. The Maury WSA would have the largest increases in industrial and commercial water demands; the Bedford WSA, the largest increases in residential water demand.

Increases in withdrawals from the Duck River throughout the basin would reduce minimum flows at key sites along the river. The reductions would increase through the year 2015. For an operational flow of 155 ft³/s (100.2 Mgal/d) at Shelbyville, flow at Columbia at year 2015 would be 119 ft³/s (76.8 Mgal/d). A further reduction to about 83.7 ft³/s (54.1 Mgal/d) would occur at Columbia for a lower operational flow at Shelbyville of about 120 ft³/s (77.6 Mgal/d).

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GLOSSARY

Significant terms defined according to their meaning in this report are listed below:

Bill difference--the difference in the customer's actual total bill and what would be charged if all units of water were sold at the marginal price (U.S. Army Corps of Engineers, 1988).

Coefficient--statistically derived measure of a property or characteristic of water use used as a factor in the computation of water demand.

Constant--y-intercept in the demand models related to gallons per housing unit per day (U.S. Army Corps of Engineers, 1988).

Constant dollars--current dollar figures reflect actual prices or costs prevailing during the specified year(s). Constant dollar figures are estimates representing an effort to remove the effects of price changes from statistical series reported in dollar terms. Constant dollar series are derived by dividing current dollar estimates by the appropriate price index for the appropriate period of time. The result is presumably a series that would exist if prices were the same throughout time (Vickers, 1989).

Housing density--number of housing units per acre (U.S. Army Corps of Engineers, 1988).

Marginal price--price paid for water at the margin (U.S. Army Corps of Engineers, 1988).

Median income--type of average which divides the distribution into two equal parts; one-half of the households fall below the median income and one-half of the households exceed the median income (U.S. Department of Commerce, 1982).

Multiple-coefficient demand models--includes the price of water to the user, as well as related economic factors such as income, among the explanatory variables. Demand models are usually constructed according to econometric methods, where the structure of the model and the list of potential explanatory variables reflect assumptions regarding causality rather than simply arising from observed correlation (U.S. Army Corps of Engineers, 1988).

Municipal water--public-supply water delivered to residential, commercial, and industrial users. The amount of water also includes public/unaccounted water.

Per capita income--average annual rate of income per person.

Per capita water use--average daily rate of use of water per person.

Price elasticity--a dimensionless measure of the relation between a percent change in water use and a percent change in price when other factors affecting water demand remain unchanged. The same concept may be applied to express the responsiveness of water use to changes in other variables (Boland and others, 1984).

Public/unaccounted sector--free-service water and distribution losses which include leakage, pipe flushing, and apparent losses caused by cumulative meter misregistration.

Single-coefficient (or multiple-coefficient) requirement models--estimate water use as a product of projected service area population and a projected value of per capita use. It can be expressed as a function of one or more explanatory variables. The models do not include the price of water, or other economic factors, as an explanatory variable. The models imply that water use is an absolute requirement, unaffected by economic choice (U.S. Army Corps of Engineers, 1988).

Standard Industrial Classification (SIC)--the statistical classification standard underlying all establishment-based Federal economic statistics classified by industry. The SIC is used to promote the comparability of establishment data describing various facets of the U.S. economy. The classification covers the entire field of economic activities and defines industries in accordance with the structure and composition of the economy (Office of Management and Budget, 1987).

Water demand--relation between water use and price, when all other factors are held constant. Demand is a negative functional relation; increased price results in decreased water use (Boland and others, 1984).

Water use--measured or estimated offshore withdrawals of water and return flows.

APPENDIXES

APPENDIX A. CALCULATION OF BILL DIFFERENCE EXPRESSED IN 1980 CONSTANT DOLLARS

[> , greater than; bill difference, the difference in the consumer's actual total bill and what would be charged if all units of water were sold at the margin (marginal price)]

Rate structure		
Use, in gallons	Cost of water service, in dollars per 1,000 gallons	Cost of waste service, in dollars per 1,000 gallons
0-50,000	0.50	1.30
50-250,000	.38	1.30
>250,000	.35	1.30
Service charge	2.50	3.50
Annual price per 1,000 gallons.	1.80	
Marginal price per 1,000 gallons.	1.65	

Water use		
Billing period	Gallons per day per housing unit	Gallons per month per housing unit
1 month	168	5,040

Bill difference calculation		
Bill difference	Cost of water service, in dollars	Cost of waste service, in dollars
Service charge	2.50	3.50
Average monthly cost per housing unit.	2.52	6.55
Bill	5.02	10.05
Total water and sewer bill	15.07	
Less price paid at the margin	8.32	
Equals annual bill difference	6.75	
Equals annual bill difference (in 1980 dollars).	4.25	

APPENDIX B. POPULATION PROJECTIONS AND NUMBER OF OCCUPIED HOUSING UNITS

[WSA, Water-service area; a, U.S. Census Bureau; b, University of Tennessee; c, $y = e^{ky}$; y, population; e, base of the natural log; k, growth constant; t, time interval in years; p, projected housing units = population divided by average persons per household]

Year	Average persons per household	Year	Population	Housing units
Bedford WSA				
1980	2.81a	1980	27,976a	9,943
1990	2.53a	1985	28,700b	10,992
		1989	30,157b	11,940
		1990	30,411a	12,041
		1995	31,705c	12,553p
		2000	33,056c	13,088p
		2015	37,462c	14,833p
Coffee WSA				
1980	2.81a	1980	38,311a	13,649
1990	2.44a	1985	40,600b	15,084
		1989	40,130b	16,433
		1990	40,339a	16,519
		1995	41,391c	16,950p
		2000	42,472c	17,392p
		2015	45,886c	18,791p
Marshall WSA				
1980	2.76a	1980	19,742a	7,144
1990	2.48a	1985	20,600b	7,923
		1989	21,029b	8,495
		1990	21,539a	8,701
		1995	22,498c	9,088p
		2000	23,499c	9,493p
		2015	26,778c	10,817p
Maury WSA				
1980	2.44a	1980	51,095a	20,902
1990	2.48a	1985	52,900b	22,286
		1989	54,426b	21,934
		1990	54,812a	22,090
		1995	56,767c	22,878p
		2000	58,794c	23,695p
		2015	65,321c	26,325p

APPENDIX C.--REGRESSION ANALYSIS FOR EMPLOYMENT PROJECTIONS

[WSA, water service area; m, model input; a, adjusted estimate; Stdev. Coef., standard deviation of the coefficient, that is, the estimated coefficient has an approximately normal distribution and it is the measure of variability of sample of the coefficient; variability in the sample; R-square, measure of the total variability in the dependent variable]

Water-service area				
YEAR	Bedford	Coffee	Marshall	Maury
1980	9,780	16,580	7,360	17,320
1981	9,180	16,960	7,430	17,100
1982	7,637	15,505	7,692	15,396
1983	7,788	15,170	7,365	15,150
1984	8,687	16,463	8,879	16,509
1985	9,034	16,947	8,127	16,645
1986	9,233	17,772	7,760	17,827
1987	10,094	18,243	8,423	18,157
1988	10,942	18,510	8,972	18,865
1989	11,115	18,947	9,450	22,457
1990	11,380	18,320	10,250	23,630
1995m	12,333	20,229	11,006	24,527a
2000m	13,733	21,734	12,386	27,742a
2015m	17,933	26,249	16,526	37,387a

Regression analysis					
WSA	Constant	Stdev. Coef.	Coefficient	Stdev. Coef.	R-square percent
Bedford	7,853	589	280	86.7	53.6
Coffee	15,413	506	301	74.6	64.4
Marshall	6,590	369	276	54.4	74.1
Maury	14,503	982	605	145	66.0