

**HYDROGEOLOGY AND ANALYSIS OF GROUND-WATER  
WITHDRAWAL IN THE MENDENHALL-D'LO AREA,  
SIMPSON COUNTY, MISSISSIPPI**

**By Eric W. Strom and William T. Oakley**

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## CONVERSION FACTORS AND VERTICAL DATUM

| <u>Multiply</u>            | <u>By</u> | <u>To obtain</u>       |
|----------------------------|-----------|------------------------|
| foot                       | 0.3048    | meter                  |
| foot per day               | 0.3048    | meter per day          |
| foot per year              | 0.3048    | meter per year         |
| foot per mile              | 0.1894    | meter per kilometer    |
| inch                       | 25.4      | millimeter             |
| inch per year              | 25.4      | millimeter per year    |
| mile                       | 1.609     | kilometer              |
| million gallons per day    | 0.04381   | cubic meter per second |
| cubic foot per second      | 0.02832   | cubic meter per second |
| million cubic feet per day | 0.3278    | cubic meter per second |
| square mile                | 2.590     | square kilometer       |
| foot squared per day       | 0.0929    | meter squared per day  |

**Temperature** in degrees Fahrenheit ( $^{\circ}\text{F}$ ) can be converted to degrees Celsius ( $^{\circ}\text{C}$ ) as follows:  $^{\circ}\text{C} = (^{\circ}\text{F}-32)/1.8$ .

**Sea level:** In this report “sea level” refers to the National Geodetic Vertical Datum of 1929 --a geodetic datum derived from a general adjustment of the first-order level nets of both the United States and Canada, formerly called Sea Level Datum of 1929.

The standard unit for transmissivity is cubic foot per day per square foot times foot of aquifer thickness. In this report, the mathematically reduced form, foot squared per day, is used for convenience.

# **HYDROGEOLOGY AND ANALYSIS OF GROUND-WATER WITHDRAWAL IN THE MENDENHALL-D'LO AREA, SIMPSON COUNTY, MISSISSIPPI**

By Eric W. Strom and William T. Oakley

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## **ABSTRACT**

The cities of Mendenhall and D'Lo, located in Simpson County, Mississippi, rely on ground water for their public supply and industrial needs. Most of the ground water comes from an aquifer of Miocene age. A study began in 1991 to describe the hydrogeology, analyze effects of ground-water withdrawal by making a drawdown map, and estimate the effects increased ground-water withdrawal might have on water levels in the Miocene age aquifer in the Mendenhall-D'Lo area.

The study area covers about 30 square miles in Simpson County, south-central Mississippi. Geologic units that crop out range from Tertiary to Quaternary in age. The sediments include alluvial and fluvial gravel, sand, and silt; deltaic sand, silt and clay; and prodeltaic and marginal marine clays. The geologic units, from oldest to youngest, are the Catahoula and Hattiesburg Formations of Miocene age; the Citronelle Formation of Pliocene or Pleistocene age; terrace deposits probably of Pleistocene age; and alluvium of Holocene age.

The significant withdrawals of ground water in the study area are from 10 wells screened in the lower sand of the Catahoula Formation. About 0.53 million gallons of water per day is currently (1994) withdrawn from these 10 wells. Analysis of the effect of withdrawals from the 10 wells was made using the Theis nonequilibrium equation and applying the principle of superposition. The study area was discretized into an equally spaced grid and drawdown was calculated at the center of each grid cell. Analysis of 1994 conditions was based on the pumpage history and aquifer properties determined for each well. The drawdown surface resulting from the analysis indicates three general cones of depression. One cone is in the northwestern D'Lo area, one in the south-central Mendenhall area, and one about 1<sup>1</sup>/<sub>2</sub> miles east of Mendenhall. Calculated drawdown ranges from 21 to 47 feet.

Drawdown-surface maps were made for 10 years and 20 years beyond 1994 using a constant pumpage. The map made for 10 years beyond 1994 indicates an average total increase in drawdown of about 5.3 feet. The map made for 20 years beyond 1994 indicates an average total increase in drawdown of about 7.3 feet. Because drawdown and pumpage have a linear relation in the Theis nonequilibrium equation, the projection scenarios may be used for extrapolation or interpolation of drawdown for other pumping rates.

## **INTRODUCTION**

The cities of Mendenhall and D'Lo, located in Simpson County, Mississippi, rely on ground water for their public supply and industrial needs. Most of the ground water comes from an aquifer of Miocene age. Regionally, water levels in the Miocene aquifers in Simpson County are declining at the rate of about 1 foot per year (Newcome and others, 1972). Continued population growth and the development of new industries may increase the rate of water-level decline. In 1991, the U.S. Geological Survey, in cooperation with the Pearl River Basin Development District and the Mississippi Department of Environmental Quality, Office of Land and Water Resources, began an investigation for the purpose of describing the hydrogeology, analyzing effects of ground-water withdrawal by making a drawdown map, and projecting the possible effects of increased ground-water withdrawals on water levels in the Miocene aquifer within the Mendenhall-D'Lo area. This report presents the results of that study.

### **General Setting of the Study Area**

The study area covers about 30 square miles in Simpson County, south-central Mississippi (fig. 1). The area is located in the Southern Pine Hills of the Gulf Coastal Plain physiographic province (Fenneman, 1938). The land surface is hilly, ranging in altitude from about 260 to 520 feet above sea level. The Strong River, the major surface-water drainage, flows southwestward between Mendenhall and D'Lo and drains into the Pearl River about 15 miles southwest of the study area. The Strong River has an alluvial plain that is about 1-mile wide in the study area. The normal mean annual temperature at D'Lo is about 63 degrees Fahrenheit; normal annual precipitation is about 59 inches.

### **Previous Investigations**

Previous investigations that include all or part of the study area have been published by the U.S. Geological Survey, the Mississippi Geological Survey, and the Mississippi Department of Natural Resources. These investigations include those by Stephenson, Logan, and Waring (1928); Newcome and others (1972); May and Marble (1976); and Gilliland and Harrelson (1981).

## **HYDROGEOLOGY**

The hydrogeology of the study area is described here in terms of the geologic setting, the hydrogeologic units and their relation to each other, ground-water movement, and ground-water withdrawal. All of the formations and deposits described have potential water-bearing zones; however, a lower sand in the Catahoula Formation of Miocene age is the principal source of ground water in the study area.

### **Geologic Setting**

The geologic setting of the study area is described by Cushing and others (1964) as resulting from subsidence that may have begun during the late Paleozoic Era and continued through the Cretaceous Period. This subsidence formed the basins of the Gulf Coast geosyncline, and of the southward plunging syncline of the Mississippi embayment. However, most of the syncline of the Mississippi embayment was not formed by the end of the Paleozoic Era, but during the Jurassic Period of the Mesozoic Era when evidence of a sedimentary basin became observable. By the end of the Cretaceous Period the Mississippi embayment had attained the approximate size and shape of today. Since the Cretaceous Period, cyclic transgression and regression of the sea have subsequently deposited an assorted, but ordered array of sediments within the Mississippi

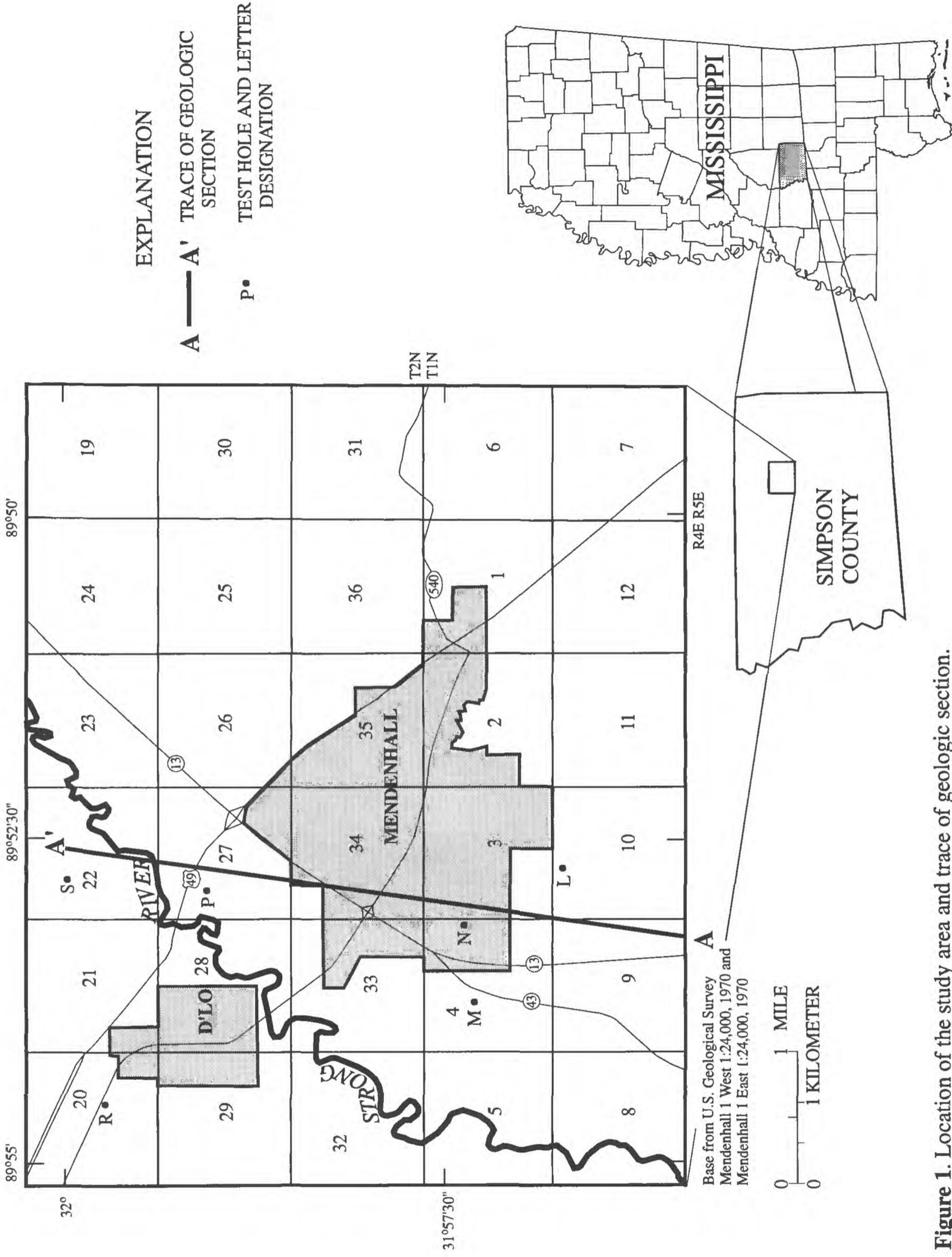


Figure 1. Location of the study area and trace of geologic section.

embayment. The nature of the sediments is directly related to past depositional environments, which in turn are related to fluctuations of sea level and the shifting of the shoreline. Older geologic units crop out in the northeast, and sequentially younger units are present at land surface to the west and south. The dip of the geologic units in the study area generally is toward the southwest.

### Description of the Hydrogeologic Units

Geologic units that crop out in the study area range from Tertiary to Quaternary age. The sediments include alluvial and fluvial gravel, sand, and silt; deltaic sand, silt and clay; and prodeltaic and marginal marine clays. The geologic units, from oldest to youngest, are the Catahoula and Hattiesburg Formations of Miocene age; the Citronelle Formation of Pliocene or Pleistocene age; terrace deposits probably of Pleistocene age; and alluvium of Holocene age (fig. 2). Descriptions of the geologic units are from May and Marble (1976) except where noted.

#### **Catahoula Formation**

The Catahoula Formation is fluvial to marginal-deltaic in depositional origin. The sediments probably represent a regressive, offlap sequence. The Catahoula Formation reaches a maximum thickness of about 450 feet in the study area and dips to the southwest at about 20 feet per mile. The formation mainly consists of deltaic silt and clay deposited in a low energy environment, and lenses of sand deposited in a high energy environment. Induration of the materials occurs primarily at surface exposures (Gilliland and Harrelson, 1981).

Many of the sand lenses in the Catahoula Formation are not continuous; however, an upper and lower sand interval exists within the formation. The upper sand consists of medium to coarse grained lenses, and ranges from 35 to 45 feet in thickness. The lower sand is fairly continuous in the study area, and ranges from 35 to 65 feet in thickness; greater thicknesses usually contain some clay or silt lenses. The lower sand primarily is a coarse to very coarse, poorly sorted quartz sand that is fluvial in nature. The upper and lower sands are both considered aquifers in the study area; however, most wells are screened in the lower sand. A geophysical log of the Catahoula Formation and overlying formations for well J33 is shown in figure 3.

The Catahoula Formation is unconformably underlain by the Vicksburg Group of Oligocene age. Clay from the Bucatunna Formation confines the Catahoula Formation from aquifers in the Vicksburg Group. The relation between the Catahoula Formation and other units is shown in figure 4.

#### **Hattiesburg Formation**

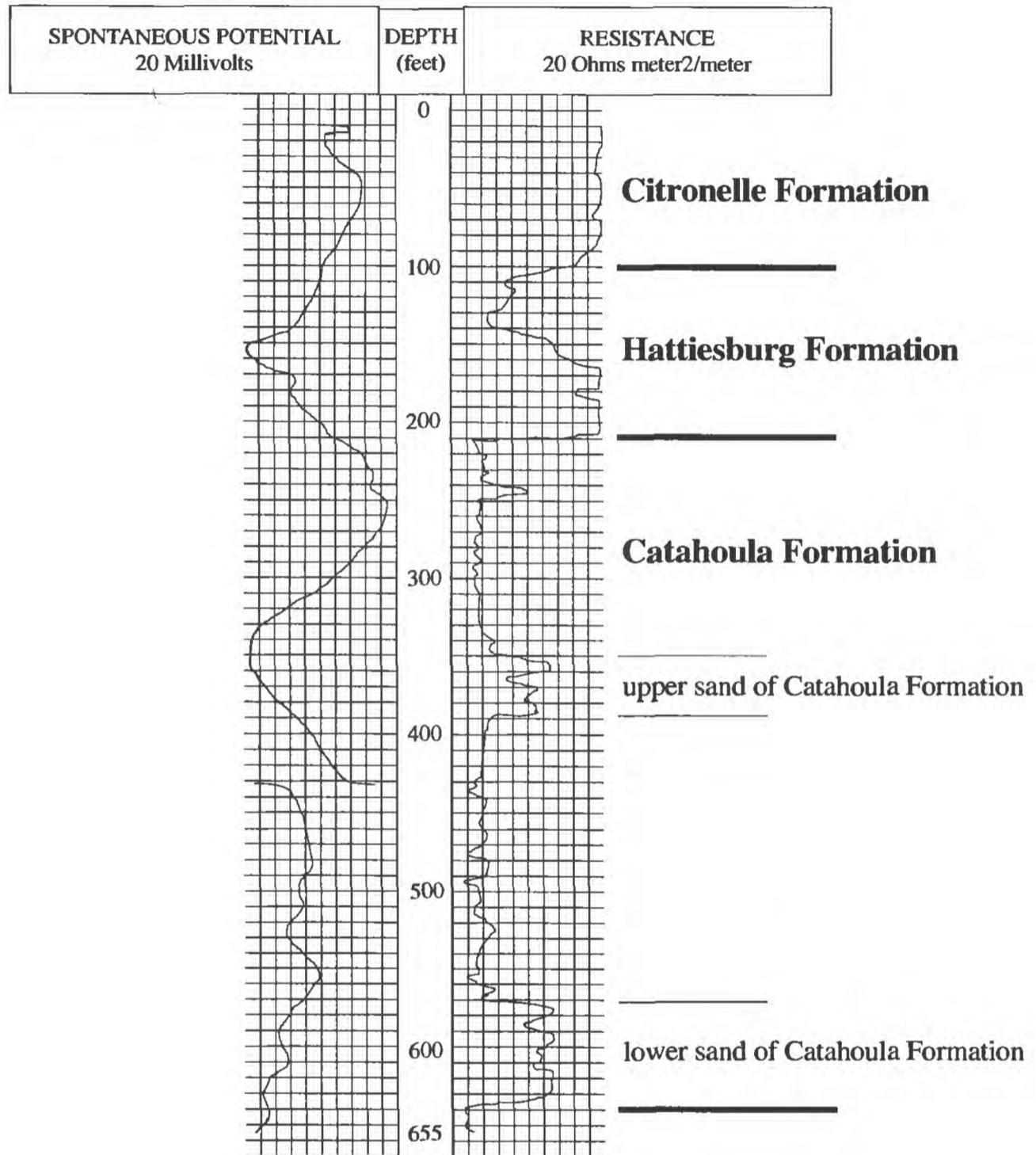
May and Marble (1976) describe a "Post-Catahoula Unit" that will be referred to as the Hattiesburg Formation in this report. Reasons for adopting this nomenclature are the same as those pointed out by Gilliland and Harrelson (1981): the "Post-Catahoula Unit" is in the same stratigraphic position as the Hattiesburg Formation and other publications, such as the geologic map of Mississippi (Bicker, 1969), show the unit as the Hattiesburg Formation.

The Hattiesburg Formation is fluvial to marginal-deltaic in depositional origin. The sediments probably represent a regressive sequence, similar to the underlying Catahoula Formation. The Hattiesburg Formation has a maximum thickness of about 130 feet in the study area and dips slightly west of south at about 20 feet per mile. The formation mainly consists of an upper argillaceous silt deposited in a low energy environment, and a lower medium to coarse grained,

| Erathem  | System     | Series                  | Group   | Geologic unit        | Hydrogeologic properties   |  |
|----------|------------|-------------------------|---------|----------------------|--|--|
| Cenozoic | Quaternary | Holocene                |         | Alluvial deposits    | Water-table aquifer of small areal extent yielding small amounts of water. |  |
|          |            | Pleistocene             |         | Terrace deposits     | Water-table aquifer of small areal extent yielding small amounts of water. |  |
|          |            | Pleistocene or Pliocene |         | Citronelle Formation | Aquifer limited in areal extent.   |  |
|          |            |                         |         |                      | Hattiesburg Formation  | Aquifer limited in areal extent.   |
|          |            |                         | Miocene |                      | Catahoula Formation  | Sands form important aquifer in the study area. Most public and industrial wells screened in the lower sand. |
|          |            |                         |         | Vicksburg            | Bucatunna Formation  | Not an aquifer.  |
|          |            |                         |         |                      | Byram Formation  | Not an aquifer.  |
|          |            |                         |         |                      | Glendon Limestone  | Generally not an aquifer.  |
|          |            |                         |         |                      | Mint Spring Formation  | Potentially an aquifer capable of yielding small amounts of water.   |

**Figure 2.** Geologic units and principal aquifers in the study area (modified from Gilliland and Harrelson, 1981).

### Electric Log 159, Simpson County, Mississippi



**Figure 3.** Geophysical log of the Catahoula, Hattiesburg, and Citronelle Formations for well J33 (modified from May and Marble, 1976).

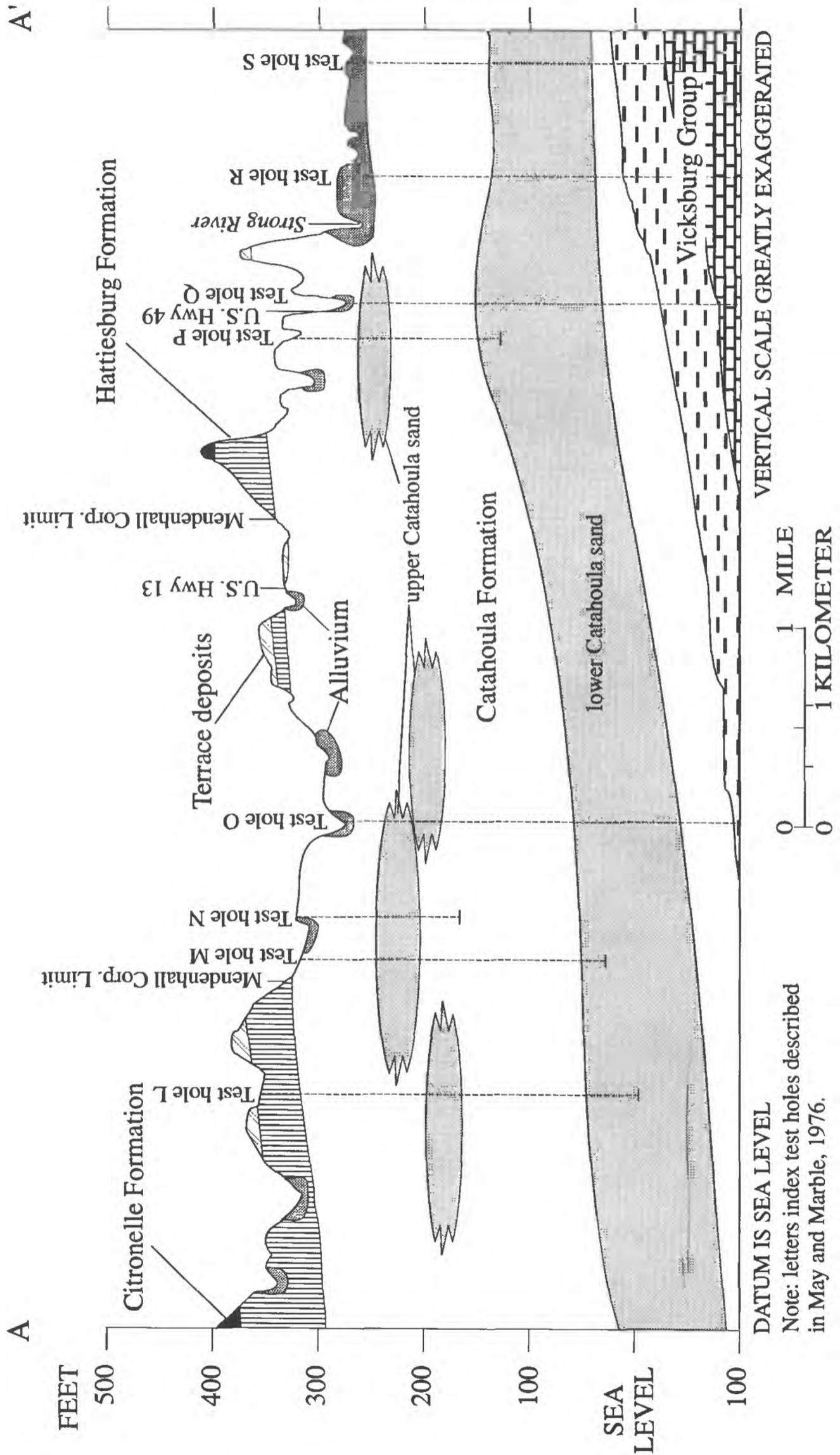


Figure 4. Geologic section showing relation of the geologic units in the study area (modified from May and Marble, 1976).

poorly sorted sand, deposited in a high energy environment. The Hattiesburg Formation is not heavily pumped in the study area.

### **Citronelle Formation**

The Citronelle Formation is fluvial in depositional origin. The formation probably formed a continuous blanket of sediment in the past (Boswell, 1979), but now occurs only at the higher altitudes in the study area. The Citronelle Formation has a maximum thickness of about 150 feet in the study area and dips slightly west of south at about 10 feet per mile. The formation mainly consists of coarse sand and gravel deposited in a high energy environment. The Citronelle Formation is not heavily pumped in the study area.

### **Terrace Deposits**

Terrace deposits occur on many of the hills at lower altitudes than the hills capped by the Citronelle Formation. Thickness of the deposits is highly variable and dips have not been determined. The deposits mainly consist of fine-to coarse-grained sand. The deposits may have resulted from sea level fluctuations during Pleistocene glaciation.

### **Alluvial Deposits**

Alluvial deposits are present in the river valleys of the study area. These deposits are the result of fluvial erosion of materials from higher elevations. Thickness of the deposits is variable, but may average about 20 feet in the Strong River alluvial plain. The deposits mainly consist of clay, sand, and gravel eroded from terrace deposits and from the Citronelle, Hattiesburg, and Catahoula Formations.

### **Ground-Water Movement**

Both confined and unconfined conditions occur in the aquifers of the study area. Aquifers in alluvial deposits, terrace deposits, the Citronelle Formation, and much of the Hattiesburg Formation are probably under unconfined conditions. Parts of the upper sand trend of the Catahoula Formation, particularly near the river valleys, may also be under unconfined conditions. The lower sand in the Catahoula Formation, however, is under confined conditions, separated from the overlying sand bed by silt and clay.

Ground-water movement in unconfined aquifers is influenced greatly by topography. Ground water generally moves from areas that are topographically high to areas that are topographically low. In the study area, most of the movement of unconfined ground water is toward the Strong River (Boswell and Arthur, 1988). Limited water-level data for the confined lower sand of the Catahoula Formation indicate flow in the lower sand similarly may be toward the Strong River and to pumping wells.

### **Ground-Water Withdrawal**

The significant withdrawals of ground water in the study area are from 10 wells screened in the lower sand of the Catahoula Formation. Information regarding pumpage and aquifer properties at each well is listed in table 1. Pumpage for the wells represents an average steady pumping rate, or the rate at which the wells would be pumped if the pumps ran continuously throughout the year. The average steady pumping rate was determined by estimating the total volume of water pumped from the well and dividing by the total time. In most cases the total

volume of water pumped was known for a group of associated wells rather than for each individual well, and pumpage was distributed equally. About 0.53 million gallons of water per day currently (1994) is withdrawn from these 10 wells. The total years the wells have been pumped are calculated through December 1994.

**Table 1.** Wells in the Mendenhall-D'Lo area and aquifer properties used to calculate drawdown

| Well | Latitude | Longitude | Years pumped | Pumpage (cubic feet per day) | Transmissivity (feet squared per day) | Hydraulic conductivity (feet per day) |
|------|----------|-----------|--------------|------------------------------|---------------------------------------|---------------------------------------|
| D38  | 315920   | 895417    | 26           | 3,475                        | 645                                   | 18                                    |
| D64  | 315908   | 895403    | 14           | 3,475                        | 912                                   | 17                                    |
| D51  | 315948   | 895435    | 21           | 9,290                        | 2,139                                 | 35.7                                  |
| D71  | 315948   | 895431    | 1            | 9,290                        | 828                                   | 28                                    |
| D67  | 315922   | 895420    | 4            | 4,812                        | 645                                   | 18                                    |
| E44  | 315752   | 894942    | 8            | 6,283                        | 825                                   | 19                                    |
| E29  | 315748   | 894944    | 25           | 6,283                        | <sup>1</sup> 1,200                    | <sup>1</sup> 35                       |
| J6   | 315734   | 895214    | 27           | 9,491                        | <sup>1</sup> 860                      | <sup>1</sup> 16                       |
| J34  | 315735   | 895236    | 22           | 9,491                        | 2,156                                 | 31.7                                  |
| J56  | 315731   | 895218    | 9            | 9,491                        | 2,340                                 | 32.5                                  |

<sup>1</sup> Slack and Darden, 1991.

## ANALYSIS OF GROUND-WATER WITHDRAWAL

Analysis of the effect of ground-water withdrawal from the 10 wells listed in table 1 was made using the Theis nonequilibrium equation and applying the principle of superposition. This method should be applicable because pumping tests for the wells indicated that the aquifer is confined and generally non-leaky in the study area. The Theis nonequilibrium equation computes drawdown in a confined aquifer at a desired distance from a pumping well. To perform the analysis, pumpage of the well, the length of time pumping occurred, and the transmissivity and storage coefficient of the aquifer must be known. The equation given by Theis (1935) is of the form:

$$h_o - h = s = \frac{Q}{4\pi T} \int_{\frac{r^2 S}{4Tt}}^{\infty} \frac{e^{-z}}{z} dz$$

where

- $h_o$  is the initial head (length) at some distance  $r$  (length) from the well,
- $h$  is the head (length) at some time  $t$  (time),
- $s$  is the resulting drawdown (length),
- $Q$  is the pumping rate (length cubed per time),
- $T$  is the transmissivity (length squared per time), and
- $S$  is the storage coefficient (dimensionless).

The Theis nonequilibrium equation is a solution to the radial form of the diffusion equation for a given set of initial and boundary conditions. Because the diffusion equation is linear, the principle of superposition allows for the determination of total drawdown caused by multiple wells being pumped simultaneously by summing the drawdown determined for each individual well.

The study area was discretized into an equally spaced grid. Each grid cell was 264 feet on a side for a total of 12,000 grid cells (fig. 5). This discretization provided the resolution necessary to delineate the surface of combined drawdown from multiple wells, and to place each well in the center of a grid cell. The Theis nonequilibrium equation was then applied at the center of each cell for each individual well using numerical approximations. Drawdown for each well in each cell was summed to produce a composite drawdown map. Drawdown was calculated using a well radius of 1 foot in cells that contained a well; however, the analysis does not account for drawdown near a well caused by other factors, such as turbulent flow or regional drawdown. A storage coefficient of 0.0002 was determined by an aquifer test only at well J6 (Slack and Darden, 1991). This value was used for each well in the analysis.

### Analysis of 1994 Conditions

Analysis of 1994 conditions was based on the pumpage records and aquifer properties determined for each well (table 1). The Theis nonequilibrium equation is based on the assumption that the aquifer is homogeneous and isotropic. For the analysis of each individual well this assumption was made. The Theis nonequilibrium equation was applied using the value of transmissivity determined from an aquifer test for each individual well for each cell in the grid. The total drawdown in each cell was then determined by summing the drawdown caused by each individual well. An alternative method would be to assume a single average value of transmissivity for all of the wells; however, error likely is reduced by using site specific values of transmissivity for each individual well because calculated drawdown is greatest at the center of a well and decreases exponentially with distance from the well.

The calculated drawdown surface (fig. 6) indicates three general cones of depression. One cone is in the northwestern D'Lo area, one cone in the south-central Mendenhall area, and one cone about 1½ miles east of Mendenhall. A generalized view of the drawdown surface (fig. 7) shows the coalescing nature of the drawdown cones caused by multiple wells.

Because the computed drawdown surface is a composite of drawdowns from wells that began pumping at different times, drawdown measured at the oldest wells should provide the best verification. The oldest wells are J6, D38, E29, J34, and D51 (table 1). Water-level measurements are no longer possible at well J6 due to reworking of the well. Water-level measurements made in fall 1994 indicate total drawdown of about 39 feet for well D38, 42 feet for well D51, and 39 feet for well J34 (table 2). The analysis indicated a total drawdown of about 42 feet at well D38,

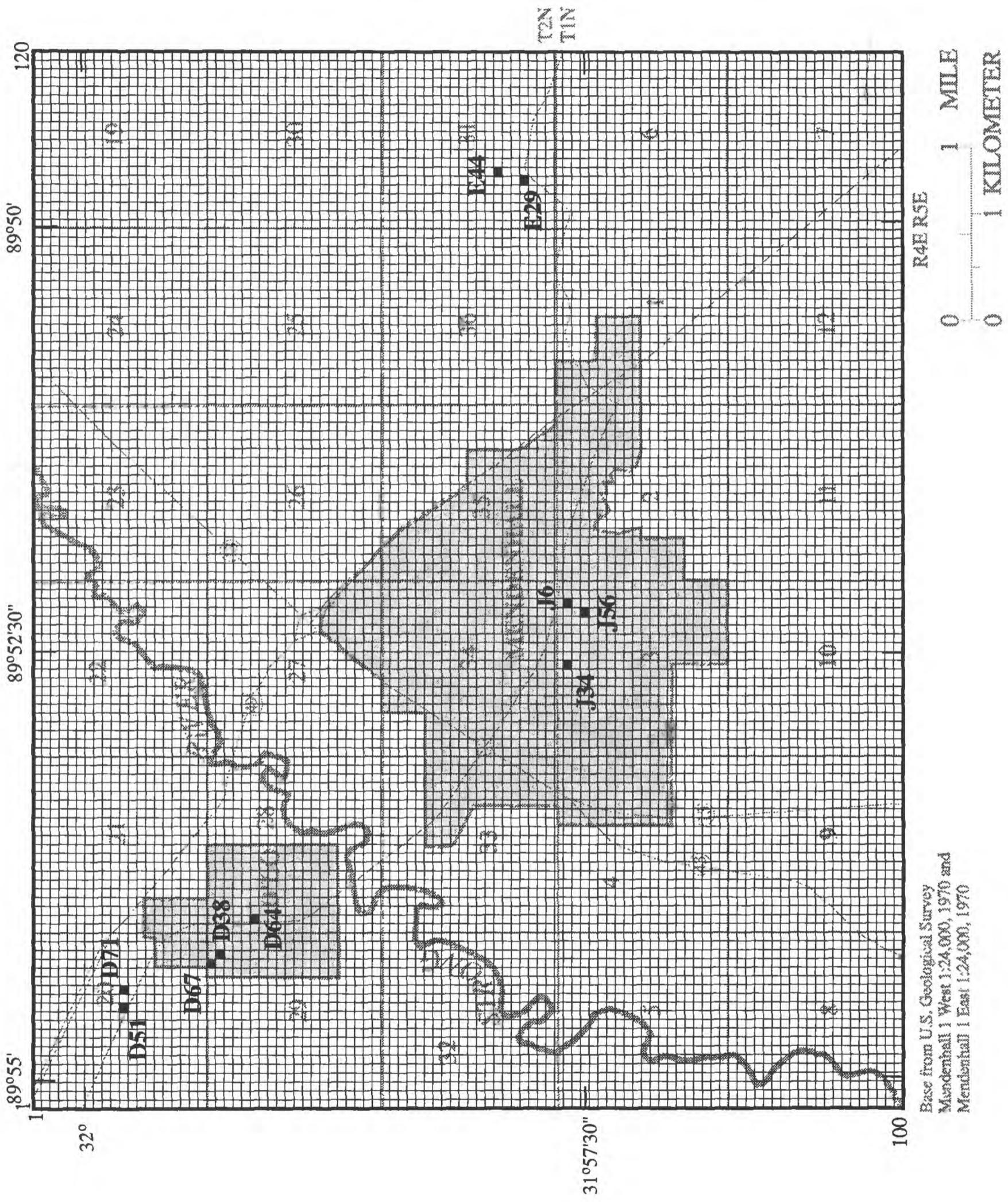


Figure 5. Grid cells and well locations used for drawdown calculations.



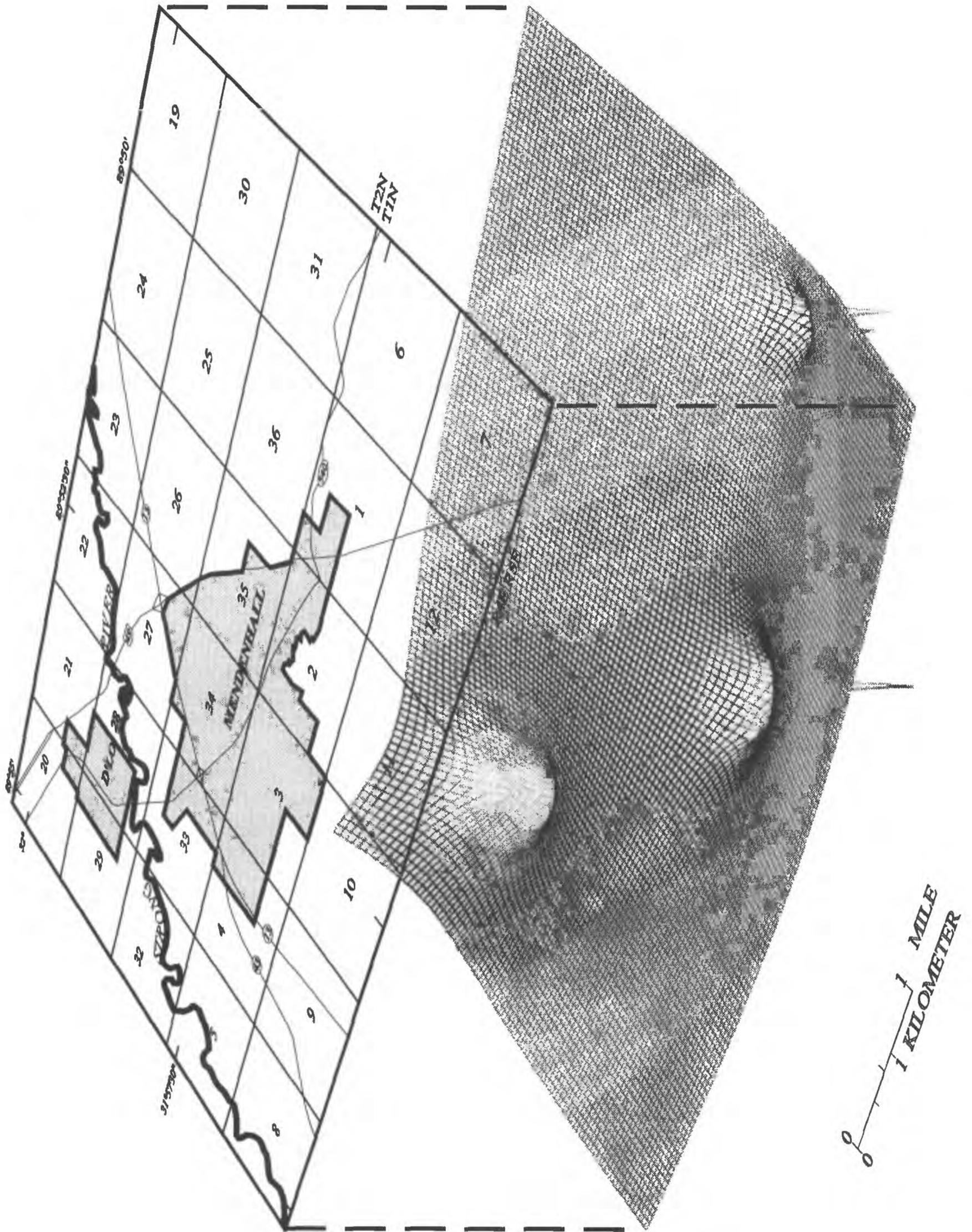


Figure 7. Generalized drawdown surface of the study area for 1994 conditions viewed from the southeast.

40 feet at well D51, and 37 feet at well J34, which compares closely to measured values of drawdown. However, well E29 had a measured drawdown of about 15 feet, and a calculated drawdown of about 35 feet. Review of the aquifer-test data confirmed the values used in the analysis, but it is possible that the transmissivity for well E29 is much higher because the well was pumped only 1 hour during the test and possible sources of recharge might not have been revealed. An upward inflection may have started in the drawdown curve at the very end of the test.

**Table 2.** Measured and calculated drawdown for selected wells

| Well | Measured drawdown (feet) | Calculated drawdown (feet) |
|------|--------------------------|----------------------------|
| D38  | 39                       | 42                         |
| D51  | 42                       | 40                         |
| J34  | 39                       | 37                         |
| E29  | 15                       | 35                         |

Only one value of storage coefficient (0.0002) was available, and this value was used at all wells; therefore, a sensitivity analysis to the change in the storage coefficient was made. Decreasing the storage coefficient from 0.0002 to 0.0001 resulted in an average increase in drawdown of about 3.4 feet. Increasing the storage coefficient from 0.0002 to 0.0003 resulted in an average decrease in drawdown of about 1.9 feet.

Because the Theis nonequilibrium equation is based on the assumption of a homogeneous aquifer and site specific transmissivities were used for each individual well in the analysis, sensitivity analysis was performed using a constant transmissivity of 1,306 feet squared per day (the arithmetic mean of the transmissivities of each individual well). The resulting calculated drawdown surface was similar in both shape and magnitude to the drawdown surface using site specific transmissivities. In general, the site specific transmissivity drawdown surface was about 1 foot closer to the observed values. A maximum difference between the two surfaces of about 9 feet occurred in the D'Lo area, with the average difference being about 0.9 foot.

### Projected Effects of Ground-Water Withdrawals

Calculated drawdown-surface maps were made for 10 years and 20 years beyond 1994 using the pumpage determined for 1994. The surface map for 10 years of pumpage beyond 1994 (fig. 8) indicates an average total increase in drawdown of about 5.3 feet. The surface map for 20 years of pumpage beyond 1994 (fig. 9) indicates an average total increase in drawdown of about 7.3 feet.

Because drawdown and pumpage have a linear relation in the Theis nonequilibrium equation, the projection maps may be used for extrapolation or interpolation of drawdown for other pumping rates. For example, the calculated drawdown for 1994 conditions in well J34 is about 37 feet (fig. 6). After 10 years of pumpage beyond 1994 the calculated drawdown is about 42 feet (fig. 8). Therefore, total additional drawdown is 5 feet. If pumpage were increased by 50 percent for all of the wells for the 10 year period, the total additional drawdown would be 1.5 times 5, or 7.5 feet, resulting in a total drawdown of about 44.5 feet.

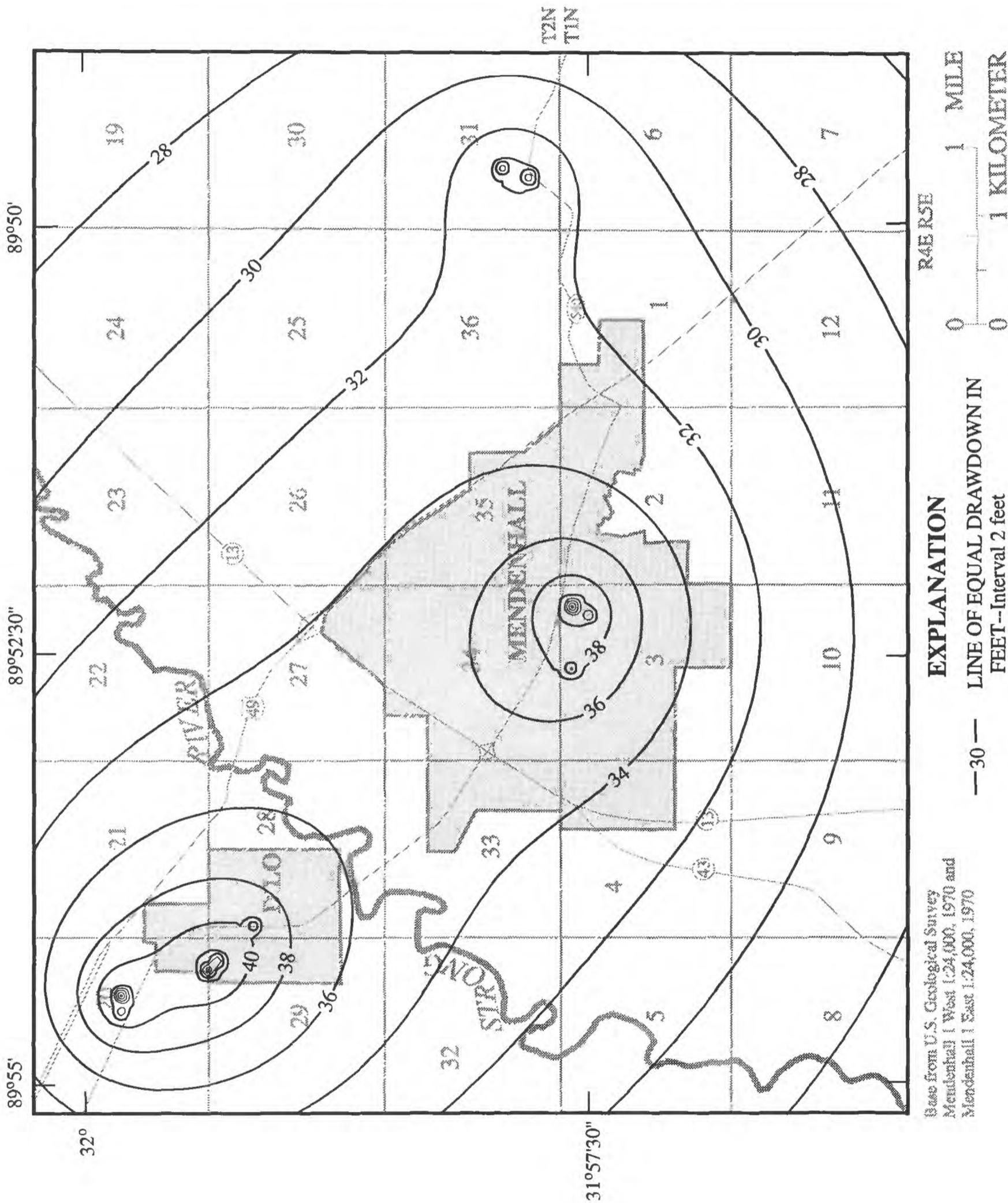


Figure 8. Calculated drawdown of water levels projected 10 years beyond 1994.

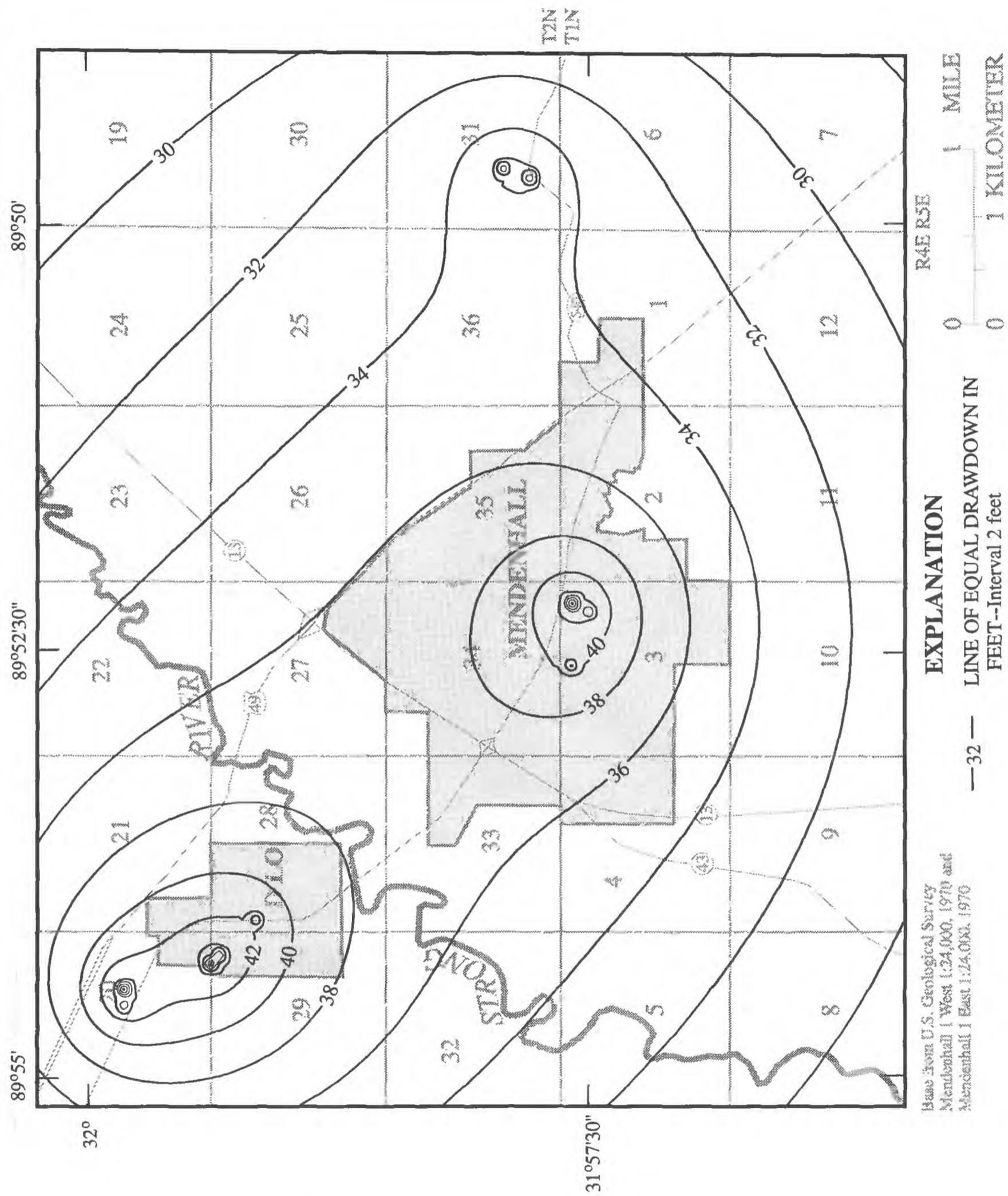


Figure 9. Calculated drawdown of water levels projected 20 years beyond 1994.

## Limitations of the Analysis

To perform the analysis, several assumptions were made: (1) the lower sand of the Catahoula Formation is confined and infinite in extent, (2) wells are of infinitesimal diameter and fully penetrate the aquifer, (3) water is released instantaneously with decline in head in the aquifer, (4) the aquifer is homogeneous and isotropic, and (5) no contributions of water are made from overlying or underlying aquifers. The first assumption is valid if the extent of the aquifer is large compared to the extent of the drawdown cones of the pumping wells. If impermeable geologic boundaries are reached by the drawdown cones, however, computed drawdown will be less than actual drawdown. Nearby sources of recharge would cause computed drawdown to be greater than actual drawdown. The second assumption ignores any storage in the well, which is a reasonable assumption for long-term analyses in which the total water pumped is large relative to wellbore storage. Wells in the study were screened to take full advantage of the sand interval. The third assumption is valid for the confined case, but would be invalid if water-table conditions were encountered. The fourth assumption was made for the analysis of each individual well; however, aquifer tests indicated variations in transmissivity. Because site-specific aquifer properties were used at each individual well, the drawdown calculated near each well probably is a better approximation than if a single uniform value of transmissivity had been applied to all wells. The fifth assumption assumes the clay and silt act as effective confining layers under pumping conditions as indicated by the pumping tests. The calculated drawdown will be greater than the actual drawdown if water is contributed from other sources.

Sparsity of historical water-level data and aquifer properties precluded the use of numerical techniques of analysis. However, the analytical technique used provides a guide for estimating drawdown in the past, as well as estimating drawdown trends that may occur in the future. The results from this investigation (feet of drawdown) do not necessarily represent precise drawdowns that will be observed in the field. The drawdown maps in figures 6 to 9 probably indicate too much drawdown in the vicinity of well E29 because transmissivity may be greater than assumed. The addition or deletion of wells, or significant changes in pumping rates would require additional analysis of the projected drawdown surfaces.

## **SUMMARY**

The cities of Mendenhall and D'Lo, in Simpson County, Mississippi, rely on ground water for their public supply and industrial needs. Most of the ground water comes from an aquifer of Miocene age. In 1991, the U.S. Geological Survey, in cooperation with the Pearl River Basin Development District and the Mississippi Department of Environmental Quality, Office of Land and Water Resources, began an investigation for the purpose of describing the hydrogeology, analyzing effects of ground-water withdrawal by making a drawdown map, and projecting the possible effects of increased ground-water withdrawals on water levels in the Miocene aquifer within the Mendenhall-D'Lo area.

The study area covers about 30 square miles in Simpson County, south-central Mississippi. Geologic units that crop out in the study area range from Tertiary to Quaternary in age. The sediments include alluvial and fluvial gravel, sand, and silt; deltaic sand, silt and clay; and prodeltaic and marginal marine clays. The geologic units, from oldest to youngest, are the Catahoula and Hattiesburg Formations of Miocene age; the Citronelle Formation of Pliocene or Pleistocene age; terrace deposits probably of Pleistocene age; and alluvium of Holocene age.

The significant withdrawals of ground water in the study area are from 10 wells screened in the lower sand of the Catahoula Formation. About 0.53 million gallons of water per day currently

(1994) is withdrawn from these 10 wells. Analysis of the effect of ground-water withdrawal was made using the Theis nonequilibrium equation and applying the principle of superposition. The study area was discretized into an equally spaced grid, and drawdown was calculated at the center of each grid cell for each individual well. Analysis of 1994 conditions was based on the pumpage records and aquifer properties determined for each well. The calculated drawdown surface indicates three general cones of depression. One cone is in the northwestern D'Lo area, one in the south-central Mendenhall area, and one about 1½ miles east of Mendenhall.

Calculated drawdown-surface maps were made for 10 years and 20 years beyond 1994 using the pumpage determined for 1994. The map for 10 years of pumpage beyond 1994 indicates an average total increase in drawdown of about 5.3 feet. The map for 20 years of pumpage beyond 1994 indicates an average total increase in drawdown of about 7.3 feet. Because drawdown and pumpage have a linear relation in the Theis nonequilibrium equation, the projection maps may be used for extrapolation or interpolation of drawdown for other pumping rates.

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