

Generalization of Stream-Temperature Data in Washington

GEOLOGICAL SURVEY WATER-SUPPLY PAPER 2029-B

*Prepared in cooperation with the
State of Washington
Department of Ecology*



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By M. R. COLLINGS

CONTRIBUTIONS TO THE HYDROLOGY OF THE UNITED STATES

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UNITED STATES DEPARTMENT OF THE INTERIOR

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CONTENTS

| | Page |
|---|------|
| Abstract | B1 |
| Introduction | 1 |
| Importance of stream temperatures | 1 |
| Previous temperature studies | 2 |
| Purpose and scope | 3 |
| Acknowledgments | 3 |
| Data used in this analysis | 3 |
| Stream-temperature data | 3 |
| Topographic data | 7 |
| Climatic data | 8 |
| Analytical procedures | 8 |
| Multiple-regression analysis | 8 |
| Residuals and subdivision of the State | 9 |
| Results | 15 |
| Evaluation of results | 17 |
| Effects of water impoundment on stream temperatures: examples ... | 19 |
| Example 1: effects of a hydroelectric power dam | 20 |
| Example 2: effects of a flood-control dam | 24 |
| Summary and conclusions | 26 |
| Selected references | 28 |

ILLUSTRATIONS

| | Page |
|---|------|
| FIGURE 1. Map of Washington showing sites of stream-temperature data collection by the U.S. Geological Survey | B5 |
| 2. Graph of a mean stream-temperature curve, for station 12-0830, Mineral Creek near Mineral | 6 |
| 3. Graph showing the 90-percent confidence interval about the maximum and minimum stream temperatures, for station 12-0825, Nisqually River near National | 6 |
| 4. Annual air-temperature amplitude isallotherms | 10 |
| 5. Mean annual air-temperature isotherms | 11 |
| 6. January and February mean monthly air temperature isotherms for western Washington | 12 |
| 7. August and October mean monthly air-temperature isotherms for western Washington | 13 |
| 8. Comparisons of standard errors of estimate of stream-temperature characteristics for eastern and western Washington | 19 |
| 9. Effects of water impoundment on stream temperatures, Cowlitz River | 22 |

TABLES

| TABLE | | Page |
|-------|--|------|
| | 1. Stream-temperature characteristics for probability curves at thermograph sites in western Washington ----- | B7 |
| | 2. Equations for determining stream-temperature characteristics ----- | 14 |
| | 3. Probable water-temperature characteristics below Mayfield Dam, Cowlitz River ----- | 21 |
| | 4. Evaluation of water-temperature changes below Mayfield Dam ----- | 24 |
| | 5. Probable water-temperature characteristics at Green River near Auburn, below Howard A. Hanson Dam .. | 24 |
| | 6. Evaluation of water-temperature changes below Howard A. Hanson Dam ----- | 25 |
| | 7. Stream-temperature characteristics, western Washington thermograph stations ----- | 32 |
| | 8. Stream-temperature characteristics, irregularly measured temperature stations ----- | 33 |
| | 9. Topographic and climatic drainage-basin characteristics, western Washington thermograph stations ----- | 39 |
| | 10. Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington ----- | 40 |

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THE UNITED STATES

GENERALIZATION OF STREAM-TEMPERATURE
DATA IN WASHINGTON

By M. R. COLLINGS

ABSTRACT

The effect of water temperature on the ecosystem of streams necessitates an analysis of various physical characteristics that influence stream temperatures. This study was conducted to determine (1) the effective relations that define site-to-site variation in stream temperatures, (2) equations and methods to estimate stream temperatures at sites where little or no data are now available, and (3) a procedure to evaluate the effect of water impoundment on natural stream temperatures.

Statistical multiple-regression analyses were used to develop equations for relations between stream temperatures and topographic and climatic characteristics of the drainage basins.

Multiple-regression techniques, generally, produced more accurate equations for estimating temperatures of streams in western Washington than for those in eastern Washington. A standard error of estimate was used to show how precisely stream temperatures may be defined by air-temperature and topographic drainage-basin characteristics. Of 24 original parameters tested, 15 were found effective to determine the equations of one or more of the 15 stream-temperature characteristics.

Effects of holding reservoirs on downstream water temperatures may be evaluated by the use of harmonic curves of probable maximum and minimum stream temperatures. By examples, it was shown that (1) below a hydroelectric-power dam winter-minimum river temperatures were raised and occur 9 days later than they would under natural conditions; and (2) below a flood-control dam, which also augments natural flows during low-flow periods, summer-minimum river temperatures were raised and occur 4 days earlier than they would under natural conditions.

INTRODUCTION

IMPORTANCE OF STREAM TEMPERATURES

In the field of water-quality control, temperature is recognized as one of the most important physical characteristics of water. Water temperatures have a direct influence on fish and other aquatic life, chemical and biological reactions, water treatment, toxicity of contaminants, taste, odor and general quality of domestic water, and industrial and agricultural water uses.

Increases in water temperatures affect fish by increasing their metabolic rates and oxygen requirements, increasing their sensitivity to toxic materials, and reducing swimming speeds (Burrows, 1963, p. 29-35).

The effects that temperatures have on concentrations of dissolved oxygen and rates of biochemical oxygen demand and on aquatic life are well documented (Wurtz and Renn, 1965) and must be considered in any program of water-quality control.

For domestic water treated before consumption, the flocculation and sedimentation rates increase with temperature increase, and the effects of chlorine on bacteria are greater at higher water temperatures (McKinney, 1962). Water is usually considered satisfactory for drinking when it is at or below 10°C (Celsius) or 50°F, but when it is at temperatures above 18.5°C (65°F), noticeable tastes and odors may occur. However, pathogens survive longer at lower temperatures (Everts, 1963).

Agriculturists prefer water above 15.5°C (60°F) for irrigation; return irrigation flows usually increase temperatures in receiving streams.

Thermal stratification in water impoundments on streams will modify the natural water temperature and oxygen concentration in the waters downstream from the impoundments. In turn, this affects the aquatic life, as does heat in water used for industrial- and powerplant-cooling purposes (Arnold, 1962).

More knowledge of the effect of water uses and watershed activity is needed to establish reasonable objectives and practical procedures to adjust and control water temperatures.

PREVIOUS TEMPERATURE STUDIES

Results of regional stream-temperature investigations generally have been presented in one of the following ways: (1) basic data listing maximum and minimum daily recorded temperatures, daily observed temperatures, and (or) irregularly measured temperatures (U.S. Geol. Survey, 1947-67; Aagaard, 1969; Moore, 1964); (2) basic-data listing, supplemented by results from regression relations among thermograph data, daily observations, and (or) irregular observations of stream temperatures and, in some cases, air temperatures—these regression relations were used to fill gaps in the record (Moore, 1969; Neece, 1968); and (3) by energy-budget equations and model-study results (Delay and others, 1964).

Moore (1969) published downstream water-temperature profiles of selected reaches of rivers in the Columbia River basin, to show the effects of dams and tributary inflow on the temperature of water in the main stem of the Columbia River.

Collings and Higgins (1972) presented stream-temperature data for the State of Washington in maps of the amplitudes, maximums, minimums, and medians of stream temperature.

PURPOSE AND SCOPE

Objectives of this study were to: (1) statistically describe and define the relation between natural stream temperatures and the topographic and climatic drainage-basin characteristics that are most effective in explaining the site-to-site variations in those stream temperatures, (2) present a procedure to estimate water temperatures at sites where little or no stream-temperature data are now available, and (3) use selected examples to show how the effect of water impoundment on natural stream temperatures may be evaluated.

Stream-temperature data were investigated for more than 400 sites; about 300 of these were west of the Cascade Range. Temperature data for the main stem of the Columbia River were omitted from this report because the river has unique or anomalous stream temperatures compared to those of most other rivers in the State and because a complex individual stream-temperature study of the Columbia River is beyond the scope of this report.

ACKNOWLEDGMENTS

This study was authorized by a cooperative agreement between the State of Washington Department of Ecology and the U.S. Geological Survey. The constructive criticism and suggestions by colleagues D. R. Dawdy and J. E. Cummins of the Geological Survey were of great benefit in preparation of the final report.

DATA USED IN THIS ANALYSIS

STREAM-TEMPERATURE DATA

Measurements of stream temperatures made at irregular intervals are the most basic method of collecting these data. Measurements are made at a site on a stream by the use of a thermometer or other type of noncontinuous recording device, usually at the time streamflow measurements are obtained by personnel of the Geological Survey. These temperature data are generally collected from 6 to 15 times a year.

More complete data can be obtained by hiring an observer to measure water temperatures at a preestablished frequency. Observation frequency may be hourly, bihourly, twice daily, daily, weekly, monthly, or at some other set time interval.

A third type of temperature-data collection is the placement of a maximum-minimum self-registering thermometer in the stream

and the recording of the highest and lowest stream temperatures for the period between visits to that site.

A thermograph is the most complete and adequate type of water-temperature data-collection device. This instrument continuously records the temperature of the water at a selected site. Maximum, minimum, and mean daily temperatures are readily obtained from a thermograph record.

The analyses of stream temperatures in Washington were made from data from the 307 temperature-collecting sites shown in figure 1. Data which were only seasonal, or had fewer than eight temporally well-spaced observations a year, were not used in the analysis. Unnatural data, such as data collected downstream from a point of thermal discharge or below an impoundment which may contain thermally stratified water, were not used for the regression analyses. Anomalous data, from naturally occurring thermal springs which would not be characteristic of most stream temperatures of a basin, were not included; nor were data not representative of that basin or stream because of the sampling location on the stream or in the channel cross section. However, some controlled and unnatural stream-temperature data were used in this report in other analyses and evaluations.

For a determination of the characteristics of the cyclic nature of Washington stream temperatures, to index the temperature differences from site to site, the basic data for each site were fitted to a harmonic curve (Collings, 1969) of the form

$$T = M + A[\sin(0.0172d + C)]$$

where T is stream temperature, in degrees Celsius ($^{\circ}\text{C}$), on day d , with d varied from 1 to 366 (January first as day 1); M is the mean annual water temperature, in $^{\circ}\text{C}$; A is the annual amplitude of the stream-temperature curve, in $^{\circ}\text{C}$; and C is the phase coefficient of the cycle, in radians (fig. 2).

At stream sites where thermograph records are available, the maximum, mean, and minimum daily stream temperatures for each year were fitted to the harmonic curve. In addition, when the record covered a sufficient period of years, monthly frequency distributions were determined. The monthly temperature frequency curves were assumed, for operational purposes, to be normally distributed. Harmonic curves, which define the 95-percent probability of occurrence of maximum and minimum temperatures (table 1)—equaling or less than maximum temperature and exceeding or equaling minimum temperature—were derived from data obtained from the frequency distributions (Collings, 1969, p. B178).

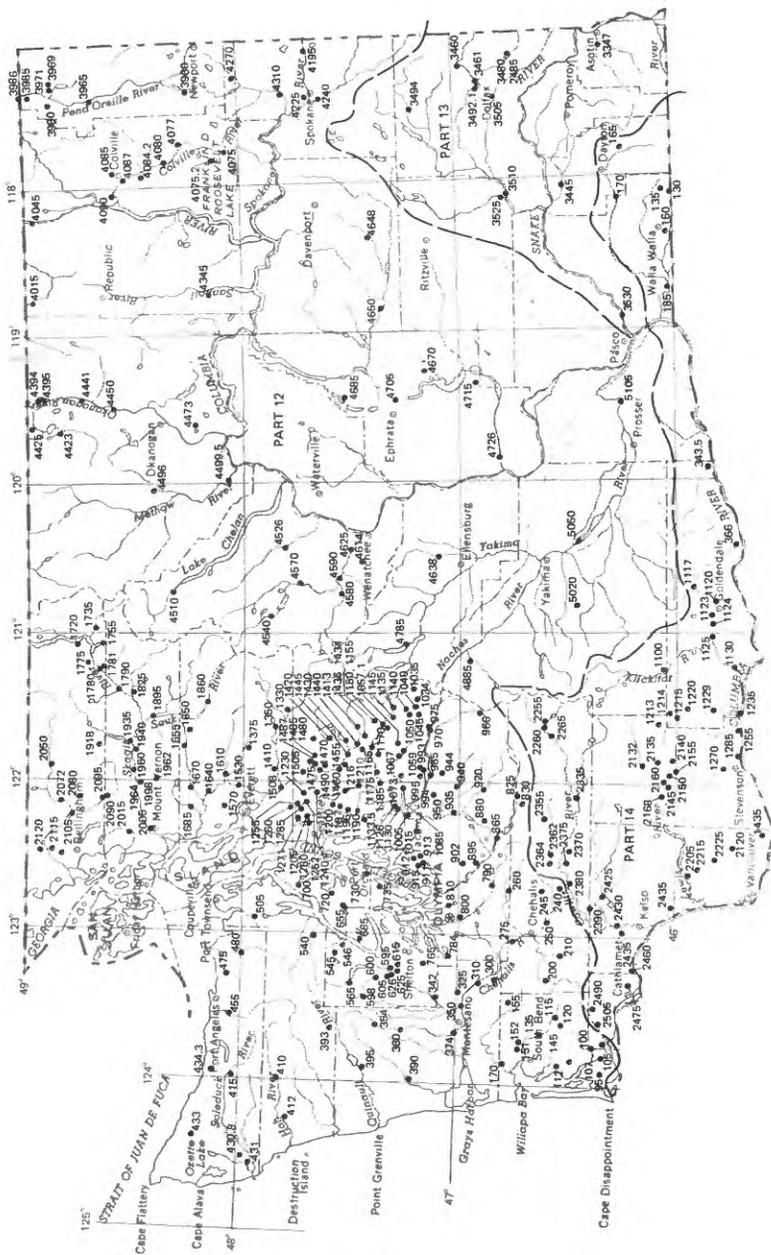


FIGURE 1.—Map of Washington showing sites of stream-temperature data collection by the U.S. Geological Survey for analysis in this study. Numbers are permanently assigned in U.S. Geological Survey numbering system and are shown in tables 7-10, with numbers prefixed by part number.

Figure 3 shows an example of fitted maximum, mean, and minimum probable stream temperatures. Also, from the frequency dis-

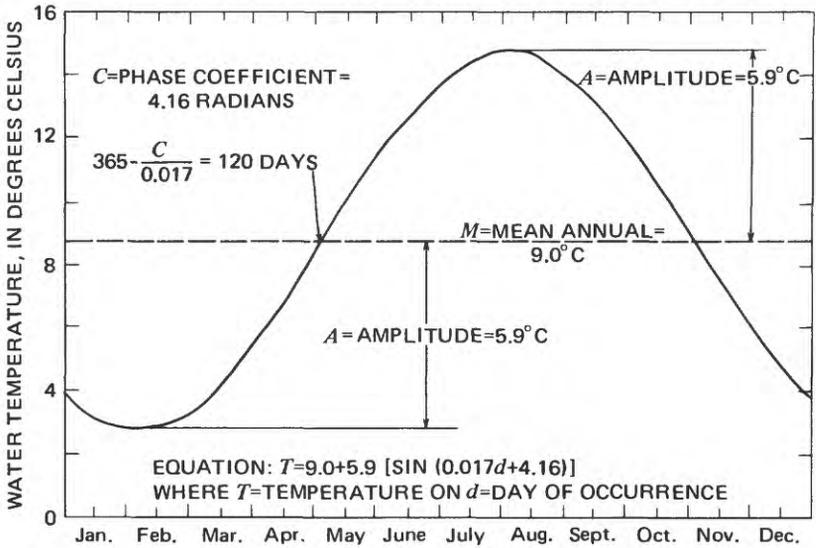


FIGURE 2.—Typical harmonic-fitted temperature graph showing mean stream-temperature curve, for station 12-0830, Mineral Creek near Mineral.

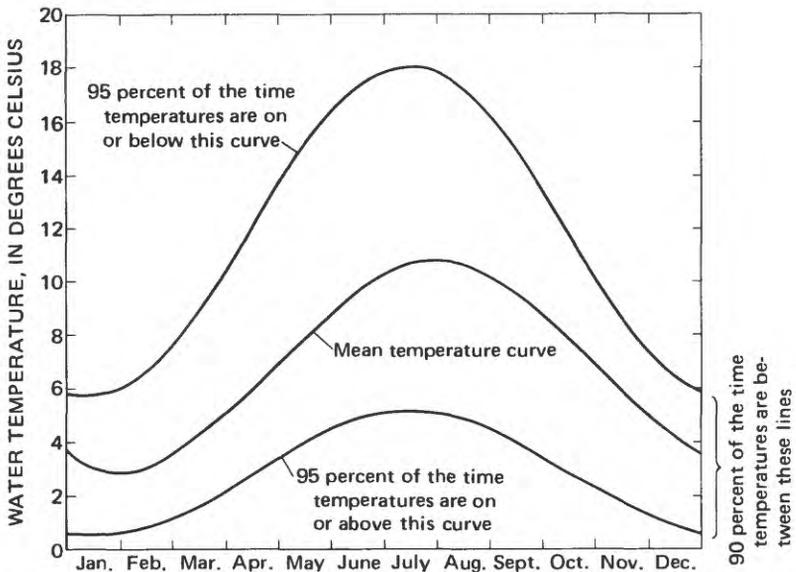


FIGURE 3.—Typical harmonic-fitted temperature graph, computed from thermograph records, showing the 90-percent confidence interval about the maximum and minimum stream temperatures, for station 12-0825, Nisqually River near National.

tributions, the standard deviations (*SD*) of the mean monthly temperatures for each month of the year were calculated for use in the regression analysis.

The values of *M*, *A*, and *C* for each stream-temperature data-collection site and of *M*, *A*, *C*, and *SD* for each long-term thermograph station, are listed in table 7.

TOPOGRAPHIC DATA

Topographic characteristics of the basins, as used in this analysis (tables 9 and 10, end of report), are defined by Benson (1962) and Collings (1971) except for definition of stream orientation which, measured in degrees from true north, is the average direction of flow of the main stem above the site of the water-temperature observation.

TABLE 1.—Stream-temperature characteristics for probability curves, from thermograph sites in western Washington

[Equation: $T=M+A [\sin (bx+C)]$. Characteristics of the mean temperature curves are listed in tables 7 and 8, along with the station name]

| Station number (fig. 1) | 95 percent probable maximum temperature (equal to or less than) | | | 95 percent probable minimum temperature (equal to or greater than) | | | Beginning of record (year) |
|--------------------------|---|-----------------------------|------------------|--|-----------------------------|------------------|----------------------------|
| | Amplitude (°C) | Phase coefficient (radians) | Mean annual (°C) | Amplitude (°C) | Phase coefficient (radians) | Mean annual (°C) | |
| 12-0115 ----- | 6.4 | 4.47 | 14.7 | 6.0 | 4.32 | 6.0 | 1952 |
| 0275 ----- | 9.2 | 4.37 | 16.3 | 7.0 | 4.28 | 7.5 | 56 |
| 0600 ----- | 6.4 | 4.39 | 12.2 | 4.0 | 4.08 | 4.5 | 56 |
| 0615 ----- | 5.6 | 4.45 | 12.7 | 3.0 | 4.05 | 5.5 | 57 |
| 0825 ----- | 6.2 | 4.46 | 11.8 | 2.3 | 4.43 | 2.8 | 53 |
| 0830 ----- | 8.4 | 4.28 | 13.2 | 5.0 | 4.23 | 5.0 | 52 |
| 1130 (see table 5) ----- | | | | | | | |
| 1175 ----- | 5.7 | 4.43 | 11.8 | 3.9 | 4.18 | 6.3 | 54 |
| 1350 ----- | 7.5 | 4.24 | 12.7 | 4.1 | 4.15 | 4.3 | 59 |
| 1640 ----- | 8.0 | 4.37 | 13.4 | 5.3 | 4.27 | 4.8 | 53 |
| 1655 ----- | 5.9 | 4.18 | 10.5 | 3.3 | 4.31 | 4.5 | 52 |
| 1685 ----- | 9.8 | 4.32 | 14.3 | 5.4 | 4.17 | 5.0 | 54 |
| 1790 ----- | 3.6 | 4.00 | 9.2 | 3.4 | 3.93 | 5.2 | 53 |
| 1825 ----- | 4.6 | 4.35 | 9.8 | 3.2 | 4.20 | 3.5 | 53 |
| 2005 ----- | 5.2 | 4.20 | 11.1 | 3.6 | 4.14 | 6.4 | 63 |
| 14-1100 ----- | 5.3 | 4.22 | 8.6 | 3.7 | 4.26 | 2.9 | 51 |
| 1130 ----- | 6.6 | 4.42 | 12.7 | 5.2 | 4.39 | 4.5 | 51 |
| 2205 ----- | 6.5 | 3.62 | 12.1 | 2.9 | 3.84 | 5.9 | 51 |
| 2225 ----- | 8.4 | 4.30 | 14.4 | 5.2 | 4.19 | 4.7 | 51 |
| 2235 ----- | 6.4 | 4.34 | 12.8 | 4.3 | 4.26 | 5.2 | 55 |
| 2325 ----- | 5.1 | 4.22 | 10.6 | 4.1 | 4.23 | 3.8 | 53 |
| 2335 (see table 3) ----- | | | | | | | |
| 2355 ----- | 8.6 | 4.29 | 13.3 | 4.4 | 4.11 | 3.7 | 52 |
| 2380 (see table 3) ----- | | | | | | | |
| 2425 ----- | 7.5 | 4.31 | 13.6 | 4.2 | 4.21 | 4.6 | 51 |
| 2430 (see table 3) ----- | | | | | | | |
| 2450 ----- | 9.6 | 4.40 | 16.3 | 6.2 | 4.37 | 5.3 | 51 |
| 2460 ----- | 6.2 | 4.37 | 13.8 | 3.9 | 4.27 | 4.5 | 52 |
| 2475 ----- | 8.1 | 4.37 | 15.2 | 5.4 | 4.29 | 5.4 | 52 |
| 2505 ----- | 6.4 | 4.39 | 14.2 | 4.6 | 4.06 | 5.6 | 52 |

CLIMATIC DATA

Normal air-temperature data from 79 climatic stations in Washington (U.S. Environmental Science Services Administration, 1967) were used to determine the cyclic characteristics of the normal air temperatures by means of fitting the data from each site to a harmonic curve. These characteristics of air temperatures (tables 9 and 10) were plotted on State maps, and lines were drawn of equal annual air-temperature amplitude (isallotherms; fig. 4), mean annual air temperature (isotherms; fig. 5), and the phase coefficient of the air temperature. The air-temperature amplitudes and mean annual air temperatures used in the regression analyses were obtained from these maps. The phase coefficient of air temperature was found to be not a significant factor for an estimate of stream temperatures, and therefore was omitted as a variable from tables 9 and 10.

The mean monthly air temperatures for western Washington only were plotted on State maps, and isotherms were drawn. Figures 6 and 7 show the mean monthly isotherms for January and February, and August and October, respectively. The mean monthly air temperatures at each stream-temperature thermograph station were determined from these mean monthly isotherm maps. January (T_1), February (T_2), August (T_8), and October (T_{10}) were the only months in which air temperatures improved the regression analysis of monthly standard deviations of stream temperatures, and therefore are the only months for which data are listed in table 8.

ANALYTICAL PROCEDURES MULTIPLE-REGRESSION ANALYSIS

A statistical multiple-regression analysis was used to develop separately, for each stream-temperature characteristic, the relation between that characteristic (dependent variable) and the topographic and climatic-basin characteristics (independent variables). With the multiple-regression techniques an equation is computed which defines relations between a dependent variable and the independent variables. Also provided is a measure of the usefulness of each independent variable to define the dependent variable and a measure of the accuracy of the resultant equation (standard error of estimate).

The standard error of estimate is a measure of how well an equation defines a dependent variable. The standard error encompasses about two-thirds of the dependent-variable site values used to determine the equation; doubling the standard error of estimate will encompass about 95 percent of the dependent-variable site values.

The usefulness of each independent variable is determined by the (1) intercorrelation coefficients—in this report if the intercorrelation coefficient between independent variables was greater than 0.5 (1.0 being perfect), one of the independent variables was omitted and the regression analysis recomputed; (2) statistical significance of the independent variable in relation to the dependent variable—all variables were tested at the 95-percent probability-of-effectiveness level; (3) variance-covariance coefficients, which allow computation of simple regressions and standard errors of estimate between any two independent variables or between a dependent and any one independent variable; and (4) amount by which the standard error of estimate was reduced when an independent variable was added to the regression equation.

Multiple-regression models are based on the linearity of the relation between the dependent variable and independent variables. In many hydrologic studies (Benson, 1962; Thomas and Benson, 1969; and Collings, 1971), findings showed that generally the variables were logarithmically linear. To satisfy the requisite of linearity, all data were transformed into logarithms (logs) and the calculations for the regression analysis were performed. In addition to the transformed model, analysis was performed on untransformed or natural data. The standard error of estimate, tests of significance, correlation coefficients, and variance-covariance relations were used as guides; thus, the multiple-regression analysis was performed several times with various combinations of transformed and untransformed variables until the most effective semilog regression equation was determined for each of the stream-temperature characteristics.

Standard deviations of monthly mean stream temperatures for long-term thermograph stations were also subjected to multiple-regression analysis (table 2). This allows the determination of the standard deviation of the mean monthly stream temperatures at any site on any stream in western Washington; thus, confidence-interval curves can be determined for the mean stream-temperature harmonic.

RESIDUALS AND SUBDIVISION OF THE STATE

After a determination was made of the most effective transformed and untransformed independent variables related to each stream-temperature characteristic, the regression analysis of all data in the State was performed and the residual for each site was calculated. A residual, in essence, is the difference between the value of the dependent variable computed from the regression equation and the original data value of that variable. (Where the logarithms of the data are used, the residual is the logarithm of the ratio of these values.)

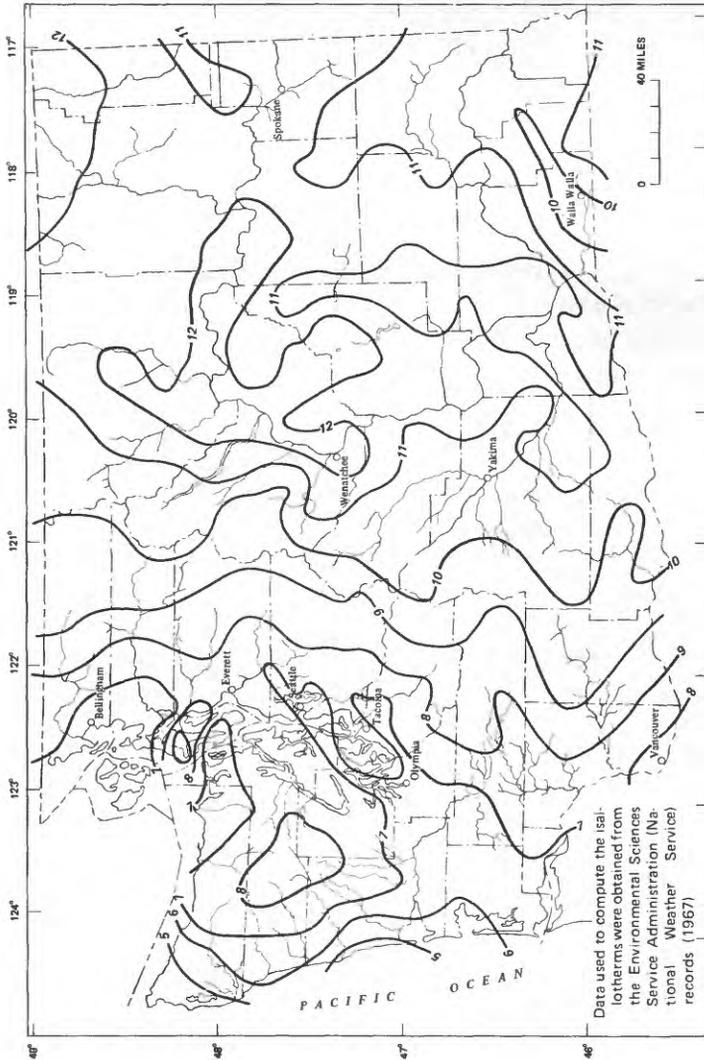


FIGURE 4.—Isallotherms showing annual air-temperature amplitude, in degrees Celsius.

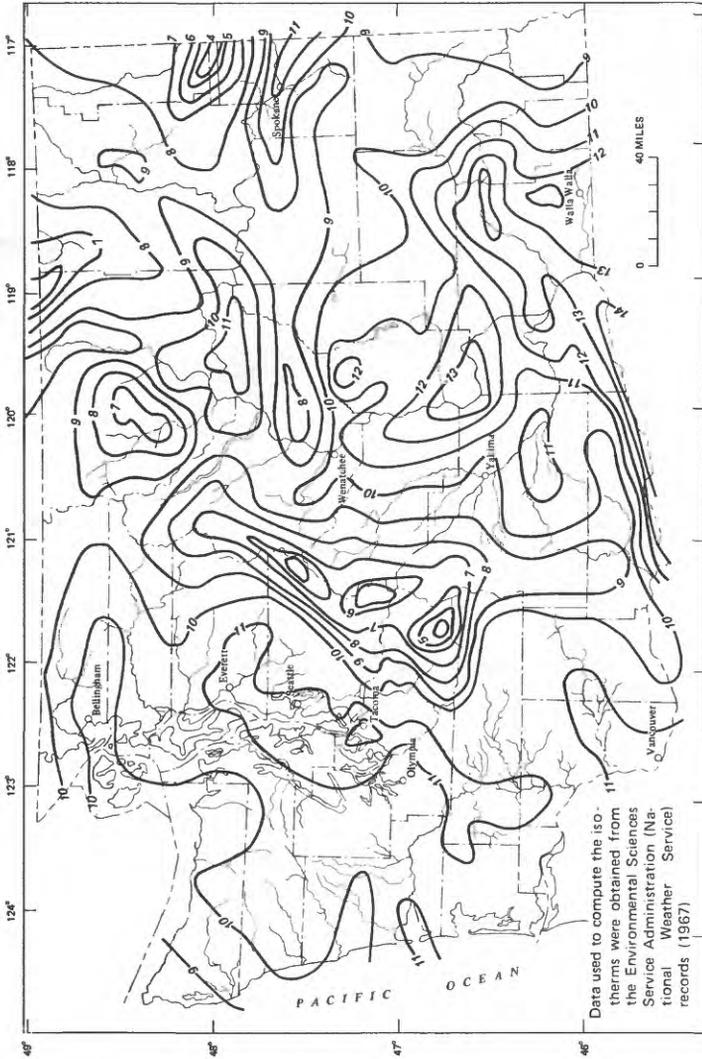


FIGURE 5.—Isotherms showing mean annual air temperature, in degrees Celsius.

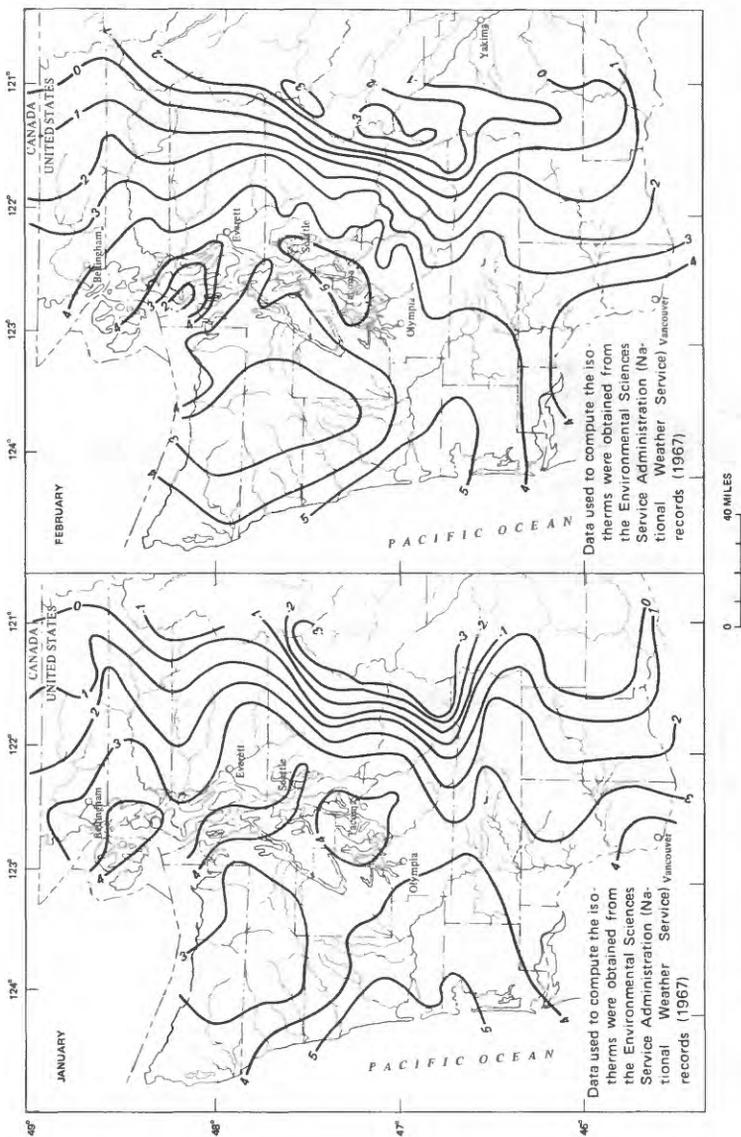


FIGURE 6.—Isotherms showing mean monthly air temperatures, in degrees Celsius, in January and February in western Washington.

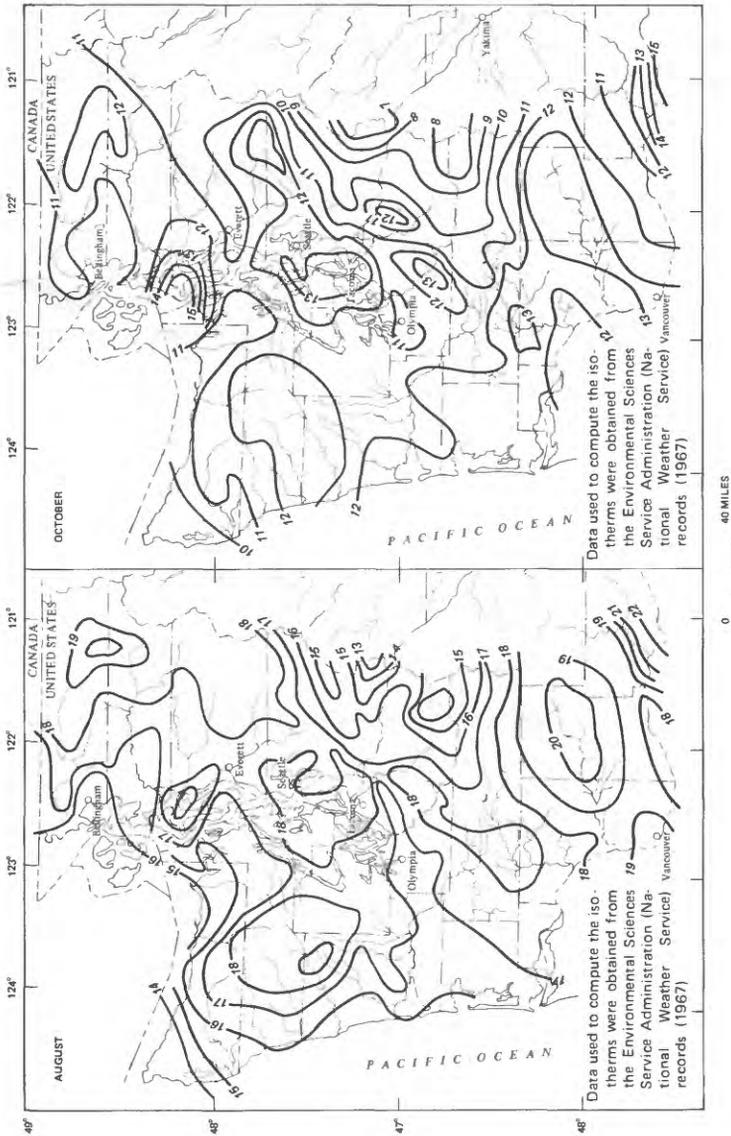


FIGURE 7.—Isotherms showing mean monthly air temperatures, in degrees Celsius, in August and October in western Washington.

The residuals from the statewide regression model, for each stream-temperature characteristic at each data site, were plotted on State maps to determine if they were truly random areally or whether trends or areas with similar high or low residuals exist. The plots (not included on the maps) indicated several groupings that possibly could be used to define subdivisions.

Generally, the areas where residuals indicated subdivisions were western, eastern, and southeastern Washington. However, the quantity of data for southeastern Washington was not large enough to determine a reliable regression model if that area were used as a subdivision. Therefore, the State was divided at the crest of the Cascade Range into eastern and western Washington, with southeastern Washington included as part of eastern Washington. Data for all the temperature sites in the State were divided on this basis, and multiple-regression analyses were performed separately for each part.

TABLE 2.—Equations for determining

| Stream-temperature characteristic Y | Regression | | | | | | |
|--|--------------------------|--|------------------------------|----------------------------------|------------------------------------|----------------------------|----------------------------------|
| | a Regression constant | φ Average direction of flow of stream (degrees) | L Length of river (miles) | E Mean altitude of basin (ft) | P Lake and pond areas (percent) | D Drainage area (sq mi) | Q Mean annual discharge (in.) |
| Western | | | | | | | |
| Amplitude ----- | 7.10 | ----- | ----- | -2.56 (-4) | ----- | ----- | ----- |
| Mean ----- | 9.36 | ----- | ----- | -1.12 (-3) | ----- | ² 1.08 | ----- |
| Phase coefficient ---- | 4.34 | ----- | ----- | ----- | ----- | ----- | -0.24 (-2) |
| <i>Standard Deviations:</i> | | | | | | | |
| January ----- | 1.12 | ----- | ----- | ----- | ----- | ----- | ----- |
| February ----- | 3.95 | -2.56 (-3) | ----- | ----- | ----- | -3.92 (-4) | ----- |
| March ----- | 1.56 | ----- | ----- | ----- | ----- | -1.33 (-4) | ----- |
| April ----- | 1.64 | ----- | ----- | ----- | ----- | ----- | ----- |
| May ----- | 2.22 | ----- | ----- | ----- | ----- | ----- | ----- |
| June ----- | 1.99 | ----- | ----- | ----- | ----- | ----- | ----- |
| July ----- | 1.78 | ----- | 0.40 | ----- | -0.32 | ----- | ----- |
| August ----- | 3.41 | ----- | ----- | ² -1.50 | ----- | ----- | 1.40 (-2) |
| September ----- | -1.26 | ² .514 | ----- | ----- | ----- | ----- | ² 1.53 |
| October ----- | 2.66 | ----- | 5.64 (-3) | ----- | ----- | -3.56 (-4) | ----- |
| November ----- | 2.33 | ----- | ----- | ² -1.37 | 5.95 (-2) | -2.90 (-4) | ----- |
| December ----- | 1.40 | ----- | 1.52 (-2) | ----- | ----- | -8.02 (-4) | ----- |
| Eastern | | | | | | | |
| Amplitude ----- | 17.33 | ----- | ----- | ----- | ----- | ----- | ² 3.46 |
| Mean ----- | 10.23 | ----- | ----- | 1.15 (-3) | ----- | ----- | -4.47 (-2) |
| Phase coefficient ---- | 4.53 | ----- | ----- | -6.27 (-5) | -6.33 (-2) | -8.24 (-6) | ----- |

¹ Number in parentheses is power of 10 by which value must be multiplied.

² Independent variable associated with this coefficient is a logarithm of the value.

For the regression constants and coefficients in table 2, the form of the equation is

$$Y = a + b_1x_1 + b_2x_2 + b_3x_3 + \dots + b_nx_n,$$

where Y is the stream-temperature characteristic, a is the regression constant, b_n is the regression coefficient, and x_n is the topographic or climatic characteristic (which may or may not be the log of the value). An example of the calculation of mean annual stream temperature (M) for station 12-0115 (fig. 1 and tables 9, 10) follows:

From table 2, the equation is

$$\text{Mean} = 9.36 - 1.12(10^{-3})(E) + 1.08(\log D) - 6.12(10^{-5})(S).$$

From table 6, the values of mean basin altitude (E), drainage area (D), and source altitude (S) are obtained and the equation becomes:

Mean =

$$9.36 - 1.12(10^{-3})(754) + 1.08(\log 41.4) - 6.12(10^{-5})(2400).$$

The values of E , D , and S could be determined (from topographic maps) for any site on any stream in western Washington and used in the equation.

The log 41.4 = 1.617 and the equation reduces to:

$$\text{Mean} = 10.1^\circ\text{C}.$$

For comparison, the mean annual temperature, determined from the observed data, for station 12-0115 is 10.2°C (table 7). Similarly, values for amplitude (A) and phase coefficient (C) may be determined from the equations in table 2. Mean annual discharge, the variable used to determine C at a site where no streamflow gaging station exists, may be determined by the methods reported in a study by Collings (1971, p. 14-15).

When these three temperature characteristics are calculated, a temperature hydrograph (similar to that in fig. 2) may be plotted from the equation,

$$T = M + A[\sin(bd + C)],$$

where

$$T = 10.1 + 5.2[\sin(0.0172d + 4.20)].$$

The highest mean water temperature of the year would be

$$M + A = 10.1 + 5.2 = 15.3^\circ\text{C}$$

and would occur on the

$$d = 365 + \frac{[(\pi/2) - C]}{b} = 365 + \frac{1.57 - 4.20}{0.0172} = 212\text{th day}$$

of the year, or July 31.

The lowest mean water temperature of the year would be

$$M - A = 10.1 - 5.2 = 4.9^\circ\text{C}$$

and would occur on the

$$d = \frac{(3/2)\pi - C}{0.0172} = 30\text{th day,}$$

or January 30.

Confidence intervals about the mean-stream-temperature harmonic curve can only be determined for stream-temperature sites in western Washington. Confidence intervals derived from a generalization of the standard deviation of monthly temperatures for eastern Washington would have poor reliability because of the small number of thermograph stations. The confidence intervals about a mean harmonic curve for a western Washington temperature site are determined as follows:

1. Compute the monthly *SD* values by using the regression constants and coefficients for the monthly *SD*'s (table 2) and determining the characteristics from maps.
2. Calculate the mean monthly temperatures (table 2).
3. Select the desired percentage interval from a table of cumulative standard normal distribution functions (Hald, 1952)—for example, the 95- and 5-percent probabilities give a 90-percent interval that is about ± 1.64 standard deviation's wide.
4. Compute the confidence interval about the mean monthly stream-temperature by multiplying the standard deviation interval (± 1.64) by each month's *SD* and adding and subtracting this value from the mean value for that month.

The values from step 4 may be plotted above and below the mean harmonic curve to form the confidence interval for that curve.

EVALUATION OF RESULTS

Statistical evaluations were the basis for including or omitting a topographic or climatic variable from the empirical relations defined by the regression analyses. The physical reasons for a variable or variables defining a stream-temperature characteristic can be postulated only from a train of deductive reasoning, which in some cases may be extremely tenuous. Thus, the regression equations do not define the causes of the areal variations in stream-temperature characteristics. Nevertheless, they do define the basin or climatic characteristic, or group of characteristics, which give a numerical evaluation of the stream-temperature characteristic at a site where previously no stream-temperature information was available.

Mean annual streamflow was found to be a significant independent variable in several of the regression relations (table 2).

However, because of high intracorrelation with other independent variables—especially drainage area—mean annual streamflow was omitted from most of the equations. In the equations (table 2) mean annual streamflow is defined in units of inches of water and is obtained by division of the total runoff by the drainage area. It was found to be a more effective variable in the equations in this form and had lower intracorrelation coefficients with other independent variables (0.4 or less in all cases). Mean annual streamflow at sites where no streamflow records are available may be determined by use of the method described by Collings (1971, p. 14–15).

The standard errors of estimate of the equations to determine the confidence intervals about the mean-stream-temperature curves are shown in table 2. However, after computation and application to the mean curve, one finds the confidence intervals are subject to somewhat greater errors. This is because they include (1) the standard error of estimate of the equations for monthly standard deviation (table 2), (2) the determination of mean monthly values from the harmonic curve, and (3) possible undefined variations resulting from the assumptions made when the curves for monthly frequency distribution are derived. Generally, the total error involved in computation of the confidence intervals for the mean-stream-temperature harmonic curve could be as great as the sum of the errors for each of the curves used in the determination.

Standard error of estimate is a measure of the accuracy of the multiple-regression equations (table 2). It shows how well a stream-temperature characteristic is defined by the topographic and (or) climatic characteristics. Figure 8 shows graphically how well each of the stream-temperature characteristics was defined at the mean value of that characteristic. The standard error of estimate for each of the defining relations is shown in table 2. The graph (fig. 8) shows that error, expressed as a percentage, is obtained by dividing the standard error of estimate by the mean value of the respective stream-temperature characteristic. Figure 8 shows only comparisons between the precision of definition of stream-temperature characteristics for each part of the State and is not a measure of the accuracy of the total range of the variables. For example, the percentage ratio of the stream-temperature characteristic may be larger for low values and smaller for higher values.

Undoubtedly stream-temperature studies in the future could improve the generalized equations defined in this report, because (1)

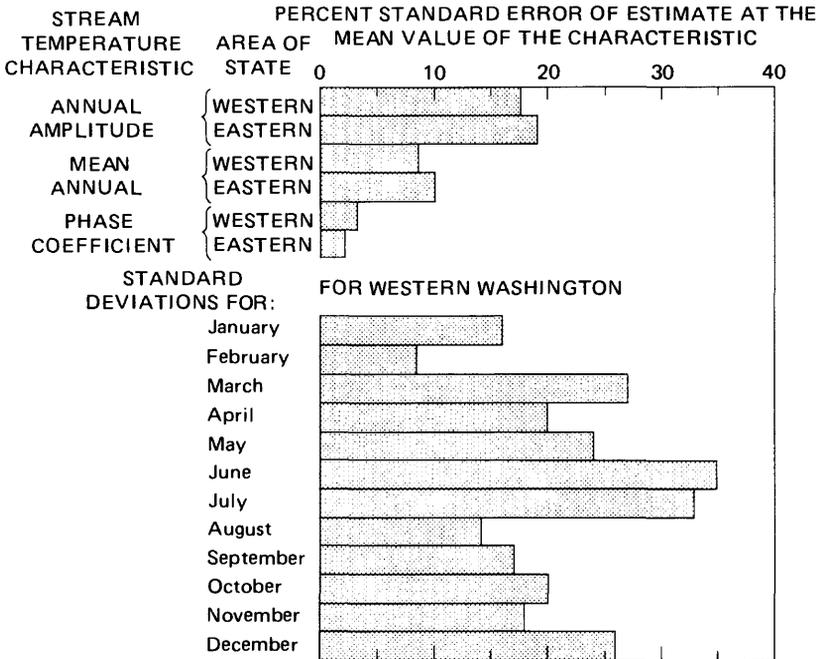


FIGURE 8.—Comparisons of standard errors of estimate, of the mean values only, of stream-temperature characteristics for eastern and western Washington.

more and longer records of stream temperatures, especially thermograph data, will be available for better areal and temporal definition, (2) new and updated topographic maps will be available to define and improve definition of the topographic basin characteristics, (3) more and longer climatic records will become available, and (4) other types of parameters and indices may possibly be defined as significant independent variables related to stream temperatures. Examples of additional parameters that might prove significant include stream-channel indices at the temperature observation site, wind velocity, cloud cover, subsurface inflow, chemical character and suspended sediment, basin geology, temperature of surrounding landmasses, and shading from vegetation or landmasses.

EFFECTS OF WATER IMPOUNDMENT ON STREAM TEMPERATURES: EXAMPLES

The effects of water impoundment on stream temperatures below an impoundment are not consistent and vary from stream to stream and dam to dam. An impoundment's effect on downstream water temperatures depends on many factors, including the size

and shape of the impoundment, elevation of the release water, holding time of the water, other physical characteristics and turbidity of the water, velocities of currents within the impounded water, altitude of the impoundment's surface, and volume of water released as compared to the natural discharge of the river.

The effects of holding reservoirs on downstream water temperatures can be evaluated by use of harmonic curves of the probable maximum and minimum temperatures. Following are examples of procedures used to evaluate the effects of impoundments on downstream water temperatures.

EXAMPLE 1: EFFECTS OF A HYDROELECTRIC POWER DAM

In this example two sites below Mayfield Dam, on the Cowlitz River, are evaluated to determine the effect of a hydroelectric power dam on stream temperatures. The dam, located at Cowlitz River mile 52.0, has been in operation since 1962. Thermograph records at sites 1.4 and 34.7 miles downstream from the dam were evaluated for the 1951-68 period. The upstream site is 14-2380, Cowlitz River below Mayfield Dam ("near Mayfield" before dam construction), and the lower station is 14-2430, Cowlitz River at Castle Rock. The periods evaluated at both stations were 1951-61 before dam construction, and 1962-68 after dam construction. A third site (14-2335, Cowlitz River near Kosmos), located 4.2 river miles upstream from Mayfield Dam and unaffected by the impoundment of water, was also evaluated for these periods before and after existence of the reservoir. The Cowlitz River near Kosmos was used as a "background" evaluation, to determine if a significant natural stream-temperature trend exists for the period investigated. The probable temperature curves for the Kosmos gage before and after impoundment (table 3) were not found to be significantly different. This finding lends validity to the assumption that any changes occurring in the river temperatures below the dam after dam construction and use would be caused by the effect of the dam and its impoundment.

At each of the thermograph sites, frequency distributions were computed for maximum, mean, and minimum stream temperatures. These distributions were used to determine the 95-percent probabilities of being equal to or less than the maximum temperatures and of equaling or exceeding the minimum temperatures, for both natural and impounded conditions. The probable stream temperatures were fitted by harmonic curves; the characteristics of the curves are listed in table 3. The sets of curves for each site define a 90-percent confidence interval for stream temperatures for each condition. (This means that 95 percent of the time maximum

TABLE 3.—Probable water-temperature characteristics below Mayfield Dam, Cowlitz River

| Water temperature | Before impoundment | | | | | After impoundment | | | | |
|--|--------------------|-----------------------|-----------------------------|------------------------------|---------------------|-------------------|-----------------------|-----------------------------|------------------------------|---------------------|
| | Probability | Annual amplitude (°C) | Phase coefficient (radians) | Mean annual temperature (°C) | Standard error (°C) | Probability | Annual amplitude (°C) | Phase coefficient (radians) | Mean annual temperature (°C) | Standard error (°C) |
| 14-2335. Cowlitz River below Kosmos, 4.2 miles above dam (unaffected by impoundment) | | | | | | | | | | |
| Mean, equal to or less than -- | 0.5 | 4.6 | 4.13 | 8.3 | 0.8 | 0.5 | 5.0 | 4.20 | 8.3 | 0.7 |
| Do ----- | .95 | 5.4 | 4.20 | 9.4 | .7 | .95 | 5.4 | 4.16 | 9.6 | .7 |
| Minimum, equal to or greater than ----- | .5 | 4.3 | 4.24 | 7.1 | .9 | .5 | 4.4 | 4.30 | 7.3 | .8 |
| Do ----- | .95 | 4.0 | 4.18 | 5.7 | 1.0 | .95 | 4.0 | 4.28 | 5.7 | .8 |
| Maximum, equal to or less than ----- | .5 | 5.3 | 4.23 | 9.1 | 1.0 | .5 | 5.7 | 4.30 | 9.2 | .9 |
| Do ----- | .95 | 5.7 | 4.23 | 10.4 | 1.0 | .95 | 6.0 | 4.25 | 10.3 | .9 |
| Site 1, 14-2380. Cowlitz River below Mayfield Dam (previously "near Mayfield"), 1.4 miles below dam | | | | | | | | | | |
| Mean, equal to or less than -- | 0.5 | 5.7 | 4.17 | 9.2 | 1.2 | 0.5 | 5.8 | 3.94 | 10.1 | 1.1 |
| Do ----- | .95 | 6.2 | 4.21 | 11.0 | 1.4 | .95 | 6.9 | 3.91 | 11.5 | 1.1 |
| Minimum, equal to or greater than ----- | .5 | 5.1 | 4.19 | 7.3 | 1.1 | .5 | 5.2 | 3.98 | 9.0 | 1.0 |
| Do ----- | 1.95 | 4.9 | 4.22 | 5.1 | 1.1 | 1.95 | 4.5 | 4.11 | 7.0 | 1.0 |
| Maximum, equal to or less than ----- | .5 | 6.1 | 4.26 | 10.8 | 1.1 | .5 | 6.0 | 4.01 | 10.8 | 1.1 |
| Do ----- | 1.95 | 6.8 | 4.26 | 12.8 | 1.1 | 1.95 | 6.8 | 3.98 | 12.3 | 1.2 |
| Site 2, 14-2430. Cowlitz River at Castle Rock, 34.7 miles below dam | | | | | | | | | | |
| Mean, equal to or less than -- | 0.5 | 6.0 | 4.16 | 10.0 | 1.3 | 0.5 | 6.0 | 4.13 | 10.6 | 1.2 |
| Do ----- | .95 | 6.6 | 4.21 | 12.2 | 1.6 | .95 | 7.1 | 4.15 | 12.5 | 1.2 |
| Minimum, equal to or greater than ----- | .5 | 5.5 | 4.23 | 8.5 | 1.3 | .5 | 5.7 | 4.11 | 9.5 | 1.2 |
| Do ----- | 1.95 | 5.8 | 4.25 | 6.1 | 1.0 | .95 | 4.6 | 4.09 | 7.2 | 1.3 |
| Maximum, equal to or less than ----- | .5 | 6.6 | 4.20 | 11.3 | 1.2 | .5 | 7.0 | 4.15 | 11.9 | 1.5 |
| Do ----- | 1.95 | 7.8 | 4.18 | 13.7 | 1.4 | .95 | 8.2 | 4.19 | 13.8 | 1.5 |

¹ Curves derived from characteristics on this line are shown in figure 9.

temperatures will be on or below the upper confidence curve, and 95 percent of the time minimum temperatures will be on or above the lower confidence curve.) The effect of the impoundment, at each of the sites below the dam as well as from site to site (fig. 9), then could be evaluated by comparison of the natural stream temperatures with the stream temperatures after dam completion.

The magnitudes and differences of the 95-percent probable minimum lowest (winter), minimum highest (summer) and maximum highest (summer) stream temperatures, and time of occurrence of these temperatures before and after water impoundment behind the dam were computed from table 3 and are shown in table 4.

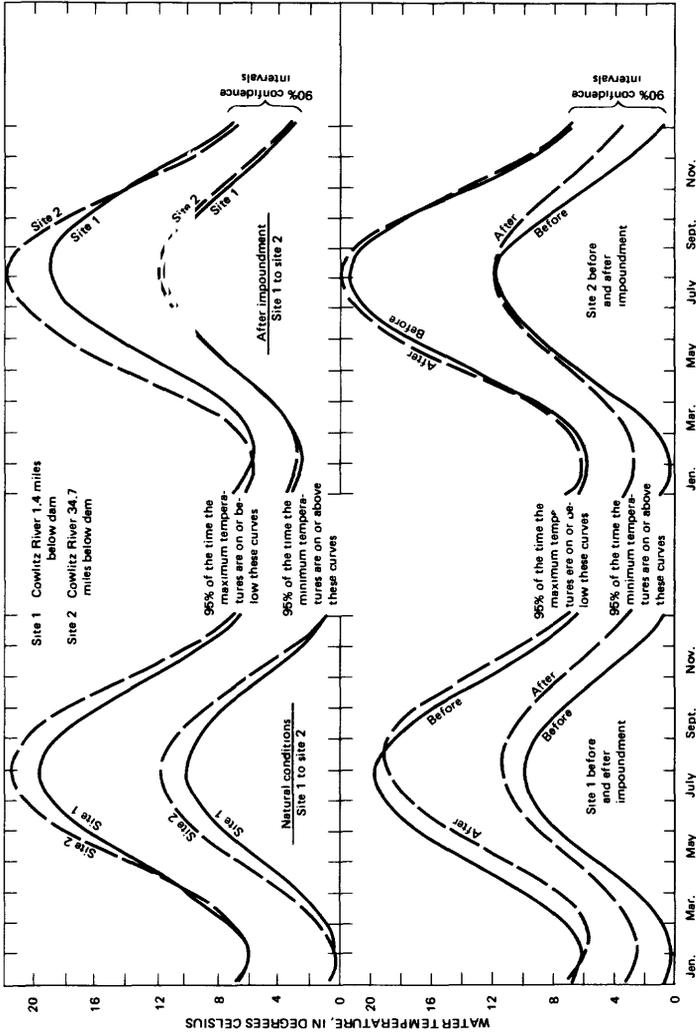


FIGURE 9.—Effects of water impoundment on stream temperatures, Cowlitz River. Graphs show the 90-percent confidence intervals about the maximum and minimum stream temperatures for natural and controlled conditions at two stream-temperature measuring sites below Mayfield Dam.

With the aid of table 4, the following inferences may be made about the effects of the dam on stream temperatures at site 1, Cowlitz River below Mayfield Dam, from natural to controlled conditions:

1. The highest 95-percent probable summer-minimum temperature increased by 1.5°C .
2. The lowest 95-percent probable winter-minimum temperature was increased by 2.3°C and occurs 7 days later.
3. The highest 95-percent probable summer-maximum temperature did not change significantly (-0.5°C), although it occurs 16 days later.

The effects of the dam on stream temperatures between Mayfield Dam (site 1) and Castle Rock (site 2) are as follows:

1. Under natural conditions, a 1.9°C increase occurred in the highest 95-percent probable summer-minimum temperature between sites 1 and 2. After impoundment the increase in the summer-minimum temperature was insignificant.
2. Under natural conditions, the lowest 95-percent probable winter-minimum temperature difference between sites was not significant ($+0.1^{\circ}\text{C}$), nor was the difference ($+0.1^{\circ}\text{C}$) between sites significant after impoundment. However, as stated above, the lowest minimum temperature at each site was increased by 2.3°C after impoundment.
3. Under natural conditions, the highest 95-percent probable summer-maximum temperature had a downstream increase of $+1.9^{\circ}\text{C}$ between sites, whereas after impoundment the increase was $+2.9^{\circ}\text{C}$ between sites, an increase of $+1^{\circ}\text{C}$.

The effects of the dam on stream temperatures at site 2, Cowlitz River at Castle Rock, are inferred from table 4 as follows:

1. The highest 95-percent probably summer-minimum temperature did not change significantly (-0.1°C).
2. The lowest 95-percent probable winter-minimum temperature was increased 2.3°C , and it occurs 9 days later.
3. The highest 95-percent probable summer-maximum temperature did not change significantly ($+0.5^{\circ}\text{C}$), nor did the time of occurrence change significantly (-1 day).

An interesting observation is that the time of occurrence of the 95-percent probable summer-maximum peak temperature at site 2 did not change significantly from before to after impoundment (August 2 to August 1, respectively) even though there was a 17-day increase at site 1 (July 28 before and August 13 after). The natural time lag in peak temperature between sites is $+5$ days (July 28 at site 1 and August 2 at site 2), and the controlled peak

TABLE 4.—*Evaluation of water-temperature*

| 95-percent probable | Site 1 | | |
|------------------------------|-----------------|-----------------------|-----------------|
| | From natural | To con- trolled | Differ- ence |
| Water temperature, °C | | | |
| Minimum: Summer ----- | 10.0 | 11.5 | +1.5 |
| Winter ----- | .2 | 2.5 | +2.3 |
| Maximum: Summer ----- | 19.6 | 19.1 | *-.5 |
| Date of occurrence | | | |
| Minimum: Summer ----- | July 30 | Aug. 5 | Days +6 |
| Winter ----- | Jan. 28 | Feb. 4 | +7 |
| Maximum: Summer ----- | July 28 | Aug. 13 | +16 |

* Value not statistically significant.

temperature at site 1 occurs 12 days later than at site 2 (August 13 at site 1 and August 1 at site 2).

EXAMPLE 2: EFFECTS OF A FLOOD-CONTROL DAM

The second example of the effects of impoundment evaluates the downstream water-temperature effects of the Howard A. Hanson Dam, a flood-control dam which also augments the natural river flows during the low-flow months. The dam is in King County on the Green River at river mile 64.5 and impounds the Howard A.

TABLE 5.—*Probable water-temperature characteristics at Green River (measuring site 12-1130) near Auburn, 32.5 miles below Howard A. Hanson Dam*

| Water temperature | Probability | Annual amplitude (°C) | Phase coefficient (radians) | Mean annual temperature (°C) | Standard error (°C) |
|--|-------------|-----------------------|--------------------------------|---------------------------------|---------------------|
| Before dam construction | | | | | |
| Minimum, equal to or greater than ---- | 0.5 | 4.7 | 4.22 | 8.0 | 0.6 |
| Do ----- | .95 | 4.8 | 4.24 | 6.1 | .6 |
| Maximum, equal to or less than ---- | .5 | 7.0 | 4.33 | 11.8 | 1.4 |
| Do ----- | .95 | 8.2 | 4.39 | 14.6 | 1.7 |
| After dam construction | | | | | |
| Minimum, equal to or greater than ---- | 0.5 | 5.1 | 4.19 | 8.2 | 0.5 |
| Do ----- | .95 | 5.8 | 4.31 | 6.7 | .8 |
| Maximum, equal to or less than ---- | .5 | 7.2 | 4.35 | 12.0 | 1.1 |
| Do ----- | .95 | 7.8 | 4.39 | 14.4 | 1.0 |

changes below Mayfield Dam

| Site 2 | | | Natural condition | | | Controlled condition | | |
|--|---------------|-------------------|-------------------|-----------|--------------------|----------------------|-----------|--------------------|
| From natural | To controlled | Difference | From site 1 | To site 2 | Difference | From site 1 | To site 2 | Difference |
| Water temperature, °C—Continued | | | | | | | | |
| 11.9 | 11.8 | *-0.1 | 10.0 | 11.9 | +1.9 | 11.5 | 11.8 | *+0.3 |
| .3 | 2.6 | +2.3 | .2 | .3 | *+1 | 2.5 | 2.6 | *+1 |
| 21.5 | 22.0 | *+5 | 19.6 | 21.5 | +1.9 | 19.1 | 22.0 | +2.9 |
| Date of occurrence—Continued | | | | | | | | |
| July 28 | Aug. 6 | <i>Days</i> +9 | July 30 | July 28 | <i>Days</i> *-2 | Aug. 5 | Aug. 6 | <i>Days</i> *+1 |
| Jan. 27 | Feb. 5 | +9 | Jan. 28 | Jan. 27 | *-1 | Feb. 4 | Feb. 5 | *+1 |
| Aug. 2 | Aug. 1 | *-1 | July 28 | Aug. 2 | 5 | Aug. 13 | Aug. 1 | -12 |

Hanson Reservoir near Palmer (station 12-1058). Thermograph records at station 12-1130, Green River near Auburn (32.5 miles below the dam), were used from 1953 to present. The dam has been in operation since December 1961.

Probability distributions and the harmonic fittings of the thermograph records were computed, and the 50- and 95-percent probable maximum and minimum stream-temperature characteristics (amplitude, mean, and phase coefficient) were determined and are shown in table 5. Magnitudes, differences and times of occurrence of stream temperatures as computed from table 5 are shown in table 6.

From table 6 it is inferred that the dam affected stream temperatures from natural to controlled conditions, as follows:

1. The 95-percent probable summer-minimum was increased by 1.6°C.
2. The change in the 95-percent probable winter-minimum low temperature is not statistically significant (-0.4°C).

TABLE 6.—*Evaluation of water-temperature changes below Howard A. Hanson Dam*

| 95-percent probable: | Water temperature (°C) | | | Date of occurrence | | |
|----------------------|------------------------|------------|-------------------|--------------------|------------|-----------------|
| | Natural | Controlled | Difference | Natural | Controlled | Days Difference |
| Minimum: | | | | | | |
| Summer ----- | 10.9 | 12.5 | +1.6 | July 29 | July 25 | -4 |
| Winter ----- | 1.3 | .9 | ¹ -0.4 | Jan. 27 | Jan. 23 | -4 |
| Maximum: | | | | | | |
| Summer ----- | 22.8 | 22.2 | ¹ -0.6 | July 20 | July 20 | 0 |

¹ Value not statistically significant.

3. The change in the 95-percent probable summer-maximum high temperature is not statistically significant (-0.6°C).

The increase in the summer-minimum temperature, after control, is probably caused by the summer low-flow augmentation (increased volume of streamflow) of water warmed by retention in the reservoir.

SUMMARY AND CONCLUSIONS

Many of the physical, chemical, and biological properties of water are related to temperature. Thus, stream temperatures are important in water-quality control because of their influence on the ecosystem of streams.

Regional stream-temperature studies usually list basic data for each site. In some cases generalizations of stream temperatures are made by simple extrapolation or interpolation. In this report, however, multiple-regression techniques were used to determine the topographic and climatic-basin characteristics most effective to explain the site-to-site variations in natural stream temperatures. A procedure was developed to estimate water temperatures at sites where little or no data are now available.

The analyses performed in this study used most of the complete and essentially natural stream-temperature data available for Washington, as well as some temperature data for stream reaches that are subject to thermal modification. The regression results, therefore, are based on the most useful stream-temperature data available and provide a generalized definition of stream temperatures in the State—one of the main objectives of this study.

In general, it was found that the multiple-regression technique produces more accurate results in western than in eastern Washington. The mean annual temperature and the annual-temperature amplitude could be estimated with greater accuracy in western Washington. The more accurate definition of these two stream-temperature characteristics in the western part of the State is primarily the result of more data. The prediction of the phase coefficient is slightly less accurate in western Washington than in eastern Washington, probably because in western Washington there are more physiographic differences—the coastal lowland, the Olympic Mountains and their rain shadow, the Puget Sound lowlands, the Willapa Hills, and the western slope of the Cascade Range. Such variety results in a diverse climate which produces greater diversity in the phase coefficient. In general the accuracy of definition of the multiple-regression equations for stream temperatures in western Washington, compared to those for eastern Washington, is due to the more humid, milder coastal climate of

western Washington, compared to greater natural variability in the semiarid, continental climate of eastern Washington.

The monthly standard deviation of temperatures for western Washington streams could be determined with more confidence in the winter months than in June and July.

The regression analysis showed that of the 24 topographic and climatic characteristics tested against each of the stream-temperature characteristics, 15 (six of which are a function of air temperatures) were significantly effective to determine one or more of the 15 stream-temperature characteristics. The independent variables found to occur most often as significant parameters (table 2) to define the stream-temperature characteristics are:

| Topographic or climatic characteristic | Number of equations ¹ where variable was found significant 95 percent of the time |
|---|--|
| Drainage area ----- | 7 |
| Channel slope ----- | 5 |
| Mean basin altitude ----- | 6 |
| Mean annual streamflow ----- | 5 |
| Altitude of data site ----- | 2 |
| Stream length ----- | 3 |
| Source altitude of stream ----- | 3 |
| Area of lakes and ponds ----- | 3 |
| Direction (orientation) of streamflow ----- | 2 |
| Mean air temperature: | |
| Amplitude ----- | 1 |
| Annual ----- | 1 |
| January ----- | 1 |
| February ----- | 1 |
| August ----- | 1 |
| October ----- | 1 |

¹ Usually more than one variable is found in an equation (table 2).

Data for the topographic and climatic characteristics evaluated in this investigation are not costly to acquire compared to the parameters that may be used to determine, for example, an energy budget. These data for this investigation are obtained from topographic maps, air-temperature isothermal maps (figs. 4, 5, 6, and 7), and from mean annual flow equations determined previously by the author (Collings, 1971, p. 14-15). In contrast, an energy budget, used to obtain temperature-prediction equations, requires relatively expensive instrumentation to determine incoming solar radiation, effective back radiation, energy losses from evaporation and conduction, and energy advected into the water by tributary streams and precipitation. However, energy-budget studies are much more sophisticated and the results are more comprehensive—evaluation of stratification, heat-exchange coefficients, mixing

rates, and other physical characteristics of a stream which are concerned with its temperature.

The generalization procedures in this report are valuable for relatively inexpensive feasibility and comparison studies to determine if additional, more intensive, investigations (such as an energy-budget study) are warranted. For example, the generalization procedures could be used for fish-hatchery site-feasibility studies, reconnaissance of downstream water-temperature effects of dams or tributary inflow, and (or) the adequacy of waters for cooling purposes in industrial plants.

Although not a major objective of this report, the statewide analysis has identified areas where basic stream-temperature data are deficient. The residual values of the stream-temperature characteristics generally show that basic temperature data are lacking in the Olympic Peninsula in western Washington and the southeastern and north-central parts of eastern Washington.

The two examples of the evaluation of stream temperatures below water impoundments (tables 3 and 5) show how the natural temperature regime of a river is affected by damming. The investigation of the impoundment by Mayfield Dam on the Cowlitz River showed an increase of probable winter-minimum stream temperatures below the dam, whereas the investigation of the impoundment by Howard A. Hanson Dam on the Green River showed a statistically insignificant decrease in probable winter-minimum stream temperatures below the dam. However, the summer-minimum stream temperature at the Green River site was increased, whereas the change in the summer-minimum temperature of the Cowlitz River at Castle Rock (site 2) was insignificant. The lower site on the Cowlitz River and the site on the Green River are about the same distance downstream from their respective dams. The opposite effects that the impoundments apparently have on minimum stream temperatures of the rivers is attributed to the difference in dam function; Mayfield Dam on the Cowlitz River is used to produce hydroelectric power, while Howard A. Hanson Dam on the Green River is used for flood control and low-flow augmentation.

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TABLES 7-10

TABLE 7.—Stream-temperature characteristics, western Washington thermograph stations

| Station number | Station name | Annual amplitude (°C) | Phase Coefficient (radians) | | | Mean annual (°C) | Standard deviations of monthly stream temperatures (°C) | | | | | | | | | | | |
|----------------|---|-----------------------|-----------------------------|----------------|----------------|------------------|---|----------------|-----------------|-----------------|-----------------|------|------|--------|-----------|---------|----------|----------|
| | | | A | C | M | | Month | | | | | | | | | | | |
| | | | | | | | January | February | March | April | May | June | July | August | September | October | November | December |
| T ₁ | T ₂ | T ₃ | T ₄ | T ₅ | T ₆ | T ₇ | T ₈ | T ₉ | T ₁₀ | T ₁₁ | T ₁₂ | | | | | | | |
| 12-0115 | Willapa River at Lebam | 5.3 | 4.13 | 10.2 | 2.8 | 2.0 | 1.1 | 1.4 | 2.0 | 2.2 | 2.7 | 2.3 | 1.7 | 1.3 | 2.3 | 1.5 | | |
| 0275 | Chehalis River near Grand Mound | 7.9 | 4.31 | 11.6 | 2.5 | 2.5 | 1.6 | 1.7 | 2.1 | 3.7 | 2.9 | 2.8 | 1.4 | 1.6 | 2.1 | 1.4 | | |
| 0600 | South Fork Skokomish River near Potlatch | 5.2 | 4.12 | 9.0 | 1.2 | 2.1 | 1.5 | 1.7 | 1.3 | 2.9 | 2.8 | 3.2 | 2.1 | 1.3 | 1.5 | 1.0 | | |
| 0615 | Skokomish River near Potlatch | 3.4 | 4.27 | 9.2 | 1.4 | .8 | 1.4 | 1.8 | 3.0 | 2.7 | 2.7 | 1.2 | 1.3 | 1.5 | 1.4 | 1.2 | | |
| 0625 | Purdy Creek near Union | 2.5 | 4.54 | 8.8 | .8 | 1.5 | 1.5 | .9 | .6 | 1.0 | .6 | .1 | 1.0 | .9 | .7 | 1.0 | | |
| 0825 | Nisqually River near National | 3.6 | 4.34 | 6.5 | 1.7 | 1.4 | 1.6 | 1.1 | 1.8 | 2.2 | 2.1 | 1.7 | 1.8 | 1.7 | 1.8 | 1.6 | | |
| 0830 | Mineral Creek near Mineral | 5.9 | 4.16 | 9.0 | 2.0 | 1.6 | 1.4 | 1.8 | 2.0 | 2.2 | 2.0 | 2.8 | 1.9 | 1.6 | 2.3 | 1.3 | | |
| 1130 | Green River near Auburn | 5.4 | 4.21 | 9.9 | 1.4 | 2.2 | 1.4 | 1.8 | 2.1 | 3.5 | 3.0 | 2.0 | 1.8 | 1.4 | 2.2 | 2.0 | | |
| 1175 | Cedar River near Landsburg | 3.7 | 4.24 | 8.9 | .8 | 1.2 | 1.2 | 1.6 | 1.5 | 1.3 | 1.1 | 1.8 | 2.1 | 2.7 | 1.2 | 1.1 | | |
| 1350 | Wallace River at Gold Bar | 5.4 | 4.15 | 9.0 | 1.3 | 1.3 | 1.2 | 1.7 | 1.4 | 2.4 | 2.4 | 2.6 | 2.3 | 1.6 | 2.1 | 2.0 | | |
| 1640 | Jim Creek near Arlington | 6.0 | 4.23 | 9.0 | 2.0 | 2.5 | 1.3 | 1.2 | 1.4 | 2.8 | 3.6 | 2.3 | 1.0 | 1.6 | 2.4 | 2.0 | | |
| 1655 | North Fork Stillaguamish River near Darrington | 4.4 | 4.01 | 7.6 | .6 | 1.0 | 1.4 | 1.5 | 1.1 | 2.6 | 3.2 | 1.7 | 3.6 | 1.7 | 2.2 | 2.0 | | |
| 1685 | Pitchuck Creek near Bryant | 6.3 | 4.14 | 9.1 | 1.7 | 1.9 | 1.9 | 1.6 | 3.4 | 4.6 | 3.9 | 3.0 | 2.2 | 1.2 | 1.7 | 1.6 | | |
| 1790 | Skagit River above Alma Creek, near Marblemount | 3.2 | 3.70 | 7.1 | 1.4 | 1.4 | 1.2 | .7 | 1.1 | 1.5 | 1.3 | 1.0 | .9 | 1.3 | 1.3 | 1.3 | | |
| 1825 | Cascade River at Marblemount | 3.3 | 4.15 | 6.5 | 1.4 | 1.4 | 1.1 | 1.4 | 1.8 | 2.1 | 2.2 | 2.4 | 1.7 | 1.4 | .9 | 1.1 | | |
| 2005 | Skagit River near Mount Vernon | 4.5 | 4.02 | 8.7 | .4 | 1.0 | .4 | 1.2 | 1.7 | 1.8 | 1.6 | 1.9 | 2.2 | 1.1 | 1.1 | 1.1 | | |
| 14-1100 | Klickitat River near Glenwood | 5.2 | 4.21 | 6.3 | .8 | 1.4 | .9 | .4 | 1.1 | 1.8 | 1.4 | 1.2 | .8 | 1.3 | 1.7 | 1.7 | | |
| 1130 | Klickitat River near Pitt | 5.6 | 4.33 | 8.7 | 1.7 | 1.9 | 1.3 | 1.2 | 1.7 | 2.1 | 1.8 | 2.0 | 1.3 | 1.3 | 1.8 | 1.7 | | |
| 2205 | Lewis River at Arsel | 4.2 | 3.60 | 9.1 | 1.8 | 2.0 | 1.7 | 1.6 | .9 | 1.5 | 2.8 | 3.0 | 1.9 | 3.3 | 2.1 | 1.1 | | |
| 2225 | East Fork Lewis River near Heisson | 6.0 | 4.21 | 9.6 | 2.2 | 1.9 | 1.9 | 1.2 | 3.1 | 3.0 | 3.8 | 2.5 | 2.4 | 1.7 | 2.3 | 1.9 | | |
| 2235 | Kalama River below Italian Creek, near Kalama | 4.5 | 4.16 | 8.8 | 1.3 | 1.9 | 1.2 | 1.4 | 2.2 | 2.6 | 2.7 | 1.8 | 1.4 | 1.4 | 2.1 | 1.3 | | |
| 2325 | Cispus River near Randle | 4.2 | 4.11 | 6.9 | 1.7 | 1.5 | .8 | .9 | 1.2 | 2.1 | 2.0 | 1.7 | 1.5 | 1.6 | 1.7 | .9 | | |
| 2335 | Cowlitz River near Kosmos | 4.9 | 4.12 | 8.1 | 2.0 | 1.3 | 1.0 | 1.3 | 1.3 | 2.9 | 3.3 | 1.8 | 2.1 | 1.3 | 1.6 | 1.2 | | |
| 2355 | West Fork Tilton River near Morton | 5.7 | 4.02 | 8.0 | 2.4 | 2.2 | 2.0 | 1.8 | 1.8 | 5.0 | 4.5 | 2.6 | 2.2 | 1.5 | 2.5 | 1.9 | | |
| 2380 | Cowlitz River below Mayfield Dam | 6.0 | 3.92 | 9.8 | 1.5 | 1.5 | 1.6 | 1.5 | 1.5 | 3.0 | 3.7 | 2.2 | 1.6 | 1.6 | 1.6 | 1.6 | | |
| 2425 | Toutle River near Silver Lake | 5.8 | 4.10 | 9.5 | 1.7 | 1.9 | 1.8 | 1.8 | 1.7 | 3.3 | 4.6 | 2.9 | 1.6 | 1.4 | 2.0 | 2.1 | | |
| 2430 | Cowlitz River at Castle Rock | 6.1 | 4.08 | 10.4 | 2.0 | 2.2 | 2.2 | 2.0 | 1.9 | 2.8 | 4.0 | 3.5 | 2.4 | 1.6 | 2.0 | 1.8 | | |
| 2450 | Coweman River near Nelsa | 6.6 | 4.30 | 10.5 | 2.5 | 2.1 | 1.9 | 2.5 | 2.5 | 2.8 | 3.0 | 2.4 | 2.3 | 1.8 | 2.4 | 1.3 | | |
| 2460 | Abernathy Creek near Longview | 4.6 | 4.18 | 9.4 | 2.3 | 1.5 | 2.6 | 2.4 | 1.5 | 1.2 | 2.4 | 2.1 | 1.5 | 2.0 | 2.2 | 2.2 | | |
| 2475 | Elochoman River near Cathlamet | 5.3 | 4.27 | 10.0 | 2.1 | 2.0 | 2.2 | 1.4 | 2.1 | 2.5 | 2.4 | 2.2 | 2.3 | 1.7 | 2.1 | 2.0 | | |
| 2505 | West Fork Grays River near Grays River | 5.0 | 4.07 | 10.2 | 1.5 | 1.9 | 1.5 | 1.7 | 2.4 | 3.3 | 2.9 | 2.9 | 1.7 | 1.7 | 1.9 | 1.4 | | |

TABLE 8.—Stream-temperature characteristics, irregularly measured temperature stations, Washington

| Station number | Station name | Annual amplitude | Phase coefficient | Mean annual |
|--------------------|---|------------------|-------------------|-------------|
| | | (°C) | (radians) | |
| | | A | C | M |
| WESTERN WASHINGTON | | | | |
| 12-0095 | Bear Branch near Naselle | 3.9 | 4.03 | 9.9 |
| 0100 | Naselle River near Naselle | 5.2 | 4.24 | 10.3 |
| 0105 | Salmon Creek near Naselle | 4.8 | 4.17 | 10.1 |
| 0107 | South Fork Naselle River near Naselle | 5.9 | 3.92 | 10.8 |
| 0110 | North Nemah River near South Bend | 5.1 | 4.14 | 11.1 |
| 0112 | Williams Creek near South Bend | 3.8 | 4.06 | 9.7 |
| 0120 | Fork Creek near Lebam | 5.1 | 4.13 | 10.1 |
| 0135 | Willapa River near Willapa | 6.7 | 4.13 | 11.6 |
| 0145 | South Fork Willapa River near Raymond | 4.0 | 4.22 | 10.1 |
| 0151 | Clearwater Creek near Raymond | 3.6 | 4.03 | 9.5 |
| 0152 | Smith Creek near Raymond | 4.0 | 4.28 | 9.9 |
| 0155 | North River near Brooklyn | 5.5 | 4.22 | 10.2 |
| 0170 | North River near Raymond | 5.5 | 4.13 | 10.6 |
| 0200 | Chehalis River near Doty | 6.2 | 4.23 | 10.3 |
| 0210 | South Fork Chehalis River at Boistfort | 7.4 | 4.35 | 11.0 |
| 0240 | South Fork Newaukum River near Onalaska | 5.9 | 4.24 | 9.7 |
| 0245 | North Fork Newaukum River near Forest | 6.4 | 4.32 | 11.2 |
| 0250 | Newaukum River near Chehalis | 7.5 | 4.21 | 11.1 |
| 0260 | Skookumchuck River near Centralia | 5.6 | 4.24 | 9.1 |
| 0300 | Rock Creek at Cedarville | 5.1 | 4.20 | 9.3 |
| 0310 | Chehalis River at Porter | 7.4 | 4.11 | 11.3 |
| 0325 | Cloquallum Creek at Elma | 5.2 | 4.21 | 10.4 |
| 0342 | East Fork Satsop River near Elma | 4.5 | 4.33 | 9.8 |
| 0350 | Satsop River near Satsop | 5.4 | 4.33 | 10.2 |
| 0354 | Wynoochee River near Gridsale | 4.4 | 3.83 | 8.6 |
| 0360 | Wynoochee River above Save Creek, near Aberdeen | 5.1 | 4.23 | 8.8 |
| 0374 | Wynoochee River above Black Creek, near Montesano | 6.3 | 4.16 | 10.8 |
| 0390 | Humtullips River near Humtullips | 6.4 | 4.22 | 10.3 |
| 0393 | North Fork Quinault River near Amanda Park | 4.2 | 3.88 | 6.2 |
| 0395 | Quinault River at Quinault Lake | 5.9 | 4.08 | 10.5 |
| 0410 | Hoh River near Forks | 3.4 | 4.25 | 8.2 |
| 0412 | Hoh River at U.S. Highway 101, near Forks | 4.1 | 4.29 | 8.7 |
| 0415 | Soleduck River near Fairholm | 4.7 | 4.07 | 7.1 |
| 0430.8 | East Fork Dickey River near LaPush | 6.1 | 4.24 | 9.5 |
| 0431 | Dickey River near LaPush | 5.2 | 4.35 | 10.1 |
| 0433 | Hoko River near Sekiu | 5.5 | 4.29 | 10.0 |
| 0434.3 | East Twin River near Pysht | 4.5 | 4.18 | 8.4 |
| 0455 | Elwha River at McDonald Bridge, near Port Angeles | 4.9 | 4.01 | 8.2 |
| 0475 | Siebert Creek near Port Angeles | 5.4 | 4.29 | 7.7 |
| 0480 | Dungeness River near Sequim | 4.3 | 4.18 | 7.0 |
| 0505 | Snow Creek near Maynard | 5.6 | 4.19 | 8.4 |
| 0540 | Duckabush River near Brannon | 3.8 | 4.06 | 7.3 |
| 0545 | Hanna Hanna River near Eldon | 2.8 | 3.95 | 7.3 |
| 0546 | Jefferson Creek near Eldon | 4.3 | 3.97 | 8.0 |
| 0565 | North Fork Skokomish River below Staircase Rapids, near Hoodspout | 4.0 | 4.00 | 6.7 |
| 0595 | North Fork Skokomish River near Potlatch | 4.4 | 4.30 | 10.2 |
| 0598 | South Fork Skokomish River near Hoodspout | 3.3 | 3.96 | 6.9 |
| 0605 | South Fork Skokomish River near Union | 4.7 | 4.11 | 9.1 |
| 0626 | Weaver Creek near Potlatch | 1.6 | 4.35 | 8.8 |
| 0655 | Gold Creek near Bremerton | 4.8 | 4.40 | 9.4 |
| 0685 | Dewatto Creek near Dewatto | 4.1 | 4.26 | 9.2 |
| 0700 | Dogfish Creek near Poulsbo | 4.0 | 4.33 | 9.2 |
| 0720 | Chico Creek near Bremerton | 6.5 | 4.27 | 10.7 |
| 0730 | Burley Creek at Burley | 3.2 | 4.43 | 9.5 |
| 0735 | Huge Creek near Wauna | 2.9 | 4.38 | 9.1 |

TABLE 8.—Stream-temperature characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Station name | Annual amplitude | Phase coefficient | Mean annual |
|------------------------------|---|------------------|-------------------|-------------|
| | | (°C) | (radians) | (°C) |
| | | A | C | M |
| WESTERN WASHINGTON—Continued | | | | |
| 12-0765 | Goldsborough Creek near Shelton | 5.0 | 4.38 | 9.8 |
| 0784 | Kennedy Creek near Kamliche | 5.4 | 4.32 | 10.3 |
| 0790 | Deschutes River near Rainier | 5.6 | 4.28 | 10.0 |
| 0800 | Deschutes River near Olympia | 5.7 | 4.51 | 11.4 |
| 0810 | Woodland Creek near Olympia | 4.0 | 4.62 | 9.7 |
| 0865 | Nisqually River at La Grande | 3.9 | 3.74 | 7.6 |
| 0880 | Ohop Creek near Eatonville | 6.9 | 4.28 | 10.7 |
| 0895 | Nisqually River at McKenna | 5.8 | 4.24 | 10.1 |
| 0902 | Muck Creek at Roy | 7.7 | 4.38 | 12.2 |
| 0911 | Flett Creek at Tacoma | 3.0 | 4.55 | 11.4 |
| 0912 | Leach Creek near Fircrest | 4.2 | 4.40 | 12.4 |
| 0913 | Leach Creek near Steilacoom | 3.1 | 4.30 | 10.1 |
| 0915 | Chambers Creek below Leach Creek, near Steilacoom | 4.9 | 4.36 | 11.5 |
| 0920 | Puyallup River near Electron | 3.3 | 4.35 | 5.8 |
| 0935 | Puyallup River near Orting | 3.6 | 4.23 | 7.6 |
| 0940 | Carbon River near Fairfax | 3.6 | 4.19 | 7.0 |
| 0944 | South Prairie Creek near Enumclaw | 4.4 | 4.17 | 6.6 |
| 0950 | South Prairie Creek at South Prairie | 5.1 | 4.21 | 8.6 |
| 0966 | White River near Greenwater | 4.3 | 4.40 | 4.6 |
| 0970 | White River at Greenwater | 3.7 | 4.20 | 6.2 |
| 0975 | Greenwater River at Greenwater | 4.7 | 4.15 | 6.5 |
| 0985 | White River near Buckley | 4.2 | 4.16 | 7.1 |
| 0993 | Boise Creek above reservoir, near Enumclaw | 4.0 | 4.17 | 7.3 |
| 0994 | Boise Creek below millpond, near Enumclaw | 5.7 | 4.17 | 11.8 |
| 0995 | Boise Creek near Enumclaw | 6.2 | 4.25 | 12.1 |
| 1005 | White River near Sumner | 6.5 | 4.22 | 11.8 |
| 1015 | Puyallup River at Puyallup | 5.5 | 4.21 | 9.5 |
| 1034 | Green River below Intake Creek, near Lester | 5.9 | 3.86 | 7.5 |
| 1035 | Snow Creek near Lester | 5.1 | 4.06 | 6.3 |
| 1040 | Friday Creek near Lester | 4.7 | 4.02 | 6.0 |
| 1045 | Green River near Lester | 5.7 | 4.01 | 8.1 |
| 1047 | Green Canyon Creek near Lester | 3.6 | 4.06 | 7.5 |
| 1050 | Smy Creek near Lester | 3.7 | 4.03 | 5.8 |
| 1057.1 | North Fork Green River near Lemolo | 4.3 | 4.10 | 7.0 |
| 1059 | Green River below Howard A. Hanson Dam | 5.3 | 3.91 | 8.2 |
| 1067 | Green River at purification plant, near Plamer | 6.0 | 3.97 | 8.6 |
| 1073 | Icy Creek near Black Diamond | 1.3 | 3.13 | 8.0 |
| 1085 | Newaukum Creek near Black Diamond | 5.4 | 4.54 | 10.2 |
| 1126 | Big Soos Creek above hatchery, near Auburn | 5.2 | 4.40 | 10.1 |
| 1133.5 | Green River at Tukwila | 5.6 | 4.21 | 10.5 |
| 1135 | North Fork Cedar River near Lester | 4.4 | 4.03 | 6.0 |
| 1140 | South Fork Cedar River near Lester | 4.5 | 4.11 | 5.8 |
| 1145 | Cedar River below Bear Creek, near Cedar Falls | 5.0 | 4.15 | 6.5 |
| 1150 | Cedar River near Cedar Falls | 4.4 | 3.98 | 6.9 |
| 1155 | Rex River near Cedar Falls | 5.7 | 4.09 | 7.0 |
| 1165 | Cedar River at Cedar Falls | 6.7 | 3.93 | 8.9 |
| 1170 | Taylor Creek near Selleck | 3.4 | 4.16 | 7.4 |
| 1185 | Rock Creek near Maple Valley | 2.1 | 4.16 | 9.0 |
| 1190 | Cedar River at Renton | 5.6 | 4.30 | 10.2 |
| 1196 | May Creek at mouth, near Renton | 4.6 | 4.44 | 9.2 |
| 1197 | Coal Creek near Bellevue | 4.5 | 4.45 | 9.9 |
| 1200 | Mercer Creek near Bellevue | 5.6 | 4.43 | 10.2 |
| 1205 | Juanita Creek near Kirkland | 4.3 | 4.36 | 10.2 |
| 1210 | Issaquah Creek near Issaquah | 5.8 | 4.27 | 10.3 |
| 1216 | Issaquah Creek near mouth, near Issaquah | 6.0 | 4.42 | 10.1 |

TABLE 8.—Stream-temperature characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Station name | Annual amplitude | Phase coefficient | Mean annual |
|-------------------------------|---|------------------|-------------------|-------------|
| | | (°C) | (radians) | (°C) |
| | | A | C | M |
| WESTERN WASHINGTON--Continued | | | | |
| 12-1230 | Cottage Lake Creek near Redmond | 5.2 | 4.40 | 10.9 |
| 1240 | Evans Creek above mouth, near Redmond | 4.6 | 4.40 | 9.6 |
| 1252 | Sammamish River near Woodinville | 6.2 | 4.17 | 11.5 |
| 1255 | Bear Creek at Woodinville | 4.9 | 4.40 | 9.6 |
| 1260 | North Creek near Bothell | 5.8 | 4.33 | 10.6 |
| 1265 | Sammamish River at Bothell | 5.8 | 4.31 | 11.1 |
| 1271 | Swamp Creek at Kenmore | 5.6 | 4.35 | 9.8 |
| 1280 | Thornton Creek near Seattle | 4.9 | 4.38 | 10.7 |
| 1330 | South Fork Skykomish River near Index | 4.8 | 4.05 | 7.8 |
| 1345 | Skykomish River near Gold Bar | 4.7 | 4.08 | 7.8 |
| 1375 | Sultan River near Startup | 4.4 | 4.18 | 7.1 |
| 1410 | Woods Creek near Monroe | 5.8 | 4.30 | 9.6 |
| 1413 | Middle Fork Snoqualmie River near Tanner | 5.0 | 4.02 | 7.6 |
| 1420 | North Fork Snoqualmie River near Snoqualmie Falls | 4.5 | 3.99 | 7.0 |
| 1430 | North Fork Snoqualmie River near North Bend | 4.6 | 4.10 | 8.2 |
| 1434 | South Fork Snoqualmie River above Alice Creek, near Garcia | 5.4 | 4.18 | 7.7 |
| 1436 | South Fork Snoqualmie River at Edgewick | 4.4 | 4.08 | 7.9 |
| 1440 | South Fork Snoqualmie River at North Bend | 4.6 | 4.04 | 8.8 |
| 1445 | Snoqualmie River near Snoqualmie | 4.8 | 4.10 | 8.4 |
| 1455 | Raging River near Fall City | 5.6 | 4.24 | 9.4 |
| 1460 | Patterson Creek near Fall City | 4.7 | 4.27 | 9.5 |
| 1470 | Griffin Creek near Carnation | 6.0 | 4.40 | 10.1 |
| 1475 | North Fork Tolt River near Carnation | 4.0 | 4.26 | 7.6 |
| 1480 | South Fork Tolt River near Carnation | 6.0 | 3.98 | 8.8 |
| 1485 | Tolt River near Carnation | 4.2 | 4.13 | 8.2 |
| 1487 | Stossel Creek near Carnation | 5.9 | 4.56 | 9.8 |
| 1490 | Snoqualmie River near Carnation | 5.8 | 4.26 | 9.8 |
| 1505 | Cherry Creek near Duvall | 5.8 | 4.22 | 10.7 |
| 1508 | Snohomish River near Monroe | 5.8 | 4.26 | 9.5 |
| 1530 | Little Pilchuck Creek near Lake Stevens | 6.2 | 4.35 | 9.9 |
| 1570 | Quilcoeda Creek near Marysville | 4.0 | 4.34 | 9.5 |
| 1610 | South Fork Stillaguamish River near Granite Falls | 5.3 | 4.13 | 8.1 |
| 1650 | Squire Creek near Darrington | 4.1 | 4.13 | 7.2 |
| 1670 | North Fork Stillaguamish River near Arlington | 5.5 | 4.06 | 8.5 |
| 1720 | Big Beaver Creek near Newhalem | 3.6 | 4.20 | 5.0 |
| 1735 | Ruby Creek below Panther Creek, near Newhalem | 5.2 | 4.18 | 5.5 |
| 1755 | Thunder Creek near Newhalem | 3.1 | 4.07 | 5.1 |
| 1775 | Stetattle Creek near Newhalem | 3.8 | 4.00 | 6.0 |
| 1780 | Skagit River at Newhalem | 3.5 | 3.67 | 6.9 |
| 1781 | Newhalem Creek near Newhalem | 4.1 | 4.08 | 5.8 |
| 1860 | Sauk River above Whitechuck River near Darrington | 3.6 | 4.17 | 6.4 |
| 1895 | Sauk River near Sauk | 4.5 | 4.07 | 7.6 |
| 1918 | Sulphur Creek near Concrete | 3.5 | 4.12 | 5.7 |
| 1935 | Baker River at Concrete | 4.1 | 3.74 | 8.4 |
| 1940 | Skagit River near Concrete | 3.6 | 4.08 | 8.7 |
| 1960 | Alder Creek near Hamilton | 3.6 | 4.20 | 8.4 |
| 1962 | Day Creek below Day Lake, near Lyman | 8.5 | 4.36 | 1.1 |
| 1964 | Day Creek near Hamilton | 6.3 | 4.08 | 8.4 |
| 1998 | East Fork Nookachamps Creek near Big Lake | 5.0 | 3.98 | 6.3 |
| 2015 | Samish River near Burlington | 5.7 | 4.40 | 10.3 |
| 2050 | North Fork Nooksack River below Cascade Creek, near Glacier | 3.0 | 4.27 | 5.4 |
| 2072 | North Fork Nooksack River near Deming | 4.7 | 4.04 | 7.8 |
| 2080 | Middle Fork Nooksack River near Deming | 3.9 | 4.06 | 6.9 |
| 2090 | South Fork Nooksack River near Wickersham | 6.1 | 4.03 | 8.2 |
| 2095 | Skookum Creek near Wickersham | 5.0 | 4.24 | 7.5 |

TABLE 8.—Stream-temperature characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Station name | Annual amplitude | | |
|-------------------------------|--|------------------|---|---------------------|
| | | (°C) | Phase coefficient ^a (radians) | Mean annual (°C) |
| | | A | C | M |
| WESTERN WASHINGTON--Continued | | | | |
| 12-2105 | Nooksack River at Deming | 5.2 | 4.18 | 8.1 |
| 2115 | Nooksack River near Lynden | 5.0 | 4.28 | 8.3 |
| 2120 | Fishtrap Creek at Lynden | 5.3 | 4.44 | 10.2 |
| 14-1117 | Butler Creek near Goldendale | 9.2 | 4.23 | 9.4 |
| 1120 | Little Klickitat River near Goldendale | 8.4 | 4.21 | 9.0 |
| 1123 | Spring Creek near Blockhouse | 1.7 | 3.28 | 10.4 |
| 1124 | Mill Creek near Blockhouse | 5.7 | 4.26 | 8.7 |
| 1125 | Little Klickitat River near Wahkiacus | 8.0 | 4.28 | 10.1 |
| 1213 | White Salmon River below Cascades Creek, near Trout Lake | 3.9 | 4.21 | 4.1 |
| 1214 | White Salmon River above Trout Lake Creek, near Trout Lake | 3.5 | 4.29 | 5.1 |
| 1215 | Trout Lake Creek near Trout Lake | 6.9 | 4.30 | 7.1 |
| 1220 | White Salmon River near Trout Lake | 4.7 | 4.28 | 6.0 |
| 1229 | White Salmon River at BZ Corner | 2.7 | 4.43 | 6.1 |
| 1235 | White Salmon River near Underwood | 2.8 | 4.35 | 7.6 |
| 1255 | Little White Salmon River near Cook | 2.0 | 4.38 | 7.1 |
| 1270 | Wind River above Trout Creek, near Carson | 4.3 | 4.15 | 7.8 |
| 1285 | Wind River near Carson | 4.2 | 4.09 | 7.9 |
| 1435 | Washougal River near Washougal | 5.8 | 4.14 | 9.6 |
| 2120 | Salmon Creek near Battle Ground | 5.2 | 4.26 | 9.7 |
| 2132 | Lewis River near Trout Lake | 4.7 | 4.11 | 5.9 |
| 2135 | Big Creek below Skookum Meadow, near Trout Lake | 4.0 | 4.08 | 3.9 |
| 2140 | Rush Creek above Meadow Creek, near Trout Lake | 5.2 | 3.84 | 3.8 |
| 2145 | Meadow Creek below Lone Butte Meadow, near Trout Lake | 2.1 | 4.27 | 3.3 |
| 2150 | Rush Creek above falls, near Cougar | 2.3 | 4.06 | 4.4 |
| 2155 | Curly Creek near Cougar | 2.3 | 4.03 | 4.2 |
| 2160 | Lewis River above Muddy River, near Cougar | 4.4 | 4.18 | 6.1 |
| 2168 | Pine Creek near Cougar | 4.0 | 4.03 | 6.0 |
| 2215 | Cedar Creek near Ariel | 5.6 | 4.36 | 10.5 |
| 2255 | Lake Creek near Packwood | 6.7 | 4.03 | 8.3 |
| 2260 | Lake Creek at mouth, near Packwood | 4.7 | 4.18 | 7.5 |
| 2265 | Cowlitz River at Packwood | 5.5 | 4.18 | 7.5 |
| 2362 | Tilton River above Bear Canyon Creek, near Cinebar | 5.8 | 4.09 | 9.4 |
| 2364 | Cinnabar Creek near Cinebar | 4.3 | 3.98 | 8.0 |
| 2370 | Klickitat Creek at Mossyrock | 6.1 | 4.29 | 11.1 |
| 2375 | Winston Creek near Silver Creek | 5.8 | 4.22 | 9.7 |
| 2390 | Salmon Creek near Toledo | 7.8 | 4.28 | 11.4 |
| 2435 | Delameter Creek near Castle Rock | 5.4 | 4.11 | 10.1 |
| 2482 | Jim Crow Creek near Grays River | 8.1 | 4.16 | 13.1 |
| 2490 | Grays River above South Fork, near Grays River | 5.2 | 4.08 | 9.5 |
| EASTERN WASHINGTON | | | | |
| 12-3960 | Calispell Creek near Dalkena | 8.4 | 4.26 | 8.4 |
| 3965 | Pend Oreille River below Box Canyon, near Ione | 9.1 | 4.10 | 10.2 |
| 3969 | Sullivan Creek above Outlet Creek, near Metaline Falls | 5.2 | 4.13 | 5.2 |
| 3971 | Outlet Creek near Metaline Falls | 7.1 | 4.18 | 9.1 |
| 3980 | Sullivan Creek at Metaline Falls | 6.8 | 3.97 | 7.3 |
| 3985 | Pend Oreille River below Z Canyon, near Metaline Falls | 9.8 | 4.09 | 9.7 |
| 3986 | Pend Oreille River at international boundary | 8.4 | 4.12 | 9.5 |
| 4015 | Kettle River near Ferry | 7.3 | 4.22 | 7.8 |
| 4045 | Kettle River near Laurier | 7.2 | 4.23 | 7.7 |
| 4075 | Sheep Creek at Springdale | 7.2 | 4.53 | 8.5 |
| 4075.2 | Deer Creek near Valley | 7.4 | 4.39 | 8.2 |
| 4077 | Chewelah Creek at Chewelah | 7.4 | 4.29 | 8.6 |
| 4080 | Colville River at Blue Creek | 8.6 | 4.36 | 9.0 |
| 4084.2 | Haller Creek near Arden | 7.3 | 4.43 | 7.5 |
| 4085 | Mill Creek near Colville | 6.4 | 4.26 | 8.2 |

TABLE 8.—Stream-temperature characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Station name | Annual amplitude | Phase coefficient | Mean annual |
|-------------------------------|--|------------------|-------------------|-------------|
| | | (°C) | (radians) | (°C) |
| | | A | C | M |
| EASTERN WASHINGTON--Continued | | | | |
| 12-4087 | Mill Creek at mouth | 7.1 | 4.34 | 9.0 |
| 4090 | Colville River at Kettle Falls | 9.0 | 4.38 | 9.3 |
| 4195 | Spokane River above Liberty Bridge, near O'is Orchards | 9.7 | 4.12 | 10.7 |
| 4225 | Spokane River at Spokane | 7.2 | 4.09 | 10.0 |
| 4240 | Hangman Creek at Spokane | 11.1 | 4.41 | 11.5 |
| 4270 | Little Spokane River at Elk | 9.6 | 4.40 | 9.6 |
| 4310 | Little Spokane River at Dartford | 7.7 | 4.43 | 9.2 |
| 4345 | Sanpoil River near Keller | 8.3 | 4.34 | 8.6 |
| 4394 | Okanogan River at Zosel millpond, at Oroville | 11.8 | 4.17 | 11.0 |
| 4395 | Okanogan River at Oroville | 11.2 | 4.24 | 11.4 |
| 4423 | Sinlahekin Creek above Chopaka Creek, near Loomis | 6.9 | 4.32 | 8.0 |
| 4425 | Similkameen River near Nighthawk | 7.8 | 4.20 | 7.9 |
| 4441 | Whitestone Creek near Tonasket | 9.9 | 4.50 | 10.4 |
| 4450 | Okanogan River near Tonasket | 9.3 | 4.34 | 9.6 |
| 4473 | Okanogan River near Malott | 9.2 | 4.26 | 10.0 |
| 4496 | Beaver Creek below South Fork, near Twisp | 5.8 | 4.31 | 4.7 |
| 4499.5 | Methow River near Pateros | 7.0 | 4.24 | 7.6 |
| 4510 | Stehekin River at Stehekin | 5.5 | 4.16 | 6.2 |
| 4528 | Entiat River near Ardenvoir | 5.4 | 4.34 | 5.4 |
| 4540 | White River near Plain | 4.3 | 4.22 | 4.9 |
| 4570 | Wenatchee River at Plain | 5.7 | 4.10 | 6.9 |
| 4580 | Icicle Creek above Snow Creek, near Leavenworth | 5.3 | 4.31 | 5.5 |
| 4590 | Wenatchee River at Peshastin | 6.6 | 4.18 | 6.9 |
| 4614 | Mission Creek above Sand Creek, near Cashmere | 7.9 | 4.31 | 7.4 |
| 4625 | Wenatchee River at Monitor | 6.9 | 4.28 | 7.4 |
| 4648 | Coal Creek at Mahler | 9.5 | 4.34 | 9.7 |
| 4650 | Crab Creek at Irby | 7.9 | 4.40 | 8.8 |
| 4670 | Crab Creek near Moses Lake | 10.1 | 4.45 | 10.8 |
| 4685 | Park Creek below Park Lake, near Coulee City | 9.2 | 4.30 | 10.4 |
| 4705 | Rocky Ford Creek near Ephrata | 3.4 | 4.33 | 9.0 |
| 4715 | Crab Creek near Warden | 7.3 | 4.42 | 8.9 |
| 4726 | Crab Creek near Beverly | 9.8 | 4.50 | 10.7 |
| 4838 | Naneum Creek near Ellensburg | 6.4 | 4.22 | 5.9 |
| 4885 | American River near Nile | 3.8 | 4.20 | 4.4 |
| 5020 | Ahtanum Creek at The Narrows, near Tappico | 6.6 | 4.16 | 7.1 |
| 5050 | Yakima River near Parker | 7.4 | 4.21 | 10.3 |
| 5105 | Yakima River near Kiona | 9.2 | 4.44 | 11.5 |
| 13-3347 | Asotin Creek below Kearney Gulch, near Asotin | 7.8 | 4.36 | 9.9 |
| 3445 | Tucannon River near Starbuck | 8.5 | 4.43 | 12.2 |
| 3460 | Palouse River near Colfax | 11.9 | 4.50 | 11.0 |
| 3461 | Palouse River at Colfax | 10.6 | 4.37 | 11.1 |
| 3480 | South Fork Palouse River at Pullman | 9.7 | 4.34 | 10.9 |
| 3485 | Missouri Flat Creek at Pullman | 9.5 | 4.46 | 10.8 |
| 3492.1 | Palouse River below South Fork, at Colfax | 10.6 | 4.35 | 11.5 |
| 3494 | Pine Creek at Pine City | 9.1 | 4.47 | 10.0 |
| 3505 | Union Flat Creek near Colfax | 11.1 | 4.54 | 11.3 |
| 3510 | Palouse River at Hooper | 11.1 | 4.40 | 12.6 |
| 3525 | Cow Creek at Hooper | 9.6 | 4.33 | 11.9 |
| 3530 | Snake River below Ice Harbor Dam | 9.9 | 3.96 | 12.5 |

TABLE 8.—*Stream-temperature characteristics, irregularly measured temperature stations, Washington—Continued*

| Station number | Station name | Annual amplitude | Phase coefficient | Mean annual |
|-------------------------------|-------------------------------------|------------------|-------------------|-------------|
| | | (°C) | (radians) | (°C) |
| | | A | C | M |
| EASTERN WASHINGTON--Continued | | | | |
| 14-0130 | Mill Creek near Walla Walla | 5.1 | 4.31 | 8.9 |
| 0135 | Blue Creek near Walla Walla | 6.0 | 4.67 | 9.8 |
| 0160 | Dry Creek near Walla Walla | 8.9 | 4.44 | 11.1 |
| 0165 | East Fork Touchet River near Dayton | 7.1 | 4.32 | 10.1 |
| 0170 | Touchet River at Bolles | 9.8 | 4.44 | 12.2 |
| 0185 | Walla Walla River near Touchet | 10.3 | 4.40 | 12.2 |
| 0343.5 | Alder Creek at Alderdale | 8.7 | 4.46 | 12.7 |
| 0366 | Rock Creek near Roosevelt | 8.7 | 4.32 | 13.9 |

TABLE 9.—*Topographic and climatic drainage-basin characteristics, western Washington thermograph stations*
 [Characteristics given below were significantly related (tested at the 95-percent confidence level) to one or more stream-temperature characteristics. Column P (below): for computation purposes, value of 0.001 is given for basins with no lake or pond areas]

| Station number | Average direction of flow of stream (degrees) | L (miles) | E of basin (ft) | P Lake and pond areas (percent) | D (sq mi) | Q Mean annual discharge (In.) | G Site altitude (ft) | S Source altitude (ft) | F Fall or slope (ft per mile) | T _A Air temperature annual amplitude (°C) | T _M Mean annual air temperature (°C) | Mean monthly air temperature (°C) | | | |
|----------------|---|-----------|-----------------|---------------------------------|-----------|-------------------------------|----------------------|------------------------|-------------------------------|--|---|-----------------------------------|-------------------------|-----------------------|-------------------------|
| | | | | | | | | | | | | T ₁ January | T ₂ February | T ₈ August | T ₁₀ October |
| 12-0115 | 295 | 10.5 | 754 | 0.01 | 41.4 | 59 | 154 | 2,400 | 115 | 6.5 | 10.7 | 4.4 | 4.5 | 14.9 | 12.3 |
| 0275 | 306 | 52 | 800 | .03 | 895 | 42 | 123 | 2,400 | 8.1 | 6.8 | 11.0 | 4.2 | 4.6 | 17.3 | 11.8 |
| 0600 | 137 | 2,505 | 163.4 | .02 | 123 | 456 | 456 | 4,300 | 80.1 | 7.5 | 10.4 | 3.5 | 3.5 | 17.6 | 11.5 |
| 0615 | 144 | 28.9 | 1,370 | .02 | 227 | 80 | 10 | 4,300 | 35.1 | 7.3 | 10.4 | 3.5 | 4.0 | 17.3 | 11.4 |
| 0625 | 10 | 1 | .38 | .001 | 1.3 | 278 | 29 | 200 | 4 | 7.3 | 10.7 | 3.5 | 4.0 | 17.3 | 11.4 |
| 0825 | 252 | 21.2 | 4,020 | .38 | 133 | 75 | 1,450 | 7,000 | 91.2 | 8.3 | 9.1 | .2 | 1.0 | 15.7 | 9.6 |
| 0830 | 324 | 11.3 | 2,740 | .07 | 75.2 | 46 | 1,340 | 4,240 | 155.2 | 8.3 | 10.0 | 1.5 | 2.0 | 16.0 | 9.9 |
| 1130 | 288 | 59.4 | 2,400 | .60 | 399.4 | 47.4 | 60 | 4,300 | 26 | 7.3 | 11.5 | 3.8 | 4.1 | 19.0 | 13.0 |
| 1175 | 280 | 27.6 | 2,400 | 2.17 | 122 | 77.2 | 600 | 3,000 | 38.9 | 7.3 | 9.5 | 2.7 | 3.0 | 11.0 | 11.0 |
| 1350 | 262 | 9.4 | 2,660 | .79 | 19 | 102 | 200 | 4,500 | 31.9 | 7.5 | 11.4 | 3.8 | 4.2 | 18.4 | 12.5 |
| 1640 | 247 | 17.4 | 1,400 | .82 | 46.2 | 54.8 | 110 | 4,240 | 158 | 7.8 | 10.6 | 2.5 | 3.5 | 15.9 | 11.8 |
| 1655 | 252 | 18.5 | 2,340 | .001 | 82.2 | 90 | 410 | 4,200 | 189 | 8.6 | 9.9 | 1.0 | 1.8 | 17.9 | 11.0 |
| 1685 | 225 | 15.5 | 1,290 | 2.6 | 52 | 67.8 | 140 | 1,205 | 81.7 | 7.2 | 10.7 | 2.5 | 3.8 | 17.2 | 13.1 |
| 1790 | 210 | 40.4 | 5,000 | 5.0 | 1,274 | 6,090 | 358 | 2,500 | 69 | 9.5 | 10.8 | 1.5 | 2.0 | 18.6 | 12.2 |
| 1825 | 297 | 2.4 | 4,400 | .17 | 168 | 81.1 | 380 | 8,261 | 107 | 9.3 | 10.4 | 1.2 | 1.5 | 19.2 | 11.8 |
| 2005 | 270 | 94.8 | 1,250 | 3.0 | 3,093 | 72.1 | 43 | 2,500 | 34.4 | 6.7 | 10.5 | 3.8 | 4.2 | 17.0 | 12.0 |
| 14-1100 | 179 | 37.6 | 4,520 | .28 | 36.0 | 30.8 | 1,703 | 8,200 | 47.9 | 10.2 | 8.7 | -1.0 | -0.5 | 18.2 | 11.1 |
| 1130 | 204 | 88.1 | 3,140 | .09 | 1,297 | 16.7 | 283 | 8,200 | 44.8 | 10.2 | 10.8 | .5 | 2.0 | 20.2 | 12.5 |
| 2205 | 247 | 71.0 | 1,788 | 11.8 | 731 | 88.7 | 367 | 12,310 | 43.8 | 7.6 | 11.3 | 3.5 | 4.0 | 18.5 | 13.1 |
| 2225 | 282 | 21.5 | 1,940 | .01 | 125 | 81 | 367 | 3,840 | 93.4 | 7.7 | 11.0 | 3.5 | 3.7 | 16.4 | 12.9 |
| 2235 | 260 | .01 | 1,880 | .01 | 198 | 84.1 | 20 | 5,670 | 80.3 | 7.2 | 10.9 | 3.1 | 4.3 | 17.6 | 11.6 |
| 2325 | 284 | 30 | 4,130 | .15 | 321 | 56 | 1,222 | 7,300 | 117.3 | 8.5 | 10.5 | 2.4 | 1.8 | 18.8 | 13.3 |
| 2335 | 252 | 56.2 | 1,042 | .65 | 1,042 | 65.2 | 1,550 | 9,364 | 36.6 | 7.9 | 10.4 | 3.8 | 2.5 | 18.2 | 12.1 |
| 2355 | 157 | 6.5 | 2,450 | .12 | 16.4 | 93.8 | 1,150 | 4,220 | 33.2 | 8.2 | 10.6 | 3.0 | 3.3 | 17.0 | 10.7 |
| 2380 | 271 | 93.5 | 3,150 | .15 | 1,400 | 59.2 | 427 | 9,360 | 42.8 | 7.9 | 10.5 | 3.5 | 3.5 | 18.0 | 12.0 |
| 2425 | 278 | 40.1 | 2,310 | .93 | 474 | 57.4 | 407 | 5,200 | 87.1 | 7.4 | 10.5 | 3.1 | 3.3 | 18.1 | 12.5 |
| 2430 | 172 | 127 | 2,540 | .26 | 2,238 | 55.0 | 20.2 | 9,364 | 10.8 | 7.4 | 10.9 | 3.4 | 3.8 | 17.9 | 12.2 |
| 2450 | 263 | 25.7 | 1,390 | .08 | 119 | 45.6 | 100 | 3,920 | 62.8 | 7.3 | 10.8 | 3.7 | 4.3 | 17.3 | 11.6 |
| 2460 | 151 | 9.0 | 1,120 | .01 | 20.3 | 64.6 | 70 | 1,840 | 168.8 | 7.1 | 10.5 | 3.7 | 4.3 | 17.2 | 11.5 |
| 2475 | 208 | 16.5 | 1,190 | .01 | 69.8 | 75 | 29.7 | 1,920 | 60.8 | 6.9 | 10.5 | 3.8 | 4.3 | 17.2 | 11.3 |
| 2505 | 176 | 6.5 | 1,180 | .01 | 15.2 | 96.7 | 71 | 2,632 | 187 | 6.9 | 10.5 | 3.8 | 3.8 | 17.1 | 12.3 |

B40 CONTRIBUTIONS TO THE HYDROLOGY OF THE UNITED STATES

TABLE 10.—*Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington*

[Characteristics given below were significantly related (tested at the 95-percent confidence level) to one or more stream-temperature characteristics. Column P (below): for computation purposes, value of 0.001 is given for basins with no lake or pond areas]

| Station number | Characteristic | | | | | | | | | | |
|--------------------|---|--------------------------|------------------------------|-------------------------------|-----------------------|-----------------------------|--------------------|----------------------|--------------------------------------|---------------------------------------|----------------------------------|
| | Average direction of flow of stream (degrees) | Length of river. (miles) | Mean altitude of basin (ft.) | Lake and pond areas (percent) | Drainage area (sq mi) | Mean annual discharge (in.) | Site altitude (ft) | Source altitude (ft) | Fall or slope of river (ft per mile) | Air temperature annual amplitude (°C) | Mean annual air temperature (°C) |
| | Q | L | E | P | D | Q | G | S | F | T _A | T _M |
| WESTERN WASHINGTON | | | | | | | | | | | |
| 12-0095 | 297 | 7.3 | 494 | 0.001 | 11.7 | 72 | 15 | 800 | 77 | 6.5 | 10.3 |
| 0100 | 225 | 18.6 | 910 | .01 | 54.8 | 106 | 24 | 2,650 | 75.3 | 6.7 | 10.4 |
| 0105 | 229 | 13.5 | 480 | .01 | 16.4 | 87.2 | 80 | 2,150 | 51.8 | 6.7 | 10.4 |
| 0107 | 357 | 5.7 | 348 | .001 | 17.9 | 76 | 20 | 400 | 30.4 | 6.7 | 10.4 |
| 0110 | 307 | 7.4 | 689 | .01 | 18 | 84 | 60 | 700 | 58.6 | 6.3 | 10.5 |
| 0112 | 270 | 7.3 | 666 | .001 | 9.4 | 74.2 | 60 | 1,760 | 115 | 6.2 | 10.5 |
| 0120 | 322 | 8.4 | 738 | .001 | 20.4 | 95.8 | 155 | 2,250 | 216 | 6.5 | 10.7 |
| 0135 | 275 | 25.2 | 641 | .01 | 130 | 66.1 | 5.7 | 2,400 | 18 | 6.3 | 10.9 |
| 0145 | 91 | 13.3 | 585 | .001 | 27.8 | 78.6 | 155 | 1,760 | 48 | 6.2 | 10.9 |
| 0151 | 20 | 3 | 622 | .001 | 4.0 | 74 | 150 | 1,040 | 222 | 6.0 | 10.8 |
| 0152 | 255 | 16.5 | 424 | .01 | 57.7 | 54.9 | 100 | 1,120 | 12 | 6.0 | 10.8 |
| 0155 | 244 | 6.9 | 660 | .001 | 29.8 | 51.4 | 190 | 1,680 | 188 | 6.3 | 10.9 |
| 0170 | 280 | 22 | 250 | .01 | 219 | 59.5 | 7 | 1,680 | 20 | 6.0 | 10.4 |
| 0200 | 2 | 21.5 | 1,000 | .01 | 113 | 68.4 | 302 | 2,400 | 55 | 6.7 | 10.9 |
| 0210 | 1 | 19.8 | 830 | .001 | 48 | 53.3 | 255 | 1,840 | 40 | 7.0 | 11.0 |
| 0240 | 230 | 14.4 | 1,280 | .1 | 42.4 | 63.4 | 540 | 3,760 | 167 | 7.7 | 10.7 |
| 0245 | 260 | 12.4 | 1,220 | .001 | 31.5 | 45.2 | 380 | 2,560 | 96 | 7.5 | 10.8 |
| 0250 | 261 | 31.4 | 900 | .02 | 155 | 42.5 | 190 | 3,760 | 46 | 7.0 | 11.1 |
| 0260 | 288 | 17.6 | 1,700 | .01 | 61.7 | 55.4 | 300 | 3,440 | 92 | 7.6 | 11.0 |
| 0300 | 98 | 7.2 | 525 | .01 | 24.8 | 44.1 | 70 | 791 | 80 | 6.4 | 10.9 |
| 0310 | 188 | 83.6 | 700 | .12 | 1,294 | 40.3 | 25 | 2,400 | 8 | 6.4 | 10.9 |
| 0325 | 215 | 14.3 | 410 | .63 | 64.9 | 50.0 | 20 | 480 | 25 | 6.6 | 10.8 |
| 0342 | 212 | 15.2 | 650 | .95 | 65.9 | 75.2 | 205 | 2,890 | 32 | 6.9 | 10.6 |
| 0350 | 193 | 28 | 500 | .25 | 299 | 91.8 | 30 | 2,890 | 19 | 6.7 | 10.8 |
| 0354 | 195 | 14.4 | 2,074 | .01 | 41.4 | 162.7 | 640 | 4,050 | 122 | 8.5 | 10.5 |
| 0360 | 200 | 23.6 | 2,000 | .001 | 74.1 | 161.5 | 492 | 4,050 | 63 | 7.8 | 10.2 |
| 0374 | 191 | 55.8 | 900 | .01 | 155 | 109 | 40 | 4,050 | 19 | 6.8 | 10.9 |
| 0390 | 217 | 35.4 | 1,000 | .01 | 130 | 133 | 117 | 3,360 | 25 | 6.0 | 9.8 |
| 0393 | 207 | 13 | 3,280 | .08 | 74.1 | 146 | 620 | 5,300 | 250 | 9.5 | 11.1 |
| 0395 | 232 | 36.5 | 2,700 | 2.08 | 264 | 144 | 185 | 7,320 | 64 | 8.0 | 10.8 |
| 0410 | 260 | 33.5 | 3,000 | .21 | 208 | 131.2 | 320 | 7,700 | 72 | 7.0 | 10.2 |
| 0412 | 263 | 43.4 | 2,620 | .17 | 253 | 131.4 | 164 | 7,700 | 68 | 6.5 | 10.0 |
| 0415 | 313 | 16.9 | 2,900 | .48 | 83.8 | 98.9 | 1,060 | 5,400 | 146 | 7.5 | 9.9 |
| 0430 | 234 | 15.5 | 532 | .16 | 39.8 | 87.1 | 70 | 1,920 | 31 | 5.5 | 9.6 |
| 0431 | 220 | 1.8 | 440 | 1.2 | 86.3 | 83.2 | 50 | 800 | 12 | 5.5 | 9.6 |
| 0433 | 8 | 18.4 | 805 | .001 | 51.2 | 92.2 | 50 | 2,300 | 30 | 5.0 | 8.5 |
| 0434 | 10 | 6.5 | 1,280 | .001 | 14 | 60.8 | 10 | 3,700 | 297 | 7.3 | 9.7 |
| 0455 | 344 | 34.4 | 3,700 | .23 | 269 | 74.4 | 200 | 5,200 | 69 | 7.5 | 10.3 |
| 0475 | 359 | 8.8 | 1,550 | .01 | 15.5 | 17 | 225 | 5,450 | 321 | 5.7 | 9.5 |
| 0480 | 40 | 20 | 4,500 | .06 | 156 | 33.3 | 569 | 7,000 | 187 | 6.6 | 9.8 |
| 0505 | 91 | 6.6 | 1,800 | .001 | 11.2 | 19.5 | 220 | 3,050 | 388 | 7.0 | 10.0 |
| 0540 | 85 | 19.5 | 4,100 | .30 | 66.5 | 83.8 | 241 | 5,000 | 159 | 7.7 | 10.4 |
| 0545 | 73 | 11.5 | 3,830 | .50 | 51.3 | 91.1 | 510 | 5,200 | 377 | 7.9 | 10.5 |
| 0546 | 64 | 9.7 | 2,660 | .43 | 21.6 | 86.8 | 500 | 5,100 | 412 | 7.9 | 10.5 |
| 0565 | 147 | 12.8 | 3,700 | .17 | 57.2 | 115 | 762 | 6,400 | 177 | 8.3 | 10.7 |
| 0595 | 195 | 6.7 | 2,665 | .10 | 18 | -- | 64 | 320 | 22 | 7.4 | 10.5 |
| 0598 | 134 | 8.5 | 1,920 | .24 | 26 | 146.7 | 750 | 4,100 | 220 | 8.4 | 10.6 |
| 0605 | 135 | 24 | 2,100 | .25 | 76.3 | 119 | 110 | 4,100 | 63 | 7.4 | 10.5 |
| 0626 | 10 | -- | -- | .001 | 2.42 | -- | 40 | 420 | -- | 7.3 | 10.6 |
| 0655 | 206 | 1.5 | 1,120 | .01 | 1.51 | 49 | 751 | 880 | 36 | 7.6 | 11.1 |

TABLE 10.—Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Characteristic | | | | | | | | | | |
|-------------------------------|---|--------------------------|-----------------------------|-------------------------------|-----------------------|-----------------------------|--------------------|----------------------|--------------------------------------|---------------------------------------|----------------------------------|
| | Average direction of flow of stream (degrees) | Length of river, (miles) | Mean altitude of basin (ft) | Lake and pond areas (percent) | Drainage area (sq mi) | Mean annual discharge (in.) | Site altitude (ft) | Source altitude (ft) | Fall or slope of river (ft per mile) | Air temperature annual amplitude (°C) | Mean annual air temperature (°C) |
| | Ø | L | E | P | D | Q | G | S | F | T _A | T _M |
| WESTERN WASHINGTON--Continued | | | | | | | | | | | |
| 12-0685 | 226 | 7.6 | 376 | 0.71 | 18.4 | 48.7 | 55 | 440 | 36 | 7.5 | 10.8 |
| 0700 | 178 | 3.0 | 289 | .001 | 5.01 | 16.1 | 20 | 170 | 49 | 7.3 | 11.1 |
| 0720 | 85 | 6.1 | 400 | 9.5 | 15.3 | 27.6 | 50 | 900 | 100 | 7.7 | 11.2 |
| 0730 | 180 | 5.3 | 250 | .001 | 10 | -- | 10 | 300 | 43 | 7.0 | 11.6 |
| 0735 | 150 | 7.5 | 316 | .21 | 6.5 | 24.1 | 100 | 460 | 55 | 7.0 | 11.5 |
| 0765 | 82 | 7.5 | 420 | 1.0 | 39.3 | 34.6 | 205 | 480 | 32 | 7.1 | 10.7 |
| 0784 | 61 | 9.7 | 700 | 4.85 | 17.4 | 46.9 | 110 | 720 | 60 | 6.9 | 10.6 |
| 0790 | 311 | 25.9 | 1,340 | .63 | 89.8 | 38.0 | 350 | 3,280 | 17 | 7.6 | 11.3 |
| 0800 | 303 | 45.9 | 950 | 1.10 | 160 | 34.7 | 95 | 3,280 | 30 | 6.8 | 10.5 |
| 0810 | 335 | 9.0 | 189 | 6.93 | 24.6 | 14.5 | 25 | 325 | 12 | 7.0 | 10.8 |
| 0865 | 285 | 37.7 | 3,200 | 1.79 | 292 | 65 | 490 | 7,000 | 85 | 8.4 | 10.5 |
| 0880 | 230 | 6 | 1,600 | .61 | 34.5 | 26.3 | 520 | 580 | 6 | 8.4 | 10.0 |
| 0895 | 295 | 54.9 | 2,740 | 1.48 | 517 | -- | 275 | 7,000 | 62 | 7.5 | 11.4 |
| 0902 | 268 | 6.7 | 350 | 1.0 | 86.8 | 9.8 | 310 | 425 | 8 | 7.2 | 11.4 |
| 0910 | 270 | -- | 400 | 2.1 | 90.4 | 12.4 | 140 | 500 | -- | 7.0 | 11.8 |
| 0911 | 180 | -- | -- | -- | 8.01 | 12.3 | 200 | -- | -- | 7.5 | 12.0 |
| 0913 | 270 | -- | -- | -- | 5.88 | 21.9 | 140 | -- | -- | 7.5 | 12.0 |
| 0915 | 265 | -- | 385 | 1.75 | 104 | 14.7 | 100 | 500 | -- | 7.5 | 12.0 |
| 0920 | 304 | 20.2 | 4,100 | .54 | 92.8 | 77.7 | 1,640 | 10,300 | 224 | 8.1 | 8.0 |
| 0935 | 316 | 23.5 | 3,000 | .82 | 172 | 54.7 | 358 | 10,300 | 182 | 7.4 | 10.6 |
| 0940 | 287 | 16.8 | 400 | .16 | 78.9 | 72.6 | 1,213 | 9,200 | 394 | 7.5 | 9.5 |
| 0944 | 312 | 6.6 | 3,650 | .41 | 22.4 | 62.8 | 1,420 | 5,600 | 414 | 7.7 | 9.5 |
| 0950 | 302 | 16.5 | 2,300 | .64 | 79.5 | 38.5 | 430 | 5,600 | 174 | 7.2 | 10.4 |
| 0966 | 50 | 8.4 | 7,100 | .003 | 16.2 | 95.1 | 3,8 ² | 14,408 | 1,000 | 9.6 | 5.3 |
| 0970 | 355 | 31.1 | 4,700 | .46 | 216 | 53 | 1,725 | 14,408 | 151 | 9.4 | 7.4 |
| 0975 | 302 | 20.2 | 4,200 | .27 | 73.5 | 38 | 1,725 | 6,130 | 129 | 9.5 | 7.4 |
| 0985 | 310 | 48.7 | 3,800 | .30 | 401 | 49.5 | 790 | 14,408 | 83 | 7.5 | 10.0 |
| 0993 | 275 | 4.5 | 2,260 | .001 | 4.6 | -- | 1,435 | 3,840 | 462 | 7.7 | 9.8 |
| 0994 | 275 | 6.5 | 1,800 | .75 | 8.3 | -- | 1,000 | 3,840 | 390 | 7.7 | 9.8 |
| 0995 | 273 | 9.2 | 1,480 | .51 | 12.3 | -- | 740 | 3,840 | 238 | 7.4 | 10.0 |
| 1005 | 306 | 71.2 | 3,326 | 2.2 | 470 | 18.1 | 58 | 14,408 | 60 | 6.9 | 10.5 |
| 1015 | 311 | 41.8 | 2,500 | .31 | 948 | 47.7 | 20 | 10,300 | 78 | 6.9 | 10.5 |
| 1034 | 17 | 8.0 | 3,680 | .001 | 34.8 | 52.8 | 1,800 | 5,520 | 615 | 9.5 | 4.6 |
| 1035 | 230 | 3.7 | 3,370 | .03 | 11.5 | 71.3 | 1,950 | 3,840 | 476 | 9.0 | 4.3 |
| 1040 | 185 | 3.1 | 3,190 | .02 | 4.67 | 79.0 | 1,760 | 4,440 | 757 | 8.8 | 4.2 |
| 1045 | 285 | 15 | 3,190 | .02 | 96.2 | 50.9 | 1,480 | 5,520 | 259 | 9.3 | 4.3 |
| 1047 | 187 | 3 | 2,950 | .001 | 3.23 | 52.1 | 1,480 | 4,100 | 818 | 9.0 | 4.2 |
| 1050 | 60 | 4.6 | 3,220 | .001 | 8.56 | 81.3 | 1,900 | 4,040 | 500 | 9.5 | 4.4 |
| 1057 | 200 | 8.1 | 2,890 | .78 | 16.5 | 68.5 | 1,250 | 4,160 | 250 | 7.5 | 9.6 |
| 1059 | 293 | 14.7 | -- | -- | 221 | 62.8 | 990 | 5,520 | 176 | 7.5 | 9.6 |
| 1067 | 292 | 35.9 | 3,100 | .09 | 231 | 50.9 | 860 | 5,520 | 118 | 7.2 | 9.7 |
| 1073 | 175 | .4 | -- | -- | .1 | -- | 540 | 640 | .2 | 6.9 | 10.0 |
| 1085 | 331 | 12.8 | 883 | .01 | 27.4 | 32.5 | 310 | 2,860 | 82 | 6.9 | 10.0 |
| 1126 | 256 | 13.5 | 450 | 1.7 | 66.7 | 23 | 70 | 420 | 25 | 7.0 | 11.3 |
| 1133 | 303 | 63 | -- | -- | 440 | 45.1 | 22 | 5,520 | 37 | 7.1 | 11.2 |
| 1135 | 254 | 3.7 | 3,830 | .01 | 9.3 | 105.3 | 2,360 | 3,600 | 317 | 8.8 | 5.8 |
| 1140 | 342 | 4 | 3,500 | .01 | 6.0 | 85.6 | 2,300 | 4,500 | 317 | 8.7 | 5.8 |
| 1145 | 300 | 7.1 | 3,460 | .01 | 25.4 | 96.1 | 1,880 | 3,600 | 189 | 8.6 | 7.2 |
| 1150 | 299 | 12.2 | 3,230 | 1.43 | 40.7 | 83.2 | 1,560 | 3,600 | 116 | 8.4 | 7.8 |
| 1155 | 321 | 6.4 | 3,360 | .001 | 13.4 | 100 | 1,700 | 4,500 | 386 | 8.2 | 8.1 |

TABLE 10.—*Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington—Continued*

| Station number | Characteristic | | | | | | | | | | |
|-------------------------------|---|---------------------------|-----------------------------|-------------------------------|-----------------------|-----------------------------|--------------------|----------------------|--------------------------------------|---------------------------------------|----------------------------------|
| | Average direction of flow of stream (degrees) | Length of river, in miles | Mean altitude of basin (ft) | Lake and pond areas (percent) | Drainage area (sq mi) | Mean annual discharge (in.) | Site altitude (ft) | Source altitude (ft) | Fall or slope of river (ft per mile) | Air temperature annual amplitude (°C) | Mean annual air temperature (°C) |
| | Ø | L | E | P | D | Q | G | S | F | T _A | T _M |
| WESTERN WASHINGTON--Continued | | | | | | | | | | | |
| 12-1165 | 302 | 21.7 | 2,800 | 3.26 | 84.2 | 50.3 | 910 | 3,600 | 58 | 7.4 | 8.7 |
| 1170 | 350 | 8.2 | 2,300 | .001 | 17.2 | 81.3 | 940 | 3,600 | 289 | 7.3 | 9.3 |
| 1185 | 5 | 7.2 | 690 | .08 | 12.6 | 22.5 | 425 | 860 | 37 | 7.5 | 10.4 |
| 1190 | 289 | 53.1 | 1,790 | 1.64 | 186 | 51.2 | 15.2 | 3,600 | 41 | 7.2 | 11.1 |
| 1196 | 298 | 8.4 | 550 | .006 | 12.7 | 23.8 | 25 | 1,450 | 41 | 6.9 | 11.2 |
| 1197 | 312 | 6.4 | 770 | .001 | 6.8 | 25.1 | 50 | 1,300 | 221 | 6.8 | 11.3 |
| 1200 | 202 | 3.9 | 305 | .001 | 12 | 22.5 | 20 | 380 | 65 | 7.0 | 11.4 |
| 1205 | 240 | 3.2 | 235 | .001 | 6.43 | 22.9 | 20 | 460 | 83 | 7.0 | 11.3 |
| 1210 | 312 | 10 | 940 | .37 | 27 | 34.8 | 210 | 2,700 | 153 | 7.3 | 10.5 |
| 1216 | 335 | 15.7 | 930 | .37 | 54.7 | 29.5 | 40 | 2,700 | 92 | 7.2 | 11.0 |
| 1230 | 178 | 7.5 | 375 | 1.78 | 10.7 | 17.2 | 210 | 600 | 42 | 7.0 | 11.1 |
| 1240 | 240 | 8.6 | 365 | .07 | 13.0 | 22.6 | 50 | 640 | 74 | 7.2 | 11.1 |
| 1252 | 339 | 29.1 | 58.2 | 5.44 | 15.7 | 28.7 | 20 | 2,700 | 24 | 7.0 | 11.2 |
| 1255 | 189 | 9.2 | 358 | .001 | 15.3 | 21.2 | 30 | 490 | 47 | 7.0 | 11.2 |
| 1260 | 173 | 9.9 | 390 | 2.14 | 24.6 | 18.8 | 70 | 550 | 49 | 7.4 | 11.2 |
| 1265 | 331 | 34.3 | 500 | 4.24 | 212 | 23.5 | 17 | 2,700 | 16 | 7.5 | 11.2 |
| 1270 | 172 | 13.5 | 394 | .61 | 23.1 | 22.8 | 3 | 600 | 43 | 7.5 | 11.3 |
| 1280 | 95 | 6.5 | 312 | .15 | 12.1 | 12.9 | 40 | 440 | 65 | 7.5 | 11.5 |
| 1330 | 292 | 27.9 | 3,800 | .90 | 355 | 92.9 | 575 | 4,950 | 88 | 8.0 | 11.4 |
| 1345 | 282 | 36 | 3,700 | .73 | 535 | 99.4 | 209 | 4,950 | 63 | 7.6 | 11.4 |
| 1375 | 262 | 18.3 | 3,120 | .40 | 74.5 | 143 | 750 | 4,250 | 94 | 7.7 | 11.3 |
| 1410 | 169 | 14.2 | 625 | 1.19 | 56.4 | 35.1 | 100 | 440 | 25 | 7.2 | 10.8 |
| 1413 | 263 | 29.6 | 3,710 | 1.3 | 154 | 110 | 780 | 6,020 | 117 | 8.0 | 8.0 |
| 1420 | 232 | 17.3 | 3,200 | .78 | 64 | 109 | 1,130 | 5,700 | 85 | 7.8 | 10.5 |
| 1430 | 213 | 24.2 | 3,100 | 1.67 | 95.7 | 89.8 | 470 | 5,700 | 68 | 7.5 | 9.5 |
| 1434 | 283 | 13.7 | 3,420 | .31 | 41.6 | 99.6 | 1,480 | 5,450 | 155 | 8.5 | 7.2 |
| 1436 | 294 | 21.7 | 3,330 | .30 | 65.9 | -- | 577 | 5,450 | 107 | 7.5 | 8.0 |
| 1440 | 296 | 27.2 | 2,900 | .51 | 81.7 | 89.4 | 432 | 5,450 | 102 | 7.2 | 9.0 |
| 1445 | 267 | 44.8 | 3,300 | 1.14 | 375 | 91.4 | 120 | 6,020 | 72 | 7.5 | 10.5 |
| 1455 | 345 | 12.5 | 1,460 | .01 | 30.6 | 65.3 | 250 | 3,000 | 179 | 7.4 | 10.5 |
| 1460 | 130 | 7.1 | 410 | .001 | 15.5 | 28.2 | 70 | 560 | 74 | 7.4 | 10.7 |
| 1470 | 245 | 10.8 | 781 | .24 | 17.1 | 31.1 | 120 | 1,580 | 53 | 7.6 | 10.7 |
| 1475 | 254 | 15.2 | 2,590 | .001 | 39.9 | 140 | 600 | 5,640 | 10.6 | 7.7 | 10.8 |
| 1480 | 273 | 3.9 | 2,940 | .03 | 19.7 | 140.5 | 1,300 | 2,980 | 294 | 8.0 | 11.0 |
| 1485 | 260 | 18.3 | 2,300 | .12 | 81.4 | 112 | 348 | 5,640 | 111 | 7.6 | 10.6 |
| 1487 | 182 | 5.5 | 790 | 2.7 | 5.58 | 40.4 | 340 | 580 | 27 | 7.5 | 10.6 |
| 1490 | 275 | 60.8 | 2,400 | .7 | 603 | 86 | 50 | 6,020 | 40 | 7.5 | 10.6 |
| 1505 | 196 | 8.2 | 2,800 | 2.0 | 19.2 | 38.6 | 90 | 950 | 98 | 7.2 | 10.7 |
| 1508 | 280 | 58.2 | -- | -- | 1,537 | 89.0 | 13.2 | 4,950 | 21 | 7.1 | 10.8 |
| 1530 | 185 | 8.7 | 376 | .09 | 17 | 22.6 | 200 | 560 | 40 | 7.8 | 11.2 |
| 1570 | 260 | 5.4 | 220 | .01 | 15.4 | 22.7 | 28.2 | 395 | 8 | 7.7 | 10.9 |
| 1610 | 282 | 33.2 | 2,600 | .08 | 119 | 122 | 310 | 6,610 | 62 | 8.1 | 10.6 |
| 1650 | 348 | 10.2 | 2,530 | .01 | 20 | 122 | 490 | 6,600 | 308 | 8.6 | 9.8 |
| 1670 | 279 | 40 | 2,300 | .01 | 262 | 91.3 | 89 | 3,210 | 35 | 7.6 | 10.5 |
| 1720 | 120 | 16 | 4,400 | .01 | 63.2 | 112 | 1,600 | 3,900 | 140 | 9.6 | 9.9 |
| 1735 | 271 | 14.1 | 5,700 | .05 | 206 | 42.5 | 1,640 | 6,690 | 285 | 9.8 | 9.8 |
| 1755 | 339 | 14.4 | 5,800 | .10 | 105 | 84.6 | 1,220 | 6,330 | 274 | 9.4 | 10.0 |
| 1775 | 137 | 7.7 | 5,000 | .10 | 22 | 112 | 925 | 6,640 | 500 | 9.4 | 10.3 |
| 1780 | 240 | 32.7 | 5,000 | 2.21 | 1,175 | 51.6 | 402 | 2,500 | 68 | 9.8 | 10.9 |
| 1781 | 352 | 7.3 | 4,140 | .31 | 27.9 | 85.1 | 1,080 | 7,280 | 663 | 9.8 | 10.9 |

TABLE 10.—Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Characteristic | | | | | | | | | | |
|------------------------------|---|--------------------------|-----------------------------|-------------------------------|-----------------------|-----------------------------|--------------------|----------------------|--------------------------------------|---------------------------------------|----------------------------------|
| | Average direction of flow of stream (degrees) | Length of river, (miles) | Mean altitude of basin (ft) | Lake and pond areas (percent) | Drainage area (sq mi) | Mean annual discharge (in.) | Site altitude (ft) | Source altitude (ft) | Fall or slope of river (ft per mile) | Air temperature annual amplitude (°C) | Mean annual air temperature (°C) |
| | θ | L | E | P | D | Q | G | S | F | T _A | T _M |
| WESTERN WASHINGTON—Continued | | | | | | | | | | | |
| 12-1860 | 319 | 19.8 | 3,700 | 0.13 | 152 | 100 | 930 | 7,360 | 84 | 8.9 | 9.5 |
| 1895 | 329 | 44.4 | 3,900 | .01 | 714 | 82.9 | 266 | 7,360 | 40 | 9.1 | 10 |
| 1918 | 310 | 8.5 | 4,350 | .001 | 8.36 | 76.2 | 1,750 | 9,700 | 866 | 8.7 | 9.4 |
| 1935 | 190 | 32.8 | -- | 1.52 | 297 | 120 | 173 | 8,240 | 51 | 8.0 | 10.4 |
| 1940 | 297 | 69.4 | 4,100 | 1.23 | 1,737 | 74.7 | 130 | 2,500 | 27 | 7.9 | 10.4 |
| 1960 | 195 | 6.5 | 1,280 | .001 | 10.7 | 42.9 | 125 | 1,350 | 197 | 7.4 | 10.4 |
| 1962 | 332 | 4.0 | 2,610 | 3.81 | 6.6 | 123.2 | 1,600 | 4,320 | 240 | 7.4 | 10.5 |
| 1964 | 332 | 9.9 | 2,350 | .77 | 32.3 | 114.9 | 140 | 4,320 | 187 | 7.1 | 10.4 |
| 1998 | 260 | 3.8 | 2,700 | .003 | 3.56 | 87.7 | 1,700 | 4,000 | 456 | 6.9 | 10.5 |
| 2015 | 218 | 19.6 | 580 | 1.82 | 87.8 | 36 | 45 | 1,650 | 19 | 6.5 | 10.3 |
| 2050 | 280 | 17.6 | 4,300 | .19 | 105 | 97.9 | 1,245 | 6,400 | 106 | 6.7 | 10.0 |
| 2072 | 272 | 36.7 | 3,270 | .18 | 282 | 74.2 | 345 | 6,400 | 71 | 7.8 | 10.2 |
| 2080 | 280 | 16.8 | 3,640 | .06 | 73.3 | 90.8 | 580 | 10,500 | 344 | 7.6 | 9.5 |
| 2090 | 283 | 25.8 | 3,000 | .29 | 103 | 95.9 | 385 | 5,300 | 58 | 7.0 | 9.9 |
| 2095 | 258 | 9.5 | 3,020 | .09 | 23.1 | 78.7 | 400 | 5,600 | 334 | 6.9 | 9.9 |
| 2105 | 288 | 43.1 | 3,000 | .24 | 584 | 77.5 | 204 | 6,400 | 62 | 7.5 | 9.5 |
| 2115 | 291 | 63.1 | -- | -- | 648 | 77.2 | 24.4 | 6,400 | 41 | 7.4 | 10 |
| 2120 | 230 | 8.2 | 154 | 1.26 | 22.3 | 18.1 | 110 | 260 | 23 | 7.2 | 9.7 |
| 14-1117 | 138 | 9.7 | 3,620 | .001 | 11.6 | 15.3 | 2,200 | 5,100 | 256 | 10.1 | 9.4 |
| 1120 | 219 | 15.6 | 3,160 | .01 | 83.5 | 11.2 | 1,690 | 4,600 | 131 | 9.8 | 9.5 |
| 1123 | 180 | 4.2 | 2,160 | .001 | 2.75 | 68.9 | 1,620 | 2,170 | 105 | 9.7 | 9.3 |
| 1124 | 210 | 12.4 | 3,230 | .23 | 26.9 | 4.5 | 1,600 | 5,600 | 241 | 9.7 | 9.2 |
| 1125 | 254 | 31.6 | 2,600 | .04 | 280 | 8.5 | 570 | 4,600 | 45 | 9.8 | 9.0 |
| 1213 | 201 | 10 | 5,190 | .003 | 32.4 | 61.1 | 3,080 | 7,900 | 477 | 10 | 9.7 |
| 1214 | 166 | 17 | 4,500 | .001 | 64.9 | 49.3 | 2,050 | 7,900 | 267 | 9.8 | 9.5 |
| 1215 | 132 | 15 | 3,450 | .54 | 69.3 | 51.7 | 2,000 | 3,950 | 149 | 9.8 | 9.6 |
| 1220 | 145 | 20.9 | 3,940 | .20 | 185 | 28 | 1,780 | 7,900 | 210 | 9.8 | 9.3 |
| 1229 | 171 | 32 | 3,470 | .14 | 269 | 40.9 | 705 | 7,900 | 133 | 9.6 | 9.5 |
| 1235 | 181 | 42.5 | 3,220 | .26 | 386 | 39.6 | 113 | 7,900 | 106 | 9.4 | 9.4 |
| 1255 | 179 | 16.5 | 2,750 | .23 | 134 | 52.8 | 150 | 4,240 | 126 | 8.9 | 9.4 |
| 1270 | 170 | 17.7 | 2,740 | .03 | 108 | 65.5 | 890 | 3,050 | 111 | 8.6 | 10.2 |
| 1285 | 145 | 27.7 | 2,460 | .03 | 225 | 69.2 | 113 | 3,050 | 66 | 8.6 | 9.9 |
| 1435 | 241 | 22.2 | 1,610 | .01 | 108 | 100 | 175 | 3,440 | 66 | 7.6 | 10.5 |
| 2120 | 328 | 4.9 | 1,000 | .01 | 18.3 | 43.3 | 355 | 2,225 | 313 | 7.5 | 10.8 |
| 2132 | 234 | 22 | 3,950 | .002 | 127 | 73 | 1,500 | 12,377 | 300 | 9.7 | 10.7 |
| 2135 | 271 | 6 | 3,780 | .01 | 132 | 61 | 3,213 | 4,700 | 167 | 9.6 | 10.7 |
| 2140 | 300 | 5.4 | 4,490 | 3.1 | 5.9 | 55.7 | 3,400 | 4,750 | 346 | 9.5 | 10.7 |
| 2145 | 358 | 6 | 3,980 | 2.1 | 11.7 | 108.4 | 3,200 | 4,800 | 239 | 9.5 | 10.8 |
| 2150 | 300 | 8.4 | 4,000 | .96 | 26 | 86.6 | 2,260 | 4,750 | 321 | 9.5 | 10.7 |
| 2155 | 310 | 6.2 | 2,960 | .001 | 11.6 | 72.4 | 2,490 | 5,000 | 403 | 9.5 | 10.7 |
| 2160 | 236 | 32.8 | 3,540 | .13 | 22.7 | 73.5 | 1,080 | 12,307 | 178 | 9.5 | 10.8 |
| 2168 | 165 | 13.5 | 3,181 | .15 | 131 | 85.6 | 1,200 | 4,040 | 131 | 9.6 | 10.8 |
| 2215 | 287 | 16.5 | 980 | .23 | 40.8 | -- | 287 | 1,940 | 104 | 7.7 | 11.2 |
| 2255 | 313 | 8.0 | 4,700 | 4.2 | 19.2 | 70.6 | 2,845 | 6,990 | 310 | 8.5 | 9.5 |
| 2260 | 313 | 12.2 | 4,170 | 2.8 | 26.5 | 61.4 | 1,190 | 6,990 | 275 | 8.4 | 9.2 |
| 2265 | 223 | 23.5 | 4,230 | .45 | 287 | 77.3 | 1,048 | 9,200 | 182 | 8.3 | 9.8 |
| 2362 | 268 | 211 | 2,330 | .13 | 141 | 81.1 | 600 | 3,300 | 60 | 8.2 | 10.6 |
| 2364 | 186 | 5 | 1,830 | .001 | 4.55 | 86.5 | 940 | 3,560 | 405 | 8.2 | 10.6 |

TABLE 10.—*Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington—Continued*

| Station number | Characteristics | | | | | | | | | | |
|-------------------------------|---|--------------------------|------------------------------|-------------------------------|-----------------------|-----------------------------|--------------------|----------------------|--------------------------------------|---------------------------------------|----------------------------------|
| | Average direction of flow of stream (degrees) | Length of river, (miles) | Mean altitude of basin (ft.) | Lake and pond areas (percent) | Drainage area (sq mi) | Mean annual discharge (in.) | Site altitude (ft) | Source altitude (ft) | Fall or slope of river (ft per mile) | Air temperature annual amplitude (°C) | Mean annual air temperature (°C) |
| | G | L | E | F | D | Q | G | S | F | T _A | T _M |
| WESTERN WASHINGTON--Continued | | | | | | | | | | | |
| 14-2370 | 20 | 3 | 985 | 0.01 | 3.29 | 34.1 | 668 | 1,000 | 49 | 8.0 | 10.4 |
| 2375 | 291 | 10.6 | 1,640 | .01 | 37.8 | 36.3 | 470 | 2,320 | 136 | 7.9 | 10.4 |
| 2390 | 266 | 23.8 | 630 | .001 | 77.6 | 25.9 | 110 | 2,500 | 44 | 7.7 | 11.1 |
| 2435 | 114 | 6.7 | 906 | .01 | 19.6 | 59.2 | 75 | 1,500 | 139 | 7.2 | 10.9 |
| 2482 | 182 | 4.0 | 490 | .001 | 5.48 | 78.8 | 25 | 1,175 | 237 | 6.9 | 10.4 |
| 2490 | 216 | 11 | 1,350 | .001 | 39.9 | 115 | 350 | 276 | 170 | 7.0 | 10.6 |
| EASTERN WASHINGTON | | | | | | | | | | | |
| 12-3960 | 190 | 12.2 | 3,650 | .41 | 68.3 | 13.6 | 2,070 | 5,167 | 126 | 11.2 | 7.0 |
| 3965 | 160 | 75.5 | 2,025 | 1.9 | 24,900 | 15.5 | 2,012 | 2,051 | 1 | 12.2 | 8.2 |
| 3969 | 251 | 15.7 | 4,760 | 1.7 | 70.2 | 18.5 | 2,540 | 6,100 | 121 | 12.3 | 8.1 |
| 3971 | 347 | 14.7 | 4,200 | 4.2 | 51.5 | 19.7 | 2,550 | 5,200 | 196 | 12.3 | 8.1 |
| 3980 | 270 | 19.6 | 4,380 | 1.5 | 142 | 19.4 | 2,050 | 6,100 | 170 | 12.3 | 8.2 |
| 3985 | 180 | 82.4 | 2,000 | 1.7 | 25,200 | 14.4 | 1,720 | 2,050 | .8 | 12.5 | 8.3 |
| 3986 | 180 | 91.4 | 1,850 | 1.85 | 25,200 | 12.5 | 1,000 | 2,050 | .5 | 12.5 | 8.3 |
| 4015 | 165 | 98.5 | 4,560 | .05 | 2,220 | 9.2 | 1,840 | 6,000 | 42 | 11.8 | 6.5 |
| 4045 | 175 | 130 | 4,560 | .33 | 3,800 | 9.0 | 1,426 | 6,000 | 35 | 12.3 | 8.2 |
| 4075 | 248 | 7.8 | 2,390 | .001 | 48.2 | 3.5 | 1,980 | 2,880 | 55 | 11.7 | 7.4 |
| 4075.2 | 91 | 11.8 | 3,160 | .001 | 36 | 6.8 | 2,060 | 4,400 | 82 | 11.5 | 7.6 |
| 4077 | 193 | 17.6 | 3,160 | .001 | 94.1 | 5.1 | 1,660 | 5,100 | 138 | 11.4 | 7.7 |
| 4080 | 332 | 66.6 | -- | .01 | 428 | 4.4 | 1,620 | 4,400 | 10 | 11.4 | 8.0 |
| 4084 | 80 | 9 | 2,570 | .001 | 37 | 2.6 | 1,600 | 4,480 | 175 | 11.5 | 9.1 |
| 4085 | 248 | 14.1 | 3,510 | .01 | 83.0 | 7.9 | 1,950 | 5,100 | 103 | 11.7 | 9.0 |
| 4087 | 241 | 22.5 | 3,240 | .001 | 146 | -- | 1,540 | 5,100 | 81 | 11.5 | 9.0 |
| 4090 | 327 | 91.3 | 3,000 | .61 | 1,007 | 3.9 | 1,500 | 4,400 | 2 | 11.5 | 8.7 |
| 4195 | 280 | 124 | 3,600 | 1.6 | 3,880 | 21.1 | 2,000 | 4,700 | -- | 11.8 | 10.4 |
| 4225 | 261 | 144 | 3,550 | 1.42 | 4,290 | 18.3 | 1,697 | 4,700 | 21 | 11.5 | 10.3 |
| 4240 | 330 | 70.8 | -- | .001 | 689 | 4.9 | 1,720 | 4,000 | 13 | 11.5 | 10.0 |
| 4270 | 224 | 1.22 | 2,800 | 1.33 | 115 | 5.2 | 1,870 | 4,720 | 63 | 10.9 | 4.7 |
| 4310 | 214 | 32.4 | 2,400 | .54 | 665 | 5.2 | 1,590 | 4,720 | 33 | 11.2 | 9.5 |
| 4345 | 176 | 58.1 | 3,900 | .69 | 880 | -- | 1,460 | 6,300 | 27 | 12.0 | 10.1 |
| 4394 | 179 | 43.1 | 6,000 | 1.1 | 3,210 | -- | 900 | 1,120 | 6 | 11.4 | 10.8 |
| 4395 | 179 | 43.2 | 6,000 | 1.1 | 3,210 | 2.8 | 900 | 1,120 | 6 | 11.4 | 10.8 |
| 4423 | 38 | 23.5 | 4,850 | .19 | 256 | -- | 1,150 | 7,920 | 204 | 11.5 | 9.5 |
| 4425 | 25 | 117 | 5,110 | .22 | 3,550 | 7.6 | 1,140 | 6,500 | 40 | 11.2 | 10.7 |
| 4441 | 71 | 10.9 | 2,190 | 4.9 | 39.5 | -- | 1,180 | 4,040 | 175 | 11.6 | 10.0 |
| 4450 | 182 | 69.2 | 4,310 | .55 | 7,270 | 4.8 | 861 | 1,123 | 4 | 12.1 | 10.1 |
| 4473 | 201 | 106 | 4,000 | .4 | 8,210 | 5 | 792 | 1,123 | 4 | 12.2 | 10.2 |
| 4496 | 230 | 8.7 | 5,020 | .05 | 58 | -- | 2,800 | 5,680 | 320 | 12.1 | 6.5 |
| 4499 | 162 | 77.4 | 4,780 | .11 | 1,780 | 10.1 | 900 | 6,600 | 30 | 12.7 | 10.3 |
| 4510 | 131 | 22.5 | 5,130 | .28 | 372 | 46.7 | 1,100 | 7,120 | 100 | 10.4 | 9.4 |
| 4528 | 146 | 34.4 | 5,230 | .03 | 207 | 24.1 | 1,563 | 8,800 | 114 | 11.0 | 9.3 |
| 4540 | 150 | 20 | 4,590 | .25 | 150 | 73.9 | 1,880 | 7,030 | 107 | 9.4 | 7.5 |
| 4570 | 152 | 32.8 | 4,540 | 1.3 | 591 | 44.8 | 1,805 | 5,800 | 59 | 9.6 | 9.5 |
| 4580 | 111 | 25 | 5,260 | .48 | 193 | 37.9 | 1,450 | 5,500 | 107 | 11.5 | 10.3 |
| 4590 | 142 | 56 | 4,590 | .94 | 1,000 | 36.6 | 1,028 | 5,800 | 43 | 11.0 | 10.3 |
| 4614 | 349 | 11.8 | 3,550 | .003 | 40 | 4.3 | 1,750 | 6,800 | 400 | 11.2 | 10.0 |
| 4625 | 142 | 70.3 | -- | -- | 1,301 | 32.2 | 680 | 5,800 | 32 | 11.5 | 9.8 |

TABLE 10.—Topographic and climatic drainage-basin characteristics, irregularly measured temperature stations, Washington—Continued

| Station number | Characteristics | | | | | | | | | | |
|-------------------------------|---|---------------------------|------------------------------|-------------------------------|-------------------------|-----------------------------|---------------------|-----------------------|---------------------------------------|---------------------------------------|----------------------------------|
| | Average direction of flow of stream (degrees) | Length of river, in miles | Mean altitude of basin (ft.) | Lake and pond areas (percent) | Drainage area (sq. mi.) | Mean annual discharge (in.) | Site altitude (ft.) | Source altitude (ft.) | Fall or slope of river (ft. per mile) | Air temperature annual amplitude (°C) | Mean annual air temperature (°C) |
| | Ø | L | M | P | D | Q | G | S | F | T _A | T _M |
| EASTERN WASHINGTON--Continued | | | | | | | | | | | |
| 12-4648 | 215 | 16 | -- | -- | 64.7 | -- | 2,000 | 2,500 | 33 | 11.1 | 9.1 |
| 4650 | 264 | 70.2 | 2,200 | 0.42 | 1,042 | 1.01 | 1,386 | 2,775 | 13 | 11.4 | 9.6 |
| 4670 | 230 | 85.3 | 2,150 | 12.6 | 2,228 | -- | 1,070 | 2,775 | 12 | 11.5 | 11.2 |
| 4685 | 209 | 4 | 1,950 | 3.4 | 317 | 2.16 | 1,092 | 2,200 | 7 | 11.7 | 9.6 |
| 4705 | 115 | 2.3 | 1,200 | .001 | 12.0 | 90.9 | 1,065 | 1,150 | 10 | 12.6 | 11.7 |
| 4715 | 225 | -- | -- | -- | 3,650 | -- | 880 | -- | -- | 10.6 | 11.0 |
| 4726 | 262 | 37.4 | -- | -- | 4,177 | -- | 500 | 1,040 | 5 | 11.4 | 12.8 |
| 4838 | 177 | 16.3 | -- | -- | 69.5 | 10.9 | 2,500 | 5,840 | 190 | 11.1 | 10.8 |
| 4885 | 65 | 24 | 4,860 | .18 | 78.9 | 34.6 | 2,700 | 5,300 | 62 | 10.1 | 7.5 |
| 5020 | 84 | 23.5 | -- | -- | 119 | -- | 1,830 | 6,970 | 102 | 10.5 | 9.5 |
| 5050 | 153 | 108.8 | -- | -- | 3,660 | -- | 886 | 3,500 | 14.2 | 11.3 | 9.9 |
| 5105 | 79 | 174.8 | -- | -- | 5,615 | -- | 454 | 3,500 | 11.0 | 10.5 | 12.5 |
| 13-3347 | 61 | 24 | 3,550 | .001 | 170 | 5.6 | 1,090 | 6,100 | 146 | 10.6 | 8.3 |
| 3445 | 283 | 50 | 3,000 | .001 | 431 | 5.2 | 730 | 6,200 | 73 | 10.9 | 13.0 |
| 3460 | 245 | 55 | 3,060 | .01 | 491 | 8.8 | 2,005 | 3,500 | 18 | 10.5 | 9.1 |
| 3461 | 283 | 58.6 | 3,050 | .01 | 497 | 8.3 | 1,957 | 3,500 | 18 | 10.2 | 9.1 |
| 3480 | 279 | 21.6 | 2,770 | .01 | 132 | 3.8 | 2,326 | 4,990 | 12 | 10.4 | 8.9 |
| 3485 | 272 | 13.8 | 2,670 | .01 | 27.1 | 3.8 | 2,326 | 3,120 | 30 | 10.4 | 8.9 |
| 3492 | 275 | 58.9 | 2,990 | .01 | 796 | 5.6 | 1,932 | 3,500 | 19 | 10.2 | 9.1 |
| 3494 | 276 | 18.5 | 2,200 | .02 | 302 | 1.9 | 2,012 | 2,420 | 18 | 10.6 | 9.5 |
| 3505 | 316 | 44.4 | 2,680 | .01 | 189 | 2.6 | 1,868 | 3,100 | 21 | 10.2 | 9.2 |
| 3510 | 247 | 124 | 2,410 | .21 | 2,500 | 3.3 | 1,040 | 3,500 | 14 | 10.8 | 11.6 |
| 3525 | 180 | 59.6 | -- | -- | 679 | .5 | 1,070 | 2,300 | 18 | 10.8 | 11.6 |
| 3530 | 221 | -- | -- | -- | 108,500 | -- | 300 | -- | -- | 10.9 | 13.8 |
| 14-0130 | 286 | 13.6 | 3,950 | .01 | 59.6 | 19.1 | 2,000 | 5,890 | 176 | 11.3 | 12.3 |
| 0135 | 290 | 8.4 | 3,190 | .001 | 17.0 | 12.3 | 1,700 | 4,650 | 294 | 10.4 | 12.6 |
| 0160 | 282 | 16.4 | 2,360 | .01 | 48.4 | 5.4 | 1,200 | 4,650 | 176 | 11.0 | 12.7 |
| 0165 | 333 | 17.6 | 3,750 | .001 | 102 | 16.2 | 1,868 | 5,600 | 170 | 10.2 | 10.3 |
| 0170 | 282 | 35.6 | 2,950 | .01 | 361 | 7.2 | 1,150 | 5,600 | 87 | 9.9 | 12.9 |
| 0185 | 252 | 54.4 | 1,000 | .15 | 1,657 | 4.1 | 495 | 5,700 | 111 | 9.9 | 12.8 |
| 0343 | 145 | 30 | 2,400 | .001 | 197 | .7 | 275 | 3,800 | 112 | 10.9 | 14.5 |
| 0366 | 145 | 21.8 | 2,390 | .001 | 213 | 2.1 | 400 | 3,650 | 147 | 10.6 | 14.4 |

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